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## APPENDIX A

### SAMPLE OF CALCULATIONS

#### 1. Preparation of 9%Ce-0.01%Rh-0.03%Pt/Al<sub>2</sub>O<sub>3</sub> Catalyst with Incipient Impregnation Method

Reagent : Cerium (III) Nitrate [Ce(NO<sub>3</sub>)<sub>3</sub> · 6H<sub>2</sub>O] ;

Purity 98% ; Molecular weight = 434.22,

manufactured by Wako Pure Chemical Industries Co., Ltd.

(Atomic weight of cerium = 140.12)

Rhodium (III) Nitrate [Rh(NO<sub>3</sub>)<sub>3</sub> ]

Purity 99.5% ; Molecular weight = 290.372 ;

manufactured by Wako Pure Chemical Industries Co., Ltd.

(Atomic weight of rhodium = 102.91)

Chloroplatinic acid (H<sub>2</sub>PtCl<sub>6</sub> · 6H<sub>2</sub>O)

Molecular weight = 517.92 ;

manufactured by PURE CHEMICAL INDUSTRIES Co., Ltd.

(Atomic weight of platinum = 195.1)

Support : Alumina (Al<sub>2</sub>O<sub>3</sub>) ; type KNH-3 ;

pore volume = 1.0 cc/g.

from Sumitomo Aluminium Smelting Co., Ltd.

Calculation for prepared 9wt%Ce-0.01wt%Rh-0.03wt%Pt catalyst

If the weight of alumina support used is X grams. So each 100 grams of the catalyst would compose of

Cerium	9	g.
Rhodium	0.01	g.
Platinum	0.03	g.
Alumina support	X	g.
Then 9 + 0.01 + 0.03 + X	= 100	g.
X	= 90.96	g.

Shown below is the calculation procedure of the amount of each ingredients for the required composition of the catalyst [Ce-Rh-Pt ; (9wt% : 0.01wt% : 0.03wt%)/Al<sub>2</sub>O<sub>3</sub>]

For 6 grams of alumina support used :

$$\begin{aligned} 1) \text{ Cerium required} &= 6 \times 9 / 90.96 \quad \text{g.} \\ &= 0.594 \quad \text{g.} \end{aligned}$$

$$\begin{aligned} \text{Cerium (Ce) } 0.594 \text{ g. prepared from the stock solution of cerium nitrate} \\ &= 0.594 \times (25 / 3.162) \\ &= 4.696 \quad \text{cc.} \end{aligned}$$

$$\begin{aligned} 2) \text{ Rhodium required} &= 6 - 0.01 / 90.96 \quad \text{g.} \\ &= 6.596 \times 10^{-4} \quad \text{g.} \end{aligned}$$

$$\begin{aligned} \text{Rhodium (Rh) } 6.596 \times 10^{-4} \text{ g. prepared from the stock solution of rhodium} \\ \text{nitrate} &= 6.596 \times 10^{-4} \times (50 / 0.1772) \quad \text{g.} \\ &= 0.186 \quad \text{cc.} \end{aligned}$$

$$\begin{aligned}
 3) \text{ Platinum required} &= 0.03 \times 6 / 90.96 \quad \text{g.} \\
 &= 1.98 \times 10^{-3} \quad \text{g.} \\
 \text{Platinum (Pt)} \quad 1.98 \times 10^{-3} \text{ g.} &\text{ prepared from the stock solution of} \\
 \text{chloroplatinic acid} &= 1.98 \times 10^{-3} \times (25 / 0.3767) \quad \text{g.} \\
 &= 0.131 \quad \text{cc.}
 \end{aligned}$$

As the pore volume of the alumina support is 1 cc/g., the total volume of impregnating solution that must be used is 6 cc. By the requirement of the incipient impregnate method, the distilled and de-ionized water is added to the above solution until the volume equals to the alumina pore volume 6 cc. This solution is used as the impregnating solution.

## 2. Calculation of metal active site on catalyst

$$\begin{aligned}
 \text{Let the weight of catalyst used} &= w \quad \text{g.} \\
 \text{height of CO peak after adsorption} &= A \quad \text{unit} \\
 \text{height of 0.18 ml standard CO peak} &= B \quad \text{unit} \\
 \text{Amounts of CO adsorbed on catalyst} &= B-A \quad \text{unit} \\
 \text{Volume of CO adsorbed on catalyst} &= [(B-A) / B] \times (0.18) \quad \text{ml.} \\
 \text{Volume of gas 1 mole at } 30^\circ\text{C} &= 24.86 \times 10^3 \quad \text{mol.} \\
 \text{Mole of CO adsorbed on catalyst} &= [(B-A) / B][0.18 / 24.86 \times 10^3] \quad \text{mole.} \\
 \text{Molecule of CO adsorbed on catalyst} &= 7.24 \times 10^{-6}[(B-A) / B](6.02 \times 10^{23}) \quad \text{molecule} \\
 \text{Metal active site} &= 4.36 \times 10^{18}[(B-A) / B] \quad \text{molecule of CO/g.cat.}
 \end{aligned}$$

## 3. BET Surface Area Calculation. [45]

From BET equation :

$$\frac{x}{v(1-x)} = \left(\frac{1}{v_m C}\right) + \left(\frac{C-1}{v_m C} \cdot x\right) \quad (\text{A-4.1})$$

where :  $x$  = ratio of partial pressure  $P / P_0$

$P_0$  = saturated vapor pressure of  $N_2$  (or adsorbed gas)

$P$  = equilibrium vapor pressure of  $N_2$

$v$  = amount of adsorption to cover the surface, c.c. at the NTP/gm of sample

$$C = \exp(E_1 - E_2 / RT) \quad (\text{A-4.2})$$

where :  $E_1$  = heat of adsorption of the first layer

$E_2$  = heat of condensation of adsorbed gas

assume  $C \rightarrow \infty$ , then

$$\frac{x}{(v \cdot (1-x))} = \left(\frac{1}{v_m C}\right) \cdot x \quad (\text{A-4.3})$$

let :  $v_m = v'_m$

$v_m$  = mean amount of adsorption to form the  $N_2$  complete monolayer

$v$  = amount of adsorption measuring by G.C.

$x = P / P_0$

$$P_b \cdot V / 273 = P_t V / T \quad (\text{A-4.4})$$

where :  $V$  = constant volume

$P_b$  = pressure at 0 °C

$P_t$  = pressure at t °C

$T$  =  $273.15 + t$ , K

$P_b = (273.15 / T) \cdot P_t = 1 \text{ atm}$

### partial pressure

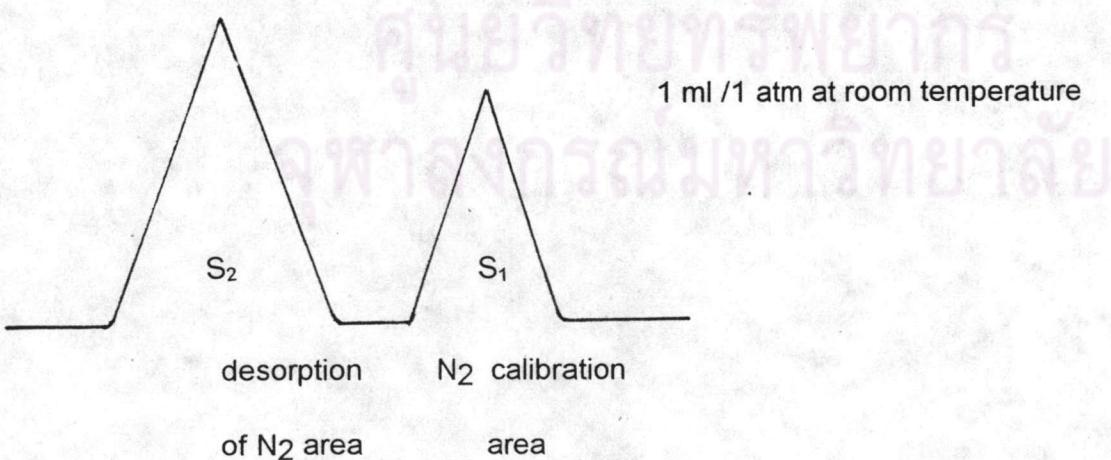
$$P = \frac{((\text{Flow of } (\text{He} + \text{N}_2)) - \text{Flow of He})}{\text{Flow of } (\text{He} + \text{N}_2) \times P_b} \quad (\text{A-4.5})$$

$$= 0.3 \text{ atm}$$

$\text{N}_2$  saturated vapor pressure ,  $P_o = 1.1 \text{ atm} = 836 \text{ mm. Hg}$

$$X = P/P_o = P/1.1$$

### How to measure v



$$V = (s_2 / s_1) \times (1 / w) \times (273.15 / T) \times V \quad \text{c.c. / g of catalyst} \quad (\text{A-4.6})$$

where :  $w$  = weight of sample

$$v'_m = \frac{v \times [1 - ((\text{flow of He + N}_2 - \text{flow of He}) / 1.1)]}{\text{flow of He + N}_2 \quad \text{c.c. NTP/g of catalyst}} \quad (\text{A-4.7})$$

$$s_b = s \times v'_m \quad (\text{A-4.8})$$

where :  $s$  = surface area from literature of  $\text{N}_2$   
 $= 4.373 \text{ m}^2/\text{c.c of N}_2$

so that :  $s_b = 4.373 \times v'_m \text{ m}^2 / \text{g of catalyst}$

#### 4. Calculation of NO, CO and $\text{C}_3\text{H}_8$ conversion

The effluent gas was analyzed by gas chromatography, the NO reduction activity was evaluated in terms of the conversion of NO into  $\text{N}_2$ .

$$\text{NO Conversion(%)} = (2 [\text{N}_2]_{\text{out}} / [\text{NO}]_{\text{in}}) \times 100$$

The CO oxidation activity was evaluated in terms of the conversion of CO into  $\text{CO}_2$

$$\text{CO Conversion (%)} = \frac{([\text{CO}]_{\text{in}} - [\text{CO}]_{\text{out}}) \times 100}{[\text{CO}]_{\text{in}}}$$

The C<sub>3</sub>H<sub>8</sub> oxidation activity was evaluated in terms of the conversion of C<sub>3</sub>H<sub>8</sub> into CO and CO<sub>2</sub>.

$$\text{C}_3\text{H}_8 \text{ Conversion(}\%) = \frac{(\text{[C}_3\text{H}_8\text{]_{in}} - \text{[C}_3\text{H}_8\text{]_{out}}) \times 100}{\text{[C}_3\text{H}_8\text{]_{in}}}$$

**APPENDIX B**  
**Physical Properties of Carbon Monoxide**

Property	Value
mol. wt.	28.011
m.p.	68.09 K
b.p.	81.65 K
H, fusion (68 K) <sup>a</sup>	0.867 kJ/mol
H, vaporization (81 K) <sup>a</sup>	6.042 kJ/mol
density [273 K, 101.33 kPa(1atm)]	1.2501 g/L
sp. gr., liquid, 79 K <sup>b</sup>	0.814
sp. gr., gas, 298 K <sup>c</sup>	0.968
critical temperature	132.9 K
critical pressure	3.496 Mpa(34.5 atm)
critical density	0.3010 g/cm <sup>3</sup>
G° formation (298 K) <sup>a</sup>	-137.16 kJ/mol
H° formation (298 K) <sup>a</sup>	-110.53 kJ/mol
S° formation (298 K) <sup>a</sup>	0.1975 kJ/mol
C <sub>p</sub> ° (298 K) <sup>a</sup>	29.1 J/mol
C <sub>v</sub> ° (298 K) <sup>a</sup>	20.8 J/mol
autoignition temperature	925 K
flammability limits in air <sup>d</sup>	
upper limit, %	74.2
lower limit, %	12.5

<sup>a</sup> To convert J to cal, divide by 4.184

<sup>b</sup> With respect to water at 277 K.

<sup>c</sup> With respect to air at 298 K.

<sup>d</sup> Saturated with water vapor at 290 K.

### Physical Properties of Nitric Oxide

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Property	Value
mol. wt.	30.1
m.p., °C	-161
b.p., °C	151.18
heat of fusion, kcal./mole	0.550
heat of vaporization, kcal./mole	3.293
heat of formation, kcal./mole	21.50
density[0 °C, 1 atm], g/L	1.2536
sp. gr., gas, [0 °C, 1 atm], (air = 1)	-93
critical temperature, °C	1.018
critical pressure, atm	64
color	colorless gas, blue liquid and solid

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**Ambient Air Quality Standard of Thailand( 1981)**

Pollutants	average value (mg/m <sup>3</sup> )				methods of measurement
	1h	8 h	24 h	1 year	
Carbon Monoxide (CO)	50	20	-	-	Non Dispersive Infrared Detection
Nitrogen Dioxide (NO <sub>2</sub> )	0.32	-	-	-	Gas Phase Chemiluminescence
Sulfur Dioxide (SO <sub>2</sub> )	-	-	0.3	1*	Pararosanniline
Suspended Particulate Matter (SPM)	-	-	0.33	0.1*	Gravimetric
Photochemical Oxidant (O <sub>3</sub> )	0.20	-	-	-	Chemiluminescence
Lead (Pb)	-	-	0.01	-	Wet Ashing

Note : \* = Geometric mean

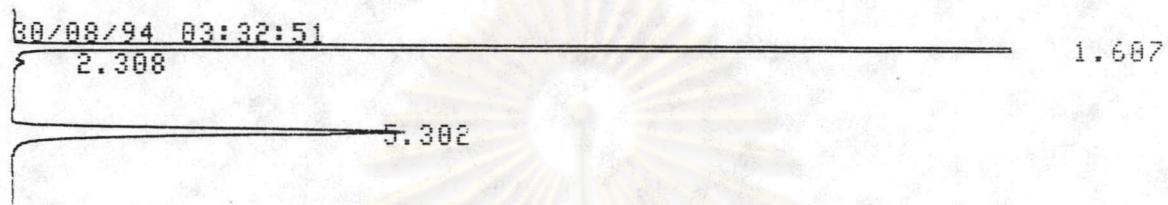
Specification of Alumina Support ( $\text{Al}_2\text{O}_3$ ) Type KHN-3  
from Sumitomo Aluminium Smelting Co., Ltd.

Chemical Composition (weight percent)

- $\text{Al}_2\text{O}_3$	60-70	%
- $\text{SiO}_2$	30-35	%
- $\text{Fe}_2\text{O}_3$	0.3-0.5	%
- $\text{TiO}_2$	0.5-0.7	%
- $\text{CaO}$	0.1-0.2	%
- $\text{MgO}$	0.2-0.4	%
- $\text{Na}_2\text{O}$	0.3-0.4	%
- $\text{K}_2\text{O}$	0.2-0.3	%
- $\text{ZrO}_2 + \text{HfO}_2$	0.03-0.04	%

Physical Properties

- Bulk Density (g/cc)	1.3-1.5
- Apparent Specific Gravity	3.1-3.3
- Packing Density (lb/ft <sup>3</sup> )	20-25
- Pore Volume (cc/g)	0.5513
- Surface Area (m <sup>2</sup> /g)	319.8757

**Sample of Chromatogram****COLUMN MS-5A**

PKNO	TIME	AREA	CONC.	NAME
1	1.607	28841	77.4407	O <sub>2</sub>
2	2.308	86	0.2317	N <sub>2</sub>
3	5.302	8315	22.3276	CO

05:20:22 557 1.0  
 2.417  
 6.115

## COLUMN PORAPAK-Q

PKNO	TIME	AREA	CONC.	NAME
1	0.557	4239	34.7166	AIR
2	1.012	5517	40.4131	CO <sub>2</sub>
3	2.417	1981	14.5087	H <sub>2</sub> O
4	6.115	1414	10.3616	C <sub>3</sub> H <sub>8</sub>



VITA

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