

เอกสารอ้างอิง

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**National
Semiconductor**

Industrial Blocks

LM2907, LM2917 Frequency to Voltage Converter

General Description

The LM2907, LM2917 series are monolithic frequency to voltage converters with a high gain op amp/comparator designed to operate a relay, lamp, or other load when the input frequency reaches or exceeds a selected rate. The tachometer uses a charge pump technique and offers frequency doubling for low ripple, full input protection in two versions (LM2907-8, LM2917-8) and its output swings to ground for a zero frequency input.

Advantages

- Output swings to ground for zero frequency input
- Easy to use; $V_{OUT} = f_{IN} \times V_{CC} \times R1 \times C1$
- Only one RC network provides frequency doubling
- Zener regulator on chip allows accurate and stable frequency to voltage or current conversion. (LM2917)

Features

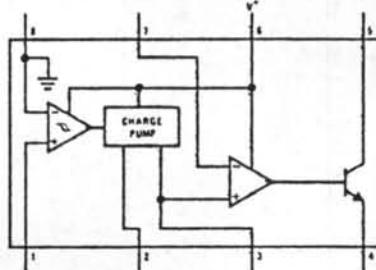
- Ground referenced tachometer input interfaces directly with variable reluctance magnetic pickups
- Op amp/comparator has floating transistor output
- 50 mA sink or source to operate relays, solenoids, meters, or LEDs

- Frequency doubling for low ripple
- Tachometer has built-in hysteresis with either differential input or ground referenced input
- Built-in zener on LM2917
- $\pm 0.3\%$ linearity typical
- Ground referenced tachometer is fully protected from damage due to swings above V_{CC} and below ground

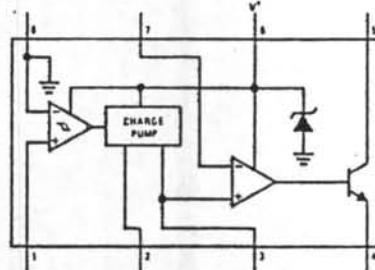
Applications

- Over/under speed sensing
- Frequency to voltage conversion (tachometer)
- Speedometers
- Breaker point dwell meters
- Hand-held tachometer
- Speed governors
- Cruise control
- Automotive door lock control
- Clutch control
- Horn control
- Touch or sound switches

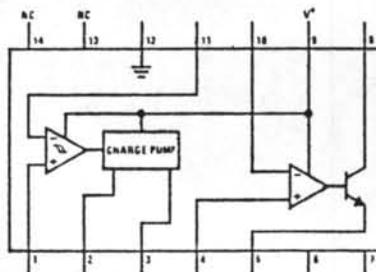
Block and Connection Diagrams Dual-In-Line Packages, Top Views



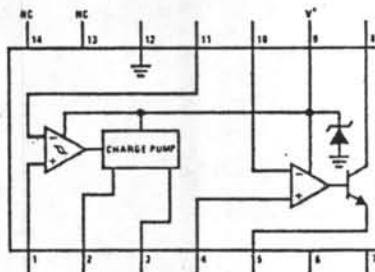
Order Number LM2907N-8
See NS Package N08B



Order Number LM2917N-8
See NS Package N08B



Order Number LM2907J
See NS Package J14A
Order Number LM2907N
See NS Package N14A



Order Number LM2917J
See NS Package J14A
Order Number LM2917N
See NS Package N14A

Absolute Maximum Ratings (Note 1)

Supply Voltage	28V	Input Voltage Range	
Supply Current (Zener Options)	25 mA	Tachometer LM2907-8, LM2917-8 LM2907, LM2917	±28V 0.0V to +28V 0.0V to +28V
Collector Voltage	28V	Op Amp/Comparator	0.0V to +28V
Differential Input Voltage		Power Dissipation	500 mW
Tachometer	28V	Operating Temperature Range	-40°C to +85°C
Op Amp/Comparator	28V	Storage Temperature Range	-65°C to +150°C
		Lead Temperature (Soldering, 10 seconds)	300°C

Electrical Characteristics $V_{CC} = 12 \text{ V}_\text{DC}$, $T_A = 25^\circ\text{C}$, see test circuit

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
TACHOMETER					
Input Thresholds	$V_{IN} = 250 \text{ mV}_\text{p-p} @ 1 \text{ kHz}$ (Note 2)	±10	±15	±40	mV
Hysteresis	$V_{IN} = 250 \text{ mV}_\text{p-p} @ 1 \text{ kHz}$ (Note 2)		30		mV
Offset Voltage	$V_{IN} = 250 \text{ mV}_\text{p-p} @ 1 \text{ kHz}$ (Note 2)				
LM2907/LM2917			3.5	10	mV
LM2907-8/LM2917-8			5	15	mV
Input Bias Current	$V_{IN} = \pm 50 \text{ mV}_\text{DC}$		0.1	1	μA
V_{OH} Pin 2	$V_{IN} = +125 \text{ mV}_\text{DC}$ (Note 3)		8.3		V
V_{OL}	$V_{IN} = -125 \text{ mV}_\text{DC}$ (Note 3)		2.3		V
Output Current: I_2, I_3	$V_2 = V_3 = 6.0\text{V}$ (Note 4)	140	180	240	μA
Leakage Current: I_2	$I_2 = 0, V_3 = 0$			0.1	μA
Gain Constant, K	(Note 3)	0.9	1.0	1.1	
Linearity	$f_{IN} = 1 \text{ kHz}, 5 \text{ kHz}, 10 \text{ kHz}$, (Note 5)	-1.0	0.3	+1.0	%
OP/AMP COMPARATOR					
V_{OS}	$V_{IN} = 6.0\text{V}$		3	10	mV
I_{BIAS}	$V_{IN} = 6.0\text{V}$		50	500	nA
Input Common Mode Voltage		0		$V_{CC}-1.5\text{V}$	V
Voltage Gain			200		V/mV
Output Sink Current	$V_C = 1.0$	40	50		mA
Output Source Current	$V_E = V_{CC} - 2.0$		10		mA
Saturation Voltage	$I_{SINK} = 5 \text{ mA}$ $I_{SINK} = 20 \text{ mA}$ $I_{SINK} = 50 \text{ mA}$		0.1	0.5	V
				1.0	V
				1.5	V
ZENER REGULATOR					
Regulator Voltage	$R_{DROP} = 470\Omega$		7.56		V
Series Resistance			10.5	15	Ω
Temperature Stability			+1		$\text{mV}/^\circ\text{C}$
TOTAL SUPPLY CURRENT			3.8	6	mA

Note 1: For operation in ambient temperatures above 25°C, the device must be derated based on a 150°C maximum junction temperature and a thermal resistance of 175°C/W junction to ambient for package 22 and 16 or a thermal resistance of 187°C/W junction to ambient for package 20.

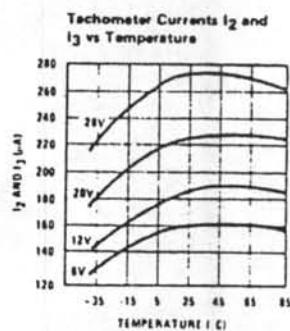
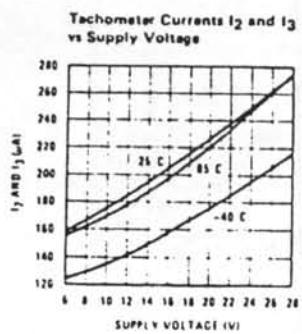
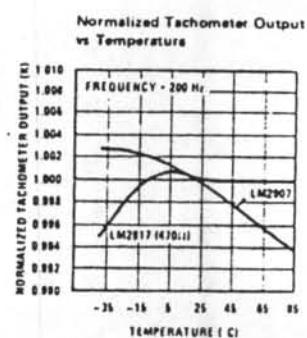
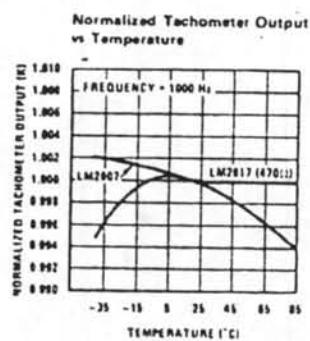
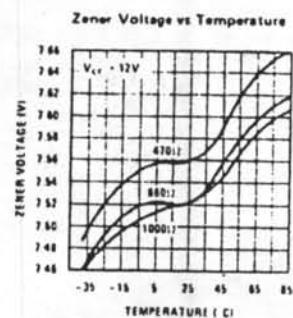
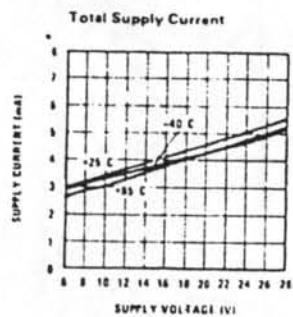
Note 2: Hysteresis is the sum $+V_{TH} - (V_{TH})$, offset voltage is their difference. See test circuit.

Note 3: V_{OH} is equal to $3/4 \times V_{CC} - 1 \text{ V}_{BE}$. V_{OL} is equal to $1/4 \times V_{CC} - 1 \text{ V}_{BE}$ therefore $V_{OH} - V_{OL} = V_{CC}/2$. The difference, $V_{OH} - V_{OL}$, and the mirror gain, I_2/I_3 , are the two factors that cause the tachometer gain constant to vary from 1.0.

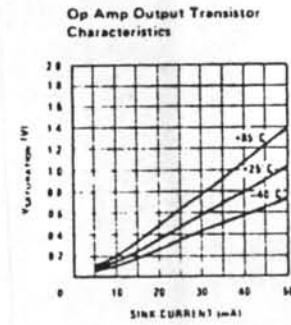
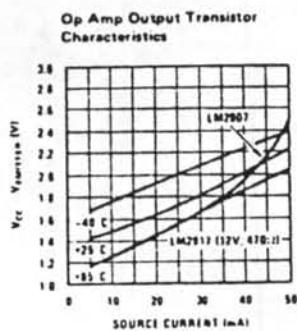
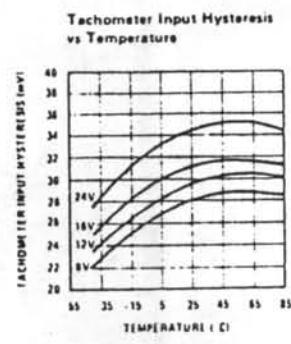
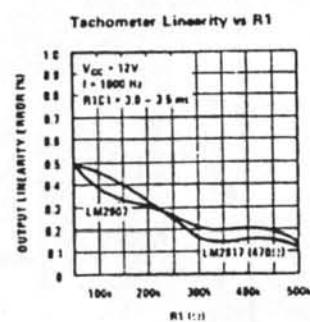
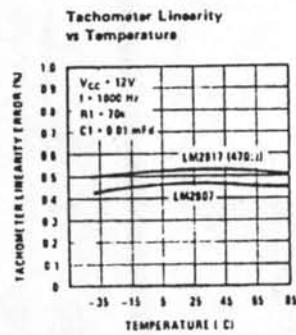
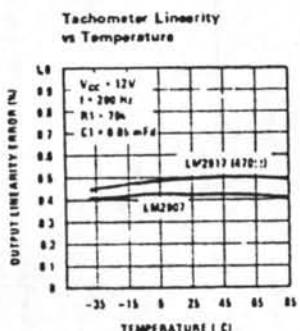
Note 4: Be sure when choosing the time constant $R_1 \times C_1$ that R_1 is such that the maximum anticipated output voltage at pin 3 can be reached with $I_3 \times R_1$. The maximum value for R_1 is limited by the output resistance of pin 3 which is greater than $10 \text{ M}\Omega$ typically.

Note 5: Nonlinearity is defined as the deviation of V_{OUT} (pin 3) for $I_{IN} = 5 \text{ kHz}$ from a straight line defined by the $V_{OUT} @ 1 \text{ kHz}$ and $V_{OUT} @ 10 \text{ kHz}$. $C_1 = 1000 \text{ pF}$, $R_1 = 68\text{k}$ and $C_2 = 0.22 \text{ mFD}$.

Typical Performance Characteristics



Typical Performance Characteristics (Continued)



General Description (Continued)

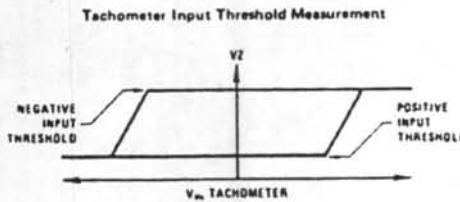
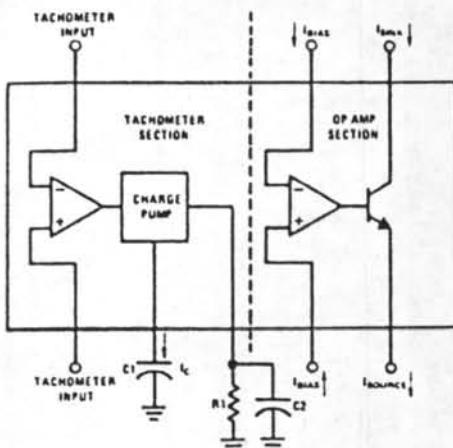
The op amp/comparator is fully compatible with the tachometer and has a floating transistor as its output. This feature allows either a ground or supply referred load of up to 50 mA. The collector may be taken above V_{CC} up to a maximum V_{CE} of 28V.

The two basic configurations offered include an 8-pin device with a ground referenced tachometer input and an internal connection between the tachometer output and the op amp non-inverting input. This version is well suited for single speed or frequency switching or fully buffered frequency to voltage conversion applications.

The more versatile configurations provide differential tachometer input and uncommitted op amp inputs. With this version the tachometer input may be floated and the op amp becomes suitable for active filter conditioning of the tachometer output.

Both of these configurations are available with an active shunt regulator connected across the power leads. The regulator clamps the supply such that stable frequency to voltage and frequency to current operations are possible with any supply voltage and a suitable resistor.

Test Circuit and Waveform



Applications Information

The LM2907 series of tachometer circuits is designed for minimum external part count applications and maximum versatility. In order to fully exploit its features and advantages let's examine its theory of operation. The first stage of operation is a differential amplifier driving a positive feedback flip-flop circuit. The input threshold voltage is the amount of differential input voltage at which the output of this stage changes state. Two options (LM2907-8, LM2917-8) have one input internally grounded so that an input signal must swing above and below ground and exceed the input thresholds to produce an output. This is offered specifically for magnetic variable reluctance pickups which typically provide a single-ended ac output. This single input is also fully protected against voltage swings to $\pm 28V$, which are easily attained with these types of pickups.

The differential input options (LM2907, LM2917) give the user the option of setting his own input switching level and still have the hysteresis around that level for excellent noise rejection in any application. Of course in order to allow the inputs to attain common-mode voltages above ground, input protection is removed

and neither input should be taken outside the limits of the supply voltage being used. It is very important that an input not go below ground without some resistance in its lead to limit the current that will then flow in the epi-substrate diode.

Following the input stage is the charge pump where the input frequency is converted to a dc voltage. To do this requires one timing capacitor, one output resistor, and an integrating or filter capacitor. When the input stage changes state (due to a suitable zero crossing or differential voltage on the input) the timing capacitor is either charged or discharged linearly between two voltages whose difference is $V_{CC}/2$. Then in one half cycle of the input frequency or a time equal to $1/2 f_{IN}$ the change in charge on the timing capacitor is equal to $V_{CC}/2 \times C_1$. The average amount of current pumped into or out of the capacitor then is:

$$\frac{\Delta Q}{T} = i_{C(AVG)} = C_1 \times \frac{V_{CC}}{2} \times (2f_{IN}) = V_{CC} \times f_{IN} \times C_1$$

The output circuit mirrors this current very accurately into the load resistor R_1 , connected to ground, such that if the pulses of current are integrated with a filter

Applications Information (Continued)

capacitor, then, $V_o = i_c \times R_1$, and the total conversion equation becomes:

$$V_o = V_{CC} \times f_{IN} \times C_1 \times R_1 \times K$$

Where K is the gain constant—typically 1.0.

The size of C_2 is dependent only on the amount of ripple voltage allowable and the required response time.

CHOOSING R1 AND C1

There are some limitations on the choice of R_1 and C_1 which should be considered for optimum performance. The timing capacitor also provides internal compensation for the charge pump and should be kept larger than 100 pF for very accurate operation. Smaller values can cause an error current on R_1 , especially at low temperatures. Several considerations must be met when choosing R_1 . The output current at pin 3 is internally fixed and therefore V_o/R_1 must be less than or equal to this value. If R_1 is too large, it can become a significant fraction of the output impedance at pin 3 which degrades linearity. Also output ripple voltage must be considered and the size of C_2 is affected by R_1 . An expression that describes the ripple content on pin 3 for a single R_1C_2 combination is:

$$V_{RIPPLE} = \frac{V_{CC}}{2} \times \frac{C_1}{C_2} \times \left(1 - \frac{V_{CC} \times f_{IN} \times C_1}{I_2}\right) \text{ pk-pk}$$

It appears R_1 can be chosen independent of ripple.

however response time, or the time it takes V_{OUT} to stabilize at a new voltage increases as the size of C_2 increases so a compromise between ripple, response time, and linearity must be chosen carefully.

As a final consideration, the maximum attainable input frequency is determined by V_{CC} , C_1 and I_2 :

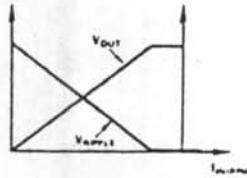
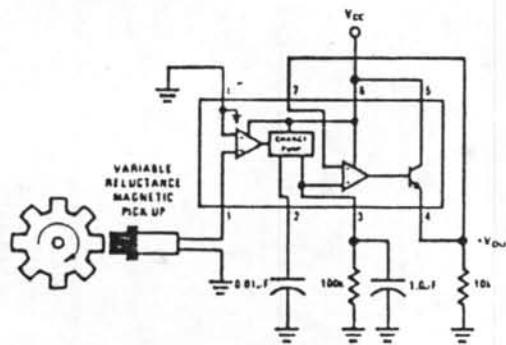
$$f_{MAX} = \frac{I_2}{C_1 \times V_{CC}}$$

USING ZENER REGULATED OPTIONS (LM2917)

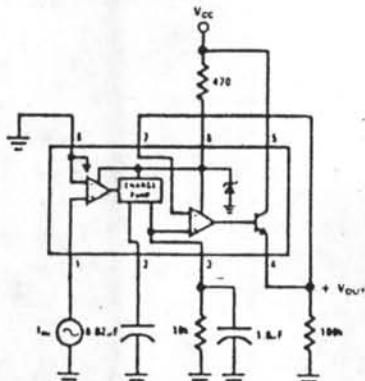
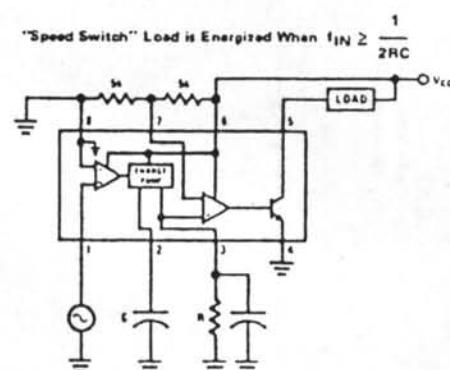
For those applications where an output voltage or current must be obtained independent of supply voltage variations, the LM2917 is offered. The most important consideration in choosing a dropping resistor from the unregulated supply to the device is that the tachometer and op amp circuitry alone require about 3 mA at the voltage level provided by the zener. At low supply voltages there must be some current flowing in the resistor above the 3 mA circuit current to operate the regulator. As an example, if the raw supply varies from 9 to 16V, a resistance of 470Ω will minimize the zener voltage variation to 160 mV. If the resistance goes under 400Ω or over 600Ω the zener variation quickly rises above 200 mV for the same input variation.

Typical Applications

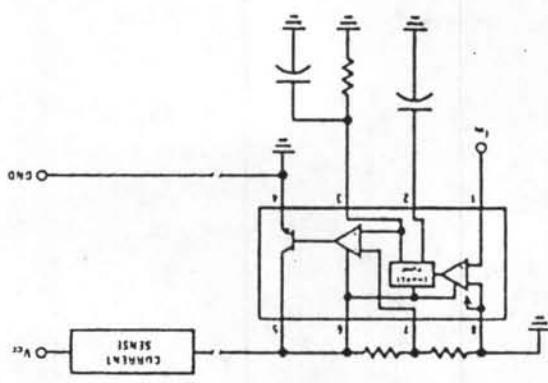
Minimum Component Tachometer



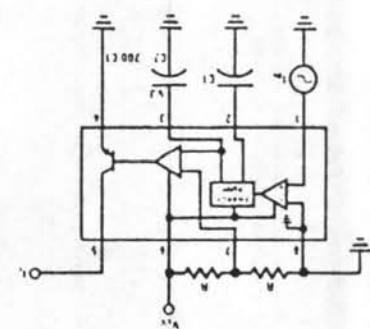
Zener Regulated Frequency to Voltage Converter



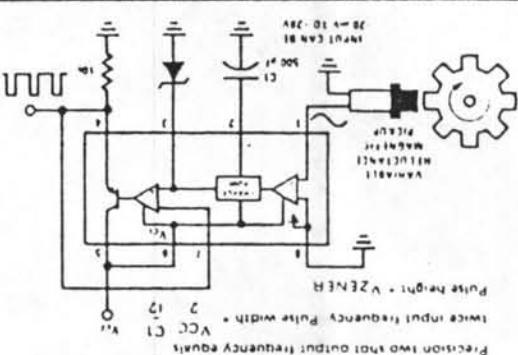
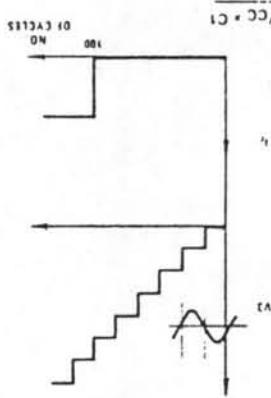
Typical Applications (Continued)



Two-Wire Hemotia Speed Switch

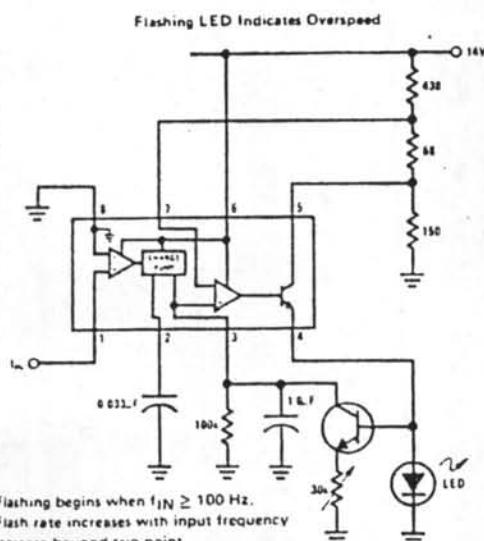
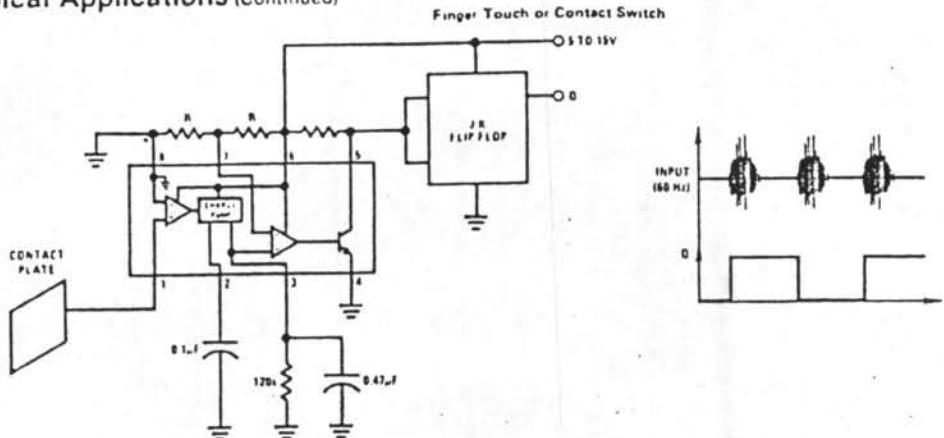


100 Cycle Delay Switch

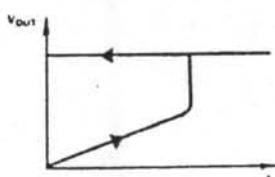
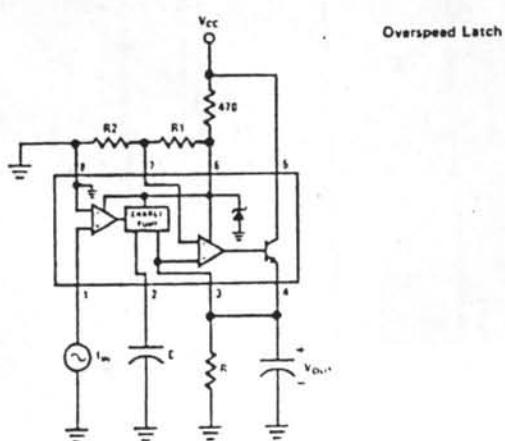
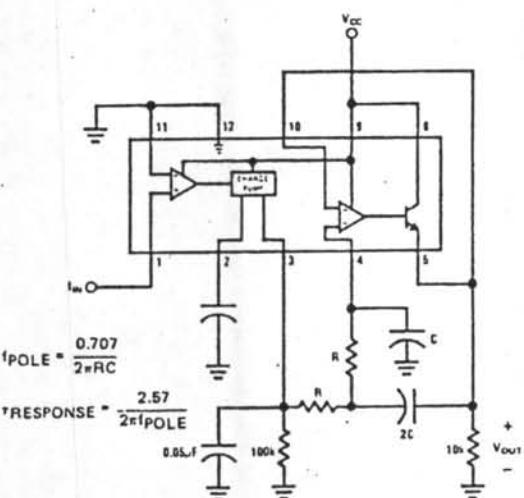


Variable Reluctance Magnetic Pickup Buffer Circuits

Typical Applications (Continued)



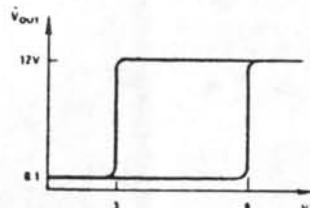
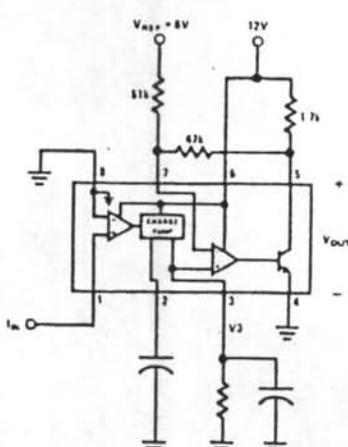
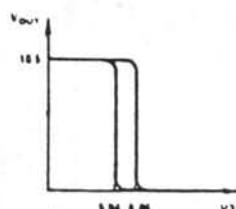
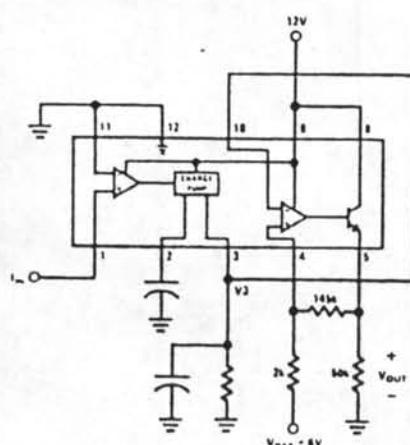
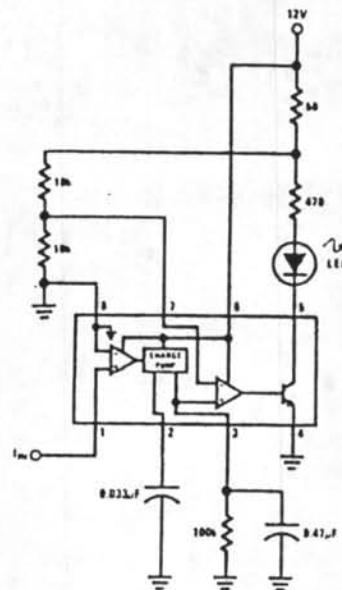
Frequency to Voltage Converter with
2 Pole Butterworth Filter to Reduce Ripple



Output latches when
 $f_{IN} = \frac{R_2}{R_1 + R_2} \frac{1}{RC}$
Reset by removing V_{CC} .

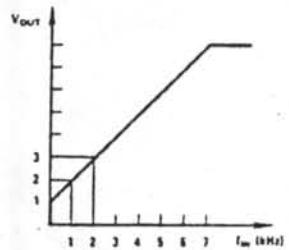
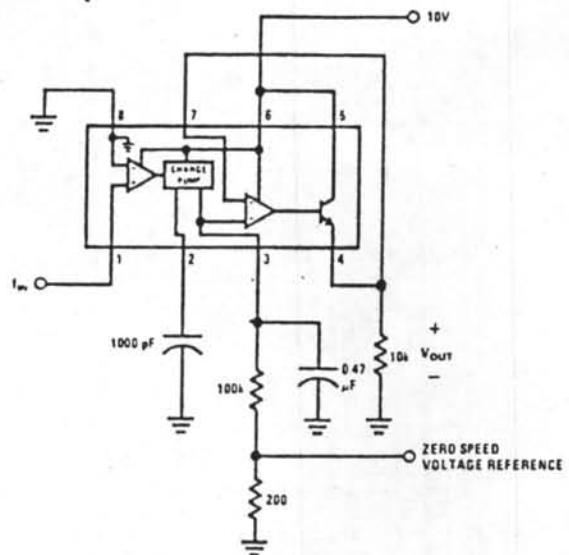
Typical Applications (Continued)

Some Frequency Switch Applications May Require Hysteresis in the Comparator Function Which Can Be Implemented in Several Ways:

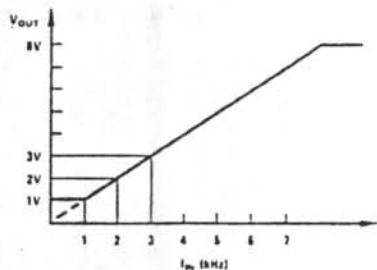
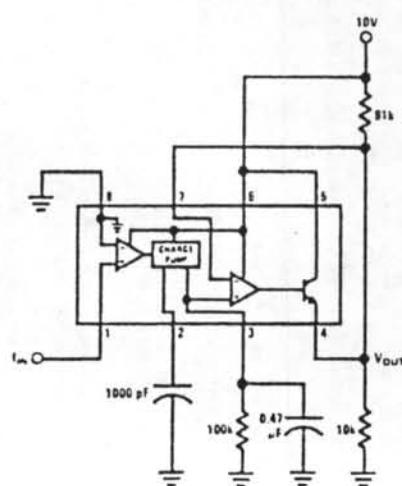


Typical Applications (Continued)

Changing the Output Voltage for an Input Frequency of Zero

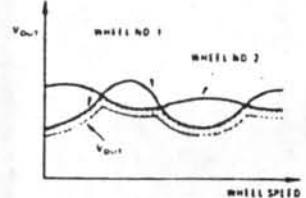
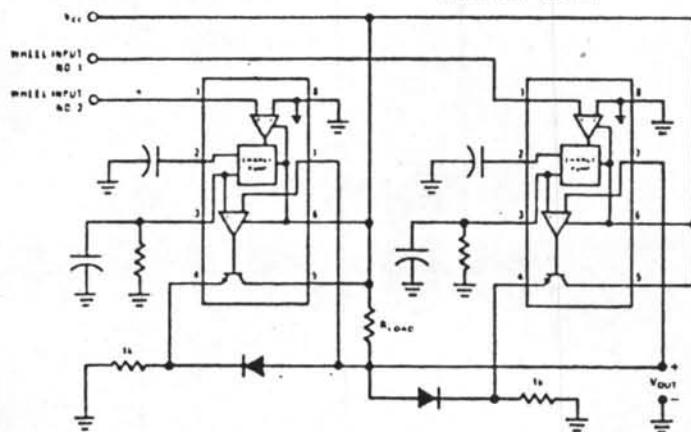


Changing Tachometer Gain Curve or Clamping the Minimum Output Voltage



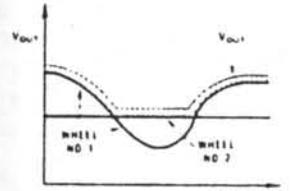
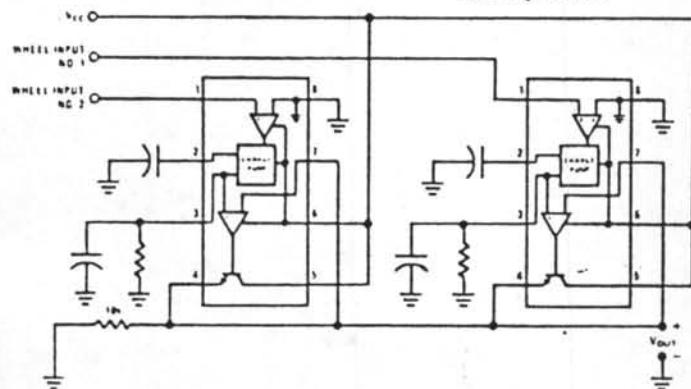
Anti-Skid Circuit Functions

"Select-Low" Circuit



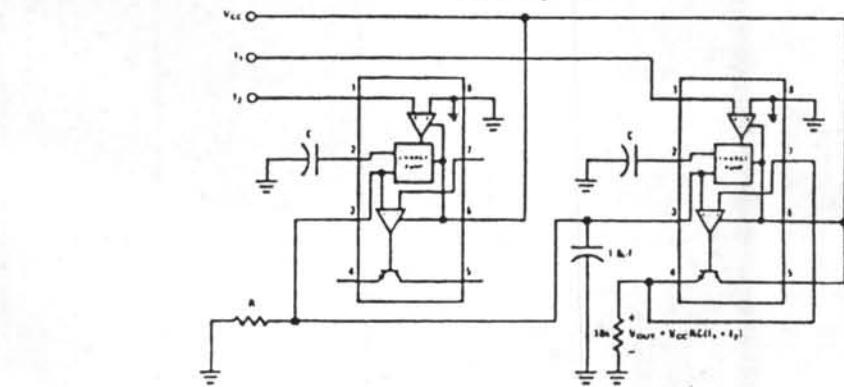
V_{OUT} is proportional to the lower of the two input wheel speeds.

"Select-High" Circuit

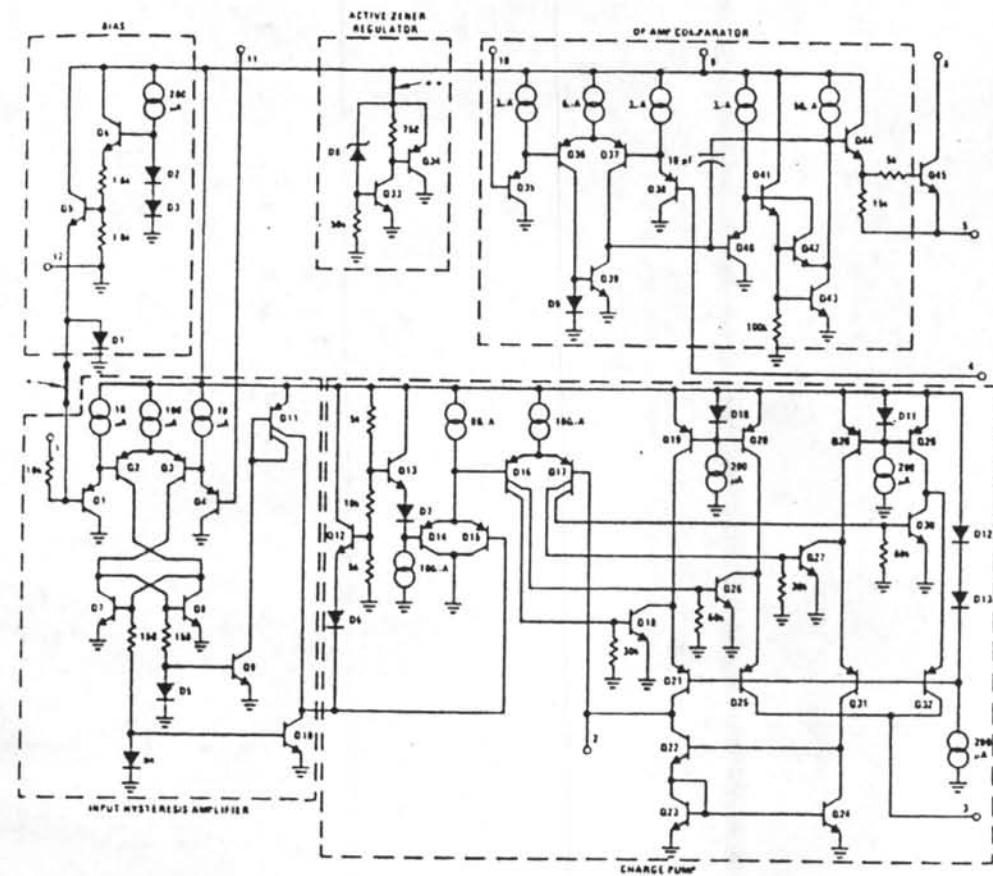


V_{OUT} is proportional to the higher of the two input wheel speeds.

"Select-Average" Circuit



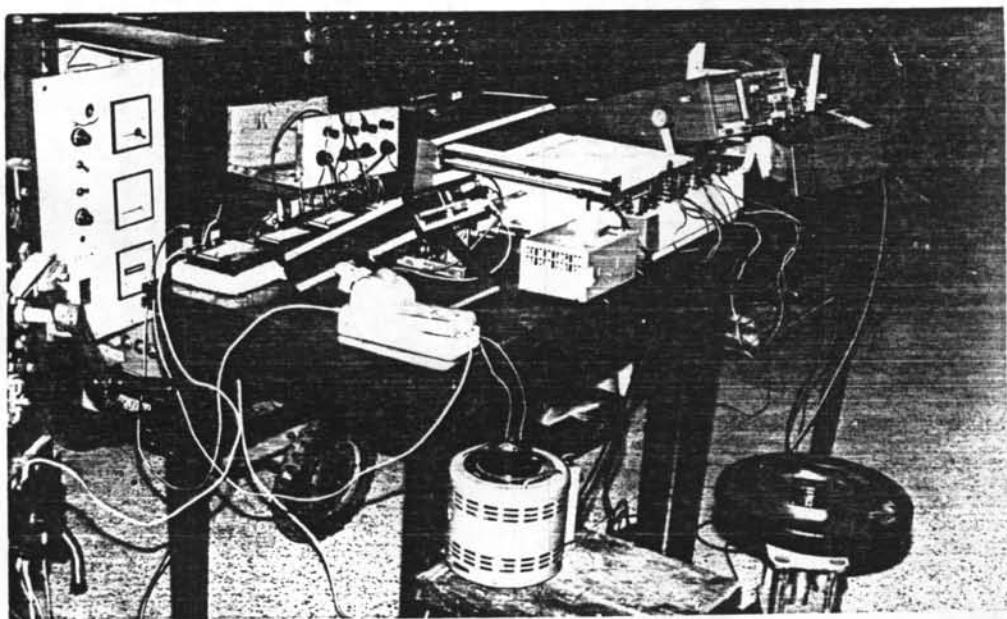
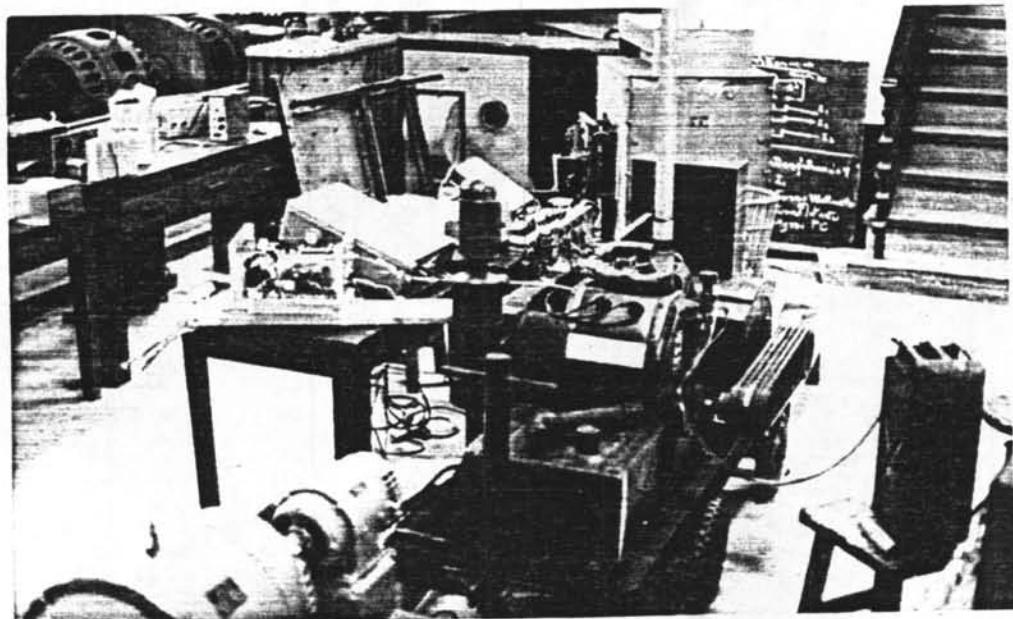
Equivalent Schematic Diagram



* Note: This connection made on LM2907-8 and LM2917-8 only.

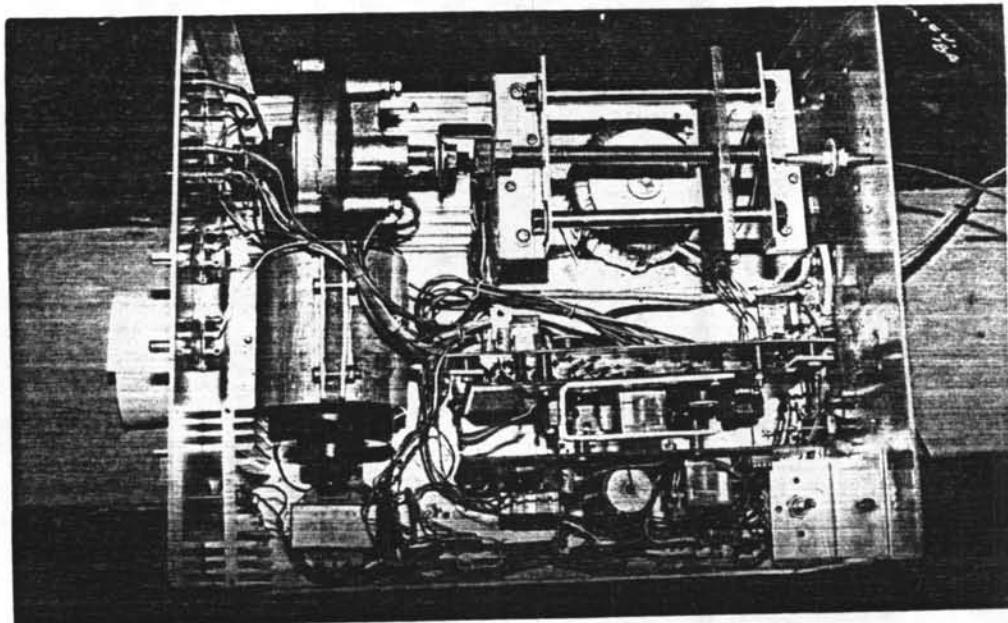
* Note: This connection made on LM2917 and LM2917-8 only.

ภาคผนวก ช.

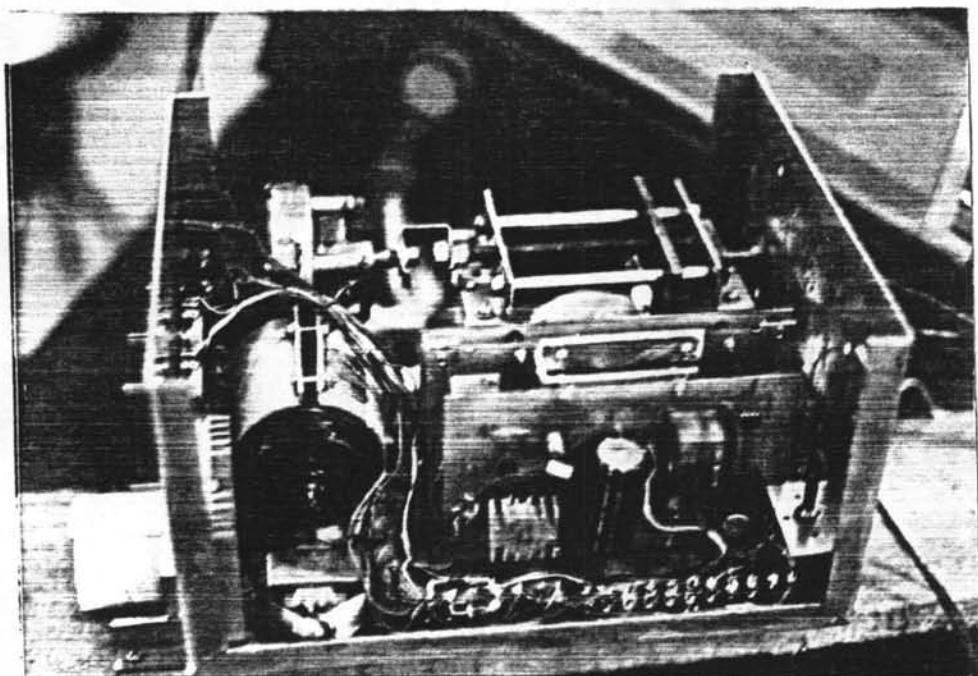


รูปแสดงอุปกรณ์และเครื่องมือที่ใช้ในการทดสอบ

ภาพค้านบน

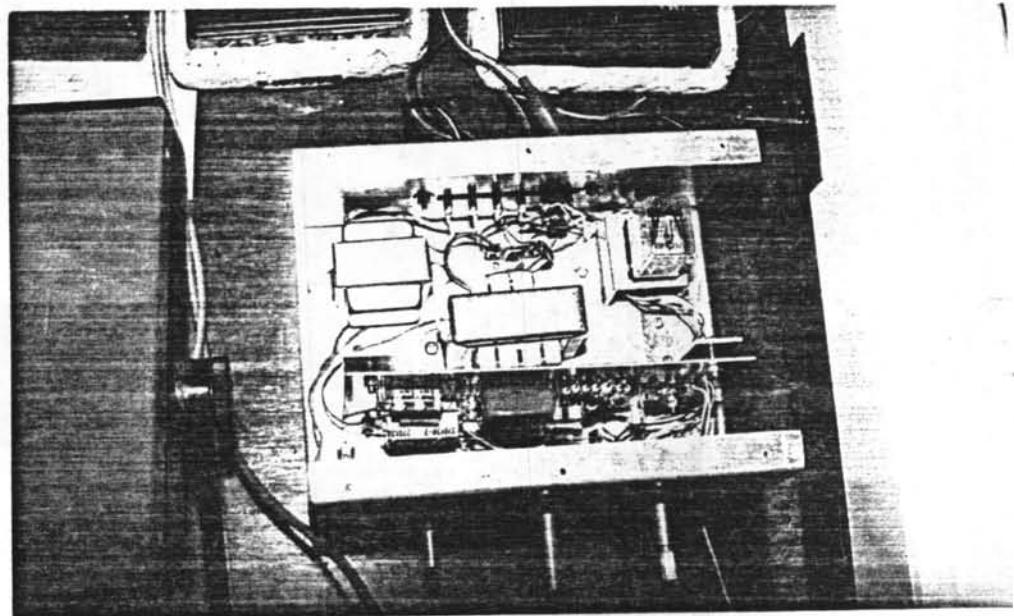


ภาพค้านข้าง

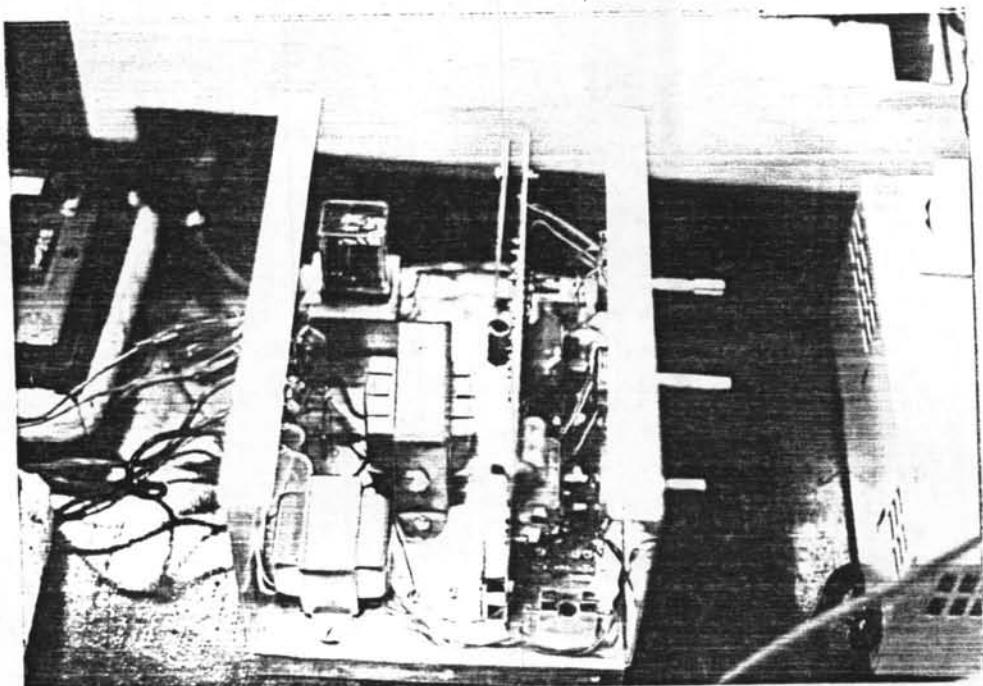


รูปแสดงส่วนประกอบและโครงสร้างของระบบควบคุมความถี่

ภาพด้านบน



ภาพด้านข้าง



รูปแสดงล่วนประกอบและโครงสร้างของระบบควบคุมแรงดันอัตโนมัติ

ประวัติผู้เขียน

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