#### **CHAPTER V**

#### RESULTS AND DISCUSSION

### 5.1 Definition of removal efficiency

This section describes the various definitions of the removal efficiency.

### 5.1.1 Apparent removal efficiency

$$\psi = \frac{(C_{in} - C_{out,anymA})}{C_{in}}$$
 [-]

### 5.1.2 Removal efficiency (by discharge effect only)

$$\psi' = \frac{(C_{out,0 \, mA} - C_{out \, al \, any \, mA})}{C_{out,0 \, mA}}$$
 [-]

In this definition,  $\psi$  represents the sole effect of corona discharge and excludes any effect of possible low-temperature adsorption and thermal decomposition inside the reactor system.

### 5.1.3 Removal efficiency per unit residence time

$$\psi'' = \frac{\psi' \times residence \ time \ at \ 25 \ ^{\circ}C}{residence \ time \ at \ T \ ^{\circ}C}$$
 (5.3)

At steady state, the equation of continuity requires that  $\rho_1 \langle \upsilon_1 \rangle A_1 = \rho_2 \langle \upsilon_2 \rangle A_2$ . Since  $A_1 = A_2$  and  $\rho$  is a function of the gas temperature, the gas velocity at temperature  $T_2$  will be faster than its velocity at room temperature  $T_1$ . Thus the mean residence time  $\theta_2 = \frac{V_r}{\langle v_2 \rangle A_2}$  of this gas at  $T_2$  is shorter than  $\theta_1 = \frac{V_r}{\langle v_1 \rangle A_1}$  at room

temperature. Here  $V_r$  is the effective volume of the corona discharge reactor. The removal efficiency per unit residence time is defined so as to take into account the effect of shortened residence time on the observed removal efficiency as the reactor temperature is increased.

### 5.1.3 Electron-based efficiency

$$\psi_{elec} = \frac{N_r}{N_{e0}} \tag{5.4}$$

The electron-based efficiency  $\psi_{elec}$  (-) is defined as the number of gas molecules removed by one discharged electron.

### 5.1.4 Energy-based efficiency

The energy-based efficiency  $\psi_{ener}$  (mol gas .J<sup>-1</sup>) is defined as the mole of gas removed per energy consumption (J), as in Eq. (5.5).

$$\psi_{ener} = \frac{(q_{out,0\,mA} - q_{out\,al\,any\,mA})}{P} \tag{5.5}$$

Where  $q_{out, 0 mA}$ ,  $q_{out at any mA}$ , P are the molar flow rate of the target gases at the reactor outlet when using zero current, the molar flow rate of the target gases at the reactor outlet when using non-zero current and the power consumption, respectively.

### 5.2 Influence of temperature

### 5.2.1 Influence of temperature on electron energy

The voltages required to generate corona discharge are measured at different gas temperatures. From the experimental results, the voltages required to generate 0.2 mA in the removal of 200 ppm CH<sub>3</sub>CHO, 200 ppm NH<sub>3</sub>, and 200 ppm (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub> - CO<sub>2</sub> are, respectively, 12.5, 8.6 and 11.5 kV at room temperature, and these voltages decrease to 4.6, 4.2 and 6 kV, respectively, as temperature rises to  $300^{\circ}$ C. These voltages are approximately 30% higher when the target gases are removed from N<sub>2</sub> - O<sub>2</sub> - CO<sub>2</sub> mixture. Their values correspond to the profile changes in the electric field strength, E, inside the reactor. Meanwhile the gas temperature also affects the gas density, N. Thus it is important to note that the electron energy corresponds to the electric field strength divided by the gas density, E/N. To approximate E/N, the electric field strength described by Eq. (5.6) is used.

$$E = V / \{ r \ln (D_1/D_0) \}$$
 (5.6)

V, r,  $D_1$ ,  $D_0$  are the applied voltage, radial distance from the cylindrical axis, inner diameter of the cylindrical anode, and diameter of the wire cathode, respectively. Thus, the mean E/N is approximated by Eq. (5.7) (Tanthapanichakoon et al. 1998).

$$\langle E/N \rangle = \frac{\int_{D_0/2}^{D_1/2} (2\pi r)(E/N) dr}{\pi ((D_1/2)^2 - (D_0/2)^2)}$$

$$= \frac{4 V}{N(D_1 + D_0) \ln(D_1/D_0)}$$
(5.7)

N is calculated as  $p/\{R\ (273+T)\}$ , where p, R, T are total pressure, gas constant, and gas temperature, respectively. From this correlation, the average  $\langle E/N \rangle$  in the case of CH<sub>3</sub>CHO is 7.0 kV m<sup>2</sup> mol<sup>-1</sup> and 5.8 kV m<sup>2</sup> mol<sup>-1</sup> at room temperature and  $300^{\circ}$ C, respectively. E positively affects the electron energy because the electrons

emitted by the corona discharge are accelerated by E. On the other hand, N negatively affects the electron energy because the frequency of collisions between electrons and gas molecules becomes higher as N increases. In the case of toluene removal at high temperatures, there exists a general tendency that  $\langle E/N \rangle$ , the averaged value of E/N across section of the reactor, in both N2 and air decreases with temperature in the high temperature range (Dhattavorn, 2000). A similar tendency is also observed for the present cases of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N. This is primarily caused by a decrease in the required voltage associated with the temperature elevation. This voltage drop associated with temperature elevation may be explained as follows: (1) the voltage required for "corona discharge breakdown" which initiates ionization around the cathode is inversely proportional to the reactor temperature (Uhm, 1999). (2) Gas heating leads to more frequent electron detachment and decomposition of ion clusters that release the electron component so that the effective mobility of negative charges in the gas becomes high (Mnatsakanyan et al., 1987). (3) Gas expansion results in a longer mean free path of charged particles (Uhm, 1999). In spite of the voltage drop associated with the temperature elevation, if the negative thinning effect of gas expansion on N is relatively more significant than that of the temperature-induced voltage drop, the temperature dependency of  $\langle E/N \rangle$  may become reversed. This phenomenon is often observed when T is below 200°C in N<sub>2</sub>.

Since the electric field strength decreases only slightly when the temperature is elevated, the electron energy at 300°C turns out to be approximately 17% lower than at room temperature. Generally, the electron energy level should affect the reaction mechanism. For example, electron attachment tends to occur when electron energy is relatively low (Massey, 1976; Moruzzi, 1966; Caledonia, 1975), while formation of radicals may take place when electron energy is very high.

### 5.2.2 Influence of temperature on removal mechanism

Rigorously speaking, the relevant reactions contributing to the removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N are affected not only by the change in electron energy level but also by other effects of the elevated temperature. To consider the reaction mechanism, one must take byproduct formation into account. As for the gaseous byproducts, CO and O<sub>3</sub> were detected mainly in the low and NO<sub>x</sub> in the high temperature ranges. In fact, the measurements of O<sub>3</sub> concentration during the removal of toluene from N<sub>2</sub> - O<sub>2</sub> mixture reveal that O<sub>3</sub> is produced up to 1370 ppm at room temperature but it rapidly drops down to 430 ppm at 100°C. When *T* is further increased above 300°C, O<sub>3</sub> concentration becomes negligible (Dhattavorn, 2000). This is because O<sub>3</sub> is unstable at high temperature (Peyrous, Pignolet and Held, 1989; Devins, 1956). Therefore, oxidation by O<sub>3</sub> should play a negligible role in the high temperature range.

Contrary to  $O_3$  formation, it is known that production of  $NO_x$  by the discharge process is favored at high temperature. This is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased with temperature and reached 300ppm at  $400^{\circ}$ C. Since  $NO_x$  formation can be attributed to the reaction of discharge-induced N radicals with  $O_2$  (Lowke and Morrow, 1995; Mukkavilli et al., 1988), N radicals should also contribute to the removal of styrene and/or  $NH_3$  from both  $N_2$  and air at high temperatures. In addition, in the removal from air, there should be the extra effect of O radicals produced by electron impact to  $O_2$  and by  $O_3$  decomposition (Peyrous et al., 1989; Loiseau et al., 1966; Hadj-Ziane et al., 1990). Therefore, the removal efficiency from air at high temperatures should be enhanced by O radicals, though  $O_3$  oxidation is not effective. In fact Peyrous et al. (1989) simulated the concentrations of  $O_3$  and O radicals in pulsed corona discharge in the presence of  $O_2$ , and showed that temperature elevation brings about higher O radical concentration and lower  $O_3$ .

When H<sub>2</sub>O is present in the gas stream, H<sup>-</sup>, OH<sup>-</sup> and a few O<sup>-</sup> anions are expected to be produced by dissociative electron attachment to H<sub>2</sub>O molecules at low temperature (Massey, 1976; Moruzzi and Phelps, 1966). The selectivity for

these ionic products should depend on the gas temperature and electron energy. At high temperature, electron detachment would become significant so that radicals of O, H, and OH may play a more important role than their anionic counterparts. These radicals are also expected to contribute to the removal of the target gases. More specifically, OH is believed to dissociate NH<sub>3</sub> to produce an aminogen radical (NH<sub>2</sub>) and H<sub>2</sub>O (Bityurin, Potapkin and Demisky, 2000).

In non-thermal corona discharge in the air at room temperature, electrons are sometimes captured by O<sub>2</sub> to form negative ions, O<sup>-</sup>, O<sub>2</sub><sup>-</sup>, O<sub>3</sub><sup>-</sup>, and clusters via electron attachment. The reversed electron detachment process, however, becomes significant at high temperature, causing ion clusters to become unstable (Mnatsakanyan, Naydis and Solozobov, 1987). Several previous works indicate that the corona discharge reactor plays host to electron attachment reactions and relevant ion cluster formation at room temperature (Sano et al., 1997; Tamon, Sano and Okasaki, 1996). However, because of high temperature effects such as electron detachment and radical formation, electron attachment and ion clustering would be less and less important as the temperature rises.

In fluidized bed combustion conditions, the effect of coexisting gases, CO<sub>2</sub> and H<sub>2</sub>O, on catalytic decomposition of NH<sub>3</sub> over limestone has been reported. In the absence of CO<sub>2</sub> and H<sub>2</sub>O, NH<sub>3</sub> was decomposed to N<sub>2</sub>. From a NH<sub>3</sub> - CO<sub>2</sub> mixture, (NH<sub>2</sub>)<sub>2</sub>CO was formed through NH<sub>3</sub> decomposition over both calcined limestone and CO<sub>2</sub>. However, from the NH<sub>3</sub> - CO<sub>2</sub> - H<sub>2</sub>O mixture, (NH<sub>2</sub>)<sub>2</sub>CO was not formed (Tadaaki Shimizu et al., 1995). CO<sub>2</sub> is perceived to be less reactive and its efficient catalytic conversion has remained elusive. Since CO<sub>2</sub> is a highly oxidized, thermodynamically stable compound, its utilization requires reaction with certain high energy substances or electro reductive processes. Catalytic hydrogenation is one of the most promising approaches to CO<sub>2</sub> fixation. Recent research has shown that high catalytic efficiency, yield, and rate of reaction can be obtained from CO<sub>2</sub> with the used of optimum conditions and catalysts (Ryoji Noyori et al., 1995).

When CO<sub>2</sub> is present in the gas stream, CO<sub>3</sub> and a few O anions are expected to be produced by dissociative electron attachment to CO<sub>2</sub> molecules at low temperature (Price and Moruzzi, 1966).

In the case of NH<sub>3</sub> removal, the removed NH<sub>3</sub> was converted to needle-like bright crystal, which was observed inside the reactor and the gas line downstream. It is reported (Sugimitsu, 1998) that NH<sub>3</sub> does not react with O<sub>3</sub> to directly form NH<sub>4</sub>NO<sub>3</sub>. Instead the following consecutive reactions are mentioned:

 $2 \text{ NH}_3 + 4\text{O}_3 = \text{NH}_4\text{NO}_2 + \text{H}_2\text{O}_2 + 4\text{O}_2$ ;  $\text{NH}_4\text{NO}_2 + \text{H}_2\text{O}_2 = \text{NH}_4\text{NO}_3 + \text{H}_2\text{O}$ . Our result is also consistent with published reports that  $\text{NH}_4\text{NO}_3$  solid is produced by corona treatment of humid air containing NH<sub>3</sub> (Bityurin et al., 2000; Kanasawa et al., 1998; Urashima, Kim and Chang, 1999). The mechanism for  $\text{NH}_4\text{NO}_3$  formation in the high temperature range is not clear but it may be considered that  $\text{NH}_3$ , H<sub>2</sub>O and  $\text{NO}_x$  as well as N and H radicals could react to form  $\text{NH}_4\text{NO}_3$ .

### 5.3 Substantiation of ozone effect

When  $O_2$  is present in  $N_2$  or a gas mixture, it readily reacts with electrons of sufficient energy level. Electron attachment on  $O_2$  has been reported in the literature (Morruzzi and Phelps, 1966; Massey, 1976; Rapp and Briglia, 1976; Chantry and Schulz, 1967)

$$O_2 + e^- \longrightarrow O_2$$
 (a)

$$O_2 + e^- \longrightarrow O + O^-$$
 (b)

Moruzzi and Phelps (1966) report that the reaction in Equation (a) occurs in the low electron energy range ( $E/p < 1.5 \text{ V.m}^{-1}.\text{Pa}^{-1}$ ). In contrast, the reaction in Equation (b) occurs in the higher electron energy range. Also in a corona - discharge reactor, the closer the electrons are to the cathode wire, the higher their energy level. When  $O_2$  collides with a high - energy electron near the cathode wire in the corona-discharge reactor, production of  $O^-$  is expected as in Equation (b). Next  $O_3$  is produced from the reaction of  $O^-$  with  $O_2$  (Loiseau et al., 1994; Hadj-Zaine et al., 1992).

In short, not only  $O_2^-$  and  $O_2^-$  radicals but some ozone  $(O_3)$  is also produced. Since  $O_3$  is very reactive, the ozonation reaction is used in some commercial devices for deodorization and sterilization. The same ozonation reaction as well as the oxidation reaction with  $O_2^-$  radicals is expected to contribute to the decomposition and removal of gas impurities in the present corona discharge reactor. The  $O_2^-$  radical is also expected to contribute to the formation of ionic clusters and removal of the gas impurities.

To substantiate the role of the ozonation, two identical reactors are connected serially. Figure 5.1 shows the experimental setup used to confirm the  $O_3$  effect.  $N_2$  -  $O_2$  mixture is supplied to the first reactor to produce  $O_3$  by corona discharge. Then a gas impurity is mixed into the effluent stream from the first reactor, and the resulting mixture is introduced to the second reactor. No voltage is supplied to the second reactor, so there is no corona discharge in the second reactor, which only provides space for the reaction of ozone with the impurity. Then the change in the concentration of the impurity at the outlet of the second reactor is measured. The decrease in the outlet concentration from the second reactor gives the  $O_3$  effect.

Chaichanawong (2003) shows that the formation of  $O_3$  from  $N_2$  -  $O_2$  mixed gas ( $N_2$  65 cc/min and  $O_2$  5 cc/min). In the first reactor,  $N_2$  -  $O_2$  mixed gas is carried out at the discharge current 0.20 mA and the effluent stream is mixed with  $N_2$  20 cc/min before feeding to the second reactor without discharge current.  $[O_3]_{in}$  and  $[O_3]_{out}$  of the second reactor are 700 ppm and 650 ppm, respectively. Next  $CH_3CHO$  (2000 ppm balanced with  $N_2$ ) at 30 cc/min is mixed with  $N_2$  70 cc/min before feeding in the second reactor.  $[CH_3CHO]_{in}$  and  $[CH_3CHO]_{out}$  are 600 ppm and 583 ppm, respectively. In contrast, when  $CH_3CHO$  (2000 ppm balanced with  $N_2$ ) at 30 cc/min is mixed with the  $N_2$  -  $O_2$  effluent stream ( $N_2$  65 cc/min and  $O_2$  5 cc/min) from the first reactor at the discharge current 0.20 mA, the outlet concentration of  $CH_3CHO$  at the outlet of the second reactor is reduced from 600 ppm to 380 ppm. It can be confirmed that  $O_3$  has an important role on  $CH_3CHO$  removal efficiency.

In addition, the effect of O<sub>3</sub> on the removal of (CH<sub>3</sub>)<sub>3</sub>N was also investigated as shown in appendix K. The results were the same as in the case of CH<sub>3</sub>CHO. In

the case of NH<sub>3</sub>, O<sub>3</sub> also has an important role on the removal efficiency (Chaiyo, 2001).

# 5.4 Blank test for the investigation of the effect of temperature on acetaldehyde, ammonia and trimethyl amine removal

The experimental results in the Appendices D - K show the results of the blank test for the investigation of temperature effect on acetaldehyde, ammonia and trimethyl amine removal. Here the concentration of the target gases at the reactor outlet was measured at various temperatures in the absence of the discharge current. Figure 5.2 shows the results of the blank test for investigation of temperature effect on acetaldehyde (CH<sub>3</sub>CHO) in N<sub>2</sub> - O<sub>2</sub> - CO<sub>2</sub> mixture. There appeared a concentration drop at room temperature, which is considered to be due to physical adsorption inside the reactor. At moderate temperature, the effect of adsorption inside the reactor slightly increased as the reactor temperature increased. However, the outlet concentration of CH<sub>3</sub>CHO again decreased at 300°C. The reverse effect at this highest temperature may be attributed to the thermal decomposition. Figure 5.3 shows the results of the blank test for investigation of temperature effect on ammonia (NH<sub>3</sub>) in N<sub>2</sub> - O<sub>2</sub> - CO<sub>2</sub> mixture. It is found that the outlet concentration of NH<sub>3</sub> slightly decreases at 300°C via the thermal decomposition. Figure 5.4 shows the results of the blank test for the investigation of temperature effect on trimethylamine (CH<sub>3</sub>)<sub>3</sub>N in N<sub>2</sub> - O<sub>2</sub> - CO<sub>2</sub> mixture. It is found that the outlet concentration of (CH<sub>3</sub>)<sub>3</sub>N decreases above room temperature. Some extraneous peaks were observed in the gas chromatogram of the effluent stream which confirmed that thermal decomposition of (CH<sub>3</sub>)<sub>3</sub>N may occur.

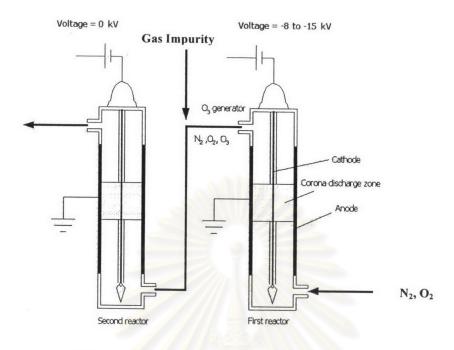


Figure 5.1 Apparatus to substantiate O<sub>3</sub> effect

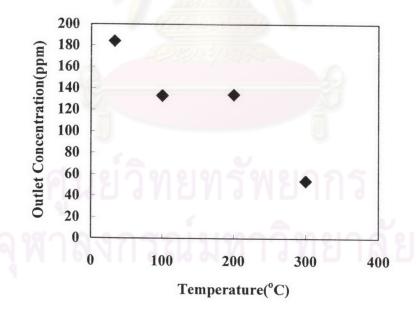


Figure 5.2 Blank tests for the removal of CH3CHO 200 ppm from  $N_2$  -  $O_2(10\%)$  -  $CO_2(10\%)$ 

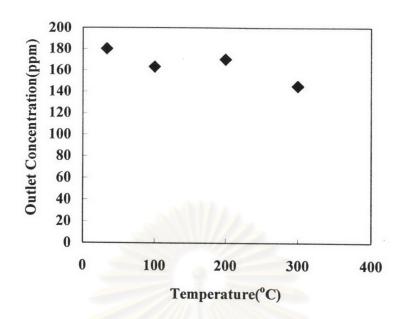


Figure 5.3 Blank tests for the removal of NH<sub>3</sub> 200 ppm from N<sub>2</sub> - O<sub>2</sub>(10%) - CO<sub>2</sub>(10%)

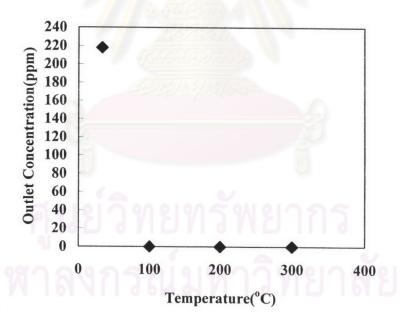


Figure 5.4 Blank tests for the removal of  $(CH_3)_3N$  200 ppm from  $N_2$  -  $O_2(10\%)$  -  $CO_2(10\%)$ 

### 5.5 Removal of acetaldehyde (CH<sub>3</sub>CHO)

### 5.5.1 Effect of temperature and coexisting $CO_2$ on the removal of $CH_3CHO$ from $N_2$

In most actual applications of gas purification, several kinds of gas components often coexist. Therefore, it is necessary to study the influence of common coexisting gases on the removal efficiency.

Figure 5.5 shows the removal efficiency  $\psi'$  of CH<sub>3</sub>CHO versus temperature. From Figure 5.5 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  decrease from room temperature up to 200°C, then the tendency reverses up to 300°C because the effect of O anion and CO3 is strong at low temperature but the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. This phenomenon is attributable to the fact that the gas mixture flows upward more quickly as its volume expands. Obviously, the presence of CO<sub>2</sub> does significantly affect the removal efficiency. It is postulated that CO2 is less electronegative than CH3CHO but the bonding strength of CO2 molecules with the anode surface is stronger than that of CH3CHO. Thus, at low temperature when a smaller number of electrons are available at low discharge currents, most electrons attach onto CH3CHO and deposit on the anode wall is composed of mostly CH3CHO. At high temperature, there is an excess of electrons that can attach to CO2. When the CO2 ions deposit on the anode surface, they replace (drive off) some of the previously deposited CH<sub>3</sub>CHO. The higher the CO<sub>2</sub> concentration, the higher the removal efficiency. Since CO2 is a highly oxidized, thermodynamically stable compound, its utilization requires reaction with certain high - energy substances or electro reductive processes. Catalytic hydrogenation is one of the most promising approaches to CO2 fixation. Recent research has shown that high catalytic efficiency, yield, and rate of reaction can be obtained from CO2 with the use of optimum conditions and catalysts (Ryoji Noyori et al., 1995). Figure 5.5 (b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi^{*}$  increases with temperature up to 100°C.

At room temperature, 100, 200 and 300°C,  $\psi_{\rm elec}$  of CH<sub>3</sub>CHO at 200 ppm -CO<sub>2</sub> (10%, 20%) are 3.9, 3.5, 1.0, 1.3 and 4.5, 3.7, 1.3, 1.2, respectively. Interestingly,  $\psi_{\rm elec}$  at 200°C of CO<sub>2</sub> (10%) become lower than 300°C, thus indicating the possible existence of an optimal temperature. The high values of  $\psi_{\mbox{\tiny elec}}$  at low temperature reveal that ion clusters may be produced. It has been reported that dissociate electron attachment of CH<sub>3</sub>CHO may produce O<sup>-</sup>, C<sub>2</sub>O<sup>-</sup>, HC<sub>2</sub>O<sup>-</sup>, CH<sub>3</sub>CO<sup>-</sup>, or CH<sub>3</sub> (Dressler and Allan, 1985). The selectivity to produce these ions depends on the level of electron energy. However, at high temperatures, electron detachment would become significant so that the positive effect of these ions is negated. Moreover, at high temperatures, the rate of detachment of the attached CH<sub>3</sub>CHO molecules on the reactor wall is sufficiently enhanced by the lowered adsorption equilibrium to overcome the effect of electrostatic attraction, thus significantly reducing the net rate of CH<sub>3</sub>CHO deposition on the wall. However,  $\psi_{\rm elec}$  at 200°C of CO<sub>2</sub> (20%) becomes higher than 300°C because of the effect of reduced residence time and removal efficiency in case of CO<sub>2</sub> (20%) is higher than CO<sub>2</sub> (10%). Obviously, the presence of CO<sub>2</sub> does significantly enhance the removal efficiency.

# 5.5.2 Effect of temperature and coexisting $CO_2$ and $O_2$ on the removal of $CH_3CHO$ from $N_2$

Figure 5.6 shows the removal efficiency  $\psi'$  of CH<sub>3</sub>CHO versus temperature. From Figure 5.6 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  remains nearly 100% from room temperature up to 300°C because of the effect of  $O_3$ ,  $CO_3$  and O anion at low temperatures and various radicals at high temperatures. This can be attributed to the fact that  $O_3$  is produced from  $O_2$  by the corona discharge reaction and is quite stable at room temperature. At room to moderate temperatures, electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro - negative compounds (Sano et al., 1997; Bityurin; 2000). N radicals should also contribute to the removal of CH<sub>3</sub>CHO from both  $N_2$  and air at high temperatures. In addition, in the removal

from air, there should be the extra effect of O radicals produced by electron impact on  $O_2$  and by  $O_3$  decomposition (Peyrous, Pignolet and Held, 1989; Loiseau et al. 1994; Hadj - Ziane, 1990). Therefore, the CH<sub>3</sub>CHO removal efficiency  $\psi'$  at high temperatures should be enhanced by O radicals although  $O_3$  oxidation is not effective. And the presence of  $CO_2$  does significantly affect the removal efficiency of CH<sub>3</sub>CHO from  $N_2$  -  $O_2$ . Figure 5.6 (b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi'$  increases with temperature increases.

At room temperature, 100, 200 and 300°C,  $\psi_{elec}$  of CH<sub>3</sub>CHO at 200 ppm-O<sub>2</sub> (10, 20%)-CO<sub>2</sub> (10%, 20%) are (3.9, 2.3, 1.8, 0.6), (3.9, 3.0, 2.7, 0.8), (4.0, 3.0, 2.7, 0.8), (3.3, 2.7, 2.1, 0.6) respectively. Interestingly, as the temperature increases,  $\psi_{elec}$  decreases, thus, indicating the possible existence of an optimal temperature. The high values of  $\psi_{elec}$  at low temperatures reveal that electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro-negative compounds (Sano et al., 1997; Bityurin; 2000). This can be attributed to the fact that O<sub>3</sub> is produced from O<sub>2</sub> by the corona discharge reaction and is quite stable at room temperature. N radicals should also contribute to the removal of CH<sub>3</sub>CHO from both N<sub>2</sub> and air at high temperatures.

# 5.5.3 Effect of temperature and coexisting CO<sub>2</sub> and H<sub>2</sub>O on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>

Figure 5.7 shows the removal efficiency  $\psi'$  of CH<sub>3</sub>CHO versus temperature. From Figure 5.7 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  decrease from room temperature up to 200°C, then the tendency reverses up to 300°C because the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. For the effect of H<sup>-</sup>, OH<sup>-</sup>, a few O<sup>-</sup> anions and CO<sub>3</sub><sup>-</sup> should contribute to the removal of CH<sub>3</sub>CHO at low to moderate temperatures. At 200°C, the presence of H<sub>2</sub>O and CO<sub>2</sub> slightly retards the removal efficiency of CH<sub>3</sub>CHO because at low discharge currents, the relatively much

smaller number of electrons tends to attach mostly to  $H_2O$  and  $CO_2$ . In addition, N radicals are consumed by their reaction with  $H_2O$  at high temperatures. Obviously, the presence of  $CO_2$  does significantly affect the removal efficiency. The higher the  $CO_2$  concentration, the higher the removal efficiency. **Figure 5.7** (b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi$  increases with temperature up to  $100^{\circ}C$ .

At room temperature, 100, 200 and 300°C,  $\psi_{\rm elec}$  of CH<sub>3</sub>CHO at 200 ppm -H<sub>2</sub>O (5250, 10500, 21800 ppm) - CO<sub>2</sub> (10%, 20%) are (3.2, 2.3, 0.6, 1.0), (3.8, 2.8, 1.3, 1.3), (3.5, 3.0, 1.4, 1.3), (3.7, 3.0, 1.5, 1.5), (4.1, 3.0, 1.4, 1.3), (4.1, 3.1 2.5, 1.5) respectively. Interestingly, as the temperature increases,  $\psi_{\mbox{\tiny elec}}$  decreases, thus, indicating the possible existence of an optimal temperature. The high values of  $\psi_{\mbox{\tiny elec}}$ at low temperature reveal that ion clusters may produce and these clusters increase when the inlet concentration increases. It has been reported that dissociative electron attachment of CH<sub>3</sub>CHO may produce O', C<sub>2</sub>O', HC<sub>2</sub>O', CH<sub>3</sub>CO', or CH<sub>3</sub>' (Dressler and Allan, 1985). The selectivity to produce these ions depends on the level of electron energy. However, at high temperatures, electron detachment would become significant so that the positive effect of these ions is negated. Moreover, at high temperatures, the rate of detachment of attached CH3CHO molecules on the reactor wall is sufficiently enhanced by the lowered adsorption equilibrium to overcome the effect of electrostatic attraction, thus significantly reducing the net rate of CH<sub>3</sub>CHO deposition on the wall. As mentioned earlier, the high values of  $\psi_{\mbox{\tiny elec}}$  at low temperature reveal that electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro-negative compounds (Sano et al., 1997; Bityurin; 2000).

# 5.5.4 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>

Figure 5.8 shows the removal efficiency  $\psi'$  of CH<sub>3</sub>CHO versus temperature. From Figure 5.8 (a), we see that, as the temperature increases, the removal

efficiency  $\psi'$  remains nearly 100% from room temperature up to 300°C. This can be attributed to the fact that O<sub>3</sub> is produced from O<sub>2</sub> by the corona discharge reaction and is quite stable at room temperature. At room to moderate temperatures, electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro-negative compounds (Sano et al., 1997; Bityurin; 2000). N radicals should also contribute to the removal of CH<sub>3</sub>CHO from both N<sub>2</sub> and air at high temperatures. In addition, in the removal from air, there should be the extra effect of O radicals produced by electron impact to O2 and by O3 decomposition (Peyrous, Pignolet and Held, 1989; Loiseau et al. 1994; Hadj - Ziane, 1990). CO<sub>3</sub>, H, OH and a few O anions should contribute to the removal of CH<sub>3</sub>CHO at low to moderate temperatures. At high temperatures, electron detachment would become significant so that radicals of O, H, and OH may play a more important role than their anionic counterparts. These radicals are also expected to contribute to the removal of the CH<sub>3</sub>CHO. And the presence of CO<sub>2</sub> does significantly affect the removal efficiency of CH<sub>3</sub>CHO from N<sub>2</sub> - O<sub>2</sub> - H<sub>2</sub>O. Figure 5.8 (b) reveals that when the negative effect of reduced residence time is taken in account, the value of w'' increases with temperature increases.

The effects of coexisting  $CO_2$ ,  $O_2$  and  $H_2O$  are shown in Figure A and B. The influence of  $CO_2$  concentration was examined and shown in cases A and B. The concentration  $CO_2$  is varied from 10% to 20% with fixed concentration  $O_2$  and  $H_2O$ . Similarly, the influence of concentration  $H_2O$  in the range of (5250 – 21800 ppm) at fixed concentrations of  $O_2$  and  $CO_2$  was examined and shown in cases C, G and K to evaluate the effect of  $H_2O$ . Here, we can not see the effects of both  $CO_2$  and  $H_2O$  in this concentration range. This is because the concentration of  $O_2$  is excessive for all runs. When  $O_2$  concentration is excessive,  $\psi'$  can reach 100% although the concentrations of  $CO_2$  and  $H_2O$  are changed.

The experimental results from the removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from single, double and tertiary components could also be explained as mentioned above.

### 5.5.5 Preliminary summary

Generally, two other types of removal efficiency are reported for a corona-discharge system. The electron - based efficiency  $\psi_{elec}$  (-) is defined as the number of gas molecules removed by one discharged electron, and the energy-based efficiency  $\psi_{ener}$  (mol gas .J<sup>-1</sup>) is defined as the mole of gas removed per energy consumption (J). At 33, 100, 200 and 300°C, the experimental values of  $\psi_{elec}$  and  $\psi_{ener}$  of the CH<sub>3</sub>CHO 200 ppm removal are as follows:

$$N_2$$
 -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 3.9, 3.5, 1.0, 1.3$   $\psi_{ener} \times 10^{-9} = 4.8, 5.6, 2.6, 4.4$   
 $N_2$  -  $O_2$  (10%) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 3.9, 2.3, 1.8, 0.6$   $\psi_{ener} \times 10^{-9} = 4.5, 3.1, 3.0, 1.2$   
 $N_2$  -  $H_2O$  (10500 ppm) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 3.5, 3.0, 1.4, 1.3$   $\psi_{ener} \times 10^{-9} = 4.1, 4.2, 2.9, 3.7$   
 $N_2$  -  $O_2$  (10%) -  $H_2O$  (10500 ppm) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 4.1, 3.3, 2.6, 0.9$   $\psi_{ener} \times 10^{-9} = 4.5, 4.4, 4.2, 2.0$ 

Generally  $\psi_{elec}$  and  $\psi_{ener}$  tends to decrease as the gas temperature increases. This trend may be ascribed to the combined effect of reduced residence time and the shift in removal mechanism. Interestingly, in the case of N<sub>2</sub> - CO<sub>2</sub>,  $\psi_{elec}$  and  $\psi_{ener}$  at 200°C become lower than at 300°C, thus indicating the possible existence of an optimal temperature.

In actual applications of gas purification, it is important to consider the energy-based efficiency  $\psi_{\it ener}$ . From the above results, it is recommended to operate from 100 to 200°C for minimizing the operating cost when air is purified because the values of  $\psi_{\it ener}$  are high.

### 5.5.6 Byproducts dected on the removal of acetaldehyde

Figure 5.9 shows the concentration of the main byproduct CO versus temperature in the presence of CO<sub>2</sub>. In Figure 5.9 as the temperature increases, the byproducts CO decrease starting from room temperature up to 200°C, then the tendency reverses up to 300°C because the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. It is known that CO can be produced by dissociative attachment reaction. This is also confirmed in our experiments.

Figure 5.10 shows the concentration of another byproduct  $NO_x$  versus temperature in the presence of  $CO_2$ . In Figure 5.10 as the temperature increases, the byproducts  $NO_x$  increase. It is known that production of  $NO_x$  by the discharge process is favored at high temperature. This is also confirmed in our experiments. While, the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased with temperature rise.

Figure 5.11 shows the concentration of the byproduct CO versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.11 as the temperature increases, the byproduct CO decreases as the temperature rises because at high temperatures  $O_3$  is unstable.

Figure 5.12 shows the concentration of byproduct  $O_3$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.12 as the temperature increases, the byproduct  $O_3$  decreases as the temperature rises. This is because  $O_3$  is unstable at high temperature (Peyrous, Pignolet and Held, 1989; Devins, 1956).

Figure 5.13 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.13 as the temperature increases, the byproducts  $NO_x$  decrease starting from room temperature up  $200^{\circ}$ C, then the tendency reverses up to  $300^{\circ}$ C. As the temperature increases, the byproduct  $O_3$  decreases with temperature rises and the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises.

Figure 5.14 shows the concentration of the byproduct CO versus temperature in the presence of H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.14 as the temperature increases, the byproducts CO increase. At low temperatures, the presence of CO<sub>2</sub> and H<sub>2</sub>O in the

gas stream  $CO_3$ , H, OH and a few O anions are expected to be produced by dissociative electron attachment to  $CO_2$  and  $H_2O$  molecules (Massey, 1976; Moruzzi and Phelps, 1966). At high temperature, electron detachment would become significant so that radicals of  $CO_3$ , O, H, and OH may play a more important role than their anionic counterparts.

Figure 5.15 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $H_2O$  and  $CO_2$ . In Figure 5.15 as the temperature increases, the byproduct  $NO_x$  increases. It is known that production of  $NO_x$  by the discharge process is favored at high temperature. This is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased with the temperature rise.

Figure 5.16 shows the concentration of the byproduct CO versus temperature in the presence of O<sub>2</sub>, H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.16 as the temperature increases, the byproduct CO decreases with the temperature rise. Since CO<sub>2</sub> and H<sub>2</sub>O are present in the gas stream, CO<sub>3</sub>, H, OH and a few O anions are expected to be produced by dissociative electron attachment to CO<sub>2</sub> and H<sub>2</sub>O molecules at low temperature (Massey, 1976; Moruzzi and Phelps, 1966).

Figure 5.17 shows the concentration of the byproduct  $O_3$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.17 as the temperature increases, the byproduct  $O_3$  decreases with the temperature rise because at high temperature,  $O_3$  is unstable (Peyrous, Pignolet and Held, 1989; Devins, 1956).

Figure 5.18 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.18 as the temperature increases, the byproduct  $NO_x$  decreases starting from room temperature up  $200^{\circ}C$ , then the tendency reverses up to  $300^{\circ}C$ . As the temperature starts to increase, the byproduct  $O_3$  decreases. At high temperatures, electron detachment would become significant so that radicals of  $CO_3$ , O, H, and OH may play a more important role than their anionic counterparts. However, the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises.

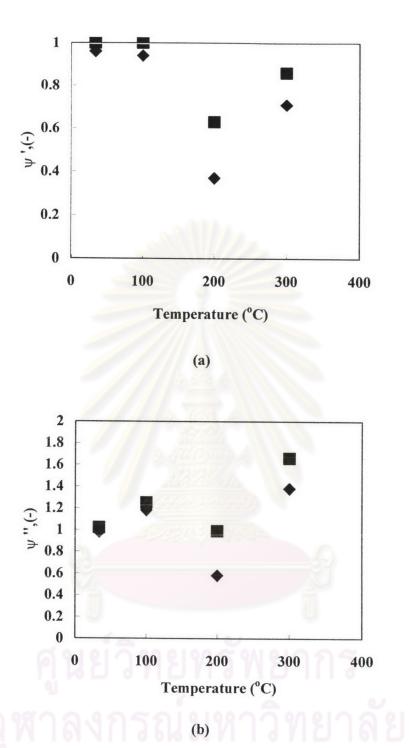


Figure 5.5 Effect of  $CO_2$  on the removal of  $CH_3CHO$  from  $N_2$ ;  $C_{in, acetaldehyde}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature:  $\bullet$   $CO_2$  (10%),  $\blacksquare$   $CO_2$  (20%)

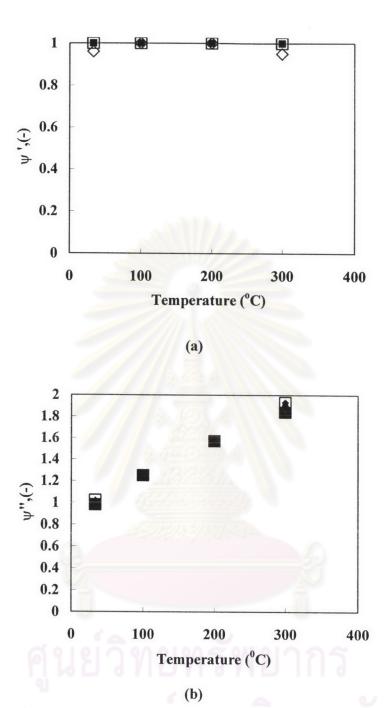


Figure 5.6 Effect of coexisting  $O_2$ -CO₂ on the removal of CH₃CHO from  $N_2$ ;  $C_{in, acetaldehyde}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature:  $\bullet$  CO₂ (10%) - O₂ (10%),  $\bullet$  CO₂ (20%) - O₂ (10%),  $\bullet$  CO₂ (10%) - O₂ (20%),  $\bullet$  CO₂ (20%) - O₂ (20%)

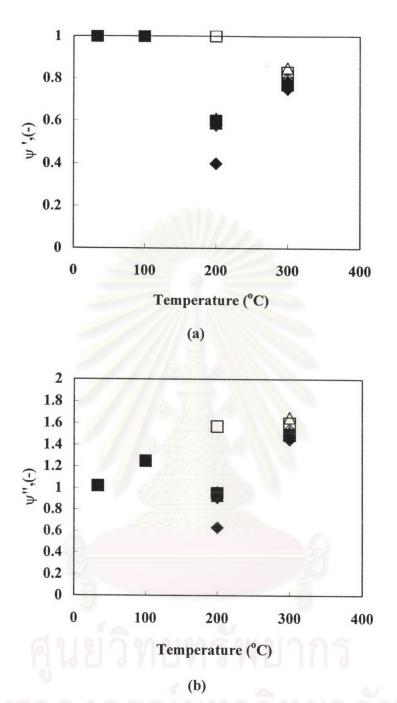


Figure 5.7 Effect of coexisting  $H_2O-CO_2$  on the removal of  $CH_3CHO$  from  $N_2$ ;  $C_{in, acetaldehyde} = 200 ppm, I = 0.2 mA, SV = 55.8 hr^{-1}$  at room temperature:

◆  $CO_2$  (10%) -  $H_2O$  (5250 ppm),

◆  $CO_2$  (20%) -  $H_2O$  (5250 ppm),

△  $CO_2$  (10%) -  $H_2O$  (10500 ppm),

△  $CO_2$  (20%) -  $H_2O$  (10500 ppm),

□  $CO_2$  (10%) -  $H_2O$  (21800 ppm),

□  $CO_2$  (20%) -  $H_2O$  (21800 ppm)

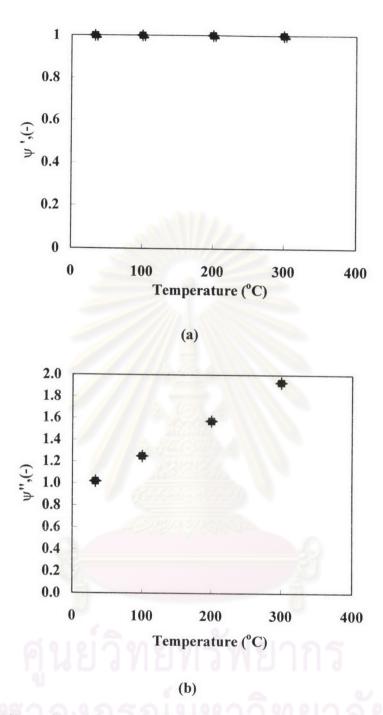


Figure 5.8 Effect of coexisting  $O_2$ -H<sub>2</sub>O-CO<sub>2</sub> on the removal of CH<sub>3</sub>CHO from  $N_2$ ;  $C_{in, acetaldehyde}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature: A ←  $CO_2(10\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),  $CO_2(20\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),  $CO_2(20\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm),  $CO_2(20\%)$ -O<sub>2</sub> (10%)-O<sub>2</sub> (10%)-O<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (21800ppm),  $CO_2(20\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (

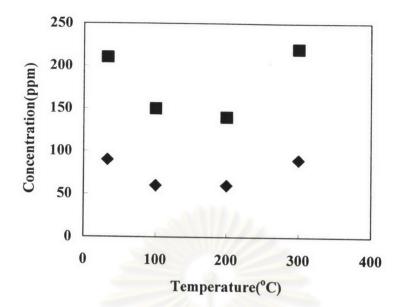


Figure 5.9 Byproduct (CO) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%),  $\blacksquare$  CO<sub>2</sub> (20%)

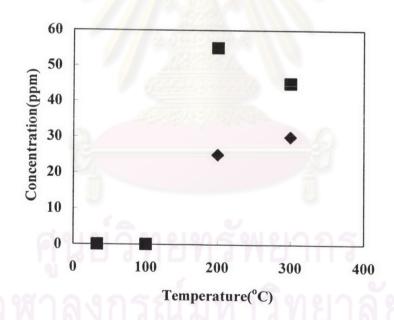


Figure 5.10 Byproduct (NO<sub>x</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%),  $\blacksquare$  CO<sub>2</sub> (20%)

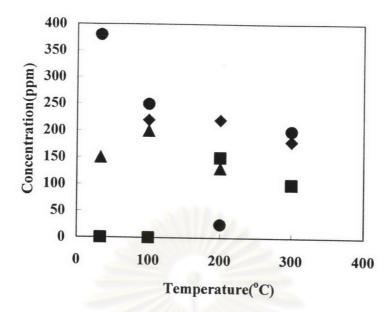


Figure 5.11 Byproduct (CO) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\triangle$  CO<sub>2</sub>(20%) O<sub>2</sub>(10%),
- $\square$  CO<sub>2</sub>(10%) O<sub>2</sub>(20%),
- $\bullet$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%)

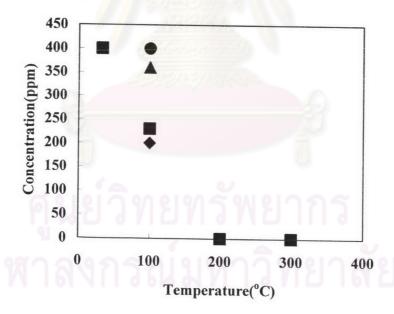


Figure 5.12 Byproduct (O<sub>3</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

- ◆ CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%),
- $\square$  CO<sub>2</sub>(10%) O<sub>2</sub>(20%),
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%)

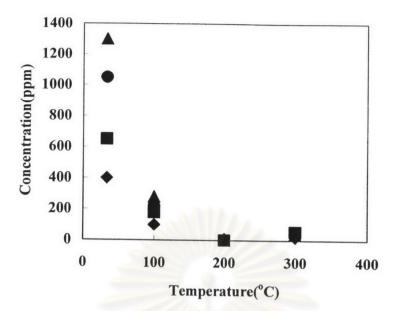


Figure 5.13 Byproduct (NO<sub>x</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

 $CO_2(10\%) - O_2(10\%),$ 

 $\triangle$  CO<sub>2</sub>(20%) - O<sub>2</sub>(10%),

 $\blacksquare$  CO<sub>2</sub>(10%) - O<sub>2</sub>(20%),

 $\bullet$  CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

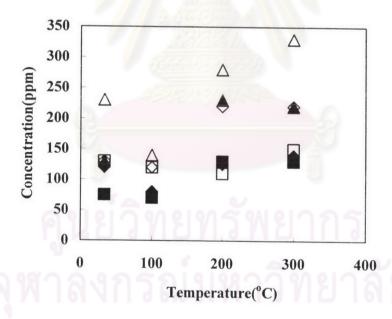


Figure 5.14 Byproduct (CO) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

◆ CO<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),

♦ CO<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

▲ CO<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm),

 $\triangle$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),

 $\blacksquare$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),

 $\square$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)

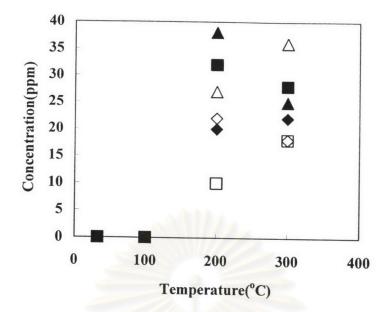
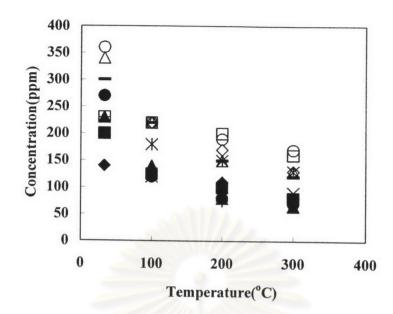


Figure 5.15 Byproduct (NO<sub>x</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- ◆ CO<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\triangle$  CO<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\square$  CO<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)



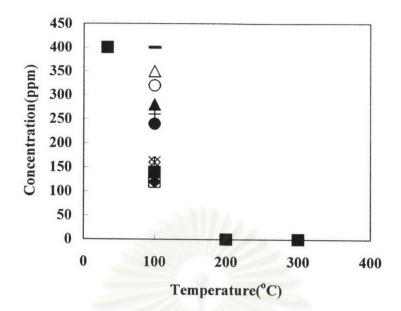


Figure 5.17 Byproduct (O<sub>3</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $CO_2(10\%) O_2(10\%) H_2O(10500ppm),$
- $\square$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- O CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- \* CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
   CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm),
- $CO_2(20\%) O_2(20\%) H_2O(21800ppm)$

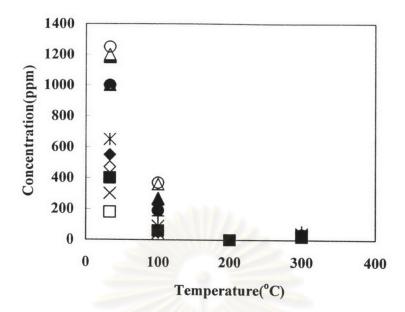


Figure 5.18 Byproduct (NO<sub>x</sub>) on the removal of CH<sub>3</sub>CHO from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub>(10%) O<sub>2</sub>(10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ▲ CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $CO_2(10\%) O_2(10\%) H_2O(10500ppm),$
- □ CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm), • CO<sub>2</sub> (10%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),
- $O_2(10\%) O_2(20\%) H_2O(10500ppm),$  $O_2(20\%) - O_2(20\%) - H_2O(10500ppm),$
- \*  $CO_2(10\%) O_2(10\%) H_2O(21800ppm)$ ,
- $\times$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- + CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm),
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

### 5.6 Removal of ammonia (NH<sub>3</sub>)

### 5.6.1 Effect of temperature and coexisting CO<sub>2</sub> on the removal of NH<sub>3</sub> from N<sub>2</sub>

Figure 5.19 shows the removal efficiency  $\psi'$  of NH<sub>3</sub> versus temperature. From Figure 5.19 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  increases monotonically from room temperature to 300°C because of the effect of CO<sub>3</sub> and O anion at low temperatures whereas at high temperatures, N radical is consumed by their reaction with CO<sub>2</sub>. Obviously, the presence of CO<sub>2</sub> positively affects the removal efficiency. The higher the CO<sub>2</sub> concentration, the higher the removal efficiency. Since CO<sub>2</sub> is a highly oxidized, thermodynamically stable compound, its utilization requires reaction with certain high-energy substances or electro reductive processes. Recent research has shown that high catalytic efficiency, yield, and rate of reaction can be obtained from CO<sub>2</sub> with the use of optimum conditions and catalysts (Ryoji Noyori et al., 1995). Figure 5.19(b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi''$  still increases as the temperature increases.

At room temperature, 100, 200 and 300°C,  $\psi_{elec}$  of NH<sub>3</sub> at 200 ppm-CO<sub>2</sub> (10%, 20%) are 0.2, 0.5, 0.7, 0.6 and 1.1, 0.8, 0.6, 0.7, respectively. Interestingly, at CO<sub>2</sub> 10%, as the temperature increases,  $\psi_{elec}$  increases from room temperature up to 200°C, above which the tendency reverses however, at CO<sub>2</sub> 20%, high temperatures has adverse effect because the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature increases.

# 5.6.2 Effect of temperature and coexisting $CO_2$ and $O_2$ on the removal of $NH_3$ from $N_2$

Figure 5.20 shows the removal efficiency  $\psi'$  of NH<sub>3</sub> versus temperature. From Figure 5.20 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  remains nearly 100% from room temperature to 300°C. As mentioned previously, this is due to the effect of O<sub>3</sub>, CO<sub>3</sub><sup>-</sup> and O<sup>-</sup> anion at low temperatures but

various radicals at high temperatures. This can partly be attributed to the fact that  $O_3$  is produced from  $O_2$  by the corona discharge reaction and is quite stable at room temperature. At room to moderate temperatures, electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro - negative compounds (Sano et al., 1997; Bityurin; 2000). N radicals should also contribute to the removal of  $NH_3$  from both  $N_2$  and air at high temperatures. In addition, in the case of removal from air, there should be the extra effect of O radicals produced by electron impact to  $O_2$  and by  $O_3$  decomposition (Peyrous, Pignolet and Held, 1989; Loiseau et al. 1994; Hadj-Ziane, 1990). Therefore, the  $NH_3$  removal efficiency  $\psi'$  at high temperatures should be enhanced by O radicals though  $O_3$  oxidation is not effective. Figure 5.20 (b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi''$  increases as the temperature increases.

At room temperature, 100, 200 and 300°C,  $\psi_{elec}$  of NH<sub>3</sub> at 200 ppm - O<sub>2</sub> (10%, 20%) - CO<sub>2</sub> (10%, 20%) are (3.8, 2.9, 2.4, 1.7), (3.9, 3.0, 2.3, 1.6), (3.2, 2.7, 2.1, 1.3), (3.8, 2.8, 2.2, 1.2) respectively. Interestingly, as mentioned in the previous section, as the temperature increases,  $\psi_{elec}$  decreases, thus indicating the possible existence of an optimal temperature. The high values of  $\psi_{elec}$  at low temperatures reveal that electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro - negative compounds (Sano et al., 1997; Bityurin; 2000). On the other hand, N radicals should contribute to the removal of NH<sub>3</sub> from both N<sub>2</sub> and air at high temperatures.

### 5.6.3 Effect of temperature and coexisting CO<sub>2</sub> and H<sub>2</sub>O on the removal of NH<sub>3</sub> from N<sub>2</sub>

Figure 5.21 shows the removal efficiency  $\psi'$  of NH<sub>3</sub> versus temperature. From Figure 5.21 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  increases from room temperature up to 200°C. Then the tendency reverses up to 300°C. As mentioned above, the effect of H<sup>-</sup>, OH<sup>-</sup>, a few O<sup>-</sup> anions and CO<sub>3</sub><sup>-</sup> should contribute to the removal of NH<sub>3</sub> at low to moderate temperatures. At high temperature, the tendency reverses because the mean residence time decreases. Figure 5.21(b) reveals that, if the negative effect of reduced residence time is taken in account, the value of  $\psi''$  continued to increase as the temperature increases.

At room temperature, 100, 200 and 300°C,  $\psi_{elec}$  of NH<sub>3</sub> at 200 ppm - H<sub>2</sub>O (5250, 10500, 21800 ppm) - CO<sub>2</sub> (10%, 20%) are (0.8, 0.9, 1.0, 1.0), (1.0, 1.0, 0.8, 0.9), (1.0, 0.7, 0.7, 0.6), (0.7, 0.8, 1.0, 0.6), (0.3, 0.6, 0.4, 0.1) and (0.1, 0.2, 0.1, 0.1) respectively. Interestingly, as the temperature increases,  $\psi_{elec}$  increases from room temperature to a moderate temperature above which the  $\psi_{elec}$  tend to significantly decrease again because the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises.

# 5.6.4 Effect of temperature and coexisting $CO_2$ , $O_2$ and $H_2O$ on the removal of $NH_3$ from $N_2$

Figure 5.22 shows the removal efficiency  $\psi'$  of NH<sub>3</sub> versus temperature. From Figure 5.22 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  remains nearly 100% from room temperature to 300°C. As mentioned previously, this is due to the effect of O<sub>3</sub>, H<sup>-</sup>, OH<sup>-</sup>, CO<sub>3</sub><sup>-</sup> and O<sup>-</sup> anion at low to moderate temperatures but that of various radicals generated from CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O at high temperatures. This can be attributed to the fact that O<sub>3</sub> is produced from O<sub>2</sub> by the corona discharge reaction and is quite stable at room temperature. At room to

moderate temperatures, electron attachment reactions contribute to, and relevant ion cluster formation enhances, the removal of numerous electro - negative compounds (Sano et al., 1997; Bityurin; 2000). N radicals should also contribute to the removal of NH<sub>3</sub> from both N<sub>2</sub> and air at high temperatures. In addition, in the case of removal from air, there should be the extra effect of O radicals produced by electron impact to O<sub>2</sub> and by O<sub>3</sub> decomposition (Peyrous, Pignolet and Held, 1989; Loiseau et al. 1994; Hadj - Ziane, 1990). At high temperatures, electron detachment would become significant so that radicals of CO<sub>3</sub>, O, H, and OH may play a more important role than their anionic counterparts. These radicals are expected to contribute to the removal of the NH<sub>3</sub>. **Figure 5.22 (b)** reveals that, if the negative effect of the reduced residence time is taken in account, the value of  $\psi^n$  increases as the temperature increases.

### 5.6.5 Preliminary summary

Generally, two other types of removal efficiency are reported for a corona-discharge system: the electron - based efficiency  $\psi_{elec}$  (-) and the energy - based efficiency  $\psi_{ener}$  (mol gas .J<sup>-1</sup>). At 33, 100, 200 and 300°C, the experimental values of  $\psi_{elec}$  and  $\psi_{ener}$  of the NH<sub>3</sub> 200 ppm removal are as follows:

$$N_2$$
 -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 0.2, 0.5, 0.7, 0.6$   $\psi_{ener} \times 10^{-9} = 0.32, 1.0, 2.1, 2.2$   
 $N_2$  -  $O_2$  (10%) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 3.8, 2.9, 2.4, 1.7$   $\psi_{ener} \times 10^{-9} = 4.6, 3.9, 3.8, 3.7$   
 $N_2$  -  $H_2O$  (10500 ppm) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 1.0, 0.7, 0.7, 0.6$   $\psi_{ener} \times 10^{-9} = 1.6, 1.4, 1.8, 1.8$   
 $N_2$  -  $O_2$  (10%) -  $H_2O$  (10500 ppm) -  $CO_2$  (10%), (I=0.2 mA):  
 $\psi_{elec} = 3.8, 2.9, 2.3, 1.7$   $\psi_{ener} \times 10^{-9} = 4.7, 4.1, 3.9, 3.9$ 

Generally,  $\psi_{elec}$  and  $\psi_{ener}$  tend to decrease as the gas temperature increases. This trend may be ascribed to the combined effect of the reduced residence time and the shift in removal mechanism. Interestingly, in the case of N<sub>2</sub> - CO<sub>2</sub>,  $\psi_{elec}$  and  $\psi_{ener}$  tend to increase as the gas temperature increases, thus indicating the possible existence of an optimal temperature.

In actual applications of gas purification, it is important to consider the energy-based efficiency  $\psi_{ener}$ . From the above results, it is recommended to operate in the range from  $100^{\circ}\text{C}$  to  $200^{\circ}\text{C}$  so as to minimize the operating cost when air is purified, Compared to the case of the removal of CH<sub>3</sub>CHO from N<sub>2</sub> - CO<sub>2</sub>,  $\psi_{ener}$  of NH<sub>3</sub> at  $200^{\circ}\text{C}$  is approximately 20% lower than that in the case of CH<sub>3</sub>CHO, thus indicating the operating cost of the removal of NH<sub>3</sub> from N<sub>2</sub> - CO<sub>2</sub> are lower than that of CH<sub>3</sub>CHO.



### 5.6.6 Byproducts dected on the removal of ammonia

Figure 5.23 shows the concentration of the byproduct CO versus temperature in the presence of CO<sub>2</sub>. In Figure 5.23 as the temperature increases, the byproduct CO increases because of the effect of O anion and CO<sub>3</sub> at low temperature. At high temperatures, electron detachment would become significant so that radicals of N, H, O, CO<sub>3</sub> and OH may play a more important role than their anionic counterparts. As mentioned previously, production of CO by dissociative attachment reaction is known.

Figure 5.24 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $CO_2$ . In Figure 5.24 as the temperature increases, the byproduct  $NO_x$  increases. As mentioned previously, it is known that production of  $NO_x$  take place by the discharge process of  $NH_3$  and  $N_2$  at high temperatures. This is also confirmed in our experiments. Though the outlet concentration of  $NO_x$  was negligible at room temperature,  $NO_x$  concentration gradually increases as the temperature rise.

Figure 5.25 shows the concentration of the byproduct CO versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.25 as the temperature increases, the byproduct CO decreases as the temperature rises because  $O_3$  is unstable at high temperature.

Figure 5.26 shows the concentration of the byproduct  $O_3$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.26 as the temperature increases, the byproduct  $O_3$  decreases. This is because  $O_3$  is unstable at high temperature (Peyrous, Pignolet and Held, 1989; Devins, 1956).

**Figure 5.27** shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In **Figure 5.27** as the temperature increases, the byproduct  $NO_x$  decrease from room temperature up 200°C, then the tendency reverses up to 300°C.

Figure 5.28 shows the concentration of the byproduct CO versus temperature in the presence of H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.28 as the temperature increases, the byproduct CO increases from room temperature up 100°C. Above 100°C the CO concentration tends to decrease because at high temperatures, H<sub>2</sub>O is unstable and

the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature increases.

**Figure 5.29** shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $H_2O$  and  $CO_2$ . In **Figure 5.29** as the temperature increases, the byproduct  $NO_x$  increases. It is known that production of  $NO_x$  by the discharge process is favored at high temperatures. This fact is also confirmed in our experiments. While, the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased as the temperature rises.

Figure 5.30 shows the concentration of the byproduct CO versus temperature in the presence of O<sub>2</sub>, H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.30 as the temperature increases, the byproduct CO increases from room temperature up 200°C, then the tendency reverses up to 300°C. At low temperatures, H<sub>2</sub>O is present in the gas stream, CO<sub>3</sub>, H<sup>-</sup>, OH<sup>-</sup> and O<sup>-</sup> anions are expected to be produced by dissociative electron attachment to CO<sub>2</sub> and H<sub>2</sub>O molecules (Massey, 1976; Moruzzi and Phelps, 1966). At high temperatures CO<sub>2</sub>, O<sub>3</sub> and H<sub>2</sub>O become unstable as the temperature rises. On the other hand, the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises.

Figure 5.31 shows the concentration of the byproduct  $O_3$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.31 as the temperature increases, the byproduct  $O_3$  decreases because at high temperatures,  $O_3$  is unstable (Peyrous, Pignolet and Held, 1989; Devins, 1956).

Figure 5.32 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.32 as the temperature increases, the byproduct  $NO_x$  decrease from room temperature up  $200^{\circ}C$ , then the tendency reverses up to  $300^{\circ}C$ .

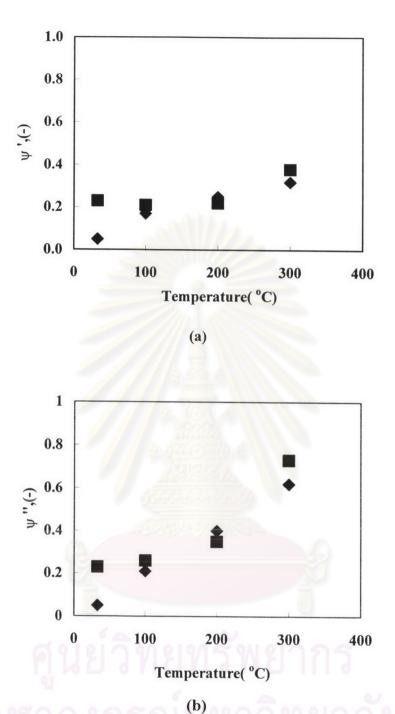
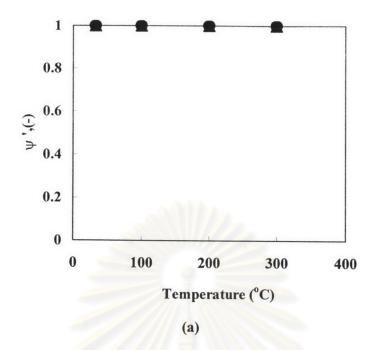


Figure 5.19 Effect of coexisting  $CO_2$  on the removal of  $NH_3$  from  $N_2$ ;  $C_{in,ammonia}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2$  (10%),  $CO_2$  CO<sub>2</sub> (20%)



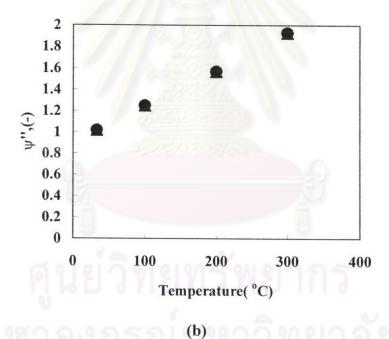
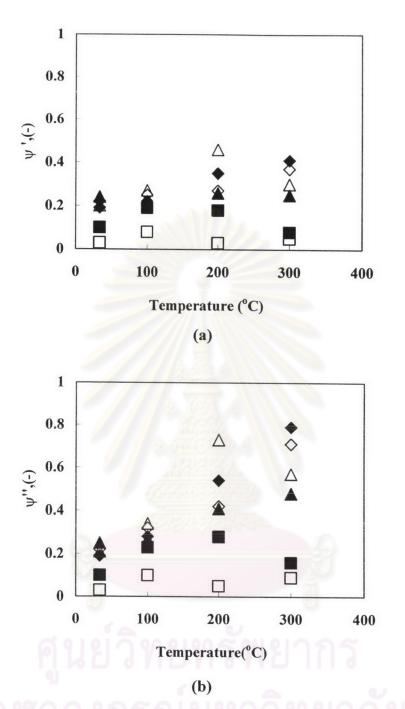


Figure 5.20 Effect of coexisting  $O_2$ - $CO_2$  on the removal of  $NH_3$  from  $N_2$ ;  $C_{in,ammonia}=200 ppm, I=0.2 mA, SV=55.8 hr^{-1} at room temperature:$   $CO_2 (10\%) - O_2 (10\%),$   $CO_2 (20\%) - O_2 (10\%),$ 

■ CO<sub>2</sub>(20%) - O<sub>2</sub>(10%), ■ CO<sub>2</sub>(10%) - O<sub>2</sub>(20%), ■ CO<sub>2</sub>(20%) - O<sub>2</sub>(20%)



 $\square$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)

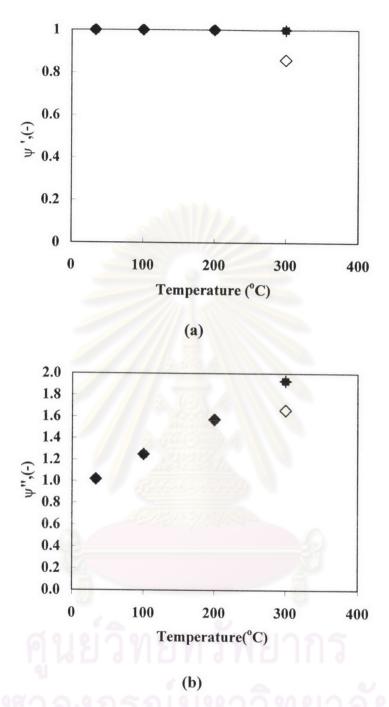


Figure 5.22 Effect of coexisting  $O_2$ -H<sub>2</sub>O-CO<sub>2</sub> on the removal of NH<sub>3</sub> from N<sub>2</sub>;  $C_{in,ammonia}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2(10\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),  $\diamondsuit$  CO<sub>2</sub> (20%)-O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),  $CO_2(10\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20

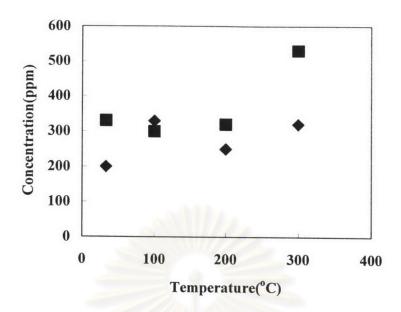


Figure 5.23 Byproduct (CO) on the removal of NH<sub>3</sub> from N<sub>2</sub>-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%),  $\blacksquare$  CO<sub>2</sub> (20%)

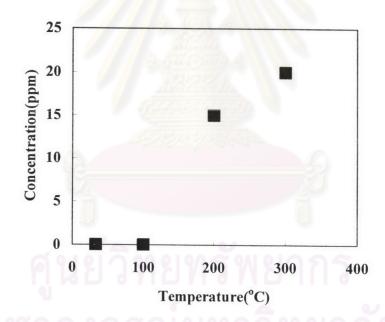


Figure 5.24 Byproduct (NO<sub>x</sub>) on the removal of NH<sub>3</sub> from N<sub>2</sub>-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%),  $\blacksquare$  CO<sub>2</sub> (20%)

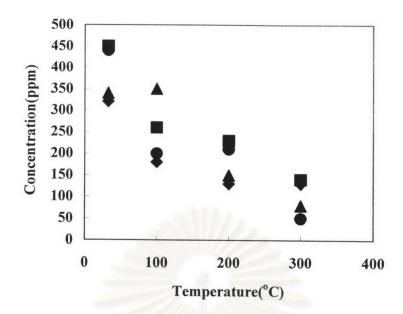


Figure 5.25 Byproduct (CO) on the removal of NH<sub>3</sub> from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

CO<sub>2</sub> (10%) - O<sub>2</sub> (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

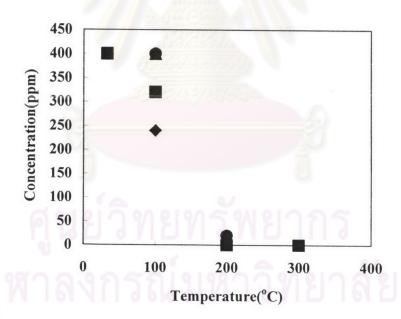


Figure 5.26 Byproduct  $(O_3)$  on the removal of  $NH_3$  from  $N_2$ - $O_2$ - $CO_2$ :

 $\bullet$  CO<sub>2</sub> (10%) - O<sub>2</sub> (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub>(10%) - O<sub>2</sub>(20%),

• CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

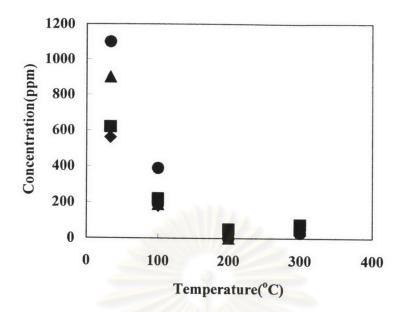


Figure 5.27 Byproduct (NO<sub>x</sub>) on the removal of NH<sub>3</sub> from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

 $\bullet$  CO<sub>2</sub> (10%) - O<sub>2</sub> (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

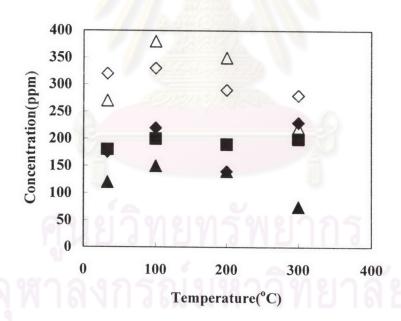


Figure 5.28 Byproduct (CO) on the removal of NH<sub>3</sub> from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

◆ CO<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),

♦ CO<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

 $\triangle$  CO<sub>2</sub>(10%) - H<sub>2</sub>O (10500ppm),

 $\triangle$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),

 $\square$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),

 $\square$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)

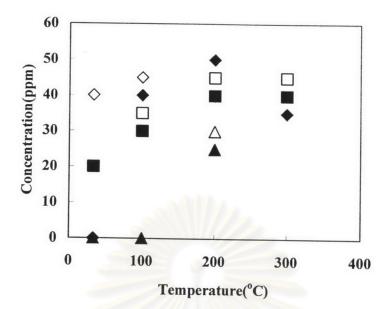


Figure 5.29 Byproduct (NO<sub>x</sub>) on the removal of NH<sub>3</sub> from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- ◆ CO<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\triangle$  CO<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\square$  CO<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

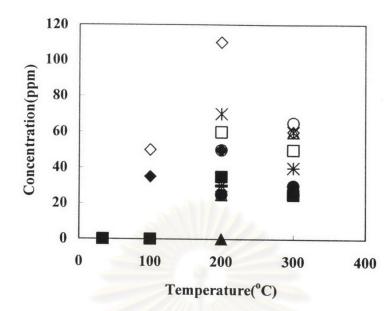


Figure 5.30 Byproduct (CO) on the removal of NH<sub>3</sub> from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\square$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\square$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- $O CO_2(20\%) O_2(20\%) H_2O(10500ppm),$
- \* CO<sub>2</sub>(10%) O<sub>2</sub>(10%) H<sub>2</sub>O (21800ppm),
- × CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- + CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm),
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

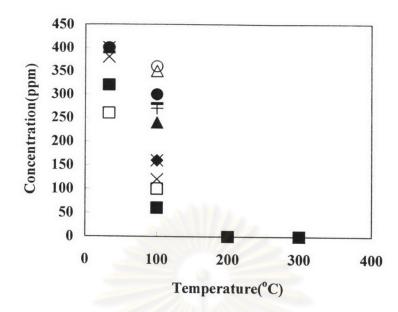


Figure 5.31 Byproduct (O<sub>3</sub>) on the removal of NH<sub>3</sub> from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\Diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\square$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $O_2(10\%) O_2(20\%) H_2O(10500ppm),$  $O_2(20\%) - O_2(20\%) - H_2O(10500ppm)$
- O CO<sub>2</sub>(20%) O<sub>2</sub>(20%) H<sub>2</sub>O (10500ppm),
- \* CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm), × CO<sub>2</sub> (20%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),
- $+ CO_2(10\%) O_2(20\%) H_2O(21800ppm),$
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

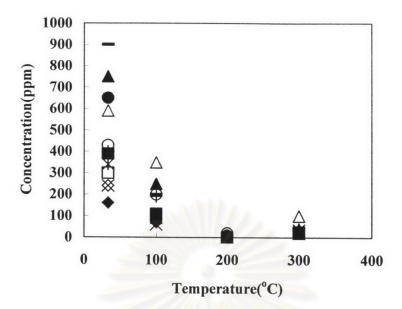


Figure 5.32 Byproduct (NO<sub>x</sub>) on the removal of NH<sub>3</sub> from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $CO_2(10\%) O_2(10\%) H_2O(10500ppm),$
- $\square$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- O CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm), \* CO<sub>2</sub> (10%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),
- $\times$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),  $\times$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $+ CO_2(10\%) O_2(20\%) H_2O(21800ppm),$
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

#### 5.7 Removal of trimethyl amine (CH<sub>3</sub>)<sub>3</sub>N

### 5.7.1 Effect of temperature and coexisting $CO_2$ on the removal of $(CH_3)_3N$ from $N_2$

Figure 5.33 shows the removal efficiency  $\psi'$  of  $(CH_3)_3N$  versus temperature. From Figure 5.33 (a), we see that, as the temperature increases, the removal efficiency  $\psi'$  remains nearly 100% from room temperature up to 200°C. In addition, the reduction of  $(CH_3)_3N$  concentration via the thermal decomposition at 300°C may contribute to the enhancement of the removal efficiency of  $(CH_3)_3N$ . Obviously, the presence of  $CO_2$  does significantly affect the removal efficiency. The higher the  $CO_2$  concentration, the higher the removal efficiency. Since  $CO_2$  is a highly oxidized, thermodynamically stable compound, its utilization requires reaction with certain high - energy substances or electro reductive processes. Figure 5.33(b) reveals that when the negative effect of reduced residence time is taken in account, the value of  $\psi''$  continues to increase as the temperature increases.

## 5.7.2 Effect of temperature and coexisting CO<sub>2</sub> and O<sub>2</sub> on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

**Figure 5.34** shows the two kinds of removal efficiency of  $(CH_3)_3N$  versus temperature. It is found that, as the temperature increases, the removal efficiency  $\psi'$  and  $\psi''$  equal to 100% even in blank tests without corona discharge at 100°C to 300°C. This means that the thermal decomposition of  $(CH_3)_3N$  contributes to complete removal efficiency of  $(CH_3)_3N$ . To distinguish the perfect effect of thermal decomposition, the removal efficiency  $\psi'$  and  $\psi''$  are arbitrarily shown as zero. As mentioned previously, the improved removal efficiency for  $(CH_3)_3N$  can be attributed to effect of  $CO_3$ ,  $O_3$  and  $O^*$  anion at low temperatures and various radicals at high temperatures. Obviously, the presence of  $O_2$  does significantly enhance the removal efficiency of  $(CH_3)_3N$ .

## 5.7.3 Effect of temperature and coexisting $CO_2$ and $H_2O$ on the removal of $(CH_3)_3N$ from $N_2$

Figure 5.35 shows the two kinds of removal efficiency of  $(CH_3)_3N$  versus temperature. It is found that, as the temperature increases, the removal efficiency  $\psi'$  and  $\psi''$  equal to 100% even in blank tests without corona discharge at 100°C to 300°C. As in 5.72 the thermal decomposition of  $(CH_3)_3N$  concentration contributes to the complete removal efficiency of  $(CH_3)_3N$  above 100°C. As mentioned previously, H, OH,  $CO_3$  and O anions should contribute to the removal of  $(CH_3)_3N$  at low to moderate temperatures. Obviously, the presence of  $H_2O$  does significantly enhance the removal efficiency of  $(CH_3)_3N$ .

## 5.74 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.36 shows the two kinds of removal efficiency of  $(CH_3)_3N$  versus temperature. It is again found that, as the temperature increases, the removal efficiency  $\psi'$  and  $\psi''$  equal to 100% even in blank test without corona discharge at  $100^{\circ}$ C to  $300^{\circ}$ C. As mentioned previously,  $CO_3$ , H, OH,  $O_3$  and O anions should contribute to the removal of  $(CH_3)_3N$  at low to moderate temperatures. Obviously, the presence of  $O_2$  and  $O_3$  significantly enhance the removal efficiency of  $(CH_3)_3N$ .

#### 5.75 Preliminary summary

Generally, two more types of removal efficiency are often reported for a corona-discharge system: the electron-based efficiency  $\psi_{elec}$  (-) and the energy - based efficiency  $\psi_{ener}$  (mol gas .J<sup>-1</sup>). At 33, 100, 200 and 300°C, the experimental values of  $\psi_{elec}$  and  $\psi_{ener}$  of the (CH<sub>3</sub>)<sub>3</sub>N 200 ppm removal are as follows:

N<sub>2</sub> - CO<sub>2</sub> (10%), (I=0.2 mA): 
$$\psi_{elec} = 4.5, 3.9, 3.0, 0.0 \qquad \psi_{ener} \times 10^{-9} = 6.1, 5.9, 5.9, 0.0$$

$$\begin{split} N_2 - O_2 & (10\%) - CO_2 (10\%), (I=0.2 \text{ mA}): \\ \psi_{elec} &= 3.8, -0.6, -0.1, 0.0 \quad \psi_{ener} \times 10^{-9} = 4.4, -8.8, -8.7, 0.0 \\ N_2 - H_2O & (10500 \text{ ppm}) - CO_2 & (10\%), (I=0.2 \text{ mA}): \\ \psi_{elec} &= 3.9, -0.1, 0.0, 0.0 \quad \psi_{ener} \times 10^{-9} = 5.3, -0.13, 0.0, 0.0 \\ N_2 - O_2 & (10\%) - H_2O & (10500 \text{ ppm}) - CO_2 & (10\%), (I=0.2 \text{ mA}): \\ \psi_{elec} &= 2.9, -0.5, 0.0, 0.0 \quad \psi_{ener} \times 10^{-9} = 3.3, -0.7, -0.07, 0.0 \end{split}$$

Typically,  $\psi_{elec}$  and  $\psi_{ener}$  tend to decrease as the gas temperature increases. This trend may be ascribed to the combined effect of the reduced residence time and the shift in removal mechanism. Interestingly, in some cases  $\psi_{elec}$  and  $\psi_{ener}$  are negative because  $(CH_3)_3N$  is thermally decomposed even without corona discharge but the corona discharge resulted in the detection of  $(CH_3)_3N$ , thus indicating a high electron energy level could affect the reaction mechanism.

In actual applications of gas purification, it is important to maximaze the energy - based efficiency  $\psi_{ener}$ . From the above results, it is recommended to operate at 300°C when air is purified. Compared to the case of the removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub> - CO<sub>2</sub>, the average value  $\psi_{ener}$  of (CH<sub>3</sub>)<sub>3</sub>N is lower than that the case of CH<sub>3</sub>CHO by approximately 10% but higher than that the case of NH<sub>3</sub> by approximately 70%. This indicates that the operating costs of the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub> - CO<sub>2</sub> are lower than that of CH<sub>3</sub>CHO but higher than that of NH<sub>3</sub>.

### 5.76 Byproducts dected on the removal of trimethyl amine

**Figure 5.37** shows the concentration of the byproduct CO versus temperature in the presence of CO<sub>2</sub>. In **Figure 5.37**, as the temperature increases, the byproduct CO increases due to CO<sub>3</sub><sup>-</sup> and O<sup>-</sup> anion at low temperature. At high temperatures, electron detachment would become significant so that radicals of O, H, and N may play a more important role than their anionic counterparts. As mentioned previously, production of CO is caused by dissociative attachment reaction.

Figure 5.38 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $CO_2$ . In Figure 5.38, as the temperature increases, the byproduct  $NO_x$  increases. As mentioned previously, it is well known that production of  $NO_x$  take place by the discharge process is favored at high temperatures. This phenomenon is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature,  $NO_x$  concentration gradually increase as the with temperature rise.

Figure 5.39 shows the concentration of byproduct CO versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.39, as the temperature increases, the byproduct CO decreases because at high temperatures,  $O_3$  is unstable.

Figure 5.40 shows the concentration of the byproduct  $O_3$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.40, as the temperature increases, the byproduct  $O_3$  decreases because  $O_3$  is unstable at high temperatures (Peyrous, Pignolet and Held, 1989; Devins, 1956).

**Figure 5.41** shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In **Figure 5.41**, as the temperature increases from room temperature up  $200^{\circ}$ C, the byproduct  $NO_x$  decreases then the tendency reverses from  $200^{\circ}$ C to  $300^{\circ}$ C.

**Figure 5.42** shows the concentration of the byproduct CO versus temperature in the presence of H<sub>2</sub>O and CO<sub>2</sub>. In **Figure 5.42**, as the temperature increases, the byproduct CO increases from room temperature to 100°C, then the tendency reverses up to 200°C and increases again at 300°C. At low temperatures, since CO<sub>2</sub> and H<sub>2</sub>O are present in the gas stream, CO<sub>3</sub>-, H-, OH- and O- anions are produced by dissociative electron attachment (Massey, 1976; Moruzzi and Phelps, 1966). At

200°C, the presence of CO<sub>2</sub> and H<sub>2</sub>O slightly retards the production of CO because at a low discharge current, the relatively much smaller number of electrons tends to attach mostly to CO<sub>2</sub> and H<sub>2</sub>O. At high temperatures, electron detachment would become significant so that radicals of CO<sub>3</sub>, O, H, N, and OH may play a more important role than their anionic counterparts. The mean residence time of the gas mixture inside the reactor decreases as the reactor temperature increases.

Figure 5.43 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $H_2O$  and  $CO_2$ . In Figure 5.43, as the temperature increases, the byproduct  $NO_x$  increases. It is known that production of  $NO_x$  by the discharge process is favored at high temperatures. This fact is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased as the temperature rises.

Figure 5.44 shows the concentration of the byproduct CO versus temperature in the presence of O<sub>2</sub>, H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.44 as the temperature increases, the byproduct CO increases from room temperature to 100°C, then the tendency reverses up to 200°C but increases again at 300°C. The reason was given in relation to Figure 5.42

Figure 5.45 shows the concentration of the byproduct  $O_3$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.45 as the temperature increases, the byproduct  $O_3$  decreases with temperature rise because  $O_3$  is unstable at high temperature.

Figure 5.46 shows the concentration of the byproduct  $NO_x$  versus temperature in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$ . In Figure 5.46 as the temperature increases, the byproduct  $NO_x$  decreases from room temperature up to  $200^{\circ}$ C, then the tendency reverses up to  $300^{\circ}$ C. The reasons were given previously in relation Figure 5.38.

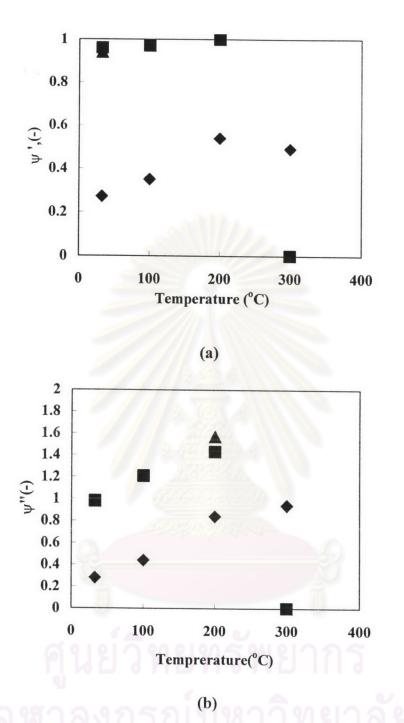


Figure 5.33 Effect of coexisting  $CO_2$  on the removal of  $(CH_3)_3N$  from  $N_2$ ;  $C_{in.trimethylamine}=200$ ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2$  (0%)  $CO_2$  (10%)  $CO_2$  (20%)

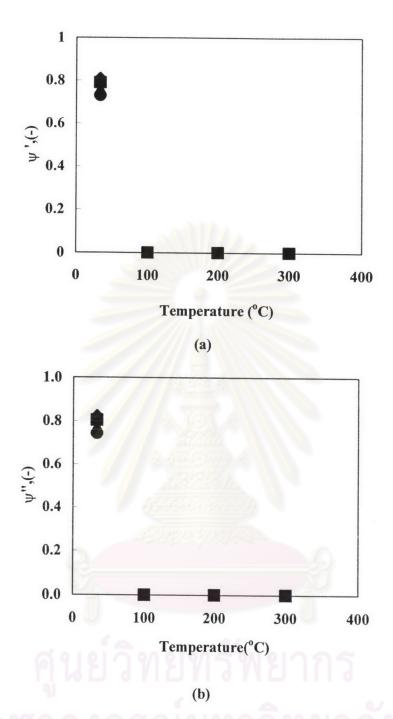
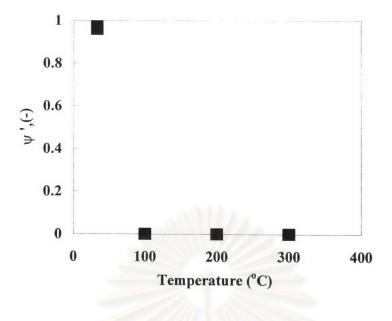


Figure 5.34 Effect of coexisting  $O_2$ - $CO_2$  on the removal of  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,trimethylamine}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2$  (10%) -  $O_2$  (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\square$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

• CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)



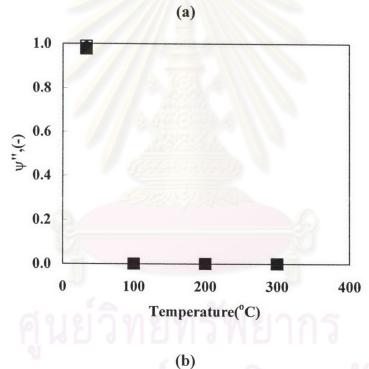


Figure 5.35 Effect of coexisting  $H_2O-CO_2$  on the removal of  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,trimethylamine}=200$ ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- $\bullet$  CO<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- ▲ CO<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\triangle$  CO<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\square$  CO<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

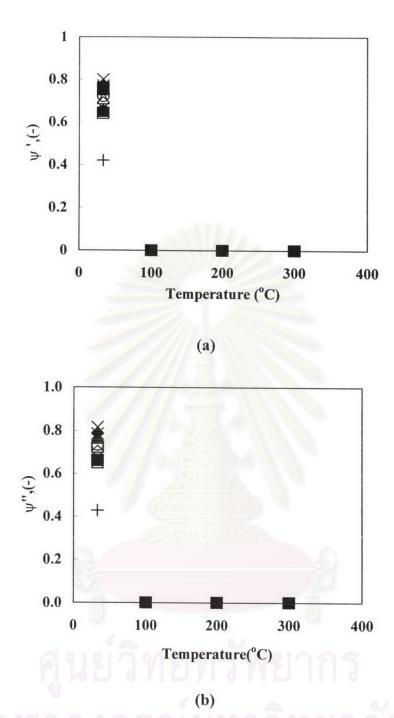


Figure 5.36 Effect of coexisting  $O_2$ -H<sub>2</sub>O-CO<sub>2</sub> on the removal of  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,trimethylamine}$ =200ppm, I=0.2mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2(10\%)$ -O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (10500ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm),  $CO_2(10\%)$ -O<sub>2</sub> (20%)-O<sub>2</sub> (20%)-H<sub>2</sub>O (21800ppm)

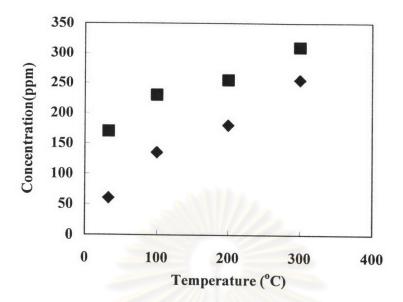


Figure 5.37 Byproduct (CO) on the removal of  $(CH_3)_3N$  from  $N_2$ - $CO_2$ :  $CO_2$  (10%),  $CO_2$  (20%)

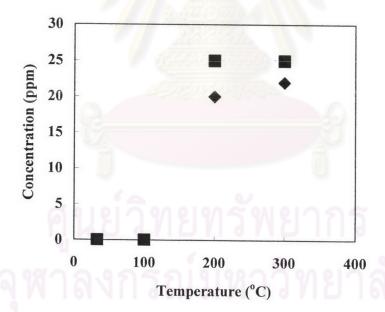


Figure 5.38 Byproduct (NO<sub>x</sub>) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%),  $\blacksquare$  (CO<sub>2</sub> 20%)

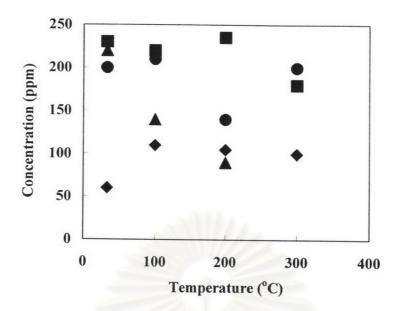


Figure 5.39 Byproduct (CO) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

 $\bullet$  CO<sub>2</sub> (10%) - O<sub>2</sub> (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\square$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

• CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

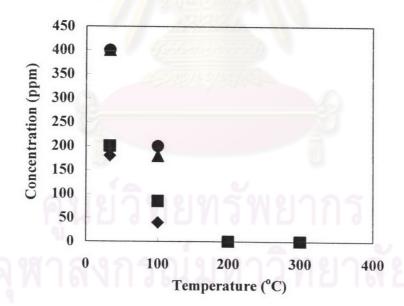


Figure 5.40 Byproduct  $(O_3)$  on the removal of  $(CH_3)_3N$  from  $N_2$ - $O_2$ - $CO_2$ :

◆ CO<sub>2</sub> (10%) - O<sub>2</sub> (10%),

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

•  $CO_2(20\%) - O_2(20\%)$ 

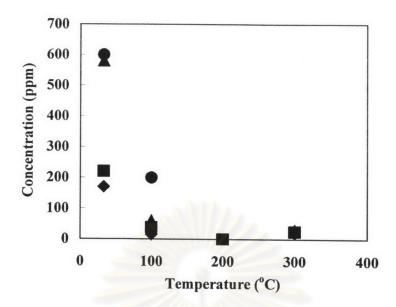


Figure 5.41 Byproduct (NO<sub>x</sub>) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

 $CO_2(10\%) - O_2(10\%),$ 

 $\triangle$  CO<sub>2</sub> (20%) - O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub> (10%) - O<sub>2</sub> (20%),

CO<sub>2</sub> (20%) - O<sub>2</sub> (20%)

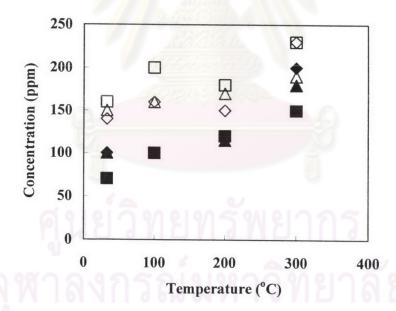


Figure 5.42 Byproduct (CO) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

CO<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),

♦ CO<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

 $\triangle$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm),

 $\triangle$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),

CO<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),

 $\square$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)

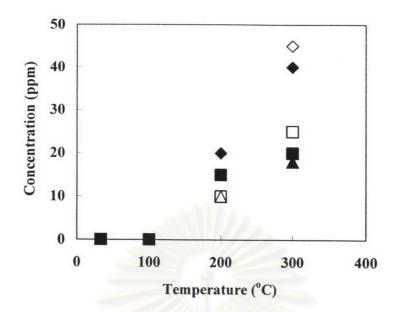


Figure 5.43 Byproduct (NO<sub>x</sub>) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:  $\bullet$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),

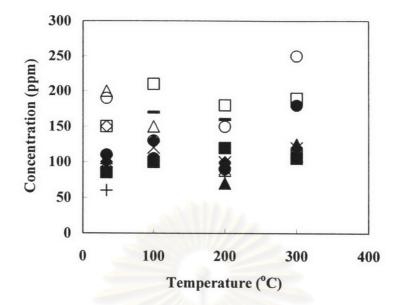
 $\diamond$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

 $\triangle$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm),

 $\triangle$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),

CO<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),

 $\square$  CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)



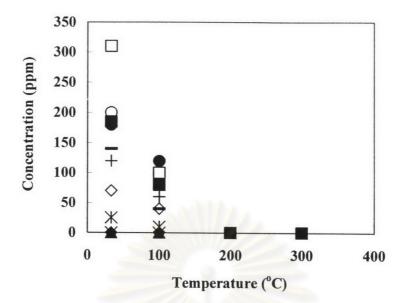
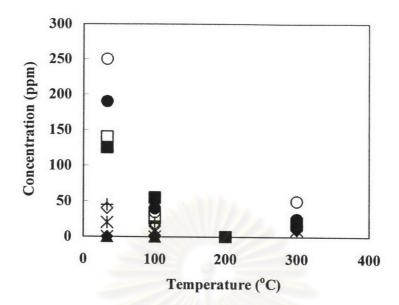


Figure 5.45 Byproduct (O<sub>3</sub>) on the removal of (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>: ◆ CO<sub>2</sub> (10%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm), ♦ CO<sub>2</sub> (20%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm), ▲ CO<sub>2</sub> (10%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm), Δ CO<sub>2</sub> (20%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

- $CO_2(10\%) O_2(10\%) H_2O (10500ppm),$   $CO_2(20\%) - O_2(10\%) - H_2O (10500ppm),$   $CO_2(10\%) - O_2 (20\%) - H_2O (10500ppm),$  $CO_2(20\%) - O_2 (20\%) - H_2O (10500ppm),$
- \* CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm), × CO<sub>2</sub> (20%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),
- +  $CO_2(10\%) O_2(10\%) H_2O(21800ppm)$ ,
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)



#### 5.8 Simultaneous removal of acetaldehyde and ammonia

### 5.8.1 Effect of temperature and coexisting CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>

Figure 5.47 shows the effect of CO<sub>2</sub> on the simultaneous removal efficiency of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>. The inlet concentrations of CH<sub>3</sub>CHO and NH<sub>3</sub> are 150 ppm and 1,000 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of CO2 has a significant enhancement effect on the simultaneous CH<sub>3</sub>CHO removal efficiency w in Figure 5.47(a). As the temperature increases from room temperature up to 200°C, the removal efficiency  $\psi'$  decreases then the tendency reverses up to 300°C because of the effect of O anion and CO3 at low temperatures and the reduced mean residence time of the gas mixture inside the reactor. As mentioned previously, it is postulated that CO2 is less electronegative than CH<sub>3</sub>CHO but the bonding strength CO<sub>2</sub> molecules with the anode surface is stronger than that of CH<sub>3</sub>CHO. At low temperatures when a small number of electrons are available at a low discharge current, most electrons attach onto CH<sub>3</sub>CHO, and the deposit on the anode wall is composed of mostly CH<sub>3</sub>CHO. At high temperatures, there is an excess of electrons that can attach to CO<sub>2</sub>. When the CO<sub>2</sub> ions deposit on the anode surface, they replace (drive off) some of the previously deposited CH<sub>3</sub>CHO. Similarly, in Figure 5.47(b), as the temperature increases, the removal efficiency  $\psi'$  of NH<sub>3</sub> decreases from room temperature up to 200°C, and then the tendency reverses up to 300°C. As expected, the presence of CO2 has a significant enhancement effect on the simultaneous removal efficiency of NH<sub>3</sub>.

# 5.8.2 Effect of temperature and coexisting CO<sub>2</sub> and O<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>

Figure 5.48 shows the effect of  $CO_2$  and  $O_2$  on the simultaneous removal efficiency of  $CH_3CHO$  and  $NH_3$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$  and  $NH_3$  are 150 ppm and 1,000 ppm, respectively, while the current is 0.3 mA. In Figure 5.48(a), as the temperature increases, the removal efficiency  $\psi'$  of  $CH_3CHO$  decrease from room temperature up to 300°C because of lesser  $O_3$  generated from  $O_2$  and reduced mean residence time of the gas mixture inside the reactor at high temperatures. Similarly, in Figure 5.48(b), as the temperature increases, the removal efficiency  $\psi'$  of  $NH_3$  decreases from room temperature up to 300°C. The presence of  $CO_2$  does significantly enhance the removal efficiency of  $CH_3CHO$  and  $NH_3$  from  $N_2$  -  $O_2$ .

# 5.8.3 Effect of temperature and coexisting CO<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>

Figure 5.49 shows the effect of  $CO_2$  and  $H_2O$  on the simultaneous removal efficiency of  $CH_3CHO$  and  $NH_3$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$  and  $NH_3$  are 150 ppm and 1,000 ppm, respectively, while the current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $CH_3CHO$  removal efficiency  $\psi'$  in Figure 5.49(a), as the temperature increases from room temperature up to  $200^{\circ}C$ , the removal efficiency  $\psi'$  of  $CH_3CHO$  decreases, then the tendency reverses up to  $300^{\circ}C$  because of the reduced mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. As mentioned previously, H', OH', O' anions and  $CO_3$  should contribute to the removal of  $CH_3CHO$  at low to moderate temperatures. At  $200^{\circ}C$ , the presence of  $H_2O$  and  $CO_2$  slightly retards the removal efficiency of  $CH_3CHO$  because at low discharge current, the relatively much smaller number of electrons tends to attach mostly to  $H_2O$  and  $CO_2$  In addition, N radicals are consumed by their

reaction with  $CO_2$  and  $H_2O$  at high temperatures. In **Figure 5.49(b)**, as the temperature increases, the removal efficiency  $\psi'$  of NH<sub>3</sub> decreases from room temperature up to  $200^{\circ}$ C, then the tendency reverses up to  $300^{\circ}$ C because this condition, the synthesis occurs of NH<sub>3</sub> again. On the other hand, the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. Obviously, the presence of  $CO_2$  does significantly enhance the removal efficiency.

### 5.84 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>

Figure 5.50 shows the effect of  $CO_2$  and  $H_2O$  on the simultaneous removal efficiency of  $CH_3CHO$  and  $NH_3$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$  and  $NH_3$  are 150 ppm and 1,000 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $CH_3CHO$  removal efficiency  $\psi'$  in Figure 5.50(a). As the temperature increases from room temperature up to  $300^{\circ}C$ , the removal efficiency  $\psi'$  decreases. As mentioned previously,  $CO_3^-$ ,  $H^-$ ,  $OH^-$ ,  $O_3$  and  $O^-$  anions should contribute to the removal of  $CH_3CHO$  at low to moderate temperatures but at high temperatures  $CO_2$ ,  $O_3$  and  $H_2O$  unstable. Similarity in Figure 5.50(b), as temperature increases, the removal efficiency  $\psi'$  decreases from room temperature up to  $300^{\circ}C$ . The presence of  $CO_2$  does significantly enhance the removal efficiency of  $NH_3$  from  $N_2 - O_2 - H_2O$ .

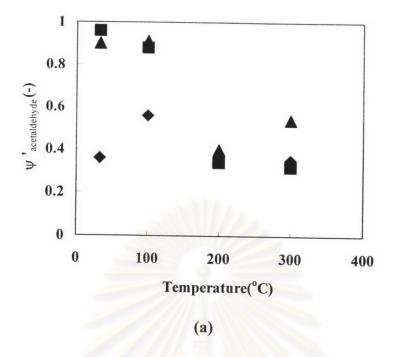
#### 5.85 Byproducts from the simultaneous removal of acetaldehyde and ammonia

**Figure 5.51** shows the concentration of byproduct CO versus temperature. In **Figure 5.51** as the temperature increases, the byproduct CO decreases from room temperature to  $100^{\circ}$ C, above which the tendency reverses up to  $300^{\circ}$ C because of the effect of O anion and CO<sub>3</sub> at low temperature. At high temperatures, the mean residence time of the gas mixture inside the reactor decreases.

Figure 5.52 shows the concentration of byproduct  $O_3$  versus temperature. In Figure 5.52 as the temperature increases, the byproduct  $O_3$  decreases because  $O_3$  is unstable at high temperatures.

Figure 5.53 shows the concentration of byproduct  $NO_x$  versus temperature. In Figure 5.53 as the temperature increases, the byproduct  $NO_x$  decreases from room temperature up 200°C, then the tendency reverses up to 300°C because the byproduct  $O_3$  decreases with the temperature rise and so does the mean residence time of the gas mixture inside the reactor.





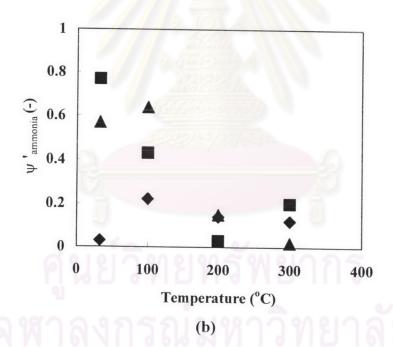
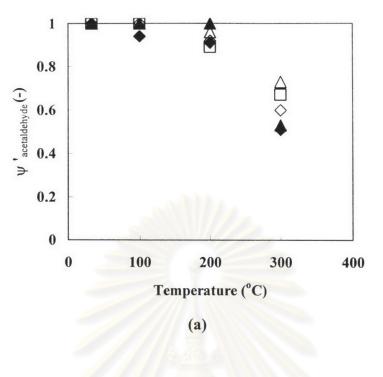
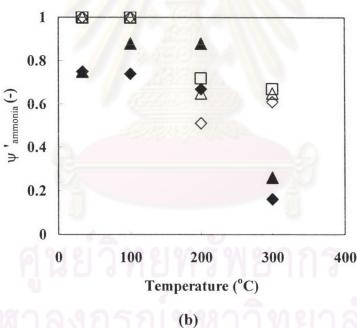


Figure 5.47 Effect of coexisting  $CO_2$  on the simultaneous removal of  $CH_3CHO$  and  $NH_3$  from  $N_2$ ;  $C_{in, acetaldehyde} = 150 ppm$ ,  $C_{in, ammonia} = 1000 ppm$ , I=0.3 mA,  $SV=55.8 \ hr^{-1}$  at room temperature :  $CO_2(0\%)$ ,  $CO_2(0\%)$ 





**Figure 5.48** Effect of coexisting  $O_2$ - $CO_2$  on the simultaneous removal of  $CH_3CHO$  and  $NH_3$  from  $N_2$ ;  $C_{in, acetaldehyde}$ =150ppm,  $C_{in, ammonia}$ =1000ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%) O<sub>2</sub> (10%),
- $\Diamond$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\square$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%),
- $\triangle$  CO<sub>2</sub> (0%) O<sub>2</sub> (20%),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%)

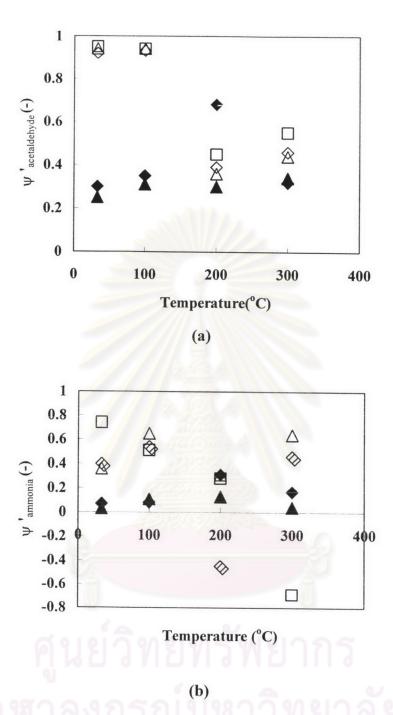


Figure 5.49 Effect of coexisting  $H_2O$ - $CO_2$  on the simultaneous removal of  $CH_3CHO$  and  $NH_3$  from  $N_2$ ;  $C_{in, acetaldehyde}$ =150ppm,  $C_{in, ammonia}$ =1000ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $CO_2(0\%) - H_2O(5250$ ppm),  $CO_2(10\%) - H_2O(5250$ ppm),  $CO_2(20\%) - H_2O(5250$ ppm),  $CO_2(0\%) - H_2O(5250$ ppm),  $CO_2(0\%) - H_2O(10500$ ppm),

 $\triangle$  CO<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm)

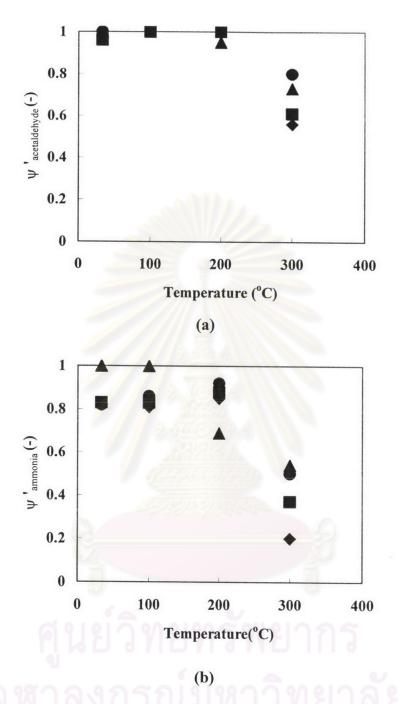


Figure 5.50 Effect of coexisting  $O_2$ -H<sub>2</sub>O-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub> from N<sub>2</sub>;  $C_{\text{in, acetaldehyde}}$ =150ppm,  $C_{\text{in, ammonia}}$ =1000ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :  $\bigcirc$  CO<sub>2</sub> (0%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),  $\bigcirc$  CO<sub>2</sub> (0%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm),  $\bigcirc$  CO<sub>2</sub> (10%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),  $\bigcirc$  CO<sub>2</sub> (0%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),

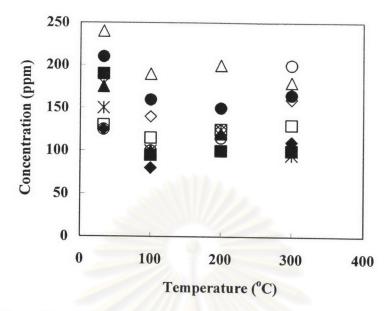


Figure 5.51 Byproduct (CO) on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub>:

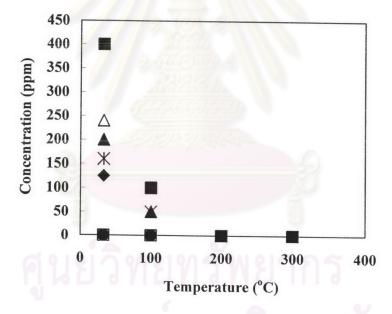


Figure 5.52 Byproduct (O<sub>3</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub>:

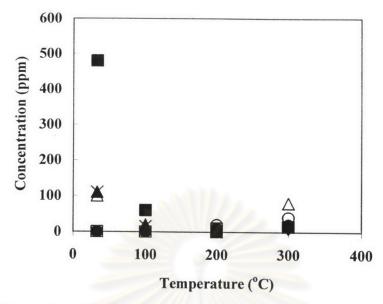


Figure 5.53 Byproduct (NO<sub>x</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and NH<sub>3</sub>:



#### 5.9 Simultaneous removal of acetaldehyde and trimethylamine

# 5.91 Effect of temperature and coexisting CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.54 shows the effect of CO<sub>2</sub> on the simultaneous removal efficiency of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>. The inlet concentrations of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N are 150 ppm and 100 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of CO<sub>2</sub> has a significant enhancement effect on the simultaneous CH<sub>3</sub>CHO removal efficiency  $\psi'$  in Figure 5.54(a), as the temperature increases, the CH<sub>3</sub>CHO removal efficiency  $\psi'$  increases from room temperature up to 100°C, above which the CH<sub>3</sub>CHO removal efficiency tends to significantly decreases because effect of O anion and CO3 at low temperatures and CO2 is unstable at high temperatures. Similarity in Figure 5.54(b), as the temperature increases, the (CH<sub>3</sub>)<sub>3</sub>N removal efficiency  $\psi'$  increase from room temperature up to 100°C, above which the (CH<sub>3</sub>)<sub>3</sub>N removal efficiency tends to significantly decreases because effect of O anion and CO3 at low temperatures and the reduced mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises, and some case equal to 100% even in blank tests without corona discharge. The higher the CO2 concentration, the higher the removal efficiency becomes.

# 5.92 Effect of temperature and coexisting CO<sub>2</sub> and O<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.55 shows the effect of  $CO_2$  and  $O_2$  on the simultaneous removal efficiency of  $CH_3CHO$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$  and  $(CH_3)_3N$  are 150 ppm and 100 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $CH_3CHO$  removal efficiency  $\psi'$  in Figure 5.55(a), as the temperature increases, the  $CH_3CHO$  removal efficiency  $\psi'$  decrease from room

temperature up to 300°C because  $O_3$  and  $CO_2$  are unstable at high temperatures. Similarity, in **Figure 5.55(b)**, as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  increases from room temperature up to 300°C, and some case equal to 100% even in blank tests without corona discharge.

## 5.93 Effect of temperature and coexisting CO<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.56 shows the effect of CO2 and H2O on the simultaneous removal efficiency of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>. The inlet concentrations of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N are 150 ppm and 100 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of CO<sub>2</sub> has a significant enhancement effect on the simultaneous CH<sub>3</sub>CHO removal efficiency  $\psi'$  in Figure 5.56(a), as the temperature increases, the CH<sub>3</sub>CHO removal efficiency w' decreases from room temperature up to 200°C, and then the tendency reverses up to 300°C. As mentioned previously, H, OH, CO3 and O anions should contribute to the removal of CH<sub>3</sub>CHO at low temperatures. At 200°C, the presence of H<sub>2</sub>O and CO<sub>2</sub> slightly retards the removal efficiency of CH<sub>3</sub>CHO because at low discharge current, the relatively much smaller number of electrons tends to attach mostly to H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.56(b), Compared to the case of only coexisting H<sub>2</sub>O, the simultaneous removal efficiency of (CH<sub>3</sub>)<sub>3</sub>N is enhance by the presence of CO<sub>2</sub>. Obviously, the presence of CO<sub>2</sub> positively affects the removal efficiency. The higher the CO<sub>2</sub> concentration, the higher the removal efficiency becomes and some case equal to 100% even in blank tests without corona discharge.

# 5.94 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.57 shows the effect of  $CO_2$ ,  $O_2$  and  $H_2O$  on the simultaneous removal efficiency of  $CH_3CHO$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$  and  $(CH_3)_3N$  are 150 ppm and 100 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $CH_3CHO$  removal efficiency  $\psi'$  in Figure 5.57(a), as the temperature increases, the  $CH_3CHO$  removal efficiency  $\psi'$  remains equal 100% from room temperature up to 300°C because effect of  $O_3$ ,  $CO_3^-$ ,  $H^-$ ,  $OH^-$  and  $O^-$  anion at low temperatures and various radicals at high temperatures. And some case equal to 100% even in blank tests without corona discharge. In Figure 5.57(b), as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  remains equal 100% at room temperature and 100°C some case, at 100°C to 300°C equal to 100% even in blank tests without corona discharge.



#### 5.95 Byproduct from the simultaneous removal of acetaldehyde and trimethyl amine

Figure 5.58 shows the concentration of byproduct CO versus temperature in the presence of CO<sub>2</sub>. In Figure 5.58 as the temperature increases, the byproduct CO increases from room temperature to 100°C, then the tendency reverses up at 200°C above which the byproducts (CO) increase again at 300°C because effect of CO<sub>3</sub> and O anion at low temperatures. At 200°C, the presence of CO<sub>2</sub> slightly retards the removal efficiency of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N because at low discharge current, the relatively much smaller number of electrons tends to attach mostly to CO<sub>2</sub>. In addition, N radicals are consumed by their reaction with CO<sub>2</sub> at high temperatures. As mentioned previously, it is knowns that production of CO by dissociative attachment reaction.

Figure 5.59 shows the concentration of byproduct  $NO_x$  versus temperature in the presence of  $CO_2$ . In Figure 5.59 as the temperature increases, the byproduct  $NO_x$  increase. As mentioned previously, it is well known that production of  $NO_x$  by the discharge process is favored at high temperatures. This phenomenon is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased as the temperature rise.

Figure 5.60 shows the concentration of byproduct CO versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.60 as the temperature increases, the byproduct CO decreases from room temperature to  $100^{\circ}$ C, then the tendency reverses up at  $200^{\circ}$ C above which the byproduct CO decreases again at  $300^{\circ}$ C. As mentioned previously, effect of  $O_3$  and  $O^{\circ}$  anion at low temperatures and at high temperatures,  $O_3$  is unstable.

Figure 5.61 shows the concentration of byproduct  $O_3$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.61 as the temperature increases, the byproduct  $O_3$  decreases from room temperature to  $300^{\circ}$ C. This is because  $O_3$  is unstable at high temperatures.

Figure 5.62 shows the concentration of byproduct  $NO_x$  versus temperature in the presence of  $O_2$  and  $CO_2$ . In Figure 5.62 as the temperature increases, the

byproduct  $NO_x$  decreases from room temperature up  $200^{\circ}C$ , then the tendency reverses up to  $300^{\circ}C$ .

**Figure 5.63** shows the concentration of byproduct CO versus temperature in the presence of H<sub>2</sub>O and CO<sub>2</sub>. In **Figure 5.63** as the temperature increases, the byproduct CO increases from room temperature to 300°C because at low temperature, the presence of CO<sub>2</sub> and H<sub>2</sub>O in the gas stream, CO<sub>3</sub>, H, OH and a few O anions are expected to be produced by dissociative electron attachment to CO<sub>2</sub> and H<sub>2</sub>O molecules (Massey, 1976; Moruzzi and Phelps, 1966).

Figure 5.64 shows the concentration of byproduct  $NO_x$  versus temperature in the presence of  $H_2O$  and  $CO_2$ . In Figure 5.64 as the temperature increases, the byproduct  $NO_x$  increases. As mentioned previously, it is known that production of  $NO_x$  by the discharge process is favored at high temperatures. This fact is also confirmed in our experiments. While the outlet concentration of  $NO_x$  was negligible at room temperature, its concentration gradually increased as the temperature rise.

Figure 5.65 shows the concentration of byproduct CO versus temperature in the presence of O<sub>2</sub> and H<sub>2</sub>O and CO<sub>2</sub>. In Figure 5.65 as the temperature increases, the byproduct CO increases from room temperature up 200°C, then the tendency reverses up to 300°C because at low temperatures, CO<sub>2</sub> and H<sub>2</sub>O are present in the gas stream, CO<sub>3</sub>, H, OH and a few O anions are expected to be produced by dissociative electron attachment to CO<sub>2</sub> and H<sub>2</sub>O molecules (Massey, 1976; Moruzzi and Phelps, 1966). At high temperatures, CO<sub>2</sub>, O<sub>3</sub> and H<sub>2</sub>O are unstable.

Figure 5.66 shows the concentration of byproduct  $O_3$  versus temperature in the presence of  $O_2$  and  $H_2O$  and  $CO_2$ . In Figure 5.66 as the temperature increases, the byproduct  $(O_3)$  decreases with temperature rise because  $O_3$  is unstable at high temperatures.

Figure 5.67 shows the concentration of byproduct  $NO_x$  versus temperature in the presence of  $O_2$  and  $H_2O$  and  $CO_2$ . From Figure 5.67 as the temperature increases, the byproduct  $NO_x$  decreases starting from room temperature up 200°C, then the tendency reverses up to 300°C. The reasons were given previously in relation to Figure 5.38.

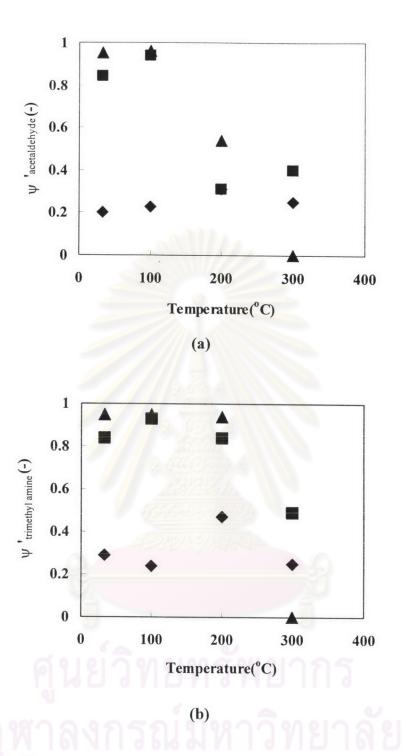


Figure 5.54 Effect of coexisting CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in,trimethylamine</sub>=100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

◆ CO<sub>2</sub> (0%), ■ CO<sub>2</sub> (10%), ▲ CO<sub>2</sub> (20%)

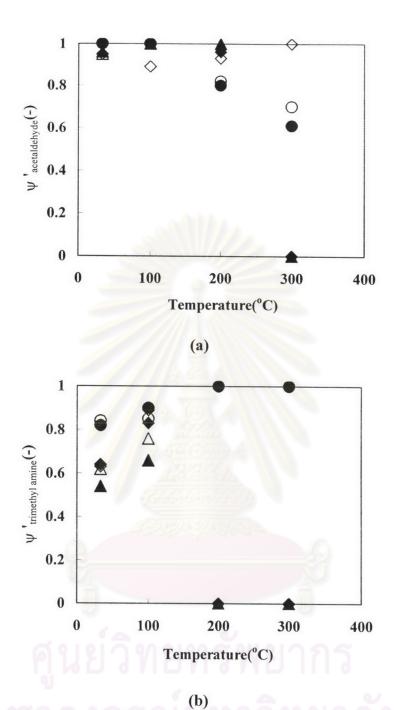
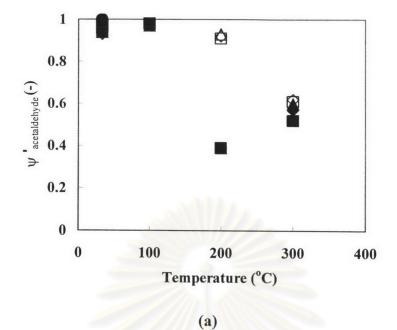
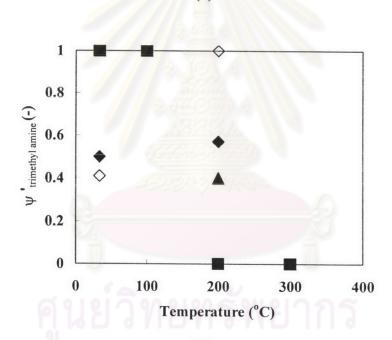


Figure 5.55 Effect of coexisting O<sub>2</sub>-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in,trimethylamine</sub>=100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature:

- CO<sub>2</sub> (0%) O<sub>2</sub> (10%),
- ▲ CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\bullet$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%),
- O CO<sub>2</sub> (0%) O<sub>2</sub> (20%),
- $\triangle$  CO<sub>2</sub>(10%) O<sub>2</sub>(20%)
- ♦ CO<sub>2</sub> (20%) O<sub>2</sub> (20%)

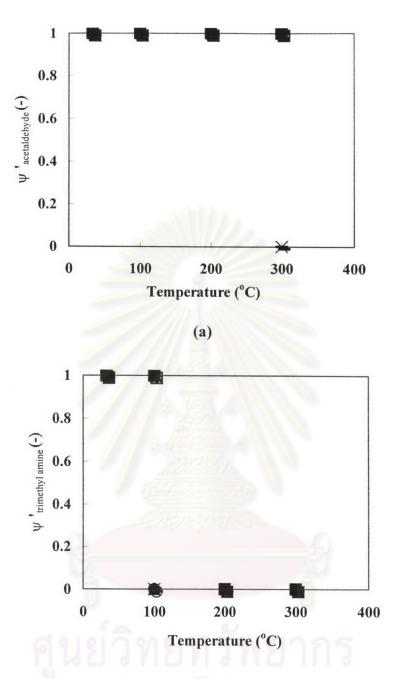




(b)

Figure 5.56 Effect of coexisting H<sub>2</sub>O-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, trimethylamine</sub>=100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

CO<sub>2</sub> (10%) - H<sub>2</sub>O (5250ppm),
CO<sub>2</sub> (20%) - H<sub>2</sub>O (5250ppm),
CO<sub>2</sub> (10%) - H<sub>2</sub>O (10500ppm),
CO<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),
CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm),
CO<sub>2</sub> (20%) - H<sub>2</sub>O (21800ppm)



(b)

Figure 5.57 Effect of coexisting  $O_2$ -H<sub>2</sub>O-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in,trimethylamine</sub>=100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature : CO<sub>2</sub>(10%)-O<sub>2</sub>(10%)-H<sub>2</sub>O (5250ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(10%)-H<sub>2</sub>O (5250ppm), CO<sub>2</sub>(10%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (5250ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (5250ppm), CO<sub>2</sub>(10%)-O<sub>2</sub>(10%)-H<sub>2</sub>O (10500ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(10%)-H<sub>2</sub>O (10500ppm), CO<sub>2</sub>(10%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (10500ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(10%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm),  $\diamondsuit$  CO<sub>2</sub>(10%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm),  $\diamondsuit$  CO<sub>2</sub>(10%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm),  $\diamondsuit$  CO<sub>2</sub>(20%)-O<sub>2</sub>(20%)-O<sub>2</sub>(20%)-H<sub>2</sub>O (21800ppm)

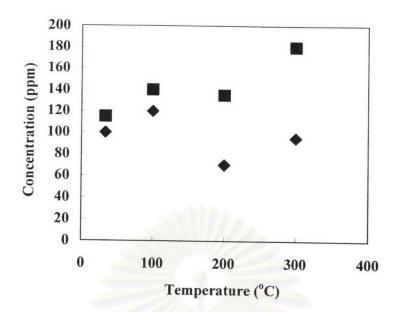


Figure 5.58 Byproduct (CO) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-CO<sub>2</sub>:

◆ CO<sub>2</sub>(10%), ■ CO<sub>2</sub>(20%)

Concentration (ppm) Temperature (°C)

Figure 5.59 Byproduct (NO $_x$ ) on the simultaneous removal of CH $_3$ CHO and (CH $_3$ ) $_3$ N from N $_2$ -CO $_2$ :

♦  $CO_2(10\%)$ , ■  $CO_2(20\%)$ 

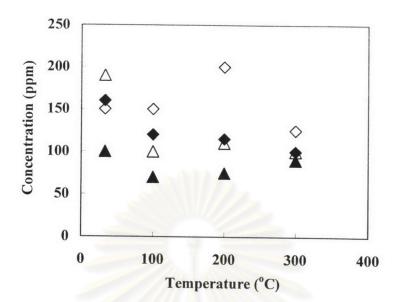


Figure 5.60 Byproduct (CO) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%),
- $\triangle$  CO<sub>2</sub>(10%) O<sub>2</sub>(20%),
- $\triangle \text{ CO}_2(20\%) O_2(20\%)$

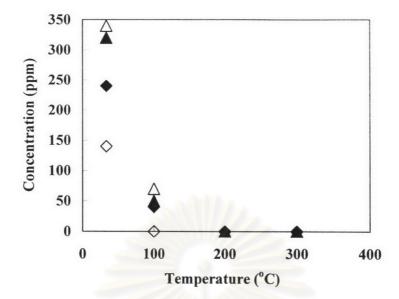


Figure 5.61 Byproduct (O<sub>3</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\Diamond$  CO<sub>2</sub>(20%) O<sub>2</sub>(10%),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%)

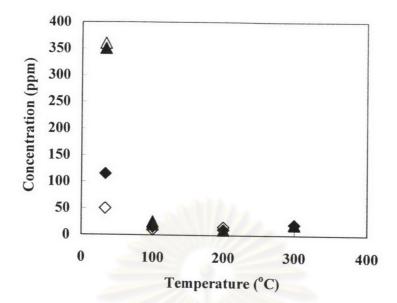


Figure 5.62 Byproduct ( $NO_x$ ) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%),
- $\Diamond$  CO<sub>2</sub>(20%) O<sub>2</sub>(10%),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%),
- $\triangle$  CO<sub>2</sub>(20%) O<sub>2</sub>(20%)

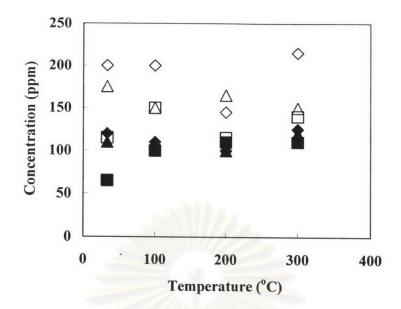


Figure 5.63 Byproduct (CO) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- ◆ CO<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\triangle$  CO<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\square$  CO<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

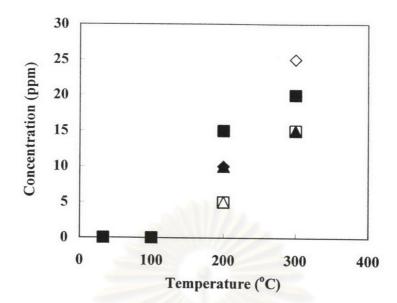


Figure 5.64 Byproduct (NO<sub>x</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- ◆ CO<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- $\triangle$  CO<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\square$  CO<sub>2</sub>(20%) H<sub>2</sub>O (21800ppm)

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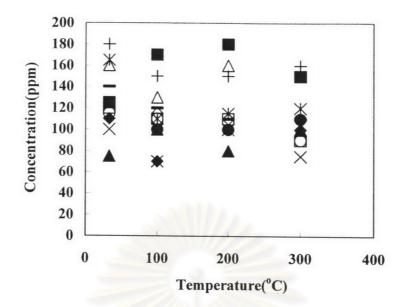


Figure 5.65 Byproduct (CO) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub>(20%) O<sub>2</sub>(20%) H<sub>2</sub>O (5250ppm),
- $CO_2(10\%) O_2(10\%) H_2O(10500ppm),$
- □ CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm), • CO<sub>2</sub> (10%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),
- $O(2(20\%) O_2(20\%) H_2O(10500ppm),$
- \* CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\times$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- +  $CO_2(10\%)$   $O_2(20\%)$   $H_2O(21800ppm)$ ,
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

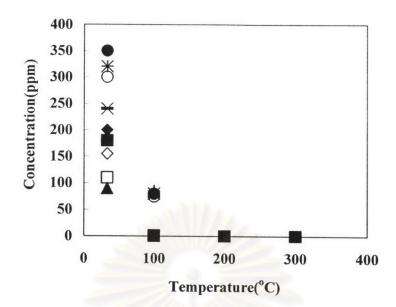


Figure 5.66 Byproduct (O<sub>3</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub>(10%) O<sub>2</sub>(20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $CO_2(10\%) O_2(10\%) H_2O(10500ppm),$
- $\square$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- O CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm), \* CO<sub>2</sub> (10%) - O<sub>2</sub> (10%) - H<sub>2</sub>O (21800ppm),
- $\times$  CO<sub>2</sub>(10%) O<sub>2</sub>(10%) H<sub>2</sub>O (21800ppm),  $\times$  CO<sub>2</sub>(20%) - O<sub>2</sub>(10%) - H<sub>2</sub>O (21800ppm),
- $+ CO_2(10\%) O_2(10\%) H_2O(21800ppm),$
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

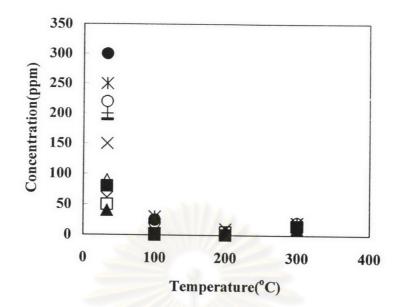


Figure 5.67 Byproduct (NO<sub>x</sub>) on the simultaneous removal of CH<sub>3</sub>CHO and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub>:

- $\bullet$  CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\diamond$  CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (10%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- $\triangle$  CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (5250ppm),
- CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm),
- □ CO<sub>2</sub> (20%) O<sub>2</sub> (10%) H<sub>2</sub>O (10500ppm), • CO<sub>2</sub> (10%) - O<sub>2</sub> (20%) - H<sub>2</sub>O (10500ppm),
- O CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (10500ppm),
- \* CO<sub>2</sub> (10%) O<sub>2</sub> (10%) H<sub>2</sub>O (21800ppm),
- $\times$  CO<sub>2</sub>(20%) O<sub>2</sub>(10%) H<sub>2</sub>O (21800ppm),
- $+ CO_2(10\%) O_2(20\%) H_2O(21800ppm),$
- CO<sub>2</sub> (20%) O<sub>2</sub> (20%) H<sub>2</sub>O (21800ppm)

#### 5.10 Simultaneous removal of ammonia and trimethyl amine

## 5.10.1 Effect of temperature and coexisting $CO_2$ on the simultaneous removal of $NH_3$ and $(CH_3)_3N$ from $N_2$

Figure 5.68 shows the effect of  $CO_2$  on the simultaneous removal efficiency of NH<sub>3</sub> and  $(CH_3)_3N$  from N<sub>2</sub>. The inlet concentrations of NH<sub>3</sub> and  $(CH_3)_3N$  are 1,000 ppm and 100 ppm, respectively, while the discharge current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant effect on the simultaneous NH<sub>3</sub> removal efficiency  $\psi'$  in Figure 5.68(a), as the temperature increases, the NH<sub>3</sub> removal efficiency  $\psi'$  decreases from room temperature up to 200°C, then the tendency reverses up to 300°C because this condition, the synthesis occurs of NH<sub>3</sub> again and the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. In Figure 5.68(b), as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  at 100% from room temperature to 200°C, at 300°C equal to 100% even in blank tests without corona discharge. Obviously, the presence of  $CO_2$  positively affect the removal efficiency  $(CH_3)_3N$ .

# 5.10.2 Effect of temperature and coexisting CO<sub>2</sub> and O<sub>2</sub>on the simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.69 shows the effect of  $CO_2$  and  $O_2$  on the simultaneous removal efficiency of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $NH_3$  and  $(CH_3)_3N$  are 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $NH_3$  removal efficiency  $\psi'$  in Figure 5.69(a), as the temperature increases, the  $NH_3$  removal efficiency  $\psi'$  remains equal 100% from room temperature to 300°C because effect of  $O_3$ ,  $CO_3$  and O anion at low temperatures and various radicals at high temperatures. In Figure 5.69(b), as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  at 100% from room temperature to 200°C and some case, from 200°C to 300°C equal to 100% even in blank tests

without corona discharge. Obviously, the presences of O<sub>2</sub> positively affect the removal efficiency.

## 5.10.3 Effect of temperature and coexisting $CO_2$ and $H_2O$ on the simultaneous removal of $NH_3$ and $(CH_3)_3N$ from $N_2$

Figure 5.70 shows the effect of  $CO_2$  and  $H_2O$  on the simultaneous removal efficiency of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $NH_3$  and  $(CH_3)_3N$  are 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant effect on the simultaneous  $NH_3$  removal efficiency  $\psi'$  in Figure 5.70(a), as the temperature increases, the  $NH_3$  removal efficiency  $\psi'$  increases because effect of H', OH',  $CO_3$  and O' anion at low temperatures and at high temperatures, N radicals are consumed by their reaction with  $CO_2$  and  $H_2O$ . As the mentioned previously, this condition, the synthesis occurs of  $NH_3$  again. In Figure 5.70 (b), as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  at 100% from room temperature to 200°C, at 300°C equal to 100% even in blank tests without corona discharge. Obviously, the presence of  $H_2O$  positively affects the removal efficiency.

## 5.10.4 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.71 shows the effect of  $CO_2$ ,  $O_2$  and  $H_2O$  on the simultaneous removal efficiency of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentration of  $NH_3$  and  $(CH_3)_3N$  are 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $NH_3$  removal efficiency  $\psi'$  in Figure 5.71(a), as the temperature increases, the  $NH_3$  removal efficiency  $\psi'$  remains equal 100% from room temperature to 300°C because effect of  $O_3$ ,  $CO_3$ , H, OH and O anion at low temperatures and various radicals at high temperatures. In Figure 5.71(b), as

temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  at 100% from room temperature to 200°C, at 300°C equal to 100% even in blank tests without corona discharge. Obviously, the presences of  $O_2$  and  $H_2O$  positively affect the removal efficiency.

#### 5.10.5 Byproducts from the simultaneous removal of acetaldehyde and ammonia

Figure 5.72 shows the concentration of byproduct CO versus temperature. In Figure 5.72 as the temperature increases, the byproduct CO increases from room temperature to 100°C, above which the tendency reverses up to 300°C as the mentioned previously, it is known that production of CO by dissociative attachment reaction.

Figure 5.73 shows the concentration of byproduct  $O_3$  versus temperature. In Figure 5.73 as the temperature increases, the byproduct  $O_3$  decreases. This is because  $O_3$  is unstable at high temperatures.

Figure 5.74 shows the concentration of byproduct  $NO_x$  versus temperature. In Figure 5.74 as the temperature increases, the byproduct  $NO_x$  decreases from room temperature up  $200^{\circ}$ C, then the tendency reverses up to  $300^{\circ}$ C.



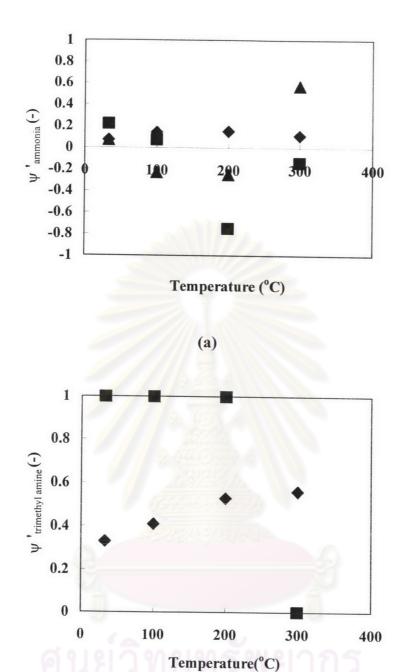


Figure 5.68 Effect of coexisting  $CO_2$  on the simultaneous removal of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,ammonia}=1000$ ppm,  $C_{in,trimethylamine}=100$ ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

(b)

◆ CO<sub>2</sub> (0%), ■ CO<sub>2</sub> (10%), ▲ CO<sub>2</sub> (20%)

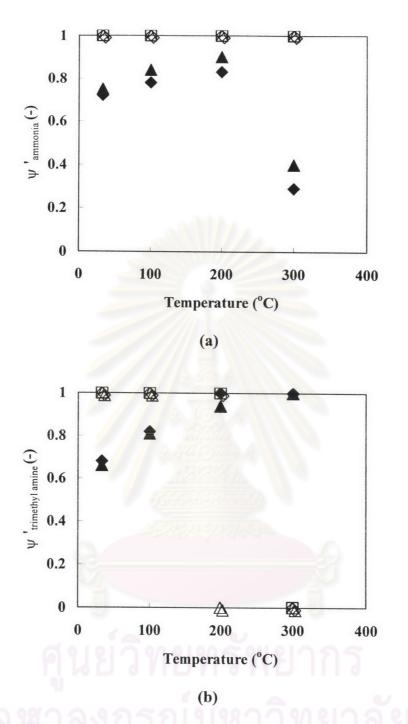
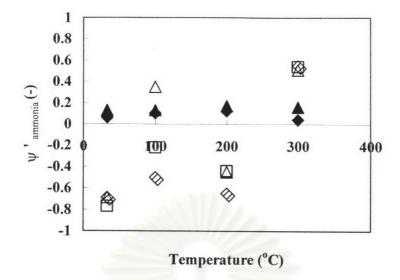


Figure 5.69 Effect of coexisting O<sub>2</sub>-CO<sub>2</sub> on the simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in,ammonia</sub>=1000ppm, C<sub>in,trimethylamine</sub>=100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%)-O<sub>2</sub> (10%),
- ♦ CO<sub>2</sub> (10%)-O<sub>2</sub> (10%),
- $\square$  CO<sub>2</sub> (20%)-O<sub>2</sub> (10%),
- ▲ CO<sub>2</sub> (0%)-O<sub>2</sub> (20%),
- $\triangle$  CO<sub>2</sub> (10%)-O<sub>2</sub> (20%)

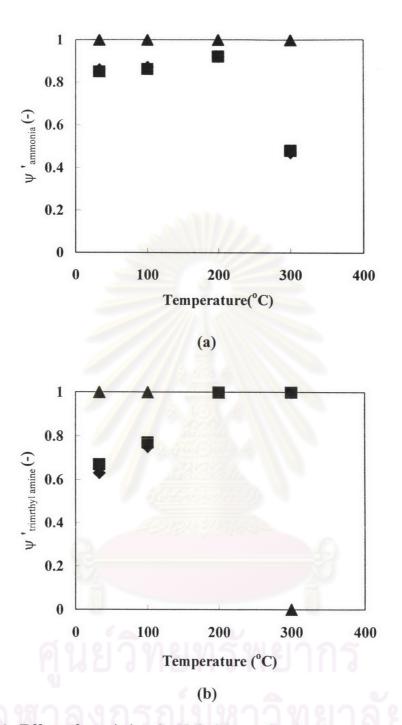


(a)

1
0.8
0.6
0.4
0.2
0
100
200
300
400
Temperature(°C)

**Figure 5.70** Effect of coexisting  $H_2O-CO_2$  on the simultaneous removal of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,ammonia}=1000$ ppm,  $C_{in,trimethylamine}=100$ ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%)-H<sub>2</sub>O (5250ppm),
- ♦ CO<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),
- $\square$  CO<sub>2</sub> (20%)-H<sub>2</sub>O (5250ppm),
- ▲ CO<sub>2</sub> (0%)-H<sub>2</sub>O (10500ppm),
- △ CO<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm)



**Figure 5.71** Effect of coexisting  $O_2$ - $H_2O$ - $CO_2$  on the simultaneous removal of  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,ammonia}$ =1000ppm,  $C_{in,trimethylamine}$ =100ppm, I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%)-O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm),
- CO<sub>2</sub> (0%)-O<sub>2</sub> (10%)-H<sub>2</sub>O (10500ppm),
- ▲ CO<sub>2</sub> (10%)-O<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm)

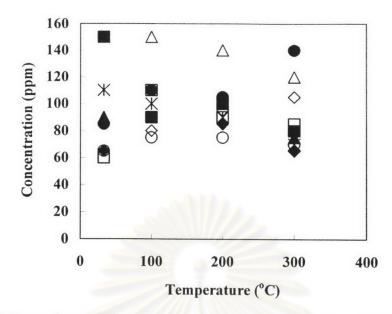


Figure 5.72 Byproduct (CO) on simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N:

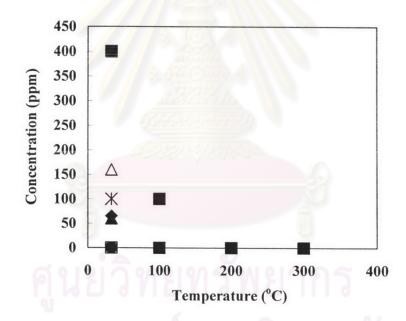


Figure 5.73 Byproduct (O<sub>3</sub>) on simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N:

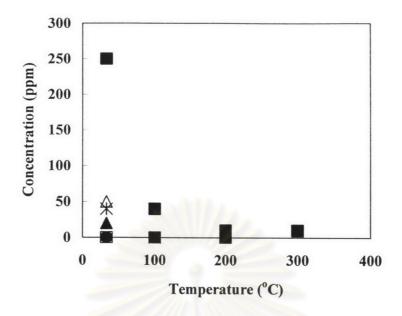


Figure 5.74 Byproduct (NO<sub>x</sub>) on simultaneous removal of NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N:



#### 5.11 Simultaneous removal of acetaldehyde, ammonia and trimethylamine

### 5.11.1 Effect of temperature and coexisting CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.75 shows the effect of  $CO_2$  on the simultaneous removal efficiency of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  are 150 ppm, 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. In Figure 5.75(a), as the temperature increases, the  $CH_3CHO$  removal efficiency  $\psi'$  decreases from room temperature to 300°C. As mentioned previously, this condition, the synthesis occurs of  $NH_3$  again and at high temperature,  $CO_2$  is unstable. In Figure 5.75(b), as the temperature increases, the  $NH_3$  removal efficiency  $\psi'$  decreases from room temperature up to 200°C, then the tendency reverses up to 300°C because the mean residence time of the gas mixture inside the reactor decreases as the reactor temperature rises. In Figure 5.75(c), as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  remains equal 100% from room temperature to 300°C. As mentioned previously, the presence of  $CO_2$  does significantly enhancement effect the removal efficiency of  $CH_3$ CHO and  $CH_3$ 3N and sinificantly retard removal efficiency of  $NH_3$ .

## 5.11.2 Effect of temperature and coexisting CO<sub>2</sub> and O<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.76 shows the effect of  $CO_2$  and  $O_2$  on the simultaneous removal efficiency of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  are 150 ppm, 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. In Figure 5.76(a), as the temperature increases, the  $CH_3CHO$  removal efficiency  $\psi'$  remains equal 100% from room temperature to  $200^{\circ}C$ , and decreases at  $300^{\circ}C$  because at high temperature,  $O_3$  and  $CO_2$  are unstable. In Figure 5.76(b), in case, no coexisting gas  $CO_2$ , as the temperature increases, the  $NH_3$  removal efficiency  $\psi'$  increases from room temperature up to  $200^{\circ}C$ , above which the  $NH_3$  removal efficiency tends to significantly decrease

because of less  $O_3$  generated from  $O_2$  and in case of the presence coexisting gas  $CO_2$ , as the temperature increases, the NH<sub>3</sub> removal efficiency  $\psi'$  remains equal 100% from room temperature to 200°C, and decreases at 300°C because at high temperature,  $O_3$  and  $CO_2$  are unstable. In **Figure 5.76(c)**, as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  remains equal 100% from room temperature to 300°C because effect of  $O_3$ ,  $CO_3^-$  and  $O^-$  anion at low temperatures and various radicals at high temperatures. Obviously, the presence of  $CO_2$  positively affect the removal efficiency  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$ .

#### 5.11.3 Effect of temperature and coexisting CO<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.77 shows the effect of CO<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal efficiency of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>. The inlet concentrations of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N are 150 ppm, 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. In Figure 5.77(a), in case, no coexisting gas CO<sub>2</sub>, as the temperature increases, the CH<sub>3</sub>CHO removal efficiency  $\psi'$  increases from room temperature up to 300°C and in case of the presence coexisting gas CO2, as the temperature increases, the CH<sub>3</sub>CHO removal efficiency  $\psi'$  decreases from room temperature up to 300°C because at high temperatures, CO<sub>2</sub> and H<sub>2</sub>O are unstable. In Figure 5.77(b), in case, no coexisting gas CO2, as the temperature increases, the NH<sub>3</sub> removal efficiency w increases from room temperature up to 200°C, above which the NH3 removal efficiency tends to significantly decrease and in case of the presence coexisting gas CO<sub>2</sub>, as temperature increases, the NH<sub>3</sub> removal efficiency  $\psi'$  decreases from room temperature up to 200°C, and then the tendency reverses up to 300°C. As mentioned previously, this condition, the synthesis occurs of NH<sub>3</sub> again. H, OH, CO<sub>3</sub> and O anions should contribute to the removal of CH<sub>3</sub>CHO at low temperatures. At 200°C, the presence of H2O and CO2 slightly retards the removal efficiency of CH<sub>3</sub>CHO because at low discharge current, the relatively much smaller number of electrons tends to attach mostly to H2O and CO2. In addition, N radicals are consumed by their reaction with CO2 and H2O at high

temperatures In **Figure 5.77(c)**, as the temperature increases, the  $(CH_3)_3N$  removal efficiency  $\psi'$  remains equal 100% from room temperature to 300°C because at low to moderate temperatures, H<sup>-</sup>, OH<sup>-</sup>, CO<sub>3</sub><sup>-</sup> and O<sup>-</sup> anions are expected to be produced by dissociate electron attachment to  $CO_2$  and  $H_2O$  molecules at low temperatures (Massay 1976, Moruzzi and Phelps 1996). At 200°C or more, electron detachment would become significant so that radicals of  $CO_3$ , O, H, and OH may play a more important role than their anionic counterparts. Obviously, the presence of  $CO_2$  does significantly enhancement effect the removal efficiency of  $CH_3CHO$  and  $CH_3$  and significantly retard removal efficiency of  $CH_3$ .

### 5.11.4 Effect of temperature and coexisting CO<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>

Figure 5.78 shows the effect of  $CO_2$ ,  $O_2$  and  $H_2O$  on the simultaneous removal efficiency of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ . The inlet concentrations of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  are 150 ppm, 1,000 ppm and 100 ppm, respectively, while the current is 0.3 mA. It is found that the presence of  $CO_2$  has a significant enhancement effect on the simultaneous  $CH_3CHO$ ,  $NH_3$ , and  $(CH_3)_3N$  removal efficiency  $\psi'$  in **Figure 5.78**, as the temperature increases, the  $CH_3CHO$ ,  $NH_3$ , and  $(CH_3)_3N$  removal efficiency  $\psi'$  decreases from room temperature up to  $300^{\circ}C$  because of less  $O_3$  generated from  $O_2$ , effect of  $H^*$ ,  $OH^*$ ,  $CO_3^-$  and  $O^-$  anions from  $H_2O$  and  $CO_2$  are unstable and reduction of the mean residence time of the gas mixture inside the reactor at high temperatures.

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#### 5.11.5 Simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>-O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub> using two reactors in series

The experiments for simultaneous removal of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$  -  $O_2$  (10%) -  $H_2O$  (10,500 ppm) -  $CO_2$  (10%) were studied using two reactors in series to decreases byproducts and / or increases the removal efficiency.

The first reactor, it was found that  $(CH_3)_3N$  was removed completely, but the concentration of  $NH_3$  still remained about 46 ppm and the concentration of  $CH_3CHO$  still remained about 12ppm using the single reactor at  $300^{\circ}C$  and 0.3 mA. Moreover, there were byproducts (CO 100 ppm and  $NO_x$  10 ppm) occurred.

Then the second reactor was added in series with the first reactor in order to decrease byproducts and / or increase the removal efficiency. The experiments were divided into two cases. In the first case, at 100°C, CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N were removed completely at 0.1 mA, however, CO, O<sub>3</sub> and NO<sub>x</sub> increasesd, when, the current discharge increased. In the second case, At 200°C, CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N were removed completely at 0.1 mA, however, CO increased when the current discharge increased, O<sub>3</sub> was non detected and NO<sub>x</sub> was removed completely at 0.1 mA.

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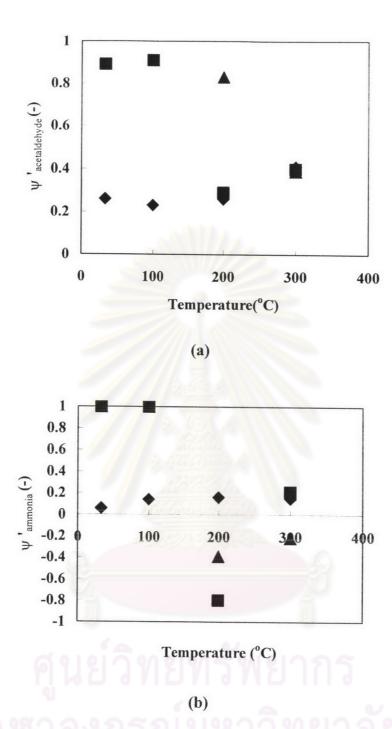


Figure 5.75 Effect of coexisting  $CO_2$  on the simultaneous removal of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ ;  $C_{in,\,acetaldehyde}=150ppm$ ,  $C_{in,\,ammonia}=1000ppm$ ,  $C_{in,\,trimethylamine}=100ppm$  I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

◆ CO<sub>2</sub> (0%), ■ CO<sub>2</sub> (10%), ▲ CO<sub>2</sub> (20%),

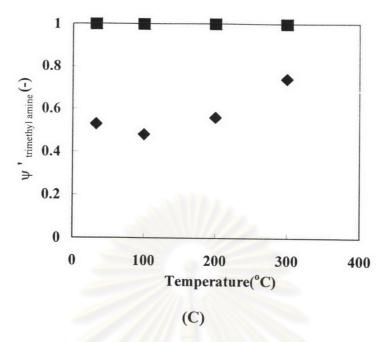
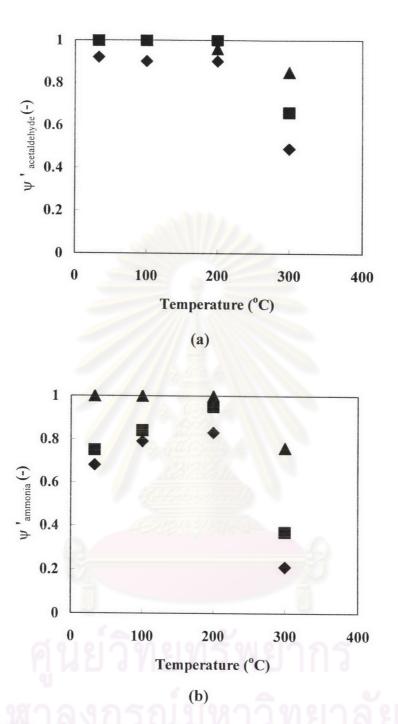


Figure 5.75 Effect of coexisting CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, ammonia</sub>=1000ppm, C<sub>in, trimethylamine</sub>=100ppm I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature:

 $\bullet$  CO<sub>2</sub> (0%), ■ CO<sub>2</sub> (10%), ▲ CO<sub>2</sub> (20%),





**Figure 5.76** Effect of coexisting O<sub>2</sub>-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, ammonia</sub>=1000ppm, C<sub>in, trimethylamine</sub>=100ppm I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%)-O<sub>2</sub> (10%),
- $\square$  CO<sub>2</sub> (0%)-O<sub>2</sub> (20%),
- ▲ CO<sub>2</sub> (10%)-O<sub>2</sub> (10%)

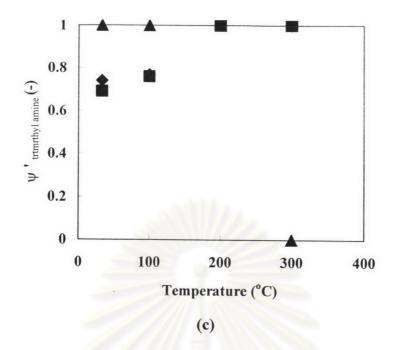


Figure 5.76 Effect of coexisting O<sub>2</sub>-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, ammonia</sub>=1000ppm, C<sub>in, trimethylamine</sub>=100ppm I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature:

 $\bullet$  CO<sub>2</sub> (0%)-O<sub>2</sub> (10%),

 $\blacksquare$  CO<sub>2</sub> (0%)-O<sub>2</sub> (20%),

▲ CO<sub>2</sub> (10%)-O<sub>2</sub> (10%)



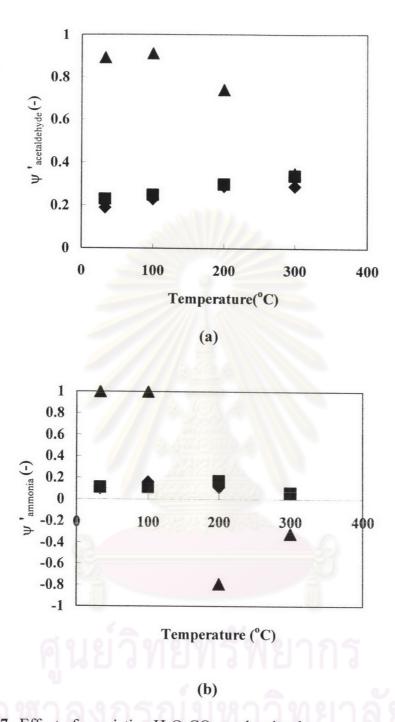


Figure 5.77 Effect of coexisting  $H_2O-CO_2$  on the simultaneous removal of  $CH_3CHO$ ,  $NH_3$  and  $(CH_3)_3N$  from  $N_2$ ;  $C_{in, acetaldehyde}=150ppm$ ,  $C_{in, ammonia}=1000ppm$ ,  $C_{in, trimethylamine}=100ppm$  I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

- ◆ CO<sub>2</sub> (0%)-H<sub>2</sub>O (5250ppm),
- $CO_2$  (0%)- $H_2O$  (10500ppm),
- ▲ CO<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm)

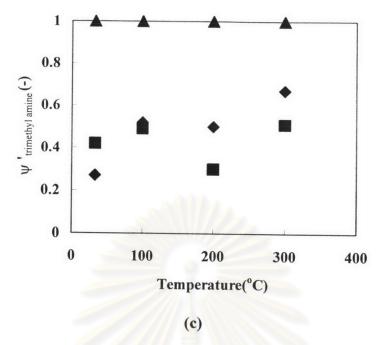


Figure 5.77 Effect of coexisting H<sub>2</sub>O-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO,
NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm,
C<sub>in, ammonia</sub>=1000ppm, C<sub>in, trimethylamine</sub>=100ppm I=0.3mA, SV=55.8 hr<sup>-1</sup> at room temperature :

CO<sub>2</sub> (0%)-H<sub>2</sub>O (5250ppm),
CO<sub>2</sub> (0%)-H<sub>2</sub>O (10500ppm),

 $\triangle$  CO<sub>2</sub> (10%)-H<sub>2</sub>O (5250ppm)

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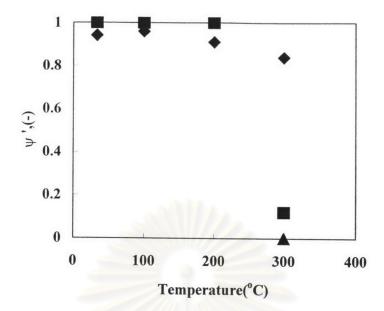


Figure 5.78 Effect of coexisting O<sub>2</sub>-H<sub>2</sub>O-CO<sub>2</sub> on the simultaneous removal of CH<sub>3</sub>CHO, NH<sub>3</sub> and (CH<sub>3</sub>)<sub>3</sub>N from N<sub>2</sub>; C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, acetaldehyde</sub>=150ppm, C<sub>in, trimethylamine</sub>=100ppm I=0.3mA, SV=77.9 hr<sup>-1</sup> at room temperature:

**♦** (CH<sub>3</sub>CHO),

 $\blacksquare$  NH<sub>3</sub>,

 $\triangle$  (CH<sub>3</sub>)<sub>3</sub>N

