## CHAPTER II

## LITERATURE REVIEW



## 1. WIROJANAGUD, P. (1974)

WIROJANAGUD suggested from the bearing capacity theories that,

$$q_c = 1.3 \times 2(\bar{\sigma}_{vo} N_q + cN_c)$$
 (2.1)

in which,

q = cone resistance.

 $\bar{\sigma}_{\mu\nu}$  = effective overburden pressure.

c = cohesion

 $N_{c}, N_{g}$  = bearing capacity factor.

For cohesive soil, to determine the undrained shear strength (assuming  $\phi = 0$ ) the quick test should be performed on saturated clay. The rate of penetration of the Dutch cone penetration test is about 2 cm./sec. can be considered as the quick test.

From Eq. (2.1)

$$q_c = 2.6 N_c S_u + 2.6 \frac{1}{\sigma}$$

Effect of surcharge (2.6  $\bar{\sigma}_{vo}$ ) will balance the weight of the driving rods, then,

$$q_c = NS_u$$
 (2.2)

in which,

S = undrained shear strength.

N = cone factor.

N depends on type of cone, type of soil and type of undrained shear strength.

From the experiment at various places, values of N were tabulated in Table 2.1 (WIROJANAGUD, 1976).

Let,

UC (w) = the predicted values of UC strength as computed
by WIROJANAGUD method.

 $FV_{(w)}$  = the predicted values of FV strength as computed by WIROJANAGUD method.

and,

 $UU_{(w)} =$  the predicted values of UU strength as computed by WIROJANAGUD method.

then,

$$UC_{(w)} = \frac{q_C}{19}$$
 \_\_\_\_\_(2.3)

$$FV_{(w)} = \frac{q_C}{16}$$
 (2.4)

$$UU_{(w)} = \frac{q_C}{17}$$
 (2.5)

## 2. SCHMERTMANN, J.H. (1975)

The relation between undrained shear strength and cone resistance for young clays with plasticity index greater than 10 were presented by SCHMERTMANN J.H. as follows:

$$UC_{(s)} = \frac{q_c - \sigma_{VO}}{18}$$
 (2.6)

|                          |                   | The second second     |                     |
|--------------------------|-------------------|-----------------------|---------------------|
| REFERENCE                | CLAY              | $N = \frac{q_c}{S_u}$ | S <sub>u</sub> Type |
| BEGEMANN<br>(1965)       | Clayey Soil       | 14                    | FV                  |
| THOMAS<br>(1965)         | London Clay       | 18                    | UU                  |
| WARD et al<br>(1965)     | London Clay       | 16                    | UU                  |
| MEIGH and CORBETT (1969) | Arabian Gulf Clay | 16                    | FV                  |
| PHAM TIEM NAM<br>(1972)  | Soft Bangkok Clay | 19                    | UC                  |
| ANAGNOSPTOPOULOS         | Patras Clay       | 17                    | UU                  |
| WIROJANAGUD<br>(1974)    | Soft Bangkok Clay | 19,14                 | FV                  |

TABLE 2.1 Values Of Cone Factor(N)

$$UU_{(s)} = \frac{q_c - \sigma_{vo}}{16}$$
 (2.8)

in which,

UC (s), FV (s) and UU (s) are the predicted values of UC, FV and UU strength as computed by SCHMERTMANN method respectively.

 $\sigma_{\mbox{\sc vo}}$  is the total overburden pressure above the depth of penetration (Z).