REFERENCES

- 1. Anagnosptopoulos, A. (1973), "Evaluation of the undrained shear strength from static cone penetration tests in a soft silty clay in Patras", Proc. European symp penetration testing, Stockholm.
- 2. Bachelier, M. and Parez L. (1965)m "Contribution of the study of soil compressibility by means of a cone penetrometer", Proc. 6th. Int. Conf. S.M. & P.E., Montreal, 1965, vol. 2, pp. 3-7.
- 3. Begemann, H.K.S., Ph. (1963), "The use of the static soil penetrometer in Holland", New Zealand engineering, vol. 18, No. 2 pp. 41-49.
- 4. Brand, E.W., Moh, Z.C. and Wirojanagud, P. (1964), "Interpretation of Dutch cone tests in soft Bangkok clay", Proc. European Symp. Penetration testing, Stockholm.
- 5. Eemetrious, Koutsoftas and Joseph A. Fisher., "In-situ undrained shear strength of two marine clays", Journal of the geotechnical engineering division, A.S.C.E. No. GT 9, September, 1976, pp. 992-1005.
- 6. Eide, O., "Correlation between cone tip resistance and field vane

 shear strength", Proc. European Sump. Penetration testing,

 vol. 21, pp. 128-129.
- 7. Haley and Aldrich (1969), "Test borings and laboratory soil test

 data for Bangkok, Thailand"., Report to Camp, Dresser and

 Mckee, by Haley and Aldrich, Inc., Cambridge, Massachusette.
- 8. Krungthep Engineering Consultants Co., Ltd., "Dutch cone penetration

 test at Donmuang site", Report to the Ministry of Ministry

 of Communications, 1979.

- 9. Krungthep Engineering Consultants Co., Ltd., "Factual report on soil investigation at Donmuang site volume 5 and 6",

 Report to the Ministry of communication for Bangkok international development project, May, 1979.
- 10. Meigh, A.C. and Corbett, B.O. (1969), "A comparison of in-situ measurements in a soft clay with laboratory tests and settlement of soil tanks", Conf. In-situ investigation in soils and rocks, London, Paper 15, pp. 173-179.
- 11. Moh, Z.C., Nelson, J.D., and Brand, E.W., "Strength and deformation behavior of Bangkok clay", Proc. 7th Icsmfe, Mexico city, vol. 1, pp. 287-295.
- 12. Muktabhant, C., Teerawong, P. and Temgamnuay, V., "Engineering

 Properties of Bangkok subsoils", Chulalongkorn University,

 Bangkok, 1966.
- 13. Pham, T.M., (1972), "Application of the Dutch cone in Bangkok area",
 A.I.T., M. Eng. Thesis, Bangkok.
- 14. Ruangvit, C., Adul, R. and Deja, S., "Estimation of pile bearing capacity by Dutch cone test", Thai engineering journal,
 No. 1, Feb., 1977, pp. 16-28.
- 15. Schmertmann, J.H. (1966), "Static cone penetrometers for soil exploration", Civil Engineering, vol. 37, No. 6, pp. 71-73.
- 16. Schmertmann, J.H., "Suggested method for deep static cone penetration

 test", Special procedures for testing soil and rock for
 engineering purposes, Special technical publication 497,

 American Society for testing and materials, 1970, pp. 71-77.

- 17. Schmertmann, J.H., "The measurement of in-situ shear strength",

 Proceedings ASCE specialty conference on in-situ

 measurements of soil properties, vol. 2, June, 1975,

 pp. 57-158.
- 18. Thomas, D. (1965), "Static cone penetration tests in London Clay", Geotechnique, vol. 15, pp. 174-179.
- 19. Wirojanagud, P. (1974), "Interpretation of Dutch cone and vane shear tests in soft Bangkok clays", A.I.T., M.Eng. thesis, Bangkok.
- 20. Wirojanagud, P. (1974), "Subsoil investigation by Dutch cone

 penetration test", Thai engineering journal No. 2, April,

 1976, pp. 76-88.

APPENDIX

CURVE FITTING SOLUTION

- 1. Equation used in curve fitting
 - 1.1 Linear regression (Lin.)

$$y = a + bx$$

1.2 Exponential curve fit (exp.)

$$y = ae^{bx}$$

1.3 Logaithmic curve fit (Log.)

$$y = a + blnX$$

1.4 Power curve fit (Pwr.)

$$y = ax^b$$

in which,

a and b are regression coefficients and can be computed by the formula as shown in Table A-1.

X and y are variables.

2. Curve fitting to the predicted and the measured UC strength.

Data from Table 4.7 were tabulated as follows,

W/LI	(x)	1.0	1.0	1.1	1.1	1.1	1.3	1.3	1.3	1.4	1.4	1.4
UC (w)	, (y ₁)	0.4	0.4	0.5	0.5	0.4	0.9	0.6	0.6	1.2	1.0	0.7
UC UC (s)	(y ₂)	0.6	1.0	0.7	1.3	0.8	1.2	1.1	0.9	1.7	1.6	0.9

TABLE A-1 Formula To Compute a,b and r²

Curve Type	а	b	Correlation, r ²
Lin,	$\left[\frac{\sum_{i=1}^{N} - b^{\sum_{i=1}^{N} i}}{n}\right]$	$\frac{\sum x_i y_i - \frac{\sum x_i \sum y_i}{n}}{\sum x_i^2 - \frac{(\sum x_i)^2}{n}}$	$\frac{\left[\sum x_{i}y_{i} - \frac{\sum x_{i}\sum y_{i}}{n}\right]^{2}}{\left[\sum x_{i}^{2} - \frac{\left(\sum x_{i}\right)^{2}}{n}\right]\left[\sum y_{i}^{2} - \frac{\left(\sum y_{i}\right)^{2}}{n}\right]}$
Exp.	$\exp\left[\frac{\sum \ln y_i}{n} - b \frac{\sum x_i}{n}\right]$	$\frac{\sum x_i \ln y_i - \frac{1}{n} (\sum x_i) (\sum \ln y_i)}{\sum x_i^2 - \frac{1}{n} (\sum x_i)^2}$	$\frac{\left[\sum x_i \ln y_i - \frac{1}{n} \sum x_i \sum \ln y_i\right]^2}{\left[\sum x_i - \frac{\left(\sum x_i\right)^2}{n}\right] \left[\sum (\ln y_i)^2 - \frac{\left(\sum \ln y_i\right)^2}{n}\right]}$
Log.	1/n (∑y _i - b∑lnx _i)	$\frac{\sum y_i \ln x_i - \frac{1}{n} \sum \ln x_i \sum y_i}{\sum (\ln x_i)^2 - \frac{1}{n} (\sum \ln x_i)^2}$	$\frac{\left[\sum y_{i} \ln x_{i} - \frac{1}{n} \sum \ln x_{i} \sum y_{i}\right]^{2}}{\left[\sum (\ln x_{i})^{2} - \frac{1}{n} (\sum \ln x_{i})^{2}\right] \left[\sum y_{i}^{2} - \frac{1}{n} (\sum y_{i})^{2}\right]}$
Pwr.	$\exp\left[\frac{\sum \ln y_i}{n} - b \frac{\sum \ln x_i}{n}\right]$	$\frac{\sum (\ln x_i)(\ln y_i) - (\sum \ln x_i)(\sum \ln y_i)}{n}$ $\sum (\ln x_i)^2 - \frac{(\sum \ln x_i)^2}{n}$	$\frac{\left[\sum (\ln x_i)(\ln y_i) - \frac{(\sum \ln x_i)(\ln y_i)}{n}\right]^2}{\left[\sum (\ln x_i)^2 - \frac{(\sum \ln x_i)^2}{n}\right]\left[\sum (\ln y_i)^2 - \frac{(\sum \ln y_i)^2}{n}\right]}$

2.1 Computation of regression coefficients for ${\bf X}$ and ${\bf y}_1$.

2.1.1 Linear regression fitting (Lin.)

From Table A-1, a =
$$\frac{\Sigma Y_{i}}{n} - b \frac{\Sigma X_{i}}{n}$$

b = $\frac{\Sigma X_{i} Y_{i} - \frac{\Sigma X_{i} Y_{i}}{n}}{\Sigma X_{i}^{2} - \frac{(\Sigma X_{i})^{2}}{n}}$
Correlation, $r^{2} = \frac{\Sigma X_{i} Y_{i} - \frac{\Sigma X_{i} Y_{i}}{n}}{\left[\Sigma X_{i}^{2} - \frac{(\Sigma X_{i})^{2}}{n}\right] \left[\Sigma Y_{i}^{2} - \frac{(\Sigma Y_{i})^{2}}{m}\right]}$
n = 11, $\Sigma X_{i} = 13.40$, $\Sigma Y_{i} = 7.20$
 $\Sigma X_{i} Y_{i} = 9.13$
 $\Sigma X_{i} Y_{i} = 96.48$
 $\Sigma X_{i}^{2} = 16.58$
($\Sigma X_{i}^{2} = 179.56$
then, b = $\frac{9.13}{16.58 - \frac{179.56}{11}}$
b = 1.4
a = $\frac{7.20}{11} - \frac{1.40 \times 13.40}{11}$
a = -1.1
and $r^{2} = 0.69$

2.1.2 Exp., Log. and Pwr. curve fit.

The variables x and y_1 were put in the calculator program of HP 67 type to compute the regression coefficients a, b and r^2 and

found to be,

For exp. curve fit,

$$r^2 = 0.34$$

$$a = 0.1$$

$$b = 1.6$$

For log. curve fit,

$$r^2 = 0.68$$

$$a = 0.3$$

$$b = 1.7$$

For pwr. curve fit

$$r^2 = 0.78$$

$$a = 0.4$$

$$b = 2.5$$

The maximum correlation r^2 will be selected, then the pwr. curve suit the condition,

or,
$$\frac{UC}{UC} = 0.4 \left(\frac{1}{w/LL}\right)^{2.5}$$

$$UC = UC_{(w)} \times 0.4 \left(\frac{1}{w/LL}\right)^{2.5}$$
or,
$$UC_{(aw)} = \frac{q_C}{19} \times 0.4 \left(\frac{1}{w/LL}\right)^{2.5}$$

$$= 0.02 q_C \left(\frac{1}{w/LL}\right)^{2.5}$$

2.2 Computation of regression coefficients for x and y_2 .

The variables x and y_2 were put in the calculator program of HP 67 type to compute the regression coefficients a, b and r^2 and found to be;

For lin. curve fit,

$$r^2 = 0.37$$

$$a = -0.6$$

$$b = 1.3$$

For exp. curve fit,

$$r^2 = 0.39$$

$$a = 0.2$$

$$b = 1.3$$

For log. curve fit

$$r^1 = 0.37$$

$$a = 0.8$$

$$b = 1.6$$

For pwr. curve fit

$$r^2 = 0.40$$

$$a = 0.8$$

$$b = 1.5$$

Then the pwr. curve suit the condition,

$$y_2 = ax^b$$

or,
$$\frac{UC}{UC}_{(s)} = 0.8 \left(\frac{1}{w/LL}\right)^{1.5} = UC_{(s)} \times 0.8 \left(\frac{1}{w/LL}\right)^{1.5}$$

or,
$$UC_{(as)} = 0.04 (q_C - \gamma_t^Z) \times (\frac{1}{w/LL})^{1.5}$$

3. Curve fitting to the predicted and measured FV strength.

Data from Table 4.9 were tabulated and they were computed in the same manner. FV and $FV_{(w)}$ will be represented by the variables y and x respectively.

For lin. curve fit,

$$r^2 = 0.99$$

a = 1.5

b = 0.5

For exp. curve fit,

$$r^2 = 0.98$$

a = 1.7

b = 0.2

For log. curve fit,

$$r^2 = 0.98$$

a = 1.7

b = 1.2

For exp. curve fit,

$$r^2 = 0.98$$

a = 1.9

b = 0.4

The linear curve fit suit the condition,

$$y = a + bx$$

FV = 1.5 + 0.5 FV_(w)
$$q_{c}$$

or, FV_(a) = 1.5 + 0.5 x q_{c}

 $= 1.5 + 0.03 q_{c}$

4. Curve fitting to the predicted and the measured UU strength

Data from Table 4.11 were tabulated in the same manner. UU and $UU_{(w)}$ will be represented by the variables y and x respectively.

For lin. curve fit,

$$r^2 = 0.06$$

$$a = 1.1$$

$$b = 0.04$$

For exp. curve fit,

$$r^2 = 0.06$$

$$a = 1.1$$

$$b = 0.03$$

For log. curve fit,

$$r^2 = 0.03$$

$$a = 1.2$$

$$b = 0.05$$

For pwr. curve fit,

$$r^2 = 0.52$$

$$a = 1.1$$

$$b = 0.1$$

The pwr. curve fit suit the condition,

$$y = ax^b$$

$$UU = 1.1 (UU_{(w)})^{0.1}$$
$$= 1.1 \times (\frac{q_{C}}{17})^{0.1}$$

$$= 1.1 \times (\frac{q_c}{17})^{0.1}$$

or,
$$UU_{(aw)} = 0.83 (q_c)^{0.1}$$

All formulae are empirical formulae and unit of all streses are in t/m²

VITA

Mr. Poosit Sunlakavisase was awarded the Bachelor's degree in Civil Engineering from Chiengmai University in 1978, he was admitted to the Graduate School of Chulalongkorn University in 1978. He is, at present, working at the Asian Engineering Consultants Co., Ltd.

