



รายการอ้างอิง

ภาษาไทย

- ปณิธาน ลักณะประสิทธิ์. 2527. การวิเคราะห์โครงสร้าง. วิศวกรรมสถานแห่งประเทศไทยในพระบรมราชูปถัมภ์.
- สมชาย ตั้งจิตเพิ่มพูน. 2531. การวิเคราะห์ไม่เชิงเส้นทางเรขาคณิตของโครงข้อแข็งระนาบด้วยไมโครคอมพิวเตอร์. วิทยานิพนธ์ตามหลักสูตรปริญญาวิศวกรรมศาสตรมหาบัณฑิต. ภาควิชาวิศวกรรมโยธา บัณฑิตวิทยาลัย จุฬาลงกรณ์มหาวิทยาลัย.

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ภาคผนวก ก

สตีเฟนสเมตริกซ์เชิงเส้นและสตีเฟนสเมตริกซ์เรขาคณิต

จากสมการ (3.7) ในบทที่ 3

$$u = [M]\{c\} \quad (3.7)$$

เมื่อ $[M] = [M_1 \ M_2]$ (ก.1)

$$M_1 = 1 - \frac{x}{L} \quad (ก.2)$$

$$M_2 = \frac{x}{L} \quad (ก.3)$$

และ $M_{1,x} = -\frac{1}{L}$ (ก.4)

$$M_{2,x} = \frac{1}{L} \quad (ก.5)$$

แทนค่าสมการ (ก.3) และ (ก.4) ลงในสมการ (3.16) จะได้

$$[K_0^a] = \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \quad (ก.6)$$

จากบทที่ 3 สมการ (3.9)

$$v = [N]\{q\} \quad (3.9)$$

เมื่อ $[N] = [N_1 \ N_2 \ N_3 \ N_4]$

$$N_1 = 1 - 3 \frac{x^2}{L^2} + 2 \frac{x^3}{L^3} \quad (n.7)$$

$$N_2 = x - 2 \frac{x^2}{L} + \frac{x^3}{L^2} \quad (n.8)$$

$$N_3 = 3 \frac{x^2}{L^2} - 2 \frac{x^3}{L^3} \quad (n.9)$$

$$N_4 = -\frac{x^2}{L} + \frac{x^3}{L^2} \quad (n.10)$$

จากสมการ (3.10) $v, x = [N, x] \{q\}$ (3.10)

เมื่อ $[N, x] = [N_{1,x} \quad N_{2,x} \quad N_{3,x} \quad N_{4,x}]$

$$N_{1,x} = -6 \frac{x}{L^2} + 6 \frac{x^2}{L^3} \quad (n.11)$$

$$N_{2,x} = 1 - 4 \frac{x}{L} + 3 \frac{x^2}{L^2} \quad (n.12)$$

$$N_{3,x} = 6 \frac{x}{L^2} - 6 \frac{x^2}{L^3} \quad (n.13)$$

$$N_{4,x} = -2 \frac{x}{L} + 3 \frac{x^2}{L^2} \quad (n.14)$$

จากสมการ (3.11)

$$v, xx = [N, xx] \{q\} \quad (3.11)$$

เมื่อ $[N, xx] = [N_{1,xx} \quad N_{2,xx} \quad N_{3,xx} \quad N_{4,xx}]$

$$N_{1,xx} = -\frac{6}{L^2} + 12 \frac{x}{L^3} \quad (n.15)$$

$$N_{2,xx} = -\frac{4}{L} + 6 \frac{x}{L^2} \quad (n.16)$$

$$N_{3,xx} = \frac{6}{L^2} - 12 \frac{x}{L^3} \quad (ก. 17)$$

$$N_{4,xx} = -\frac{2}{L} + 6 \frac{x}{L^2} \quad (ก. 18)$$

จากสมการ (3.17)

$$[K_o^b] = \int_L EI [N_{,xx}]^T [N_{,xx}] dx \quad (3.17)$$

แทนค่าสมการ (ก.15) ถึง (ก.18) ลงใน (3.17) จะได้

$$[K_o^b] = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ & 4L^2 & -6L & 2L^2 \\ & & 12 & -6L \\ \text{สมมาตร} & & & 4L^2 \end{bmatrix} \quad (ก. 19)$$

และจากสมการ

$$[K_G^b] = \int_L P [N_{,x}]^T [N_{,x}] dx \quad (3.19)$$

แทนค่าสมการ (ก.11) ถึง (ก.14) ลงใน (3.19) จะได้

$$[K_G^b] = \frac{P}{30L} \begin{bmatrix} 36 & 3L & -36 & 3L \\ & 4L^2 & -3L & -L^2 \\ & & 36 & -3L \\ \text{สมมาตร} & & & 4L^2 \end{bmatrix} \quad (ก. 20)$$

ภาคผนวก ข.

รายละเอียด (Source Code) ของโปรแกรม CU-NTABS

BLARGE

C***\$NOFLD\$CALLS

C PROGRAM CU-NTABS(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE1,
C 1 TAPE2,TAPE3,TAPE11,TAPE12,TAPE13,TAPE15,TAPE16)

C PROGRAM CU-NTABS :

C THIS PROGRAM IS PART OF FULFILLMENT OF MASTER DEGREE THESIS,
C 'A PROGRAM FOR GEOMETRIC NONLINEAR ANALYSIS OF FRAME-SHEAR WALL
C BUILDINGS', GRADUATE SCHOOL, CHULALONGKORN UNIVERSITY 1995.

C THESIS ADVISOR : PROF. DR. PANITAN LUKKUNAPRABIT
C DEVELOPED BY : MR. VICHORN PANICHACARN

C MAY 1995

C PROGRAM SUPER-ETABS AN ENHANCED VERSION OF THE ETABS PROGRAM

C DEVELOPED BY ... B. F. MAISON AND C. F. NEUSS
C J. G. BOUMKAMP, INC.
C BERKELEY, CALIFORNIA

C JANUARY 1983

C PROGRAM ETABS ... A GENERAL PROGRAM FOR THE STATIC AND DYNAMIC
C ANALYSIS OF FRAME AND SHEAR WALL THREE-
C DIMENSIONAL BUILDINGS AND SYSTEMS

C DEVELOPED BY ... E. L. WILSON, H. H. DOVEY AND J. P. HOLLINGS
C DEPARTMENT OF CIVIL ENGINEERING
C UNIVERSITY OF CALIFORNIA, BERKELEY

C SEPTEMBER 1974, REVISED MARCH 1979

C MICRO

C CONVERSION BY ... B. F. MAISON AND G. A. RODRIGUEZ

C FEBRUARY 1985

C CORRECTIONS TO ETAB1.FOR (MICRO VERSION) ... JANUARY 1987 ... BFM
C MODIFIED TO GENERATE DYNAMIC PROPERTIES FOR SLAM ... JUNE 1988
C MODIFIED TO CREATE RESTART TAPE FOR SLAM-2 ... APRIL 1990

.....
C NO RESPONSIBILITY IS ASSUMED BY THE AUTHORS OR BY CHULALONGKORN
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C (INCLUDING WARRANTIES OF FITNESS AND MERCHANTABILITY) SHALL APPLY.

C IF THIS PROGRAM HAS GIVEN YOU NEW ANALYSIS CAPABILITY RESULTING
C IN INDIRECT PROFITS, YOU MAY WISH TO SUPPORT FURTHER WORK IN THIS
C AREA BY GIVING AN UNRESTRICTED GRANT TO THE AUTHORS UNIVERSITY.

C IMPLICIT REAL*8 (A-H)

C IMPLICIT REAL*8 (O-Z)

COMMON/GEN/ NST,NCF,NTF,NLD,NAT,NFQ,NSD,BHED(9),FHED(7),NBS
C 1 ,RLAB(3),IB,IS,T(6)

COMMON/JUNK/IFIL(3),MM,MN,JFIL(65)

COMMON/BUNK/AFIL(260)

COMMON/STIF/ STF(336)

COMMON /DYN/ NTIME,DT,NPC,DAMP

COMMON /CNTR/ A(26000)

DIMENSION KODE(3)

CHARACTER*14 FLINP,FLQUT

CHARACTER*4 RLAB,BHED,FHED

C RLAB(1)=' X '

C RLAB(2)=' Y '

```

      RLAB(3)='RDTN'
C
      MTOT=20000
C
C      WRITE(*,4999)
C      WRITE(*,5000)
C      WRITE(*,5001)
C      WRITE(*,5002)
C      WRITE(*,5003)
C      WRITE(*,5004)
C      WRITE(*,5005)
      WRITE(*,*)'-----'
      WRITE(*,*)'  PROGRAM CU-NTABS'
      WRITE(*,*)'-----'
      WRITE(*,333)
333  FORMAT( ' * ENTER INPUT FILE * ')
      READ(*,334) FLINP
334  FORMAT(A)
      WRITE(*,335)
335  FORMAT( ' * ENTER OUTPUT FILE * ')
      READ(*,336) FLOUT
336  FORMAT(A)
C
      OPEN(1, FILE='TAPE1', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(2, FILE='TAPE2', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(3, FILE='TAPE3', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(5, FILE=FLINP)
      OPEN(6, FILE=FLOUT, STATUS='NEW')
      OPEN(11, FILE='TAPE11', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(12, FILE='TAPE12', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(13, FILE='TAPE13', STATUS='NEW', ACCESS='SEQUENTIAL',
        *FORM='UNFORMATTED')
      OPEN(15, FILE='TAPE15', STATUS='NEW', ACCESS='DIRECT',
        *FORM='UNFORMATTED', RECL=20)
      OPEN(16, FILE='TAPE16', STATUS='NEW')
C
C
C      WRITE(6,2999)
C      WRITE(6,3000)
C      WRITE(6,3001)
C      WRITE(6,3002)
C      WRITE(6,3003)
C      WRITE(6,3004)
C      WRITE(6,3005)
      WRITE(6,*) 'PROGRAM CU-NTABS'
      WRITE(6,6001) FLINP
      WRITE(6,6002) FLOUT
8001 FORMAT (T2,14HINPUT FILE : ,T17,A14)
8002 FORMAT (T2,14HOUTPUT FILE : ,T17,A14)
      ILP = 1
      TDIS = 0.0
      TTIME = 0.0
C
C      READ AND PRINT OF GENERAL INFORMATION
C
100 READ(5,1000) NST,NDF,NTF,NLD,NAT,NFQ,NSD,KODE,ICHEK,ITYPE,
  1  IMAXL,TANORM,( BHED(I),I=1,4 )
      GRAY = 0.0
      IF( ICHEK.NE.0 ) MTOT = 300000
      IF(ILP .EQ. 1) THEN
        NPT = 6
      ELSE
        NPT = 16
      ENDIF
      IF(NST.GT.0) GO TO 40
C ... ADDED BY BFM .. JANUARY 1987

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N6=N5+N5*NB*3
N7=N6+NB*NB*3
N8=N7+NB*NC*2
N9=NB+3*NPAN
C
C COMPUTE STIFFNESS FOR REDUCED STORAGE
C
CALL STIFF(MA,B,R,NV,NB)
C
N10=N9+MA
N11=N10
N12=N11+NFEB
N13=N12+5*NPAN
N14=N13+3*NTRU
N15 = N14 + 3*NTRU
N16=N15+2*NC
IF(N16.GT.MTOT) CALL MEMORY (N16-MTOT)
IF( ICHEK.NE.0 ) WRITE(NPT,4000) N16
CALL FORM(A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(N8),A(N9),
1 A(N10), NBT,NB,NC,NCP,NBP,NB,NFEB,NPAN,A(N11),A(N12),NV,1
2 ,A(N13),A(N14),NTRU,A(N15),KODE(3),ICHEK,NPT )
CALL SECOND (TTT)
TTT=TTT-TT
WRITE (NPT,2003) 1,TTT
200 CONTINUE
CALL SECOND (T(2))
C
C SOLVE STATIC LOAD CASES
C
N3=N2+NBS*NBS
N4=N3+5*NBS
N5=N4+NFS*NFS
N6=N5+3*NFS
N7=N6+NST*NTF*2
N8=N7+5*NTF
N9=N8+4*NTF
N10=N9
IF( DABS(GRAV).GT.1.0D-10 )N10=N9+NBS*2
IF(N10.GT.MTOT)CALL MEMORY(M10-MTOT)
IF( ICHEK.NE.0 ) WRITE(NPT,4001) N10
CALL LAT (A(1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),NBS,NFS,
1 NTF,A(N8),NBT,GRAV,ICHEK,A(N10),NPT,ITYPE)
CALL SECOND (T(3))
C
C MODE SHAPES AND FREQUENCIES AND SPECTRUM RESPONSE
210 CALL SECOND( T(3) )
M1 = N1 + 8*NBT
IF(NAT.LT.0)M1=N1+14*NBT
M2 = M1 + NFO*NFO
N2 = M2 + NFO*NFO
IF( (NAT.NE.3) .AND. (NAT.NE.6) .AND. (NAT.NE.-6) .AND.
1 (NAT.NE.7) ) N2 = M1
N3=N2+NBS*NBS
N4=N3+NBS
N5=N4+NBS
N6=N5+NBS
N7=N6+NBS*NBS
N8 = N7 + NBS*NFO
IF( DABS(GRAV).LT.1.0D-10 ) N8 = N7
N9 = N2 + ( NFO + 5 ) * NBS
N10 = N8 + 4*NBS
N8 = MAX0( N8,N9,N10 )
IF( N8.GT.MTOT ) CALL MEMORY( N8 - MTOT )
IF( ICHEK.EQ.0 ) GO TO 212
WRITE(NPT,4002) N8
NAT = IABS( NAT )
GO TO 214
212 N8D = 0
IF( NAT.GT.0 ) CALL BLAM( A(1),A(N1),A(N2),A(N3),A(N4),A(N5),
1 A(N6),NBS,NBT )
CALL EARTH(A(1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N8),A(N7),

```

```

CLOBE (1,STATUS='DELETE')
CLOBE (2,STATUS='DELETE')
CLOBE (3,STATUS='DELETE')
CLOBE (11,STATUS='DELETE')
CLOBE (12,STATUS='DELETE')
CLOBE (13,STATUS='DELETE')
CLOBE (15,STATUS='DELETE')
CLOBE (16,STATUS='DELETE')
STOP

C
40 CALL BECOND (T(1))
   I3=3
   I8=0
   IF(NSD.EQ.0) GO TO 50
   I3=1
   I8=NSD-1
50 N89=N8T*13
   NFB=N8T*3
   IF(NFQ.GT.N88) NFQ=N88
   IF(NAT.EQ.0) NFQ=0
C   WRITE(6,*) '))))))))))))))))))))))))))))))))))))))'
C   WRITE(6,*) 'LOOP No. ',I3P
C   WRITE(6,*) '))))))))))))))))))))))))))))))))))))))'
   WRITE(NPT,2000) (BHED(I),I=1,8),N8T,NDF,NTF,NLD,NAT
   WRITE(NPT,1998)
   WRITE (NPT,1999) NFQ,NSD,KODE,ICHEK,I TYPE,IMAXL,TANORM
   REWIND 2
   REWIND 3

C
C   READ AND PRINT OF STORY INFORMATION
C
   N1 = 1+N8T
C ... CORRECTED BY BFM ... JANUARY 1987
C   N2 = 1 + 14*N8T
   N2 = N1+14*N8T
   N3 = N2+2*N8T
   N4 = N3+2*N8T
   N5 = N4+N8T
   I = 3*N8T
   CALL INPUT (A(1),A(N1),A(N2),A(N3),A(N4),A(N5),N8T,I,RLAB,KODE,
I *      NPT)
   CALL BECOND( T(2) )
   IF( NAT.LT.0 ) GO TO 210

C
C   READ AND PRINT OF FRAME PROPERTIES AND FORM LATERAL STIFFNESSES
C
   DO 200 I=1,NDF
   CALL BECOND (TT)
   READ (5,1001) M,NS,NC,NB ,NCP,NBP,NFEF,NPAN,NTRU,FHED
   WRITE (NPT,2001) FHED,M,NS,NC,NB,NCP,NBP,NFEF,NPAN,NTRU

C
   IF (I3P.NE.1) GOTO 113
   VWP = 0.0
   DO 111 NV = 1,NB
     DO 111 MV = 1,NC
       NREC = NC*(NV-1)+MV
111   WRITE (15,REC = NREC) VWP
     DO 112 LV = 1,NPAN
       NREC = NB*NC+LV
112   WRITE (15,REC = NREC) VWP

C
113 NA=0
   MM=3*NC
   NCP=NCP+1
   NBP=NBP+1
   NN=8*NC+3*NB+3
   N1=1+N8T
   N2=N1+14*N8T
   N3 = N2 + 14*NCP
   N4 = N3 + 11*NBP
   N5=N4+7*NFEF

```

```

      1      NBS,NST,NMD,A(N6),A(N1),A(N2),NFO,GRAV )
C---- OPT 8 CALCS DONE NOW SAME AS NAT = 3
      214 IF( NAT.EQ.7 ) NAT = 3
           IF( ICHEK.EQ.1 ) NTIME=0
           IF( ICHEK.EQ.1 ) NPC=0
C
C      COMPUTE DYNAMIC RESPONSE
C
      IF( (NAT.NE.4) .AND. (NAT.NE.8) .AND. (NAT.NE.9) ) GO TO 250
      MLD = 5 + NTIME
      N3 = N2 + MLD*NBS
      N4 = N3 + NTIME*NBS
      IF( NAT.EQ.4 ) N4 = N3
      N5 = N4 + 2*IABS( NPC )
      N6 = N5 + NTIME
      N7 = N6 + NBS
      L1 = N7 + NBS
      L2 = N4 + 4*NBS
      L3 = N4 + NBS*NBS
      IF( DABS(GRAV).LT.1.0D-10 ) L3 = 1
      N8 = MAX0( L1,L2,L3 )
      IF( NAT.EQ.4 ) N8 = N7
      IF( N8.GT.MTOT ) CALL MEMORY( N8 - MTOT )
      IF( ICHEK.EQ.0 ) GO TO 220
      N9=NBS+1
      IF(NAT.EQ.8.OR.NAT.EQ.9)N9=N9+NBS
      WRITE(NPT,4003)N9,N9
      GO TO 250
220 CALL DYNA(A(1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(N4),
      1 A(N4),NBS,NST,GRAV )
250 CALL SECOND (T(4))
      IF( (NAT.EQ.6) .OR. (NAT.EQ.8) ) GO TO 300
C---- OPT 8 CALCS DONE NOW SAME AS NAT = 4
      IF( NAT.EQ.9 ) NAT = 4
C
C      COMPUTE FRAME DISPLACEMENTS
C
      IF(NAT.LE.2) NFO=0
      IF( NAT.EQ.1 ) GO TO 300
      MLD=5+NFO
      IF(NAT.EQ.4)MLD=5+NTIME
      N3=N2+MLD*NBS
      N4=N3+NST*NTF*2
      N5=N4+NFB*MLD
      N6=N5+5*NTF
      N7=N6-NTF*4
      IF(N7.GT.MTOT) CALL MEMORY(N7-MTOT)
      IF( ICHEK.EQ.0 ) GO TO 290
      IF( NAT.NE.4 ) WRITE(NPT,4004) N7
      N8 = NBS + NTF
      IF( NAT.EQ.4 ) WRITE(NPT,4005) N7,N8
      GO TO 300
290 CONTINUE
      CALL DISP (A(N1),A(N2),A(N3),A(N4),A(N5),NBS,NTF,MLD,NST,NFB,A(N6)
      1)
300 CALL SECOND (T(5))
C
C      CALCULATE AND PRINT DISPLACEMENTS AND STRESSES
C
      IF( NAT.EQ.1 ) GO TO 400
      IF( (NAT.EQ.6) .OR. (NAT.EQ.8) ) GO TO 400
      CALL FRAME( MTOT,NMD,NFS,KODE(3),ICHEK,NPT,TANORM,TNORM,TD18
      1 ,ILP,ITYPE )
400 CALL SECOND (T(6))
      TT=T(6)-T(1)
      DO 500 I=1,5
500 T(I)=T(I+1)-T(1)
      T(6)=TT
C      WRITE (6,2002) T
      TTAME = T(6)
      TTIME = TTIME+TTAME

```

```

IF ( ITYPE .EQ. 0 ) GOTO 98
IF ( ILP .EQ. IMAXL ) GOTO 101
IF ( THORM .LE. TANORM ) GOTO 102
ILP = ILP + 1
REWIND 5
GOTO 98
101 WRITE (6,1002) ILP
GOTO 98
102 WRITE (6,1003) ILP
98 WRITE (6,1004) TTIME
99 GO TO 100
C .
1000 FORMAT( 7I5,1X,5I11,14,F10.0,4A4 )
1002 FORMAT( 2(/),T5,'DIVERGE UNTIL ITERATION NO. ',14 )
1003 FORMAT( 2(/),T5,'CONVERGE IN ITERATION NO. ',14 )
1004 FORMAT( 1(/),T5,'TOTAL TIME',F7.2,' SEC.' )
1001 FORMAT(9I5,7A4)
2000 FORMAT( /,6A4,/
126H TOTAL NUMBER OF STORIES---,14/
126H NUMBER OF DIFF. FRAMES---,14/
126H TOTAL NUMBER OF FRAMES---,14/
126H NUMBER OF LOAD CONDITIONS,14/
126H TYPE OF ANALYSIS-----,14/
1/40H EQ.0-STATIC LOADS ONLY ,/
1 40H EQ.1-MODE SHAPES AND FREQUENCIES ONLY, /
1 40H EQ.2-STATIC AND MODE SHAPE ANALYSES ,/
1 41H EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL ,/
1 80H EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPON
18E ENVELOPES ONLY) /
1 44H EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE ,/
2 56H EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE) ,/
2 29H EQ.7-TYPE 3 AND 8 ANALYSES ,/
1 87H EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES O
1R STEP-BY-STEP RESPONSE) ,/
2 29H EQ.9-TYPE 4 AND 8 ANALYSES ,/21H EQ.10-SLAM RESTART )
1998 FORMAT( 23H EQ.11-SLAM-2 RESTART,/
2 76H EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS
2AND MODES USED ,/ )
1999 FORMAT (26H NUMBER OF FREQUENCIES----,14,/
1 26H STORY TRANSLATION CODE---,14,/
2 26H LAT FORCE GENERATION CODE ,212,/
2 26H STRESS CHECK KEY-----,14,/,
2 26H DATA CHECK KEY-----,14,/,
2 26H TYPE OF SOLUTION-----,14,/,
2 26H MAXIMUM NO. OF CYCLES---,14,/,
2 40H CONVERGENCE TOLERANCE OF EQUILIBRIUM ,F10.6)
2001 FORMAT (/,1H ,7A4,/
127H FRAME ID NUMBER-----,14,/
127H NUMBER OF STORY LEVELS---,14,/
127H NUMBER OF COLUMN LINES---,14,/
127H NUMBER OF BAYS-----,14,/
127H NUMBER OF DIFF. COL. PROP.,14,/
127H NUMBER OF DIFF. BEAM PROP.,14,/
127H NUMBER OF DIFF. FEF-----,14,/
127H NUMBER OF PANEL ELEMENTS-- ,14,/
127H NUMBER OF BRACING ELEMENTS ,14/)
2002 FORMAT (///19H TIME LOG (MINUTES) ,//
1 41H FORM FRAME STIFFNESSES..... = ,F7.2/
2 41H SOLVE STATIC LOAD CASES..... = ,F7.2/
3 41H MODE SHAPES AND FREQUENCIES..... = ,F7.2/
4 41H COMPUTE FRAME DISPLACEMENTS..... = ,F7.2/
5 41H COMPUTE AND PRINT STRESSES AND DISPLS. = ,F7.2//
6 41H TOTAL TIME..... = ,F7.2)
2003 FORMAT (/,14H0...FRAME TYPE 13,4H ,/
1 4X,33H TIME REQUIRED TO FORM STIFFNESS = ,F6.2)
2999 FORMAT( 1H ,18( / ) )
3000 FORMAT( 31X,5(1HB),2X,1HB,3X,1HB,2X,4(1HB),3X,5(1HB),2X,4(1HB),
1 9X,5(1HB),2X,5(1HB),2X,4(1HB),3X,4(1HB),3X,5(1HB) )
3001 FORMAT( 30X,1HB,6X,1HB,3X,1HB,2X,1HB,3X,1HB,2X,1HB,6X,1HB,3X,
1 1HB,8X,1HB,8X,1HB,4X,1HB,3X,1HB,2X,1HB,3X,1HB,2X,1HB )
3002 FORMAT( 28X,5(1HB),2X,1HB,3X,1HB,2X,5(1HB),2X,3(1HB),4X,5(1HB),

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1 3X,2(1HB),3X,3(1HB),6X,1HB,4X,5(1HB),2X,5(1HB),2X,5(1HB) )
3003 FORMAT( 32X,1HB,2X,1HB,3X,1HB,2X,1HB,6X,1HB,6X,1HB,3X,1HB,6X,
1 1HB,6X,1HB,4X,1HB,3X,1HB,2X,1HB,3X,1HB,6X,1HB )
3004 FORMAT( 27X,5(1HB),2X,5(1HB),2X,1HB,6X,5(1HB),2X,1HB,4X,1HB,7X,
1 5(1HB),4X,1HB,4X,1HB,3X,1HB,2X,5(1HB),2X,5(1HB) )
3005 FORMAT( //,59X, 13H$UPER - ETABS //,
* 46X, 40HAN ENHANCED VERSION OF THE ETABS PROGRAM, //,
1 60X, 12HDEVELOPED BY, //, 52X, 28HB F. MAISON AND C. F. NEUSS, //,
2 51X, 31HJO BOUMKAMP, INC., BERKELEY, CA, //, 60X, 13HJANUARY 1983 ,
3 //, 47X, 37HPROGRAM ETABS ORIGINALLY DEVELOPED BY, //, 44X,
4 44HE L. WILSON, H. H. DOVEY AND J. P. HOLLINGS, //,
5 47X, 38HUNIVERSITY OF CALIFORNIA, BERKELEY, CA, //, 49X,
6 34HSEPTEMBER 1974, REVISED MARCH 1979 ,
7 3( //, 58X, 19HMICRO CONVERSION BY ,
8 / , 49X, 32HB F. MAISON AND G. A. RODRIGUEZ,
9 / , 58X, 13HFEBRUARY 1985 ,
A / , 54X, 22HCORRECTED JANUARY 1987 )
4000 FORMAT( / , 10X, 52H * ROUTINE FORM ( FRAME STIFFNESS ) REQUIRES MTOT
1 = , 18, / )
4001 FORMAT( / , 10X, 65H * ROUTINE LAT ( SOLUTION OF STATIC LOAD CASES )
1 REQUIRES MTOT = , 18, / )
4002 FORMAT( / , 10X, 66H * ROUTINE EARTH ( FREQ, MODE SHAPES, RESP SPEC )
1 REQUIRES MTOT = , 18, / )
4003 FORMAT( / 45H * ROUTINE DYN ( TIME HIST ) REQUIRES MTOT = , 18,
1 3H + , 18, 31H X (NO.TIME STEPS TO BE USED) ,
1 39H + 2 X (NO_OR, ACCELERATION VALUES) )
4004 FORMAT( / , 10X, 47H * ROUTINE DISP ( FRAME DISP ) REQUIRES MTOT =
1 , 18, / )
4005 FORMAT( / , 47H * ROUTINE DISP ( FRAME DISP ) REQUIRES MTOT = , 18,
1 3H + , 18, 31H X (NO.TIME STEPS TO BE USED) )
4999 FORMAT( 2( //, 34X, 11H WELCOME TO , 2( / ) )
5000 FORMAT( 5X, 5(1HB), 2X, 1HB, 3X, 1HB, 2X, 4(1HB), 3X, 5(1HB), 2X, 4(1HB) ,
1 9X, 5(1HB), 2X, 5(1HB), 2X, 4(1HB), 3X, 4(1HB), 3X, 5(1HB) )
5001 FORMAT( 4X, 1HB, 6X, 1HB, 3X, 1HB, 2X, 1HB, 3X, 1HB, 2X, 1HB, 6X, 1HB, 6X, 1HB, 3X,
1 1HB, 6X, 1HB, 6X, 1HB, 4X, 1HB, 3X, 1HB, 2X, 1HB, 3X, 1HB, 2X, 1HB )
5002 FORMAT( 3X, 5(1HB), 2X, 1HB, 3X, 1HB, 2X, 5(1HB), 2X, 3(1HB), 4X, 5(1HB) ,
1 3X, 2(1HB), 3X, 3(1HB), 6X, 1HB, 4X, 5(1HB), 2X, 5(1HB), 2X, 5(1HB) )
5003 FORMAT( 6X, 1HB, 2X, 1HB, 3X, 1HB, 2X, 1HB, 6X, 1HB, 6X, 1HB, 3X, 1HB, 6X,
1 1HB, 6X, 1HB, 4X, 1HB, 3X, 1HB, 2X, 1HB, 3X, 1HB, 6X, 1HB )
5004 FORMAT( 1X, 5(1HB), 2X, 5(1HB), 2X, 1HB, 6X, 5(1HB), 2X, 1HB, 4X, 1HB, 7X,
1 5(1HB), 4X, 1HB, 4X, 1HB, 3X, 1HB, 2X, 5(1HB), 2X, 5(1HB) )
5005 FORMAT( //, 30X, 21H MICRO CONVERSION BY ,
1 / , 22X, 37H B. F. MAISON AND G. A. RODRIGUEZ ,
2 / , 25X, 24H FEBRUARY 1985 , 3( // )
END
SUBROUTINE INPUT(SN,SD,PA,PB,HH,F,NST,NN,RLAB,KODE,NPT)
C
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION SD(NST,14),PA(NST,2),PB(NST,2),SN(NST)
DIMENSION D(7),AB(2),HH(NST),F(NN,2),KODE(3)
C
CHARACTER*4 SN
Integer*4 sn, rlab
CHARACTER*1 AB
DATA AB / 'A', 'B' /
C
C READ AND PRINT STORY DATA
C
WRITE (NPT,3000)
DO 200 N=1,NST
LN=NST+1-N
READ (5,1000) SN(N), (SD(N,I), I=2,10), PA(N,1), PA(N,2), SD(N,12),
1 SD(N,13), PB(N,1), PB(N,2)
200 WRITE (NPT,2000) LN,SN(N), (SD(N,I), I=2,8)
C
C PRINT CUMULATIVE STORY QUANTITIES
C
HT=0.
DO 201 N=1,NST
201 HT=HT+SD(N,2)
WRITE(NPT,3002)

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```

R1=HT
R2=0.
R3=0.
DO 202 N=1,NST
LN=NST+1-N
IF(N.NE.1)R1=R1-BD(N-1,2)
R2=R2+BD(N,3)
R3=R3+BD(N,4)
202 WRITE(NPT,2000)LN,BN(N),R1,R2,R3
C
C---- LOOP OVER LAT LOAD CASES A AND B
C
DO 50 K=1,2
IF( KODE(K).LE.0 ) GO TO 50
C---- CODE FORCE GENERATION
READ(5,4000) ITYP,D
IF( ITYP.EQ.1 ) WRITE(NPT,4001) AB(K), ( D(I),I=1,7 )
IF( ITYP.EQ.2 ) WRITE(NPT,4002) AB(K),( D(I),I=1,3 )
X = 0.0
TM = 0.0
DO 15 I=1,NST
J = NST + 1 - I
X = X + BD(J,2)
TM = TM + BD(J,3)
15 HH(J) = X
C
P = 1.0
IF( ITYP.EQ.1 ) GO TO 18
C---- ATC
P = 1.0
IF( D(1).GE.2.5 ) P = 2.0
IF( (D(1).GT.0.5) .AND. (D(1).LT.2.5) ) P = 1.0 + (D(1)-0.5)/2.0
18 SUM = 0.0
DO 20 I=1,NST
X = BD(I,3)*( HH(I)**P )
SUM = SUM + X
20 HH(I) = X
C
DO 25 I=1,NST
25 HH(I) = HH(I)/SUM
IF( ITYP.EQ.2 ) GO TO 30
C---- UBC
V = D(2)*D(3)*D(4)*D(5)*D(6)*D(7)*TM
FT = 0.07*D(1)*V
IF( FT.GT.( 0.25*V ) ) FT = 0.25*V
IF( D(1).LE.0.70 ) FT = 0.0
WRITE(NPT,4006) FT
WRITE(NPT,4007) V
V = V - FT
GO TO 32
C---- ATC
30 V = D(2)*D(3)*TM
WRITE(NPT,4008) P
WRITE(NPT,4007) V
32 DO 35 I=1,NST
35 HH(I) = HH(I)*V
IF( ITYP.EQ.1 ) HH(I) = HH(I) + FT
DO 48 I=1,NST
N = 0
IF( K.EQ.2 ) N = 3
GO TO ( 42,44,46 ), KODE(K)
42 SD(I,9+N) = HH(I)
SD(I,10+N) = 0.0
GO TO 48
44 SD(I,9+N) = 0.0
SD(I,10+N) = HH(I)
GO TO 48
46 SD(I,9+N) = HH(I)
SD(I,10+N) = HH(I)
48 CONTINUE
50 CONTINUE

```



```

C
WRITE (NPT,3001)
DO 300 N=1,NBT
LN=NBT+1-N
SD(N,11) = -SD(N,9)*(PA(N,2)-SD(N,8))+SD(N,10)*(PA(N,1)-SD(N,5))
SD(N,14) = -SD(N,12)*(PB(N,2)-SD(N,8))+SD(N,13)*(PB(N,1)-SD(N,5))
300 WRITE (NPT,2001) LN,(SD(N,1),1=9,14),PA(N,1),PA(N,2),PB(N,1),
1 PB(N,2)
C---- PUT LOADS IN F FOR CALC
DO 80 M=1,NBT
I = 3*( M - 1 ) + 1
DO 55 J=1,3
K = J - 1
F(I+K,1) = SD(M,9+K)
55 F(I+K,2) = SD(M,12+K)
80 CONTINUE
C---- RETURN IF NO STAT LAT LOADS
DO 82 I=1,2
DO 82 J=1,NN
IF( DABS(F(J,I)) .GT. 1.0D-10 ) GO TO 84
82 CONTINUE
RETURN
C
C---- CALC STORY SHEARS
C
84 N = 3*NBT - 3
IF(NBT.EQ.1)GO TO 86
DO 65 I=1,2
DO 65 J=1,N
65 F(J+3,1) = F(J+3,1) + F(J,1)
86 WRITE(NPT,4003)
WRITE(NPT,4009)
WRITE(NPT,4005)
IF (NPT.EQ.16) GOTO 150
CALL PROUT( F,NN,2,BN,NBT,RLAB,3,0 )
150 CONTINUE
C
C---- CALC OTM
C
DO 80 I=1,2
F(3,1) = 0.0
DO 80 K=1,2
80 F(K,1) = F(K,1)*SD(1,2)
IX = 4
IY = 5
IT = 6
IF(NBT.EQ.1)GO TO 90
DO 85 J=2,NBT
X = SD(J,2)
F(IX,1) = F(IX,1)*X + F(IX-3,1)
F(IY,1) = F(IY,1)*X + F(IY-3,1)
F(IT,1) = 0.0
IX = IX + 3
IY = IY + 3
85 IT = IT + 3
90 CONTINUE
WRITE(NPT,4004)
WRITE(NPT,4009)
WRITE(NPT,4005)
IF (NPT.EQ.16) GOTO 180
CALL PROUT( F,NN,2,BN,NBT,RLAB,3,0 )
180 CONTINUE
4000 FORMAT( 15,5X,7F10.0 )
4001 FORMAT( //,21X,50(1H-),/,
* 20X,50H UBC STATIC LATERAL LOADS GENERATED FOR LOAD CASE
*E ,A1,/,21X,50(1H-),
1 //,26X,16H PERIOD VALUE =,F10.3,/,
2 26X,16H GRAVITY VALUE =,F10.3,/,
3 26X,16H Z =,F10.3,/,
4 26X,16H I =,F10.3,/,
5 26X,16H K =,F10.3,/,

```

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6      26X,16H      C      =,F10.5,/
7      26X,16H      B      =,F10.3,/
4002 FORMAT( //,21X,50(1H-),/
*      20X,60H ATC STATIC LATERAL LOADS GENERATED FOR LOAD CASE
*E     ,A1,/ ,21X,50(1H-),
1      //,26X,16H PERIOD VALUE =,F10.3,/
2      26X,16H GRAVITY VALUE =,F10.3,/
3      26X,16H      C      =,F10.5,/
4003 FORMAT( ///,1H ,12(1H-),/,13H STORY SHEARS ,/,1H ,12(1H-),/ )
4004 FORMAT( ///,1H ,25(1H-),/,26H STORY OVERTURNING MOMENTS ,/,1H ,
1 25(1H-),/ )
4005 FORMAT( 20X,65H OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATER
1AL LOAD CASE A ,/,20X,65H OUTPUT COLUMN 2 CONTAINS RESULTS FROM ST
2ATIC LATERAL LOAD CASE B ,/ )
4006 FORMAT( 26X,16H TOP FORCE      =,F10.3 )
4007 FORMAT( 26X,16H BASE SHEAR   =,F10.3,// )
4008 FORMAT( 26X,16H POWER K      =,F10.3 )
4009 FORMAT(69H NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-D
ZELTA EFFECTS. / )
RETURN
C
1000 FORMAT (1X,A4,5X,7F10.0/9F10.0)
2000 FORMAT (18,4X,A4,7F13.2)
2001 FORMAT (18,6F13.2,3X,4F8.1)
3000 FORMAT (////11H STORY DATA ,//,10H LEVEL NO. ,3X,2H1D 6X,6HHEIGHT ,
1 6X,7HMASS(M),6X,5HMR**2,6X,4HX(M),6X,4HY(M),10X,3HK-X,10X,3HK-Y)
3001 FORMAT (///40H STRUCTURE LATERAL LOADS . . CASES A AND B ,//
1 10H LEVEL NO. ,7X,4HFX-A,6X,4HFX-B,6X,5HMDM-A,6X,4HFX-B,6X,4HFX-B
2 6X,5HMDM-B,6X,2HXA,6X,2HYA,6X,2HXB,6X,2HYB )
3002 FORMAT(//22H CUMULATIVE STORY DATA ,//,10H LEVEL NO. ,3X,2H1D,6X,
1 6HHEIGHT,6X,7HMASS(M),6X,5HMR**2)
END
SUBROUTINE ECHO (LBC,NS,NR,NL,L,NPROP,NPT)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (C-Z)
COMMON /JUNK/ NLD,LOC(60),IFIL(6)
DIMENSION LBC(NS,NR,NL)
C
C PRINT MEMBER LOCATIONS AS GENERATED
C
DO 200 J=1,NR,30
JJ=J+29
IF (JJ.GT.NR) JJ=NR
WRITE (NPT,2000) (I,I=J,JJ)
WRITE (NPT,2002)
DO 200 I=1,NS
DO 100 K=J,JJ
LOC(K)=LBC(I,K,L)
IF (LOC(K).EQ.NPROP) LOC(K)=0
100 CONTINUE
M=NS+1-I
200 WRITE (NPT,2001) M,(LOC(K),K=J,JJ)
C
RETURN
2000 FORMAT (/,6HDSTORY,30I4)
2001 FORMAT (14,2X,30I4)
2002 FORMAT (1H )
END
SUBROUTINE SLAM( SN,A,F,W,XM,IQ,B,MBS,MBT )
-----
C ROUTINE TO CREATE A RESTART TAPE FOR PROGRAMS SLAM OR SLAM-2
-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (C-Z)
DIMENSION F(MBS,MBS),S(MBS,MBS),XM(MBS),W(MBS),IQ(1),A(MBT,4),
1 SN(MBT)
COMMON/GEN/ NBT,NDF,NTF,NLD,NAT,NFQ,NSD,BHED(6),FHED(7),NSB
1 ,RLAB(3),IB,IS,T(6)
CHARACTER*4 SN,RLAB,BHED,FHED
C
C COMPUTE MODE SHAPES AND FREQUENCIES

```

```

C
  NFO = NBS
  DM1 = 1.0
  TPI = 6.0*DATAN(DM1)
  DO 100 I=1,NBT
    I1=13*(I-1)+1
    XM(I1)=A(I,3)
    XM(I1+1)=A(I,3)
  100 XM(I1+2)=A(I,4)
  REWIND 1
  READ(1) B
  REWIND 1
  WRITE(1) NST,NBS,IB,I3,RLAB
  WRITE(1) BN,XM,( A(I,2),I=1,NBT ),B
C
  REWIND 2
  READ(2) B
  IF( NAT.EQ.10 ) GO TO 120
  WRITE(1) B
  WRITE(6,5002)
  GO TO 920
C
  120 DO 150 I=1,NBS
    IF(XM(I).GT.0.) GO TO 150
    WRITE (6,3002)
    STOP
  150 XM(I)=1.0/DSORT(XM(I))
C
  DO 800 IK=1,2
    WRITE(6,5000) IK
C
  DO 200 I=1,NBS
    DO 200 J=1,NBS
  200 S(I,J)=B(I,J)*XM(I)*XM(J)
C
  CALL EIGEN(6,NBS,0,F,NR,W,IQ)
C
  DO 250 I=1,NBS
    W(I)=B(I,1)
    DO 250 J=1,NBS
  250 F(I,J)=F(I,J)*XM(I)
  DO 300 I=1,NFO
    WM=W(I)
    DO 270 J=1,NBS
      IF(W(J).GT.WM) GO TO 270
      WM=W(J)
    K=J
  270 CONTINUE
C
  W(K)=W(I)
  W(I)=TPI/DSORT(WM)
  DO 300 J=1,NBS
    WM=F(J,K)
    F(J,K)=F(J,I)
  300 F(J,I)=WM
  WRITE(6,4000)
  DO 522 I=1,NFO
    X = 1.0/W(I)
    Y = TPI/W(I)
  522 WRITE(6,4001) I,W(I),X,Y
  DO 600 I=1,NFO,B
    IH=I+7
    IF(IH.GT.NFO) IH=NFO
    WRITE (6,2003) (J,J=1,IH)
    DO 600 N=1,NBT
      LN=NBT+1-N
      NN=13*(N-1)
      WRITE (6,2002)
      DO 600 J=1,I3
  600 WRITE (6,2004) LN,BN(N),RLAB(J+IB),( F(NN+J,K),K=1,IH)
    WRITE(1) W,F

```

```

C
  IF( IK.GT.1 ) GO TO 800
  REWIND 2
  READ(2) 8
C---- CALC STATE 2 STIFFNESS
  READ(5,1006) IL,IXY,BPR,EC
  IF( I3.EQ.3 ) GO TO 610
  EC = 0.0
  IXY = IB
610 WRITE(6,3003) IL,IXY,BPR,EC
  IF( I3.EQ.3 ) GO TO 620
C---- PLANAR ANAL
  IDOF = MST - IL + 1
  JDOF = IDOF
  EC = 0.0
  S(IDOF, IDOF) = S(IDOF, IDOF) + BPR
  GO TO 640
C---- 3D ANAL
620 IDOF = 3*( MST - IL ) - IXY + 1
  JDOF = IDOF - IXY + 2
  S(IDOF, IDOF) = S(IDOF, IDOF) + BPR
  S(JDOF, JDOF) = S(JDOF, JDOF) + BPR*EC*EC
  S(IDOF, JDOF) = S(IDOF, JDOF) - BPR*EC
  S(JDOF, IDOF) = S(IDOF, JDOF)
640 WRITE(1) IL,IXY,BPR,EC, IDOF, JDOF
C
800 CONTINUE
C
  WRITE(8,5001)
820 CLOSE( 2,STATUS='DELETE' )
  CLOSE( 3,STATUS='DELETE' )
  CLOSE(11,STATUS='DELETE' )
  CLOSE(12,STATUS='DELETE' )
  CLOSE(13,STATUS='DELETE' )
  STOP
C
1006 FORMAT( 2I5,2F10.0 )
2002 FORMAT( 1H )
2003 FORMAT( /// 12H MODE SHAPES,/,18H LEVEL ID DIRN ,8I13)
2004 FORMAT( 15,3X,A4,2X,A4,2X,8F13.6)
3002 FORMAT( /// 22H NEGATIVE OR ZERO MASS ,/,21H EXECUTION TERMINATED
1)
3003 FORMAT( //,10X,12H LEVEL =,13,/,
1 10X,12H DIRECTION =,13,/,
2 10X,15H SPRING STIFF =,F12.1,/,
3 10X,15H ECCENTRICITY =,F12.1,/)
4000 FORMAT(/,1H ,13X,4HMODE,10X,7HNATURAL,3X,8HFREQUENCY,4X,8HCIRCULAR
1 ,/,13X,8HNUMBER,10X, 8HPERIOD,7X,4H(HZ),4X,8HFREQUENCY,/)
4001 FORMAT( 10X,17,6X,F12.6,2F12.4 )
5000 FORMAT( ///,10X,26(1H-),/,10X,5HSTATE,12,19H DYNAMIC PROPERTIES,
1 /,10X,26(1H-),// )
5001 FORMAT( //,10X,34HSLAM RESTART FILE CREATED ON TAPE1,/)
5002 FORMAT( //,10X,36HSLAM-2 RESTART FILE CREATED ON TAPE1,/)
  END

```

```

SUBROUTINE FORM(SD,CP,BP,FEF,LB,LDB,LC,LP,S,R,NST,NB,NC,NCP,
1 NSP,NB,NFEF,NPAN,IFEF,PP,MN,IF,LT,TP,NTRU,CLN,KODE,ICHEK,NPT)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION SD(NST,14),CLN(NC,2),CP(14,NCP),BP(11,NSP),FEF(7,NFEF),
1 LB(NB,NB,3),LDB(NB,NB,3),LC(NB,NC,2),LP(3,NPAN),IFEF(NFEF),
1 PP(5,NPAN),LT(3,NTRU),TP(3,NTRU)
C
COMMON/JUNK/ NLD,N,ND,MM,MN,LM(12),IFIL(53)
COMMON/BUNK/P(12,3),TT(8),AFIL(216)
COMMON/STIF/ ABA(12,12),BA(8,12),T(8,12)
CHARACTER*1 HI
DATA HI /'1'/'
C
NLD=3
C
C READ AND PRINT OF COLUMN LINE COORDINATES
C
WRITE(NPT,1000)
READ(5,2501) (M,(CLN(J,I),I=1,2),J=1,NC)
WRITE(NPT,2000)(J,(CLN(J,I),I=1,2),J=1,NC)
C
C READ AND PRINT OF COLUMN PROPERTIES
C
100 L=NCP-1
IF(L.EQ.0) GO TO 105
IF( KODE.EQ.0 ) WRITE(NPT,2001)
IF( KODE.NE.0 ) WRITE(NPT,5001)
DO 10 I=1,L
READ(5,1001) M,( CP(J,I),J=1,8 )
IF( KODE.NE.0 ) READ(5,4000) ( CP(J,I),J=10,14 )
WRITE(NPT,4003) I,( CP(J,I),J=1,8 )
IF( KODE.NE.0 ) WRITE(NPT,4001) ( CP(J,I),J=10,14 )
10 CONTINUE
IF( KODE.LE.0 ) GO TO 105
C---- CALC ALLOWABLE FORCES
DO 18 I=1,L
DO 12 J=10,14
IF( CP(J,I).LE.0.0 ) GO TO 18
12 CONTINUE
CP(10,I) = CP(2,I)*CP(10,I)
CP(11,I) = CP(11,I)*CP(13,I)
CP(12,I) = CP(12,I)*CP(14,I)
GO TO 18
18 CP(10,I) = 0.0
18 CONTINUE
105 DO 110 I=1,14
110 CP(I,NCP)=0.
C
C READ AND PRINT OF BEAM PROPERTIES
C
L=NSP-1
IF(L.EQ.0) GO TO 115
IF( KODE.EQ.0 ) WRITE(NPT,2002)
IF( KODE.NE.0 ) WRITE(NPT,5002)
DO 20 I=1,L
READ(5,1002) M,( BP(J,I),J=1,9 )
IF( KODE.NE.0 ) READ(5,4000) ( BP(J,I),J=10,11 )
WRITE(NPT,4003) I,( BP(J,I),J=1,9 )
IF( KODE.NE.0 ) WRITE(NPT,4002) ( BP(J,I),J=10,11 )
20 CONTINUE
IF( KODE.LE.0 ) GO TO 115
C---- CALC ALLOWABLE FORCES
DO 30 I=1,L
30 BP(10,I) = BP(10,I)*BP(11,I)
115 DO 120 I=1,11
120 BP(I,NSP)=0.
C
C READ AND PRINT OF FIXED END BEAM LOADS
C
IF( NFEF.EQ.0 ) GO TO 208

```

```

205 READ (5,1003) (M,IFEF(I),(FEF(J,I),J=1,7),I=1,NFEF)
WRITE (NPT,2003) (I,IFEF(I),(FEF(J,I),J=1,5),I=1,NFEF)
C
C READ (OR GENERATE) AND PRINT OF BEAM LOCATION CARDS - LB
C
209 IF (NB.EQ.0) GO TO 300
210 WRITE (NPT,2004)
DO 260 M=1,NB
K=0
DO 250 N=1,NB
IF (K.NE.0) GO TO 220
LN=NB+1-N
READ(5,1004) I,(LB(N,M,L),L=1,NLD),K,(LDB(N,M,L),L=1,NLD)
WRITE(NPT,1004) I, LN,(LB(N,M,L),L=1,NLD),K,(LDB(N,M,L),L=1,NLD)
IF (LB(N,M,NLD).EQ.0) LB(N,M,NLD)=NBP
GO TO 250
220 K=K-1
DO 230 L=1,NLD
LB(N,M,L)=LB(N-1,M,L)
230 LDB(N,M,L)=LDB(N-1,M,L)
250 CONTINUE
260 WRITE (NPT,3000)
WRITE (NPT,3004)
CALL ECHO (LB,NB,NB,3,3,NBP,NPT)
IF (NFEF.EQ.0) GO TO 300
DO 270 L=1,NLD
WRITE (NPT,4004) (HI,I=1,L)
CALL ECHO (LDB,NB,NB,3,L,100000,NPT)
270 CONTINUE
C
C READ (OR GENERATE) AND PRINT COLUMN LOCATIONS - LC
C
300 WRITE (NPT,2005)
DO 360 M=1,NC
K=0
DO 350 N=1,NB
IF (K.NE.0) GO TO 320
LN=NB+1-N
READ(5,1005) KK,(LC(N,M,I),I=1,2),K
WRITE(NPT,1005)KK,LN,(LC(N,M,I),I=1,2),K
IF (LC(N,M,1).EQ.0)LC(N,M,1)=NCP
GO TO 350
320 K=K-1
DO 330 I=1,2
LC(N,M,I)=LC(N-1,M,I)
350 CONTINUE
360 WRITE (NPT,3000)
WRITE (NPT,3005)
CALL ECHO (LC,NB,NC,2,1,NCP,NPT)
C
C READ AND PRINT OF PANEL CARDS - LP,PP
C
IF(NPAN.EQ.0) GO TO 365
READ (5,1006) (LP(1,I),LP(2,I),LP(3,I),(PP(J,I),J=1,5),I=1,NPAN)
WRITE(NPT,2006)(LP(1,I),LP(2,I),LP(3,I),(PP(J,I),J=1,5),I=1,NPAN)
C
C READ AND PRINT DIAGONALS
C
365 IF (NTRU.EQ.0) GO TO 380
READ(5,1007) ( LT(1,I),LT(2,I),LT(3,I),TP(1,I),TP(2,I),TP(3,I),
1 I=1,NTRU )
IF( KODE.EQ.0 ) WRITE(6,2007) ( LT(1,I),LT(2,I),LT(3,I),TP(1,I),
1 TP(2,I),I=1,NTRU )
IF( KODE.NE.0 ) WRITE(6,5007) ( LT(1,I),LT(2,I),LT(3,I),TP(1,I),
1 TP(2,I),TP(3,I),I=1,NTRU )
C--- CALC ALLOWABLE FORCE
DO 40 I=1,NTRU
40 TP(3,I) = TP(2,I)*TP(3,I)
C
C PRINT BEAM PROPERTIES AND LOADS
C

```

```

C
C   REDUCE E BY B,E
C
  JB=0
  DO 540 J=MNP,NNL
  JJ=J-MN
  IB=1
  DO 530 I=2,MM
  IM=I-1
  KF=MAXD(KH(I),KH(J))
  SB=0.0
  IF (KF.GT.IM) GO TO 530
  DO 520 K=KF,IM
520  SB=SB+B(IB+K)*E(K,JJ)
  E(I,JJ)=E(I,JJ)-SB
530  IB=IB+1
540  CONTINUE
  DO 830 I=1,MM
  DO 830 J=1,NE
830  EB(I,J)=0.0
  L=3*(N-1)
  DO 840 I=1,MM
  DO 840 J=1,6
840  EB(I,J+L)=EB(I,J+L)+EF(I+MM,J)
  DO 845 I=1,MM
  DO 845 J=1,NLD
845  EB(I,J+NNM)=EB(I,J+NNM)+PF(I+MM,J)
C
C   RED EB BY C,E
C
  DO 570 J=MNP,NNL
  JJ=J-MN
  DO 560 I=MNP,MN
  II=I-MM
  KF=MAXD(KH(I),KH(J))
  SB=0.0
  IF (KF.GT.MM) GO TO 560
  DO 550 K=KF,MM
550  SB=SB+C(K,II)*E(K,JJ)
560  EB(II,JJ)=EB(II,JJ)-SB
570  CONTINUE
  REWIND NTE
  REWIND NT8L
  WRITE (NTE) EB
C
C   OVERWRITE B BY BL
C
  READ (NT8L) BL
  L=3*(N-1)
  K=(L*(L+1))/2
  DO 880 J=1,6
  DO 880 I=1,J
880  BL(K+L+1)=BL(K+L+1)+EF(I+MM,J)
880  K=K+L+J
C
C   RED BL BY E,E
C
  JB=0
  DO 700 J=MNP,NNL
  JJ=J-MN
  JM=J-1
  JM=MIND(JM,NNN)
  IF (MNP.GT.JM) GO TO 810
  DO 600 I=MNP,MM
  KF=MAXD(KH(I),KH(J))
  II=I-MN
  SB=0.0
  IF (KF.GT.MM) GO TO 600
  DO 580 K=KF,MM
580  SB=SB+E(K,II)*E(K,JJ)
600  BL(JB+1)=BL(JB+1)-SB

```

```

    TF(5,11)=B/XLR
    TF(3,10)=1.+B/XLR
    TF(8,11)=1.+B/XLR
    DO 150 I=1,12
    DO 150 J=1,12
150 TT(I,J)=0.
    TT(1,1)=BNA
    TT(2,2)=BNA
    TT(1,2)=-CSA
    TT(2,1)=CSA
    TT(3,3)=1.
    DO 155 I=3,9,3
    DO 152 I=1,3
    DO 152 J=1,3
152 TT(I+I,I+J)=TT(I,J)
155 CONTINUE
    TT(1,3)=-YL1*BNA-XL1*CSA
    TT(2,3)=-YL1*CSA+XL1*BNA
    TT(7,9)=TT(1,3)
    TT(8,9)=TT(2,3)
    DO 190 I=1,6
    DO 190 I1=1,10,3
    I2=I1+2
    DO 180 J=11,12
    XX=0.
    DO 170 K=11,12
170 XX=XX+TF(I,K)*TT(K,J)
180 T(I,J)=XX
190 CONTINUE
    RETURN
C
C   BEAM LOCAL TRANSFORMATION
200 D1=-1./XLR
    TF(1,2)=-1.
    TF(1,5)=1.
    TF(2,1)=1.+A/XLR
    TF(3,1)=A/XLR
    TF(2,4)=B/XLR
    TF(3,4)=1.+B/XLR
    TF(2,3)=-D1
    TF(3,3)=-D1
    TF(2,6)=D1
    TF(3,6)=D1
    DO 210 I=1,3
    DO 210 J=1,3
210 TT(I,J)=0.
    TT(1,1)=BNA
    TT(2,2)=BNA
    TT(1,2)=-CSA
    TT(2,1)=CSA
    TT(3,3)=1.
    DO 230 J=1,3
    DO 230 I1=1,4,3
    I2=I1-1
    DO 230 J1=1,3
    XX=0.
    DO 220 K=1,3
220 XX=XX+TF(J,I2+K)*TT(K,J1)
    I=J1+12
230 T(J,I)=XX
    RETURN
C
C   PANEL TRANSFORMATION
C
300 D1=1./XLR
    D2=1./A
C
    IF(MK.EQ.5) GO TO 305
C
    TF(1,4)=-D1
    TF(2,4)=-D1

```



```

TF(1,1)=D1
TF(2,1)=D1
TF(2,5)=-D2
TF(2,6)=D2
TF(1,2)=-D2
TF(1,3)=D2
TF(3,5)=-0.5
TF(3,6)=-0.5
TF(3,2)=0.5
TF(3,3)=0.5

```

C

```

KN=3
GO TO 315

```

C

```

305 TF(1,1)=D1
TF(1,4)=-D1
TF(1,2)=-D2/2.
TF(1,3)=D2/2.
TF(1,5) = -D2/2.
TF(1,6) = D2/2.

```

C

```

KN=1

```

C

```

315 DO 310 I=1,6
DO 310 J=1,10
310 TT(I,J)=0.
TT(1,1)=CSA
TT(1,2)=SNA
TT(1,3)= B
TT(2,4)=1.
TT(3,5)=1.
TT(4,6)=CSA
TT(4,7)=SNA
TT(4,8)= B
TT(5,9)=1.
TT(6,10)=1.
DO 330 I1=1,4,3
I2=I1-1
JJ=0
IF(I1.EQ.4) JJ=5
DO 330 J1=1,5
XX=0.
DO 320 K=1,3
320 XX=XX+TF(J,I2+K)*TT(K,J1)
I=J1+JJ
330 T(J,I)=XX
RETURN

```

C

C DIAGONAL TRANSFORMATION

C

```

400 T(1,1)=DOOB(XLR)*CSA
T(1,2)=DOOB(XLR)*SNA
T(1,3)= DOOB(XLR)*XL1
T(1,4)=DBIN(XLR)
T(1,5)=-T(1,1)
T(1,6)=-T(1,2)
T(1,7)=-T(1,3)
T(1,8)=-T(1,4)
RETURN

```

END

SUBROUTINE STIFF (IO,B,R,NN,NS)

IMPLICIT REAL*8 (A-H)

IMPLICIT REAL*8 (O-Z)

DIMENSION B(1)

COMMON/JUNK/NLD,N,ND,MM,MN,LM(12),IFIL(53)

COMMON/BUNK/ P(12,3),TT(8),AFIL(216)

COMMON/STIF/EB(12,12),BA(B,12),T(B,12)

COMMON/FTAPES/ NTS,NTE,NTBL,NEKB

NEKB=3

NTS=11

NTE=12

```

NTSL=13
NLD=3
MN=2*MM
MNS=MN+6
LB=(MM*(MM+1))/2
LC=MM*MM
NE=MN+NLD-MN
LE=MM*NE
NNM=MN-MN
LBL=(MM*(MM+1))/2+NNM*NLD
NNL=MN+NLD
N1=1
N2=N1+MAX0(LB,LE)
N3=N2+LC
N4=N1+LBL
N3=MAX0(N3,N4)
N4=N3+MAX0(LB,LE)
N5=N4-MNS*6
N6=N5-MN*3
N7=N6+NNL
N8=N7-MM
IF (IO.GT.0) GO TO 50
IO=N8-N1
RETURN
50 GO TO (100,200,300,400,500) , IO
C
C   IO=1  ZERO ARRAYS
C
100 NL=N8-1
   DO 110 I=N1,NL
110 B(I)=0.0
   REWIND NTSL
   REWIND NTS
   REWIND NTE
   WRITE (NTS) (B(I),I=1,LB)
   WRITE (NTE) (B(I),I=1,LE)
   WRITE (NTSL) (B(I),I=1,LBL)
   RETURN
C
C   IO=2  SHIFT STORAGE
C
200 REWIND NTS
   READ (NTS) (B(I),I=1,LB)
   NL=N8-N1
   DO 210 I=N2,NL
210 B(I)=0.0
   RETURN
C
C   IO=3  REDUCE EQN,B WRITE BS EQNS ON TAPE 3 (NBKS)
C
300 MNS=MN+6
   CALL SHRINK (B(N1),LB,B(N6),MM,NNL,B(N7),S(N2),S(N3),B(N3),B(N1),
1      B(N1),NE,LBL,B(N4),B(N5),MNS,MN,N8)
   RETURN
C
C   IO=4  WRITE LAT STIF ON TAPE 2
C
400 NFR=MN-MN-3
   NT2=2
   NF=N1
   NL=(NFR*(NFR+1))/2
   M=LBL-NNM
   L=M-NNM
   K=L-NNM
   WRITE (NT2) N,NFR,(B(I),I=NF,NL),(B(K+1),I=1,NFR),
1      (B(L+1),I=1,NFR),(B(M+1),I=1,NFR)
   RETURN
C
C   IO=5  ADD ELEMENT STIFF TO FRAME STIFFNESS
C
500 MNS=MN+6

```

```

C -----          BB=(MM*(MM+1))/2
C
C MAXIMUM STORAGE GOVERNED BY THAT REQUIRED FOR ANY THREE BLOCKS
C
C IMPLICIT REAL*8 (A-H)
C IMPLICIT REAL*8 (O-Z)
C DIMENSION B(LB),KH(NNL),C(MM,MM),BB(LB),SD(MM)
1      ,E(MM,NE),EB(MM,NE),BL(LBL),EF(MN6,6),PF(MN,3)
COMMON/JUNK/NLD,N,ND,1D,JD,LM(12),FIL(53)
COMMON/BUNK/ P(12,3),TT(8),AFIL(216)
COMMON/FTAPE/NTS,NTE,NTSL,NSKS
C
C NLD=3
C MN=2*MM
C MNP=MM+1
C MNP=MM+1
C NNN=MM+3*N+3
C NN=NNL-NLD
C NNM=NN-MN
C
C DETERMINE PROFILE OF (B,C,BB)
C
C JB=0
C DO 50 J=1,MM
C KH(J)=1
C DO 40 I=1,J
C IF (B(JB+I)) 50,40,50
40 KH(J)=I+1
50 JB=JB+J
C DO 70 J=1,MM
C KH(J+MM)=1
C DO 60 I=1,MM
C IF (C(I,J)) 70,60,70
60 KH(J+MM)=I+1
70 CONTINUE
C
C REDUCTION OF B
C
C BD(1)=B(1)
C JB=1
C DO 300 J=2,MM
C BD(J)=0.0
C JM=J-1
C IF (J.EQ.2) GO TO 260
C IB=1
C DO 250 I=2,JM
C IM=I-1
C BB=0.0
C KF=MAX0(KH(I),KH(J))
C IF (KF.GT.IM) GO TO 250
C
C REDUCE B BY B,B
C
C DO 200 K=KF,IM
200 BB=BB+B(IB+K)*B(JB+K)
C B(JB+I)=B(JB+I)-BB
250 IB=IB+1
C
C RED COL BY SELF
C
260 BB=0.0
C KF=KH(J)
C IF (KF.GT.JM) GO TO 290
C KD=(KF*(KF+1))/2
C DO 280 K=KF,JM
C IF (B(KD)) 270,280,270
270 T=B(JB+K)/B(KD)
C BB=BB+T*B(JB+K)
C B(JB+K)=T
280 KD=KD+K+1
C B(JB+J)=B(JB+J)-BB

```

```

290 SD(J)=B(JB+J)
300 JB=JB+J
C
C   REDUCTION OF C, BB
C
    JB=0
    DO 500 J=MNP, MN
    JJ=J-MM
    JM=J-1
    IB=1
    DO 450 I=2, JM
    II=I-MM
    IM=I-1
    KL=MINO(IM, MM)
    KF=MAXO(KH(I), KH(J))
    IF (KF.GT.KL) GO TO 450
    BB=0.0
    IF (I.GT.MM) GO TO 430
C
C   RED C BY B, C
C
    DO 420 K=KF, KL
420 BB=BB+B(IB+K)*C(K, JJ)
    C(I, JJ)=C(I, JJ)-BB
    GO TO 450
C
C   RED BB BY C, C
C
430 DO 440 K=KF, KL
440 BB=BB+C(K, II)*C(K, JJ)
    BB(JB+I)=BB(JB+I)-BB
450 IB=IB+I
C
C
C   RED COL BY SELF
    BB=0.0
    KF=KH(J)
    IF (KF.GT.MM) GO TO 500
    DO 460 K=KF, MM
    IF (SD(K)) 455, 460, 455
455 T=C(K, JJ)/SD(K)
    BB=BB+T*C(K, JJ)
    C(K, JJ)=T
460 CONTINUE
    BB(JB+JJ)=BB(JB+JJ)-BB
500 JB=JB+JJ
    REWIND NTS
    WRITE (NTS) BB
    WRITE (NSKB) B, C
C
C   OVERWRITE BB WITH (E, EB)
C
    REWIND NTE
    READ (NTE) E
    L=3*(N-1)
    DO 810 I=1, MM
    DO 810 J=1, 8
810 E(I, J+L)=E(I, J+L)+EF(I, J)
    DO 820 I=1, MM
    DO 820 J=1, 3
820 E(I, J+MM)=E(I, J+MM)+PF(I, J)
C
C   DETERMINE PROFILE OF (E, EB)
C
    DO 90 J=MNP,>NNL
    JJ=J-MM
    KH(J)=1
    DO 90 I=1, MM
    IF (E(I, JJ)) 90, 90, 90
90 KH(J)=I+1
90 CONTINUE

```

```

      AJ(3,1)=D(M,K,1)
      AJ(3,2)=D(M,K,2)
C
      DO 225 I1=1,3
      DO 225 J1=1,13
      JJ=J1+18
      AR(I1,JJ)=0.
      DO 225 KK=1,3
225 AR(I1,JJ)=AR(I1,JJ)+B(12+I1,J2+KK)*AI(KK,JJ)
C
      DO 275 I1=1,13
      I1=I1+18
C
      IF(N.NE.NT) GO TO 260
      DO 250 L=1,3
      DO 250 KK=1,3
250 RR(IR+I1,L)=RR(IR+I1,L)+AJ(I1,KK)*R(12+KK,L)
C
260 DO 275 J1=1,13
      JJ=J1+18
      AB(I1,JJ)=0.
      DO 275 KK=1,3
275 AB(I1,JJ)=AB(I1,JJ)+AJ(I1,KK)*AR(KK,JJ)
C
      NN=13*(NT-1)
C
      DO 300 I=1,13
      I1=13*(M-NT)+I
      DO 300 J=1,13
      JJ=13*(N-NT)+J
300 SB(NN+I,NN+JJ)=SB(NN+I,NN+JJ)+AB(I+18,J+18)
400 CONTINUE
C
      AA(K,1)=1F
      AA(K,2)=1FC
      AA(K,3)=AI(1,1)
      AA(K,4)=AI(1,2)
      AA(K,5)=NT
500 CONTINUE
      IF(1CHEK.NE.0) RETURN
C
C---- MOD OF LAT STIFFNESS FOR P-DELTA EFFECTS
C
      IF( NAT.GT.9 ) REWIND 1
      IF( NAT.GT.9 ) WRITE(1) SB
      IF( DABS(GRAV).LT.1.0D-10 ) GO TO 655
      IPD=0
501 XMT=0.0
      XMMT = 0.0
      DO 650 I=1,NST
      H = A(1,2)
      XMT = XMT + A(1,3)
      XMMT = XMMT + A(1,4)
      MM = ( I - 1 ) * 13
C
      DO 600 J=1,13
      IF( J.NE.3 ) PDEL = XMT*GRAV/H
      IF( J.EQ.3 ) PDEL = XMMT*GRAV/H
      NN = MM + J
      SB(NN,NN) = SB(NN,NN) - PDEL
      IF( I.GE.NST ) GO TO 600
      SB(NN,NN+13) = SB(NN,NN+13) + PDEL
      SB(NN+13,NN) = SB(NN+13,NN) + PDEL
      SB(NN+13,NN+13) = SB(NN+13,NN+13) - PDEL
600 CONTINUE
650 CONTINUE
      IF(IPD.EQ.1)GO TO 730
C
C---- END OF P-DELTA MODS
C
655 NT2 = 2

```

```

REWIND NT2
WRITE (NT2) SB,XM
IF(NAT.EQ.1) RETURN
IF(DABS(GRAV).LT.1.0D-10)GO TO 657
DO 656 I=1,NBS
DO 656 J=1,2
656 RRR(I,J)=RR(I,J+3)
657 CONTINUE
C DO 658 I = 1,NBS
C IF ( SB(I,1) .LE. 0.0 ) THEN
C WRITE (0,*) ' MATRIX SB '
C WRITE (0,*) 'SB(' ,I ,',',I ,') = ',SB(I,1)
C GOTO 659
C ELSE
C WRITE (0,*) 'SB(' ,I ,',',I ,') = ',SB(I,1)
C ENDIF
C 658 CONTINUE
C GOTO 660
C 659 WRITE (0,1101)
C WRITE (0,1102)
C STOP
C 1101 FORMAT (T5,'.....')
C 1102 FORMAT (T5,'ZERO ON DIAGONAL OF STRUCTURE STIFFNESS MTX. ')
C 660 CONTINUE
CALL SOLVE(SB,NBS,RR,5)
C
C PRINT STRUCTURE DISPLACEMENTS
C
IF ( ITYPE .EQ. 0 ) THEN
WRITE(0,1001)
WRITE(0,1003)
CALL PROUT( RR,NBS,5,BN,NBT,RLAB,13,16 )
ENDIF
C
WRITE (2) RR
WRITE (2) AA,D,HED
IF(DABS(GRAV).LT.1.0D-10)GO TO 750
DO 725 I=1,NBS
DO 725 J=1,NBS
725 SB(I,J)=0.0
IPD=1
GO TO 501
C
C----CALCULATE P-DELTA FORCES
C
730 CONTINUE
DO 740 I=1,NBS
K1=I-13
K2=I+13
IF(K1.LE.0)K1=1
IF(K2.GT.NBS)K2=NBS
DO 735 J=1,2
XX=0.
DO 732 K=K1,K2
732 XX=XX+SB(I,K)*RR(K,J+3)
735 RRR(I,J)=RRR(I,J)-XX
740 CONTINUE
750 CONTINUE
C
C---- CALC DRIFTS
N = NBT - 1
DO 722 I=1,5
IF(NBT.EQ.1)GO TO 721
DO 720 J=1,N
JJ = 13*( J - 1 ) + 1
RR(JJ,1) = ( RR(JJ,1) - RR(JJ+13,1) )/A(J,2)
IF( 13.NE.3 ) GO TO 720
RR(JJ+1,1) = ( RR(JJ+1,1) - RR(JJ+4,1) )/A(J,2)
RR(JJ+2,1) = RR(JJ+2,1) - RR(JJ+5,1)
720 CONTINUE
721 JJ = 13*( NBT - 1 ) + 1

```

```

380 IF(NB.EQ.0) GO TO 372
  WRITE(NPT,2011)
  DO 370 M=1,NB
    WRITE (NPT,2012) M
    DO 370 N=1,NB
      LN=NB+1-N
      NN=LB(N,M,3)
370 WRITE(NPT,2010) LN,(BP(J,NN),J=1,9),(LDB(N,M,L),L=1,NLD)
C
C   PRINT COLUMN PROPERTIES
C
372 WRITE (NPT,2013)
  DO 375 M=1,NC
    WRITE (NPT,2014) M
    DO 375 N=1,NB
      LN=NB+1-N
      NN=LC(N,M,1)
375 WRITE(NPT,2016) LN,(CP(J,NN),J=1,9)
  IF( ICHEK.NE.0 ) GO TO 815
C
C   STORY BY STORY FORMATION AND REDUCTION OF STIFFNESS MATRIX
C
  K=NB-NB
  MM=3*NC
  MN=8*NC
  NN=MM+3*NB+3
  CALL STIFF(1,B,R,NN,NB)
C
  DO 700 N=1,NB
C
  CALL STIFF(2,B,R,NN,NB)
C
C   1. FORM COLUMN MATRICES
C
  DO 390 I=1,12
  DO 390 L=1,NLD
390 P(I,L)=0.0
  NF=8
  ND=12
  DO 500 M=1,NC
    MC=LC(N,M,1)
    IF(MC.EQ.NCP) GO TO 500
    XL =SD(N+K,2)
    KK=LC(N,M,2)
    B1=CLN(KK,1)-CLN(M,1)
    B2=CLN(KK,2)-CLN(M,2)
    B3=B1*B1+B2*B2
    B3=DSQRT(B3)
    IF(B3.LE.0.) STOP1
    CSA=B1/B3
    SNA=B2/B3
    XL1=CLN(M,1)
    YL1=CLN(M,2)
    NREC = NC*(N-1)+M
    READ (15,REC = NREC) VVP
C   WRITE (8,*) '*****'
C   WRITE (8,*) 'SUBROUTINE FORM'
C   WRITE (8,*) 'STORY NO. ',N
C   WRITE (8,*) 'COLUMN LINE NO. ',M
C   WRITE (8,*) 'AXIAL IN COLUMN = ',VVP
C   WRITE (8,*) '*****'
  CALL COLUMN(1,MC,XL,SNA,CSA,NCP,XL1,YL1,CP,VVP)
C
  LM(8)=3*M
  LM(5)=LM(8)-1
  LM(4)=LM(5)-1
  LM(11)=LM(5)+MM
  LM(10)=LM(4)+MM
  LM(12)=LM(8)+MM
  LM(3)=MM+3*N
  LM(2)=LM(3)-1

```

```

      SNA=B2/B3
      D=B3
      AR=CLN(KI,1)*CLN(KJ,2)-CLN(KJ,1)*CLN(KI,2)
      DF=AR/B3
      NREC = NC*NB+L
      READ (15,REC = NREC) VVP
C     WRITE (6,*) '#####'
C     WRITE (6,*) 'SUBROUTINE FORM'
C     WRITE (6,*) 'STORY NO. ',N
C     WRITE (6,*) 'PANEL NO. ',L
C     WRITE (6,*) 'AXIAL IN PANEL = ',VVP
C     WRITE (6,*) '#####'
      CALL PANEL (1,L,XL,D,DF,SNA,CSA,NPAN,PP,VVP)
C
      LM(3)=MN+3*N
      LM(2)=LM(3)-1
      LM(1)=LM(2)-1
      LM(4)=3*KI
      LM(5)=3*KJ
      LM(6)=MN+3*N+3
      LM(7)=LM(6)-1
      LM(8)=LM(7)-1
      LM(9)=MM+3*KI
      LM(10)=MM+3*KJ
      CALL STIFF(5,B,R,MN,NS)
600 CONTINUE
C
C     FORM DIAGONAL STIFFNESS
C
610 IF (NTRU EQ 0) GO TO 710
      DO 620 I=1,B
      DO 620 J=1,NLD
620 P(I,J)=0.
      NF=1
      ND=B
      DO 690 L=1,NTRU
      NP=NB-LT(1,L)+1
      IF (NP.EQ.N) GO TO 690
      YL=BD(M+K,2)
      KJ=LT(2,L)
      KI=LT(3,L)
      B1=CLN(KJ,1)-CLN(KI,1)
      B2=CLN(KJ,2)-CLN(KI,2)
      B3=B1*B1+B2*B2
      B3=DSQRT (B3)
      CSA=B1/B3
      SNA=B2/B3
      VANG=DATAN(YL/B3)
      DL=DSQRT(B3*B3+YL*YL)
      AR=CLN(KI,1)*CLN(KJ,2)-CLN(KJ,1)*CLN(KI,2)
      D1=AR/B3
      CALL DIAG(1,L,VANG,DL,SNA,CSA,NTRU,D1,TP)
C
      LM(3)=MN+3*N
      LM(2)=LM(3)-1
      LM(1)=LM(2)-1
      LM(4)=3*KJ
      LM(7)=MN+3*N+3
      LM(6)=LM(7)-1
      LM(5)=LM(6)-1
      LM(8)=MM+3*KI
      CALL STIFF(5,B,R,MN,NS)
690 CONTINUE
710 CONTINUE
C
C     REDUCE STIFFNESS MATRIX FOR LEVEL N
C
      CALL STIFF(3,B,R,MN,NS)
C
700 CONTINUE
C

```



```

C   WRITE LATERAL STIFFNESS ON TAPE
C
  810 N=NBST+1-NB
      CALL STIFF(4,B,R,NN,NB)
      WRITE (3)CLN,CP,BP,FEF,LB,LDB,LC,LP,IFEF,PP,LT,TP
  815 WRITE(3) IF,NC,NB,NCP,NBP,NFEF,NPAN,NTRU,NB
C
      RETURN
  1000 FORMAT(/,24H COLUMN LINE COORDINATES,/,5H LINE,14X,1HX,14X,1HY)
  2000 FORMAT(15,5X,F10.2,5X,F10.2)
  1001 FORMAT(15,F15.0,F10.0,2F5.0,3F10.0,2F5.0)
  2001 FORMAT(/,10H COLUMN ID,11X,1HE,11X,1HA,6X,6HMAJ,BA,6X,6HMIN,BA,
    16X,6HTORS,1,7X,6HMAJ,1,7X,6HMIN,1,3X,6HRIGID TOP,3X,6HRIGID BOT,/)
  1002 FORMAT(15,F15.0,F5.0,2F10.0,5F5.0)
  2002 FORMAT(/,10H BEAM ID,11X,2HE,9X,2HBA,6X,6HTORS,1,6X,6HFLEX,1
    1,9X,6HK1,9X,6HKJ,9X,6HKIJ,5X,7HRIGID,1,5X,7HRIGID J,/)
  1003 FORMAT(215,7F10.0)
  2003 FORMAT(/,10H FEF ID,6X,4HCODE,10X,2HML,10X,2HVL,10X,2HMR,10X,
    1,2HVR,11X,1HY,/,,(2110,5F12.3))
  1004 FORMAT(915)
  2004 FORMAT(/,15H BEAM LOCATIONS,/,45H/ BAY LEV IC JC BID GEN V
    1L1 VL2 VL3 )
  3004 FORMAT(/,25H GENERATED BEAM LOCATIONS )
  4004 FORMAT(/,34H GENERATED BEAM LOADS...LOAD CASE 3A1)
  1005 FORMAT(515)
  2005 FORMAT(/,17H COLUMN LOCATIONS,/,26H/ LINE LEV CID KCOL GEN )
  3005 FORMAT(/,27H GENERATED COLUMN LOCATIONS )
  1006 FORMAT(315,5F10.0)
  2006 FORMAT(/,12H PANEL CARDS,/,20H LEVEL COL I COL J,12X,1HE,14X,
    11HA,14X,1HI,13X,2HBA,14X,1HG,/,,(14,217,2X,5F15.2))
  1007 FORMAT(315,3F10.0)
  2007 FORMAT(/,22H BRACING ELEMENT CARDS,/,16H LEV UC LC,14X,
    11HE,14X,1HA,/,,(1X,315,2F15.5))
  3000 FORMAT(1H)
  2010 FORMAT(14,2X,F12.2,6F10.2,5X,15,5X,15,5X,15)
  2011 FORMAT(/,26H BEAM PROPERTIES AND LOADS/)
  2012 FORMAT(12H BAY NUMBERS,15,/,129H LEVEL E BA TO
    1RS I FLEX I K11 KJJ KIJ WI WJ
    1 VERT1 VERT2 VERT3 )
  2013 FORMAT(/,16H COLUMN PROPERTIES,/)
  2014 FORMAT(/,16H COLUMN LINE NO.,15,/,99H LEVEL E A
    1 MAJ BA MIN BA TORS I MAJ I MIN I DT
    1DB,/)
  2016 FORMAT(14,2X,F12.2,6F10.2)
  2501 FORMAT(15,2F10.0)
  4000 FORMAT(5F10.0)
  4001 FORMAT(22X,3F12.2,12X,2F12.2)
  4002 FORMAT(22X,F12.2,12X,F12.2)
  4003 FORMAT(110,9F12.2)
  5001 FORMAT(/,10H COLUMN ID,11X,1HE,11X,1HA,6X,6HMAJ,BA,6X,6HMIN,BA,
    16X,6HTORS,1,7X,6HMAJ,1,7X,6HMIN,1,3X,6HRIGID TOP,3X,6HRIGID BOT,/)
    2 32X,2HFA,6X,6HMAJ,FB,6X,6HMIN,FB,16X,6HMAJ,BA,7X,6HMIN,BA,/)
  5002 FORMAT(/,10H BEAM ID,11X,2HE,9X,2HBA,6X,6HTORS,1,6X,6HFLEX,1
    1,9X,6HK1,9X,6HKJ,9X,6HKIJ,5X,7HRIGID,1,5X,7HRIGID J,/)
    2 32X,2HFB,16X,6HSEC,BA,/)
  5007 FORMAT(/,22H BRACING ELEMENT CARDS,/,16H LEV UC LC,14X,1HE
    1,14X,1HA,13X,2HFA,/,,(1X,315,2F15.5,F15.2) )
      END
C-----
      SUBROUTINE COLUMN(IO,MC,XL,ENA,CBA,NCP,XL1,YL1,CP,VP)
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      DIMENSION CP(14,NCP),TB(6,6),TBF(6,12),TFBF(12,12),TFBFT(12,12),
    1 TFT(12,6),TTT(12,12),BMG(12,12)
      COMMON/STIF/ ASA(12,12),BA(6,12),T(6,12)
      COMMON/JUNK/ MLD,N,MD,MM,MN,LM(12),IFIL(53)
      COMMON/BUNK/ P(12,3),TF(6,12),TT(12,12),AFIL(6)
C
C   COLUMN STIFFNESS AND FORCE MATRICES
C
C   TRANSFORMATION MATRICES

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```

DT=CP(8,MC)
DB=CP(9,MC)
XLR=XL-DT-DB
CALL TRANS(1,XLR,DT,DB,BNA,CSA,XL1,YL1,0.00,0.00)
C
C COLUMN MEMBER STIFFNESS
E=CP(1,MC)
AZ=CP(2,MC)
AY=CP(3,MC)
AX=CP(4,MC)
AAZ=CP(5,MC)
AAY=CP(6,MC)
AAX=CP(7,MC)
BHFY=0.
BHFZ=0.
E1Y=AAY*E/(XLR*XLR)
E1X=AAX*E/(XLR*XLR)
IF(AY.GT.0.) BHFY=14.4*E1Y/(AY*E)
IF(AX.GT.0.) BHFZ=14.4*E1X/(AX*E)
COMMY=2.*E1X*XLR/(1.-2.*BHFZ)
COMMX=2.*E1Y*XLR/(1.-2.*BHFY)
C
B1=0.414*E*AAZ/XLR
B2=COMMX*(2.-BHFY)
B3=COMMY*(1.-BHFZ)
B4=E*AZ/XLR
B5=COMMY*(2.+BHFZ)
B6=COMMX*(1.-BHFZ)
C
C WRITE(6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
C WRITE(6,*) 'SUBROUTINE COLUMN'
C WRITE(6,*) 'AXIAL IN COLUMN =',VP
C WRITE(6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
IF(10.EQ.2) GOTO 15
C
C-----Kc
DO 130 I = 1,6
DO 130 J = 1,6
130 TB(I,J) = 0.0
TB(1,1) = B1
TB(2,2) = B2
TB(2,3) = B3
TB(3,2) = B3
TB(3,3) = B2
TB(4,4) = B4
TB(5,5) = B5
TB(5,6) = B6
TB(6,5) = B6
TB(6,6) = B5
C
C-----KcAc
CALL MULTIP(TB,6,6,TF,6,12,TBF)
C
C-----Act
CALL TRANS(TF,6,12,TFT)
C
C-----ActKcAc
CALL MULTIP(TFT,12,6,TBF,6,12,TFBF)
C
C-----GEOMETRIC NONLINEAR STIFFNESS MATRIX
DO 140 I = 1,12
DO 140 J = 1,12
140 BMD(I,J) = 0.0
BMD(2,2) = (6.*VP)/(5.*XLR)
BMD(2,4) = VP/10.
BMD(2,8) = ((-1.)*6.*VP)/(5.*XLR)
BMD(2,10) = BMD(2,4)
BMD(4,2) = BMD(2,4)
BMD(4,4) = (4.*VP*XLR)/30.
BMD(4,8) = (-1.)*BMD(2,4)
BMD(4,10) = ((-1.)*VP*XLR)/30.

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```

      BMG(8,2) = BMG(2,8)
      BMG(8,4) = BMG(4,8)
      BMG(8,8) = BMG(2,2)
      BMG(8,10) = (-1.)*BMG(2,4)
      BMG(10,2) = BMG(2,10)
      BMG(10,4) = BMG(4,10)
      BMG(10,8) = BMG(8,10)
      BMG(10,10) = BMG(4,4)
C
C-----ADD GEOMETRIC NONLINEAR STIFFNESS MATRIX TO TFSF
      CALL PLUS(TFSF,12,12,BMG,TFSF)
C
C-----Ac(KcAcBc
      CALL MULTIP(TFSF,12,12,TT,12,12,TFSFT)
C
C-----Bct
      CALL TRANBP(TT,12,12,TTT)
C
C-----BctAc(KcAcBc
      CALL MULTIP(TTT,12,12,TFSFT,12,12,ABA)
C
      RETURN
C
      B2 = B2+((4.*VP*XLR)/30.)
      B3 = B3-((VP*XLR)/30.)
C
C FORCE-FRAME DISPLACEMENT MATRIX
      DO 10 I=1,12
      BA(1,I)=B1*T(1,I)
      BA(2,I)=B2*T(2,I)+B3*T(3,I)
      BA(3,I)=B3*T(2,I)+B2*T(3,I)
      BA(4,I)=B4*T(4,I)
      BA(5,I)=B5*T(5,I)+B6*T(6,I)
      BA(6,I)=B6*T(5,I)+B5*T(6,I)
      BA(7,I) = (BA(2,I)+BA(3,I))/XLR
10 BA(8,I) = (BA(5,I)+BA(6,I))/XLR
      RETURN
C
      END
C-----
SUBROUTINE BEAM (IO,MB,XL,SHA,CSA,NBP,BP)
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  DIMENSION BP(11,NBP)
C
COMMON/STIF/ ABA(12,12),BA(8,12),T(8,12)
COMMON/JUNK/ NLD,N,ND,MM,MN,LM(12),IFIL(63)
COMMON/BUNK/ P(12,3),TX(8),AFIL(216)
C
C BEAM STIFFNESS AND FORCE MATRICES
C
C TRANSFORMATION MATRIX
WI=BP(8,MB)
WJ=BP(9,MB)
XLR=XL-WI-WJ
CALL TRANS(2,XLR,WI,WJ,SHA,CSA,0.D0,0.D0,0.D0,0.D0)
C
C MEMBER STIFFNESS
E=BP(1,MB)
SHFZ=0.
EIX=BP(4,MB)*E/(XLR*XLR)
IF(BP(2,MB).GT.0.) SHFZ=14.4*EIX/(BP(2,MB)*E)
COMMX=(XLR*EIX)/(1.+2.*SHFZ)
C
      B1=0.414*E*BP(3,MB)/XLR
      B2=COMMX*BP(5,MB)*(1.+0.5*SHFZ)
      B3=COMMX*BP(6,MB)*(1.+0.5*SHFZ)
      B4=COMMX*BP(7,MB)*(1.-SHFZ)
C
C FORCE-FRAME DISPLACEMENT MATRIX
      DO 10 I=1,6

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```

      BA(1,1)=B1*T(1,1)
      BA(2,1)=B2*T(2,1)+B4*T(3,1)
10  BA(3,1)=B4*T(2,1)+B3*T(3,1)
C
C
      IF(10.EQ.2) RETURN
C  STIFFNESS MATRIX ABA
      DO 120 I=1,6
      DO 120 J=1,6
      ABA(I,J)=0.
      DO 110 K=1,3
110  ABA(I,J)=ABA(I,J)+T(K,1)*BA(K,J)
120  ABA(J,I)=ABA(I,J)
C
C  FIXED END FORCES
      DO 180 L=1,NLD
      TX(3)= P(2,L)
      TX(1)= BNA*P(1,L)
      TX(2)=-CSA*P(1,L)
      TX(6)= P(4,L)
      TX(4)= BNA*P(3,L)
      TX(5)=-CSA*P(3,L)
      DO 150 I=1,6
150  P(I,L)=TX(I)
160  CONTINUE
      RETURN
C
      END
C-----
SUBROUTINE PANEL (IO,L,XL,D,DF,BNA,CSA,NPAN,PP,VP)
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  DIMENSION PP(5,NPAN),TB(3,3),VBF(3,6),TFBF(6,6),TFBFT(6,10),
  1  VFT(6,3),VTT(10,6),BMB(6,6),VF(3,6),VT(6,10),
  2  VASA(10,10)
C
  COMMON/STIF/ ABA(12,12),BA(6,12),T(6,12)
  COMMON/JUNK/ NLD,N,ND,MM,MN,LM(12),IFIL(53)
  COMMON/BUNK/ P(12,3),TF(6,12),TT(12,12),AFIL(6)
C
C  PANEL STIFFNESS AND FORCE MATRICES
C
  NP=3
C
C  CHECK PANEL TYPE (DEFAULT TO PURE SHEAR PANEL IF FLEX I= ZERO)
C
  IF(PP(3,L).LE.0.) NP=6
C
C  TRANSFORMATION MATRIX
C
  CALL TRANS(NP,XL,D,DF,BNA,CSA,0.00,0.00,0.00,0.00)
  DO 180 I = 1,3
  DO 180 J = 1,6
180  VF(I,J) = TF(I,J)
  DO 190 I = 1,6
  DO 190 J = 1,10
190  VT(I,J) = TT(I,J)
C
  IF(NP.EQ.5) GO TO 50
C
C  FLEXURAL PANEL STIFFNESS (NP=3)
C
  E=PP(1,L)
  SHFY=0.
  EIX=E*PP(3,L)/(XL*XL)
  IF(PP(4,L).GT.0.) SHFY=6.*EIX/(PP(4,L)*PP(5,L))
  COMK=(EIX*XL*2.)/(1.+2.*SHFY)
C
  B1=COMK*2.*(1.+0.5*SHFY)
  B2=COMK*(1.-SHFY)
  B3=E*PP(2,L)/XL

```

```

C
C WRITE (6,*) '-----'
C WRITE (6,*) 'SUBROUTINE PANEL'
C WRITE (6,*) 'AXIAL IN PANEL = ',VP
C WRITE (6,*) '-----'
  IF (10.EQ.2) GOTO 160
C
C-----Kc : LINEAR STIFFNESS MATRIX
  DO 160 I = 1,3
    DO 160 J = 1,3
160   TB(I,J) = 0.0
      TB(1,1) = B1
      TB(1,2) = B2
      TB(2,1) = B2
      TB(2,2) = B1
      TB(3,3) = B3
C
C-----KcAp
  CALL MULTIP(TB,3,3,VF,3,6,VBF)
C
C-----Apt
  CALL TRANSP(VF,3,6,VFT)
C
C-----AptKcAp
  CALL MULTIP(VFT,6,3,VBF,3,6,TFBF)
C
C-----GEOMETRIC NONLINEAR STIFFNESS MATRIX
  DO 170 I = 1,6
    DO 170 J = 1,6
170   BNG(I,J) = 0.0
      BNG(1,1) = (6.*VP)/(5.*XL)
      BNG(1,2) = ((-1.)*VP)/(10.*D)
      BNG(1,3) = (-1.)*BNG(1,2)
      BNG(1,4) = (-1.)*BNG(1,1)
      BNG(1,5) = BNG(1,2)
      BNG(1,6) = BNG(1,3)
      BNG(2,1) = BNG(1,2)
      BNG(2,2) = (4.*VP*XL)/(30.*D*D)
      BNG(2,3) = (-1.)*BNG(2,2)
      BNG(2,4) = BNG(1,3)
      BNG(2,5) = ((-1.)*VP*XL)/(30.*D*D)
      BNG(2,6) = (-1.)*BNG(2,5)
      BNG(3,1) = BNG(1,3)
      BNG(3,2) = BNG(2,3)
      BNG(3,3) = BNG(2,2)
      BNG(3,4) = BNG(1,2)
      BNG(3,5) = BNG(2,6)
      BNG(3,6) = BNG(2,5)
      BNG(4,1) = BNG(1,4)
      BNG(4,2) = BNG(2,4)
      BNG(4,3) = BNG(3,4)
      BNG(4,4) = BNG(1,1)
      BNG(4,5) = BNG(1,3)
      BNG(4,6) = BNG(1,2)
      BNG(5,1) = BNG(1,5)
      BNG(5,2) = BNG(2,5)
      BNG(5,3) = BNG(3,5)
      BNG(5,4) = BNG(4,5)
      BNG(5,5) = BNG(2,2)
      BNG(5,6) = BNG(2,3)
      BNG(6,1) = BNG(1,6)
      BNG(6,2) = BNG(2,6)
      BNG(6,3) = BNG(3,6)
      BNG(6,4) = BNG(4,6)
      BNG(6,5) = BNG(5,6)
      BNG(6,6) = BNG(2,2)
C
C-----ADD GEOMETRIC NONLINEAR STIFFNESS MATRIX TO TFSB
  CALL PLUS(TFSB,6,6,BNG,TFSB)
C
C-----AptKcApBp

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      CALL MULTIP(TF8F,6,6,VT,6,10,TF8FT)
C
C-----Bp1
      CALL TRANSP(VT,6,10,VTT)
C
C-----Bp1Ap1KcApBp
      CALL MULTIP(VTT,10,6,TF8FT,6,10,YABA)
      DO 200 I = 1,10
        DO 200 J = 1,10
200   ABA(I,J) = YABA(I,J)
C
      RETURN
C
150 B1 = B1+((4.*VP*XL)/30.)
    B2 = B2-((VP*XL)/30.)
C
C FORCE-FRAME DISPLACEMENT MATRIX
C
      DO 10 I=1,10
        BA(1,I)=B1*T(1,I)+B2*T(2,I)
        BA(2,I)=B2*T(1,I)+B1*T(2,I)
        BA(3,I)=B3*T(3,I)
10   BA(4,I)=(BA(1,I)+BA(2,I))/XL
C
      RETURN
C
C BMEAR PANEL STIFFNESS (NP=5)
C
50 IF(10.EQ.2) XL=1.
    B1=PP(2,L)*PP(5,L)*XL
C
C FORCE-FRAME DISPLACEMENT MATRIX
C
      DO 20 I=1,10
        BA(1,I)=B1*T(1,I)
20   BA(2,I)=BA(1,I)/PP(2,L)
C
      KK=1
C
30 IF(10.EQ.2) RETURN
C
C STIFFNESS MATRIX
      DO 120 I=1,10
        DO 120 J=1,10
          ABA(I,J)=0.
          DO 110 K=1,KK
110   ABA(I,J)=ABA(I,J)+T(K,I)*BA(K,J)
120   ABA(J,I)=ABA(I,J)
      RETURN
C
      END
C
      SUBROUTINE BECOND (T)
C
C IMPLICIT REAL*8 (A-H)
C IMPLICIT REAL*8 (O-Z)
C INTEGER*2 IHRB,IMIN,ISEC
C CALL CLOCK(IHRB,IMIN,ISEC)
C T = DBLE(IHRB)*60 + DBLE(IMIN) + DBLE(ISEC)/60
C
C RETURN
C
      END
C
      SUBROUTINE PLUS(VA,IROWA,ICOLVA,VB,VC)
C
      DOUBLE PRECISION VA(IROWA,ICOLVA),VB(IROWA,ICOLVA),
1     VC(IROWA,ICOLVA)
      DO 5 I = 1,IROWA
        DO 5 J = 1,ICOLVA
5     VC(I,J) = VA(I,J) + VB(I,J)
      RETURN
      END

```

```

C
SUBROUTINE MINUS(VA, IROWA, ICOLVA, VB, VC)
C-----
CThis is a subprogram for matrix subtraction  $A - B = C$ 
CVA(20,20) is local matrix A dimension 20 * 20
CVB(20,20) is local matrix B dimension 20 * 20
C VC(20,20) is local result matrix C dimension 20 * 20
C-----
DOUBLE PRECISION VA(20,20), VB(20,20), VC(20,20)
DO 20 I = 1, IROWA
DO 15 J = 1, ICOLVA
  15 VC(I, J) = VA(I, J) - VB(I, J)
  20 CONTINUE
RETURN
END
C
SUBROUTINE MULTIP(VA, IROWA, ICOLVA, VB, IROWB, ICOLVB, VC)
C-----
CThis is a subprogram for matrix multiplication  $VA * VB = VC$ 
CIROWA is number of row of matrix VA
CICOLVA is number of column of matrix VA
CIROWB is number of row of matrix VB
CICOLVB is number of column of matrix VB
C-----
DOUBLE PRECISION VA(IROWA, ICOLVA), VB(IROWB, ICOLVB),
  1 VC(IROWA, ICOLVB)
IF ( ICOLVA.NE. IROWB) GOTO 40
DO 35 I = 1, IROWA
DO 30 J = 1, ICOLVB
VC(I, J) = 0.
DO 25 K = 1, IROWB
  25 VC(I, J) = VC(I, J) + (VA(I, K)*VB(K, J))
  30 CONTINUE
  35 CONTINUE
GOTO 45
40 WRITE (*,*) 'COLUMN 1ST .NE. ROW 2ND'
45RETURN
END
C
SUBROUTINE DISPLY(VA, IROWA, ICOLVA)
C-----
CThis is a subprogram for displaying matrix on datafile or screen.
C-----
DOUBLE PRECISION VA(IROWA, ICOLVA)
WRITE (8,*) ' '
DO 75 I = 1, IROWA
  75 WRITE (8,100) (VA(I, J), J=1, ICOLVA)
  100 FORMAT (10D12.5)
RETURN
END
C
SUBROUTINE TRANSP(VA, IROWA, ICOLVA, VB)
C-----
C This is a subprogram for matrix transposition.
C IROWA is number of row of matrix VA.
C ICOLVA is number of column of matrix VA.
C-----
DOUBLE PRECISION VA(IROWA, ICOLVA), VB(ICOLVA, IROWA)
DO 115 I = 1, ICOLVA
DO 115 J = 1, IROWA
115 VB(I, J) = VA(J, I)
RETURN
END

```

```

SUBROUTINE EIGEN(H,N,IEGEN,U,NR,X,IQ)
C
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  DIMENSION H(N,N),U(N,N),X(N),IQ(N)
C
  IF (IEGEN) 15,10,15
10 DO 14 I=1,N
  DO 14 J=1,N
  IF(I-J) 12,11,12
11 U(I,J)=1.0
  GO TO 14
12 U(I,J)=0.
14 CONTINUE
C
15 NR = 0
  IF (N-1) 1000,1000,17
C
C SCAN FOR LARGEST OFF DIAGONAL ELEMENT IN EACH ROW
C X(I) CONTAINS LARGEST ELEMENT IN ITH ROW
C IQ(I) HOLDS SECOND SUBSCRIPT DEFINING POSITION OF ELEMENT
C
17 NM1=N-1
  DO 30 I=1,NM1
  X(I) = 0.
  IPL=I+1
  DO 30 J=IPL,N
  IF ( X(I) - DABS( H(I,J))) 20,20,30
20 X(I)=DABS(H(I,J))
  IQ(I)=J
30 CONTINUE
C
C SET INDICATOR FOR SHUT-OFF,RAP=2**-27,NR=NO OF ROTATIONS
RAP=7.450560596E-9
HTEST=1.0E32
C
C FIND MAXIMUM OF X(I) S FOR PIVOT ELEMENT AND
C TEST FOR END OF PROBLEM
C
40 DO 70 I=1,NM1
  IF (I-1) 60,60,45
45 IF ( XMAX- X(I)) 60,70,70
60 XMAX=X(I)
  IPIV=I
  JPIV=IQ(I)
70 CONTINUE
C
C IS MAX. X(I) EQUAL TO ZERO, IF LESS THAN HTEST, REVISE HTEST
IF ( XMAX) 1000,1000,90
90 IF (HTEST) 90,90,95
95 IF (XMAX - HTEST) 90,90,148
90 HDIMIN = DABS( H(I,1) )
  DO 110 I = 2,N
  IF (HDIMIN- DABS( H(I,1))) 110,110,100
100 HDIMIN=DABS(H(I,1))
110 CONTINUE
C
  HTEST=HDIMIN*RAP
C
C RETURN IF MAX.H(I,J)LESS THAN(2**-27)ABS(H(K,K)-MIN)
IF (HTEST- XMAX) 148,1000,1000
148 NR = NR+1
C
C COMPUTE TANGENT, SINE AND COSINE,H(I,I),H(J,J)
150 DM1 = 2.0
  TANG=DBIGN(DM1,(H(IPIV,IPIV)-H(JPIV,JPIV))*H(IPIV,JPIV)/
  *DABS(H(IPIV,IPIV)-
  1H(JPIV,JPIV))-DBQRT((H(IPIV,IPIV)-H(JPIV,JPIV))**2
  2+4.0*H(IPIV,JPIV)**2))
  COSINE=1.0/DBQRT(1.0+TANG**2)
  SINE=TANG*COSINE

```



```

      H11=H(IPIV,IPIV)
      H(IPIV,IPIV)=COSINE**2*(H11-TANG*(2.*H(IPIV,JP1V)+TANG*H(JP1V,JP1V
1)))
      H(JP1V,JP1V)=COSINE**2*(H(JP1V,JP1V)-TANG*(2.*H(IPIV,JP1V)-TANG*H
11))
      H(IPIV,JP1V)=0.
C
C   PSEUDO RANK THE EIGENVALUES
C   ADJUST SINE AND COS FOR COMPUTATION OF H(IK) AND U(IK)
      IF ( H(IPIV,IPIV) - H(JP1V,JP1V) ) 152,153,153
152 HTEMP = H(IPIV,IPIV)
      H(IPIV,IPIV) = H(JP1V,JP1V)
      H(JP1V,JP1V) = HTEMP
C   RECOMPUTE SINE AND COS
      DM1 = 1.0
      HTEMP = DSIGN (DM1, -SINE) * COSINE
      COSINE = DABS (SINE)
      SINE = HTEMP
153 CONTINUE
C
C   INSPECT THE ICS BETWEEN I+1 AND N-1 TO DETERMINE
C   WHETHER A NEW MAXIMUM VALUE SHOULD BE COMPUTED SINCE
C   THE PRESENT MAXIMUM IS IN THE I OR J ROW.
C
      DO 350 I=1,NM1
          IF(I-IPIV)210,350,200
200 IF(I-JP1V)210,350,210
210 IF(IQ(I)-IPIV)230,240,230
230 IF(IQ(I)-JP1V)350,240,350
240 K=IQ(I)
250 HTEMP=H(I,K)
      H(I,K)=0.
      IPL1=I+1
      X(I) =0.
C
C   SEARCH IN DEPLETED ROW FOR NEW MAXIMUM
C
      DO 320 J=IPL1,N
          IF ( X(I) - DABS( H(I,J) ) ) 300,300,320
300 X(I) = DABS(H(I,J))
          IQ(I)=J
320 CONTINUE
      H(I,K)=HTEMP
350 CONTINUE
C
      X(IPIV) =0.
      X(JP1V) =0.
C
C   CHANGE THE OTHER ELEMENTS OF H
C
      DO 530 I=1,N
C
      IF(I-IPIV)370,530,420
370 HTEMP = H(I,IPIV)
      H(I,IPIV) = COSINE*HTEMP + SINE*H(I,JP1V)
      IF ( X(I) - DABS( H(I,IPIV) ) ) 380,390,390
380 X(I) = DABS(H(I,IPIV))
      IQ(I) = IPIV
390 H(I,JP1V) = -SINE*HTEMP + COSINE*H(I,JP1V)
      IF ( X(I) - DABS( H(I,JP1V) ) ) 400,530,530
400 X(I) = DABS(H(I,JP1V))
      IQ(I) = JP1V
      GO TO 530
C
420 IF(I-JP1V)430,530,460
430 HTEMP = H(I,JP1V)
      H(I,JP1V) = COSINE*HTEMP + SINE*H(I,IPIV)
      IF ( X(IPIV) - DABS( H(IPIV,I) ) ) 440,450,450
440 X(IPIV) = DABS(H(IPIV,I))
      IQ(IPIV) = I
450 H(I,IPIV) = -SINE*HTEMP + COSINE*H(I,JP1V)

```

```

      IF ( X(I) - DABS( H(I,JP1V) ) ) 400,530,530
C
480 HTEMP = H(IP1V,1)
      H(IP1V,1) = COSINE*HTEMP + SINE*H(JP1V,1)
      IF ( X(IP1V) - DABS( H(IP1V,1) ) ) 490,500,500
490 X(IP1V) = DABS(H(IP1V,1))
      IQ(IP1V) = 1
500 H(JP1V,1) = -SINE*HTEMP + COSINE*H(IP1V,1)
      IF ( X(JP1V) - DABS( H(JP1V,1) ) ) 510,530,530
510 X(JP1V) = DABS(H(JP1V,1))
      IQ(JP1V) = 1
530 CONTINUE
C
C TEST FOR COMPUTATION OF EIGENVECTORS
C
      IF (IEGEN)40,540,40
540 DO 550 I=1,N
      HTEMP=U(I,IP1V)
      U(I,IP1V)=COSINE*HTEMP+SINE*U(I,JP1V)
550 U(I,JP1V)=-SINE*HTEMP+COSINE*U(I,IP1V)
      GO TO 40
1000 RETURN
      END
      SUBROUTINE RESP (PA,X,PERD,NTIME,NPC,DDT,DAMP)
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      DIMENSION PA(2,1),X(1)
C
C EVALUATION OF MODAL RESPONSE ... USING EXPLICIT INTEGRATION
C
      DM1 = 1.0
      W=8.0*DATA1(DM1)/PERD
      WW=WW*W
      ZW=DAMP*W
      TZW=2.*ZW
      WD=W*DSQRT(1.0-DAMP**2)
      FB=TZW/(WW*WW)
      FA=ZW/WW
      FV=ZW*WW
      FVD=WW*(2.*DAMP**2-1.0)
      FBB=(2.*DAMP**2-1.0)/WW
C
      L=0
      I1=1
      VO=0.
      VDO=0.
      TO=PA(1,1)
10 DT=DDT
50 B=(PA(2,I1+1)-PA(2,I1))/(PA(1,I1+1)-PA(1,I1))
      A=PA(2,I1)+B*(TO-PA(1,I1))
      TT=TO+DT
      IF(PA(1,I1+1).GT.TT) GO TO 100
      DELT=PA(1,I1+1)-TO
      GO TO 200
100 DELT=DT
C
200 EX=DEXP(-ZW*DELT)
      FT=WD*DELT
      CS=DCOS(FT)
      SN=DSIN(FT)
      VT=(VDO+ZW*VO-FA*A+FBB*B)*SN/WD
      VT=VT+(VO-A/WW+FB*B)*CS
      VT=VT*EX+A/WW-FB*B+B*DELT/WW
C
      VDT=(A-WW*VO-ZW*(VDO-B/WW))*SN/WD
      VDT=EX*((VDO-B/WW)*CS+VDT)+B/WW
C
      VDDT=(B+FV*VO+FVD*VDO-ZW*A)/WD
      VDDT=EX*((A-WW*VO-TZW*VDO)*CS+VDDT*SN)
C
      VO=VT

```

```
VDD=VDT
```

```
IF(PA(1,11+1).GT.TT) GO TO 500
DT=DT-DELT
I1=I1+1
TO=PA(1,I1)
IF( DABS(DT).LT.1.0D-10 ) GO TO 600
GO TO 50
```

```
C
```

```
500 TO=TO+DT
600 L=L+1
X(L)=VT
IF(L.LT.NTIME) GO TO 10
```

```
C
```

```
RETURN
END
SUBROUTINE LOAD(XM,NLD,NPT)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION XM(10,NLD)
```

```
C
```

```
WRITE (NPT,2000)
DO 100 L=1,NLD
READ(5,1000) ( XM(I,L),I=1,10 )
100 WRITE(NPT,2001) L,( XM(I,L),I=1,10 )
WRITE (NPT,2002)
RETURN
```

```
C
```

```
1000 FORMAT( 5F10.0,5F5.0 )
2000 FORMAT ( //,32H LOAD CONDITION DEFINITION CARDS //,5H0LOAD ,11X,
1 1H1,10X,2H11,9X,3H111,11X,1HA,11X,1HB,12H SPECTRUM-1,12H SPECT
1RUM-2,12H SPECTRUM-3,12H SPECTRUM-4,12H TIME HIST )
2001 FORMAT( 15,10F12.2 )
2002 FORMAT ( ///,43H SPECTRUM-1... ROOT MEAN SQUARE COMBINATION //,
1 37H SPECTRUM-2... SUM OF ABSOLUTE VALUES //,
2 37H SPECTRUM-3... DOUBLE SUM COMBINATION //,
3 45H SPECTRUM-4... COMPLETE QUADRATIC COMBINATION )
```

```
C
```

```
END
SUBROUTINE DISP (SD,R,D,RF,A,MBS,MTF,MLD,MBT,NFS,HED)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION SD(MBT,8),R(MBS,MLD),D(MBT,MTF,2),RF(NFS,MLD),A(MTF,5)
1 ,HED(MTF,4)
COMMON/GEN/ IFIL(24),RLAB(3),IB,IC,BFIL(6)
COMMON/BUNK/ AI(3,3),AJ(3,5),AFIL(236)
CHARACTER*4 HED,RLAB
```

```
C
```

```
C COMPUTE FRAME DISPLACEMENTS FROM STRUCTURE DISPLACEMENTS
```

```
C
```

```
READ(2) A,D,HED
REWIND 2
DO 500 K=1,MTF
I=MTF+1-K
DO 25 L=1,3
DO 25 J=1,3
25 AI(L,J)=0.
```

```
C
```

```
IF=A(1,1)
IFC=A(1,2)
AI(1,1)=A(1,3)
AI(1,2)=A(1,4)
AI(2,2)=AI(1,1)
AI(2,1)=-AI(1,2)
NT=A(1,5)
AI(3,3)=1.
NB=MBT+1-NT
NFR=NB*3
DO 300 N=NT,MBT
NN=(N-1)*13
N1=(N-NT)*3
```

```

      AI( 1,3)=D(N,1,1)
      AI( 2,3)=D(N,1,2)
      DO 225 IJ=1,3
      DO 225 L=1,MLD
      RF(N1+IJ,L)=0.
      DO 225 KK=1,13
      K1=KK+18
225 RF(N1+IJ,L)=RF(N1+IJ,L)+AI(IJ,K1)*R(NH+KK,L)
300 CONTINUE
C
      WRITE (2) IF,IFC,NFR,((RF(N,L),N=1,NFR),L=1,MLD),(MED(I,J),J=1,4)
500 CONTINUE
C
      RETURN
      END
      SUBROUTINE FRAME( MTOT,NMD,NFB,KODE,ICHEK,NPT,TANORM,TNORM,TDIS
1          ,ILP,ITYPE )
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      COMMON /CNTR/ A(26000)
      COMMON/GEN/ NBT,NCF,NTF,NLD,NAT,NFQ,KFIL(18),RLAB(3),IS,IS,
1          AFIL(6)
      COMMON/ DYN / NTIME,DT,NPC,DAMP
      COMMON/JUNK/ FHED(4),IF,IFC,IFIL,II,JFIL(62)
      COMMON/STIF/ ASA(12,12),BA(8,12),T(8,12)
      CHARACTER*4 FHED,RLAB
C
C      OUTPUT DISPLACEMENTS AND FORCES
C
      N0=1+3*NBT
      IF( NAT.EQ.3 ) N0 = 1 + 9*NBT + 2*NFO*NFO
      IF( ICHEK.EQ.0 ) CALL LOAD( A(N0),NLD,NPT )
      REWIND 2
      KO=0
      M=0
      MLD=5+NFO
      IF (NAT.EQ.4) MLD=5+NTIME
C---- M1, M2 = LOCATIONS OF DBC + CDC MATRICES
      M1 = 1 + 9*NBT
      M2 = M1 + NFO*NFO
      N1 = N0 + 10*NLD
      NBK = 1
C
      DO 500 I=1,NTF
      IF( ICHEK.NE.0 ) GO TO 100
      II=NTF+1-I
      IF ( ITYPE .EQ. 1 ) THEN
          NPT = 18
      ENDIF
      CALL SORT( A(N1),A(N0),A(M1),A(M2),NFB,NLD,MLD,NAT,NMD,NFR,NFO
1          ,TANORM,TNORM,TDIS,NPT )
      IF(IF.EQ.M) GO TO 200
      IF(KO.EQ.0) GO TO 100
      IF(KO.NE.1) GO TO 100
C
      DO 50 K=1,NBK
50 BACKSPACE 3
C
      100 BACKSPACE 3
      READ (3) M,NC,NS,NCP,NBP,NFEF,NPAN,NTRJ,NB
      NBK8=2*NB
      BACKSPACE 3
      IF( ICHEK.NE.0 ) GO TO 300
      KO=1
      200 IF(IFC.NE.0) GO TO 500
      IF(KO.NE.2) GO TO 300
C
      DO 250 K=1,NBK8
250 READ (3) XX
C
      300 CALL SECOND (TB)

```

```

MM=3*NC
NN=8*NC+3*NB+3
N2=N1+NFB*MLD
N3=N2+NC*2
N4 = N3 + 14*NCP
N5 = N4 + 11*NBP
N6=N5+7*NFEF
N7=N6+NB*NS*3
N8=N7+NS*NB*3
N9=N8+NB*NC*2
N10=N9+3*NPAN
LB=(MM*(MM+1))/2
LC=MM*MM
LE=MM*(3*NS+3)
LKH=NN
N11=N10+LB+LE+LC+LKH
N12=N11+NN*MLD
N13=N12+NFEF
N14=N13+5*NPAN
N15=N14+8*NFO
N16=N15+3*NTRU
N17 = N16 + 3*NTRU
IF(N17.GT.MTOT) CALL MEMORY (N17-MTOT)
IF( ICHK EQ 0 ) GO TO 450
IF( NAT.NE.4 ) WRITE(6,3000) N17
N18 = NN + NFB
IF( NAT.EQ.4 ) WRITE(6,3001) N17,N18
GO TO 460
450 CONTINUE
N = 1+NST
CALL OUTPUT(A(1),A(N),A(N0),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),
1A(N7),A(N8),A(N9),A(N10),A(N11),NST,NB,NC,NCP,NBP,NS,NFEF,MPAN,
2A(N12),A(N13),NN,MM,NLD,MLD,KO,A(N14),NMD,A(N15),A(N16),NTRU,NFR,
3NFB,NFO,A(M1),A(M2),KODE,ILP,NPT )
460 CALL SECOND( TE )
TE=TE-TS
11=NTF+1-1
C WRITE (6,2000) 11,TE
KO =2
500 NBK=NBKS+1
C
RETURN
2000 FORMAT ( /,12H ...FRAME NO 13,3H... /
1 4X,36H TIME REQUIRED FOR STRESS COMPUTATION = F6.2)
3000 FORMAT( /,10X,53H * ROUTINE OUTPUT ( ELEMENT FORCES ) REQUIRES MTO
1T = ,16, / )
3001 FORMAT( /, 53H * ROUTINE OUTPUT ( ELEMENT FORCES ) REQUIRES MTO
1T = ,16,3H + ,16,31H X (NO.TIME STEPS TO BE USED) )
END
SUBROUTINE SORT( U,%M,DSC,CCO,NFB,NLD,MLD,NAT,NMD,NFR,NFO
1 ,TANORM,THORM,TD18,NPT )
C
IMPLICIT REAL*8 (A-M)
IMPLICIT REAL*8 (O-Z)
DIMENSION HDM(6),LNUM(6)
DIMENSION DNUM(6)
DIMENSION U(NFB,MLD),%M(10,NLD),DSC(NFO,NFO),CCO(NFO,NFO)
COMMON /JUNK/FHED(4),IF,IFC,NB,NFRM,IFIL(62)
COMMON /BUNK/ UU(6,3),UMIN(6,3),AFIL(212)
COMMON/GEN/ JFIL(24),RLAB(3),IB,13,BFIL(6)
COMMON/DYN/NTIME,DT,NPC,DAMP
CHARACTER*4 FHED,RLAB
CHARACTER*3 HT,HD1,HD2
CHARACTER*1 HDM
DATA HT/'DT=' /
DATA HD1,HD2/'MAX','MIN' /
C
C LOAD CASE COMBINATION AND OUTPUT OF DISPLACEMENTS
C
READ (2) IF,IFC,NFR,((U(N,L),N=1,NFR),L=1,MLD),FHED
IF (IFC.NE.0) GO TO 600

```

```

C
  LLD=NLD+NMD
  DO 500 LL=1,LLD,8
  LH=LL+7
  IF (LH.GT.LLD) LH=LLD
  IH=LH+1-LL
  WRITE (NPT,2000) NFRM,IF,FHED
  IF (NAT.GE.3) WRITE(6,3000)
  IF (NMD.GT.0) WRITE(6,3001)
  DO 80 L=LL,LH
  LNUM(L+1-LL)=L
  HDM(L+1-LL)='H'
  IF (L.LE.NLD) GO TO 80
  LNUM(L+1-LL)=L-NLD
  HDM(L+1-LL)='M'
80  CONTINUE
  WRITE (NPT,2001) (HDM(I),LNUM(I),I=1,IH)
C
C  STATIC DISPLACEMENT COMPONENTS
C
  NB=NFR/3
  DO 400 N=1,NB
  NL=NB+1-N
  DO 400 I=1,3
  NV=(N-1)*3+I
  DO 100 L=LL,LH
  I=L-LL+1
  UU(I,I)=0
  DO 100 J=1,5
100  UU(I,I)=UU(I,I)+U(NV,J)*XM(J,L)
  IF (NAT.GE.3) GO TO 150
  IF (N.EQ.1) THEN
  IF (I.EQ.1) THEN
    TNORM1 = UU(1,1)-TDIB
    TNORM2 = (TNORM1*TNORM1)/(UU(1,1)*UU(1,1))
    TNORM = DBQRT(TNORM2)
C    WRITE (6,*) 'UU(1,1) = ',UU(1,1)
C    WRITE (6,*) 'TDIB = ',TDIB
C    WRITE (6,*) 'TNORM = ',TNORM
    IF (TNORM.LE.TANORM) THEN
      WRITE (6,2101)
      NPT = 6
    ENDIF
    TDIB = UU(1,1)
  ENDIF
  ENDIF
  WRITE (NPT,2002) NL,RLAB(I),(UU(I,I),I=1,IH)
  GO TO 400
C
C  DYNAMIC DISPLACEMENT COMPONENTS
C
150  NAT=NAT-3
  S1=0.
  S2=0.
  TH=0.
  DO 200 I=6,MLD
  UA=DABS(U(NV,I))
  IF (NATT) 180,160,180
160  S1=S1+UA*UA
  S2=S2+UA
  GO TO 200
180  IF (UA.GT.TH) TH=UA
200  CONTINUE
  S1=DBQRT(S1)
  S3 = 0.0
C---- CHECK IF DBC CALC REQD
  IF( (DBC(1,1).LT.0.0) .OR. (NAT.NE.3) ) GO TO 210
C---- DBC COMBO
  DO 202 I=1,NFQ
  X = U(NV,I+5)
  DO 202 J=1,NFQ

```

```

202 B3 = B3 + X*DBC(I,J)*U(NV,J+5)
      B3 = DBSQRT( B3 )
210 B4 = 0.0
C---- CHECK IF CGC COMBO REQD
      IF( (CGC(1,1).LT.0.0) .OR. (NAT.NE.3) ) GO TO 216
      DO 212 I=1,NFO
        X = U(NV,I+5)
      DO 212 J=1,NFO
212 B4 = B4 + X*CGC(I,J)*U(NV,J+5)
      B4 = DBSQRT( B4 )
216 DO 250 L=LL,LH
      I=L-LL+1
      IF (L.GT.NLD) GO TO 220
      UD = B1*M(6,L) + B2*M(7,L) + B3*M(8,L) + B4*M(9,L) +
      1 TH*M(10,L)
      UMIN(I,1)=UU(I,1)-UD
      UU(I,1)=UU(I,1)+UD
      GO TO 250
220 UMIN(I,1)=U(NV,L+5-NLD)
      UU(I,1)=UMIN(I,1)
250 CONTINUE
      WRITE (6,2003) NL,HD1,RLAB(1), (UU(I,1), I=1,1H)
      WRITE (6,2004) HD2,RLAB(1), (UMIN(I,1), I=1,1H)
      IF (11.EQ.3) WRITE (6,2114)
400 CONTINUE
500 CONTINUE
C PRINT OF TIME HISTORY DISPLACEMENTS
C
      IF (NAT.NE.2) GO TO 600
      WRITE (6,2005)
      DO 700 LL=6,MLD,8
        LH=LL+7
        IF (LH.GT.MLD) LH=MLD
        IH=LH+1-LL
        DO 660 L=LL,LH
          DNUM(L+1-LL)=(L-5)*DT
660 HDM(L+1-LL)=HT
          WRITE (6,2006) (HDM(I),DNUM(I), I=1,1H)
C
      DO 870 N=1,NB
        NL=NB+1-N
        DO 870 I=1,3
          NV=(N-1)*3+1
          DO 865 L=LL,LH
            I=L-LL+1
            UU(I,1)=U(NV,L)
865 CONTINUE
          WRITE (6,2003) NL,HD1,RLAB(1), (UU(I,1), I=1,1H)
870 CONTINUE
C
700 CONTINUE
C
800 RETURN
C
2000 FORMAT (//,24H ...OUTPUT FOR FRAME NO 13,4H ... ,//
1 10X,12HFRAME TYPE = 13/10X,12HFRAME ID ,7A4,//
2 32H0 ..LATERAL FRAME DISPLACEMENTS... )
2001 FORMAT (//,6H LEVEL,7X,8(11X,A1,I2))
2002 FORMAT (16,4X,A4,5X,8F14.7)
2003 FORMAT (16,2X,A3,1X,A4,2X,(8F14.7))
2004 FORMAT (8X,A3,1X,A4,2X,8F14.7)
2005 FORMAT (23H TIME HISTORY RESPONBE )
2006 FORMAT (13X,8(5X,A3,F6.3))
3001 FORMAT (//,45H CONTRIBUTION TO SPECTRAL RESPONSE FROM EACH ,/,
1 80H INDIVIDUAL MODE LISTED UNDER HEADINGS M 1 M 2 ETC
2 )
2114 FORMAT (1H )
3000 FORMAT (//,23H MAX...STATIC + DYNAMIC /
1 23H MIN...STATIC - DYNAMIC )
2101 FORMAT (///,T10,'FRAME DISPLACEMENT',/,T3,'LEVEL')
      END

```

```

END
SUBROUTINE BKSUB (B,C,E,LS,MM,NNM,R,NN,MLD,KH)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION B(LS),C(MM,MM),E(MM,NNM),R(NN,MLD),KH(NN)
C
C   COMPUTE FRAME DISPLACEMENTS AT ONE LEVEL
C
NBKS=3
BACKSPACE NBKS
BACKSPACE NBKS
READ (NBKS) B,C
READ (NBKS) E,((R(I,J),I=1,MM),J=1,3),KH
BACKSPACE NBKS
BACKSPACE NBKS
MM=2*MM
MMP=MM+1
DO 400 L=1,MLD
DO 300 J=MMP,NN
KF=KH(J)
IF (KF.GT.MM) GO TO 300
IF (J.GT.NN) GO TO 250
DO 240 K=KF,MM
240 R(K,L)=R(K,L)-C(K,J-MM)*R(J,L)
GO TO 300
250 DO 260 K=KF,MM
260 R(K,L)=R(K,L)-E(K,J-MM)*R(J,L)
300 CONTINUE
IB=LS
DO 400 I=1,MM
I=MM+1-I
KK=I-1
KF=KH(I)
IB=IB-1
IF (KF.GT.KK) GO TO 400
DO 340 K=KF,KK
340 R(K,L)=R(K,L)-B(IB+K)*R(I,L)
400 CONTINUE
RETURN
END
SUBROUTINE STRESS( R,MM,NN,MLD,MLD,M,FM,NMD,NFQ,DBC,CGC,KODE,A,
1 NFF,VRR,NREC,B1,ILP,NPT )
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION R(NN,MLD),MM(10,NLD),FM(8,NFQ),DBC(NFQ,NFQ),CGC(NFQ,NFQ)
1 ,A(1)
COMMON/JUNK/ FHED(4),IF,IFC,ND,NF,LM(12),FIL(50)
COMMON/BUNK/ F(8,10),Q(3,3),P(10),PMIN(10),AFIL(151)
COMMON/GEN/ JFIL(4),NAT,KFIL(24),BFIL(6)
COMMON/STIF/ ABA(12,12),BA(8,12),T(8,12)
CHARACTER*3 HD1,HD2
CHARACTER*4 FHED
DATA HD1,HD2 / 'MAX', 'MIN' /
C
C   LOAD CASE COMBINATION AND OUTPUT OF MEMBER FORCES
C
LLD=NLD+NMD
DO 100 I=1,NF
DO 100 J=1,8
100 F(I,J)=0.0
IF(NF.NE.3) GO TO 150

```



```

      DO 120 L=1,3
      F(2,L)=Q(1,L)
    120 F(3,L)=Q(2,L)
C
C   CALCULATE STATIC FORCES
C
    150 DO 200 K=1,ND
      KK=LM(K)
      DO 200 I=1,NF
      DO 200 J=1,5
    200 F(I,J)=F(I,J)+SA(I,K)*R(KK,J)
C
C   CALCULATE DYNAMIC FORCES
C
      NATT=NAT-3
      IF( NATT ) 550,250,512
    250 DO 500 I=1,NF
      DO 400 J=6,MLD
      X=0.0
      DO 300 K=1,ND
      KK=LM(K)
    300 X=X+SA(I,K)*R(KK,J)
      FM(I,J-5) = X
    400 CONTINUE
    500 CONTINUE
C
C---- RESPON SPEC MODAL COMBO
C
      DO 502 K=1,NF
      X1 = 0.0
      X2 = 0.0
      DO 501 I=1,NFQ
      X = FM(K,I)
C---- BRBS
      X1 = X1 + X*X
C---- ABS
    501 X2 = X2 + DABS( X )
      F(K,6) = DSQRT( X1 )
      F(K,7) = X2
      F(K,8) = 0.0
    502 F(K,9) = 0.0
C---- CHECK IF DSC COMBO RECD
      IF( DSC(1,1) .LT. 0.0 ) GO TO 506
      DO 505 K=1,NF
      X1 = 0.0
      DO 504 I=1,NFQ
      X = FM(K,I)
      DO 504 J=1,NFQ
    504 X1 = X1 + X*DSC(I,J)*FM(K,J)
    505 F(K,8) = DSQRT( X1 )
C---- CHECK IF ODC COMBO RECD
    506 IF( ODC(1,1) .LT. 0.0 ) GO TO 550
      DO 510 K=1,NF
      X1 = 0.0
      DO 508 I=1,NFQ
      X = FM(K,I)
      DO 508 J=1,NFQ
    508 X1 = X1 + X*ODC(I,J)*FM(K,J)
    510 F(K,9) = DSQRT( X1 )
      GO TO 550
C
C---- TIME HIST
C
    512 DO 520 I=1,NF
      F(I,10) = 0.0
      DO 520 J=6,MLD
      X = 0.0
      DO 515 K=1,ND
      KK = LM(K)
    515 X = X + SA(I,K)*R(KK,J)
      XA = DABS( X )

```

```

      IF( XA.GT.F(1,10) ) F(1,10) = XA
520 CONTINUE
C
C   PRINT MEMBER FORCES FOR ALL LOAD CONDITIONS
C
550 DO 700 L=1,LLD
C   STATIC FORCE COMPONENTS
      DO 600 I=1,NF
        P(I)=0.
        DO 600 J=1,5
600 P(I)=P(I)+F(I,J)*XM(J,L)
        IF (NF.NE.8) GOTO 605
        IF (ILP.NE.1) THEN
          IK = LM(1)
          IKK = LM(7)
          VRT = R(IK,4)*XM(4,L)+R(IK,5)*XM(5,L)
          VRB = R(IKK,4)*XM(4,L)+R(IKK,5)*XM(5,L)
          IF (B1.GT.0.0) THEN
            P(7) = (P(2)+P(3)+(P(4)*(VRT-VRB)))/VRR
          ELSE
            P(7) = (P(2)+P(3)-(P(4)*(VRT-VRB)))/VRR
          ENDIF
        ENDIF
C
C   WRITE (6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
C   WRITE (6,*) 'SUBROUTINE STRESS'
C   WRITE (6,*) 'JUST CAL. AXIAL IN COL. = ',P(4)
C   WRITE (6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
      WRITE (15,REC = NREC) P(4)
C
605 IF (NF.NE.4) GOTO 606
      IF (ILP.NE.1) THEN
        IK = LM(1)
        IKK = LM(6)
        VRT = R(IK,4)*XM(4,L)+R(IK,5)*XM(5,L)
        VRB = R(IKK,4)*XM(4,L)+R(IKK,5)*XM(5,L)
        IF (B1.GT.0.0) THEN
          P(4) = (P(1)+P(2)+(P(3)*(VRT-VRB)))/VRR
        ELSE
          P(4) = (P(1)+P(2)-(P(3)*(VRT-VRB)))/VRR
        ENDIF
      ENDIF
C
C   WRITE (6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
C   WRITE (6,*) 'SUBROUTINE STRESS'
C   WRITE (6,*) 'JUST CAL. AXIAL IN PANEL = ',P(3)
C   WRITE (6,*) '!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!'
      WRITE (15,REC = NREC) P(3)
C
606 IF(NATT) 610,620,620
C---- CALC STRESS RATIOS IF REQUESTED
610 IF( KODE.NE.0 ) CALL CODE( P,A,NFF )
      IF ( NFF .EQ. 8 ) THEN
        WRITE ( NPT,2003 ) M,L,P(2),P(3),P(4),P(7)
      ELSEIF ( NFF .EQ. 3 ) THEN
        WRITE ( NPT,2003 ) M,L,P(2),P(3)
      ELSEIF ( NFF .EQ. 4 ) THEN
        WRITE ( NPT,2003 ) M,L,P(1),P(2),P(3),P(4)
      ELSE
        WRITE(NPT,2000) M,L,( P(I),I=1,NFF )
      ENDIF
      GO TO 700
C   DYNAMIC FORCE COMPONENTS
620 DO 650 I=1,NF
      IF (L.GT.NLD) GO TO 640
      P1=F(1,6)*XM(6,L)+F(1,7)*XM(7,L)+F(1,8)*XM(8,L)
        + F(1,9)*XM(9,L) + F(1,10)*XM(10,L)
      PMIN(I)=P(I)-P1
      P(I)=P(I)+P1
      GO TO 650
640 PMIN(I)=PM(I,L-NLD)
      P(I)=PMIN(I)
650 CONTINUE

```

```
      IF( KODE.LE.0 ) GO TO 652
C---- CALC STRESS RATIOS
      CALL CODE( P,A,NFF )
      CALL CODE( PMIN,A,NFF )
      652 WRITE(6,2001) M,L,HD1,( P(I),I=1,NFF )
          WRITE(6,2002) L,HD2,( PMIN(I),I=1,NFF )
      700 CONTINUE
C
      RETURN
C
      2003 FORMAT( 2I6,5X,4F16.7 )
      2001 FORMAT( 2I6,2X,A3,8F12.4,2F6.2 )
      2002 FORMAT( 6X,16,2X,A3,8F12.4,2F6.2 )
      END
```

```

SUBROUTINE OUTPUT(BN,SD,XM,U,CLN,CP,BP,FEF,LB,LDB,LC,LP,B,R,NST,
1 NB,NC,NCP,NBP,NB,NFEF,NPAN,IFEF,PP,NN,MM,NLD,MLD,KO,FM,NND,LT,
2 TP,NTRU,NFR,NFS,NFQ,DBC,OCQ,KODE,ILP,NPT)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION CLN(NC,2),CP(14,NCP),BP(11,NBP),FEF(7,NFEF),SD(NST,2),
1 LB(NS,NB,3),LDB(NS,NB,3),LC(NS,NC,2),LP(3,NPAN),IFEF(NFEF),PP(5,N
2PAN),B(1),R(NN,MLD),U(NFS,MLD),XM(10,NLD),LT(3,NTRU),TP(3,NTRU)
3 ,DBC(NFQ,NFQ),OCQ(NFQ,NFQ),BN(NST)

```

C

```

COMMON/JUNK/ FHED(4),IF,IFC,ND,NF,LM(12),IFIL(80)
COMMON/BUNK/ F(8,10),Q(3,3),P(10),PMIN(10),AFIL(151)
COMMON/BTIF/ ABA(12,12),BA(8,12),T(8,12)
CHARACTER*4 FHED,BN

```

C

C SET FOUNDATION DISPLACEMENTS AND LATERAL DISPLACEMENTS

C

```

IF(KO.EQ.2) GO TO 50
BACKSPACE 3
READ (3)CLN,CP,BP,FEF,LB,LDB,LC,LP,IFEF,PP,LT,TP
BACKSPACE 3

```

50 MN=8*NC

DO 475 L=1,MLD

DO 425 K=1,MM

425 R(K,L)=0.0

DO 450 N=1,NFR

KK=MM+N

KM=MM+NFR

450 R(KK,L)=U(N,L)

DO 475 I=1,3

475 R(KM+I,L)=0.

C

C STORY BY STORY CALCULATION OF MEMBER FORCES

C

N=NB

C

C CALCULATE ROTATIONS AND VERTICAL DISPLACEMENT AT LEVEL N

C

300 CONTINUE

NNM=NN-2*MM

KC=(MM*(MM+1))/2

KE=MM*MM+KC

KQH=MM*NNM+KE

CALL BKSUB(B(1),B(KC+1),B(KE+1),KC,MM,NNM,R,NN,MLD,B(KQH+1))

C

C CALCULATE COLUMN FORCES

C

LV=NB -N+1

K=NST-NB

WRITE (NPT,2000) FHED,IF,LV,BN(N+K)

WRITE(NPT,2007)

IF(KODE.EQ.0) WRITE(NPT,2001)

IF(KODE.NE.0) WRITE(NPT,3001)

NF=8

NFF = 8

IF(KODE.NE.0) NFF = 10

ND=12

DO 500 M=1,NC

MC=LC(N,M,1)

IF(MC.EQ.NCP) GO TO 510

XL =SD(N+K,2)

KK=LC(N,M,2)

B1=CLN(KK,1)-CLN(M,1)

B2=CLN(KK,2)-CLN(M,2)

B3=B1*B1+B2*B2

B3=DSQRT(B3)

IF(B3.LE.0.) STOP1

CSA=B1/B3

SMA=B2/B3

XL1=CLN(M,1)

YL1=CLN(M,2)

```

NREC = NC*(N-1)+M
READ (15,REC = NREC) VVP
C :WRITE (6,*) '#####'
C WRITE (6,*) 'SUBROUTINE OUTPUT'
C WRITE (6,*) 'STORY NO. ',N
C WRITE (6,*) 'COLUMN LINE NO. ',M
C WRITE (6,*) 'AXIAL IN COLUMN = ',VVP
C WRITE (6,*) '#####'
CALL COLUMN(2,MC,XL,SNA,CBA,NCP,XL1,YL1,CP,VVP)
C
LM(6)=3*M
LM(5)=LM(6)-1
LM(4)=LM(5)-1
LM(11)=LM(5)+MM
LM(10)=LM(4)+MM
LM(12)=LM(6)+MM
LM(3)=MM+3*N
LM(2)=LM(3)-1
LM(1)=LM(2)-1
LM( 9)=LM(3)+3
LM(8)=LM( 9)-1
LM(7)=LM(8)-1
VR = XL-CP(8,MC)-CP(9,MC)
CALL STRESS( R,MM,NN,NLD,MLD,M,FM,NMD,NFQ,DSG,OCG,KODE,CP(1,MC),
1 NFF,VR,NREC,B1,IUP,NPT )
GO TO 490
510 WRITE(6,2009) M
490 GO TO 500
500 CONTINUE
C
C CALCULATE BEAM FORCES
C
IF(NB.EQ.0) GO TO 565
WRITE(NPT,2008)
IF( KODE.EQ.0 ) WRITE(NPT,2002)
IF( KODE.NE.0 ) WRITE(NPT,3002)
NF=3
NFF = 3
IF( KODE.NE.0 ) NFF = 5
ND=8
DO 600 M=1,NB
MB=LB(N,M,3)
IF(MB.EQ.NBP) GO TO 515
K1=LB(N,M,1)
KJ=LB(N,M,2)
B1=CLN(KJ,1)-CLN(K1,1)
B2=CLN(KJ,2)-CLN(K1,2)
B3=B1*B1+B2*B2
B3=DBQRT (B3)
CBA=B1/B3
SNA=B2/B3
XL=B3
XLR=XL-BP(8,MB)-BP(9,MB)
CALL BEAM (2,MB,XL,SNA,CBA,NBP,BP)
C
LM(3)=3*K1
LM(2)=LM(3)-1
LM(1)=LM(2)-1
LM( 8)=3*KJ
LM( 5)=LM( 8)-1
LM(4)=LM( 5)-1
DO 540 L=1,3
DO 528 I=1,2
528 Q(I,L)=0.
J=LDB(N,M,L)
IF (J) 540,540,530
530 V=FEF(5,J)*XLR/2.
YM=V*XLR/8.
Q(1,L)= FEF(1,J)+YM
Q(2,L)=-FEF(3,J)-YM
540 Q(3,L)=0.0

```

```

CALL STRESS( R,MM,NN,NLD,MLD,M,FM,MMD,NFQ,DBC,CGC,KODE,BP(1,MB),
1      NFF,0.0,0.0,0.0,ILP,NPT )
GO TO 590
515 WRITE(6,2010) M
590 GO TO 800
800 CONTINUE
C
C   CALCULATE PANEL FORCES
C
IF(NPAN.EQ.0) GO TO 585
DO 770 L=1,NPAN
NP=NB-LP(1,L)+1
IF (NP.NE.N) GO TO 770
GO TO 772
770 CONTINUE
GO TO 585
772 WRITE(NPT,2004)
LNF=0
ND=10
DO 800 L=1,NPAN
NF=4
NP=NB-LP(1,L)+1
IF(NP.NE.N) GO TO 800
IF(PP(3,L).GT.0.) GO TO 780
NF=2
780 IF(LNF.EQ.NF) GO TO 790
IF(NF.EQ.2) WRITE(NPT,2011)
IF(NF.EQ.4) WRITE(NPT,2003)
LNF=NF
790 XL=SD(N+K,2)
KI=LP(2,L)
M=KI
KJ=LP(3,L)
B1=CLN(KJ,1)-CLN(KI,1)
B2=CLN(KJ,2)-CLN(KI,2)
B3=B1*B1+B2*B2
B3=DBQRT (B3)
CSA=B1/B3
SMA=B2/B3
AR=CLN(KI,1)*CLN(KJ,2)-CLN(KJ,1)*CLN(KI,2)
DF=AR/B3
D=B3
NREC = NC*NB+L
READ (15,REC = NREC) VVP
C   WRITE (6,*) '#####'
C   WRITE (6,*) 'SUBROUTINE OUTPUT'
C   WRITE (6,*) 'STORY NO. ',N
C   WRITE (6,*) 'PANEL NO. ',L
C   WRITE (6,*) 'AXIAL IN PANEL = ',VVP
C   WRITE (6,*) '#####'
CALL PANEL( 2,L,XL,D,DF,SMA,CSA,NPAN,PP,VVP)
C
LM(3)=MM+3*N
LM(2)=LM(3)-1
LM(1)=LM(2)-1
LM(4)=3*KI
LM(5)=3*KJ
LM(8)=MM+3*N+3
LM(7)=LM(8)-1
LM(6)=LM(7)-1
LM(9)=MM+3*KI
LM(10)=MM+3*KJ
CALL STRESS( R,MM,NN,NLD,MLD,M,FM,MMD,NFQ,DBC,CGC,KODE,DLM,NF,
1      XL,NREC,B1,ILP,NPT )
C   WRITE (6,2005)
800 CONTINUE
C
585 IF (NTRU.EQ.0) GO TO 690
DO 850 L=1,NTRU
NP=NB-LT(1,L)+1
IF(NP.NE.N) GO TO 650

```

```

      IF( KODE.EQ.0 ) WRITE(6,2006)
      IF( KODE.NE.0 ) WRITE(6,3006)
      GO TO 660
650 CONTINUE
      GO TO 690
680 NF=1
      NFF = 1
      IF( KODE.NE.0 ) NFF = 2
      ND=B
      DO 680 L=1,NTRU
      NP=NB-LT(1,L)+1
      IF (NP.NE.N) GO TO 680
      KJ=LT(2,L)
      MY=KJ
      KI=LT(3,L)
      B1=CLN(KJ,1)-CLN(KI,1)
      B2=CLN(KJ,2)-CLN(KI,2)
      B3=B1*B1+B2*B2
      B3=DSQRT (B3)
      CSA=B1/B3
      SNA=B2/B3
      YL=SD(N+K,2)
      DL=DSQRT (B3*B3+YL*YL)
      VANG=ATAN(YL/B3)
      AR=CLN(KI,1)*CLN(KJ,2)-CLN(KJ,1)*CLN(KI,2)
      D1=AR/B3
      CALL DIAG(2,L,VANG,DL,SNA,CSA,NTRU,D1,TP)
C
      LM(3)=MN+3*N
      LM(2)=LM(3)-1
      LM(1)=LM(2)-1
      LM(4)=3*KJ
      LM(7)=MN+3*N+3
      LM(6)=LM(7)-1
      LM(5)=LM(6)-1
      LM(8)=3*KI+MM
      CALL STRESS( R,MM,MN,MLD,MLD,MY,FM,NMD,NFQ,DBC,CCG,KODE,TP,NFF,
1      0.0,0.0,0.0,1LP,NPT )
      WRITE (6,2005)
680 CONTINUE
C
C   SHIFT DISPLACEMENTS
C
690 DO 570 K=1,MM
      KK=MM+K
      DO 570 L=1,MLD
      R(KK,L)=R(K,L)
570 R(K,L)=0.0
C
610 N=N-1
      IF (N.NE.0) GO TO 300
C
610 RETURN
C
2000 FORMAT(//,1H ,21H MEMBER FORCES ..... ,9HFRAME ID ,A4,10X,10HFRAM
1E TYPE , 13/,T23,9HLEVEL NO,13,T58,9HLEVEL ID ,A4)
2001 FORMAT(T3,4HLINE,T9,4HLOAD,T24,10HTOP MOMENT,T40,10HBOT MOMENT,
1 T55,11HAXIAL FORCE,T71,11HSHEAR FORCE)
3001 FORMAT(//,1H ,2X,9HLINE LOAD, 9X,9HTORSIONAL,9X,10HMAJOR AXIS,11X,
1 5HAXIAL,10X,10HMINOR AXIS,11X,5HMAJOR,7X, 5HMINOR,1X,5HRATIO,1X,
2 5HRATIO ,/,
3 23X,8HMOMENT,4X,10HTOP MOMENT,2X,10HBOT MOMENT,5X,5HFORCE,4X,
4 10HTOP MOMENT,2X,10HBOT MOMENT,5X,5HSHEAR,7X,5HSHEAR,2X,3HTOP,
5 3X,3HBOT )
2002 FORMAT(T4,3HBAY,T9,4HLOAD,T26,8HI MOMENT ,T42,8HJ MOMENT)
3002 FORMAT( 12H BAY LOAD, 6X,11HTORS MOMENT, 5X, 9HI MOMENT,
1 3X, 9HJ MOMENT, 3X, 9HI RATIO , 3X, 9HJ RATIO )
2003 FORMAT(T2,5HI COL,T9,4HLOAD,T24,10HTOP MOMENT,T40,10HBOT MOMENT,
1 T55,11HAXIAL FORCE,T71,11HSHEAR FORCE)
2004 FORMAT(/,13H PANEL FORCES)
2005 FORMAT (1H )

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SUBROUTINE OPT6(D,R,XM,W,DSC,CQC,KOD,BN,A,BC,B,Z,MBS,MST,NFQ,NMD,
1 13,18,GRAY)
C-----
C  ROUTINE TO PERFORM RESPONSE SPECTRUM OPTION 6 CALCULATIONS
C-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION D(MBS,NFQ),R(MBS,4),XM(MBS),W(NFQ),DSC(NFQ,NFQ),
1 CQC(NFQ,NFQ),KOD(5),A(MBT,1),RLAB(6),NAM(4),BC(2),B(MBS,MBS),
2 Z(MBS,NFQ),BN(MBT)
CHARACTER*4 NAM,RLAB
DATA NAM /'BRSS','DSC','CQC','ABS'/
DATA RLAB /'X','Y','ROTN','R','S','ROTN'/
C
C---- D = MODAL DISP, INERTIA FORCES, SHEARS, OTM
C  R = ARRAY TO COLLECT COMBINED MODAL RESPONSES
C  XM = MASS ARRAY
C  DSC = DSC MATRIX
C  CQC = CQC MATRIX
C  KOD = PRINT CODE ARRAY
C  BN = STORY NAMES
C  A = STORY DATA
C  BC = SIN - COS OF EQ ANGLE
C  B = GEOM STIFFNESS ARRAY
C  Z = P-DELTA MODAL FORCES
C  *NOTE B AND Z SHARE STORAGE WITH R
C
WRITE(6,1000)
NUM = 0
DO 10 I=1,4
IF( KOD(I) LE 0 ) GO TO 10
NUM = NUM + 1
KOD(I) = NUM
10 CONTINUE
WRITE(6,1200)
IF( NUM.LE.0 ) RETURN
C
REWIND 1
WRITE(1) (( D(I,J),I=1,MBS ), J=1,NFQ )
C
IK = 0
MM = 1
IF( KOD(5).EQ.1 ) IK = 3
IF( KOD(5).EQ.2 ) MM = 2
DO 500 M=1,MM
C
WRITE(6,1001)
IF( IK.LE.0 ) GO TO 14
C---- TRANSFORM TO EQ DIRECTION COOR SYSTEM
DO 100 J=1,NFQ
I1 = 1
DO 100 I=1,MST
X = D(I1,J)
Y = D(I1+1,J)
D(I1,J) = X*BC(1) - Y*BC(2)
D(I1+1,J) = X*BC(2) + Y*BC(1)
100 I1 = I1 + 3
14 IF( NMD.LE.0 ) GO TO 15
C---- PRINT OUT INDIV MODAL DISP
WRITE(6,1300)
WRITE(6,1600)
CALL PROUT(D,MBS,NMD,BN,MST,RLAB(1+IK),13,18)
C---- COMBINE MODAL DISP
15 CALL COMBO(D,R,DSC,CQC,KOD,MBS,NFQ)
C---- PRINT OUT COMBINED RESULTS
WRITE(6,1400)
DO 16 I=1,4
IF( KOD(I).LE.0 ) GO TO 16
WRITE(6,1100) KOD(I),NAM(I)
16 CONTINUE
CALL PROUT(R,MBS,NUM,BN,MST,RLAB(1+IK),13,18)

```



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C
C---- CALC MODAL DRIFTS
  N = MBT - 1
  DO 30 I=1,NFQ
    IF(MBT.EQ.1)GO TO 21
    DO 20 J=1,N
      JJ = 13*( J - 1 ) + 1
      D(JJ,1) = ( D(JJ,1) - D(JJ+13,1) )/A(J,2)
      IF( 13.NE.3 ) GO TO 20
      D(JJ+1,1) = ( D(JJ+1,1) - D(JJ+4,1) )/A(J,2)
      D(JJ+2,1) = D(JJ+2,1) - D(JJ+5,1)
    20 CONTINUE
  21 JJ = 13*( MBT - 1 ) + 1
    D(JJ,1) = D(JJ,1)/A(MBT,2)
    IF( 13.EQ.3 ) D(JJ+1,1) = D(JJ+1,1)/A(MBT,2)
  30 CONTINUE
  WRITE(6,1002)
  IF( NMD.LE.0 ) GO TO 32
C---- PRINT OUT INDIV MODAL DRIFTS
  WRITE(6,1300)
  WRITE(6,1600)
  CALL PROUT(D,MBS,NMD,SN,MBT,RLAB(1+IK),13,16)
C---- COMBINE MODAL DRIFTS
  32 CALL COMBO(D,R,D8C,C8C,KOD,MBS,NFQ)
C---- PRINT OUT COMBINED RESULTS
  WRITE(6,1400)
  DO 33 I=1,4
    IF( KOD(I).LE.0 ) GO TO 33
    WRITE(6,1100) KOD(I),NAM(I)
  33 CONTINUE
  CALL PROUT(R,MBS,NUM,SN,MBT,RLAB(1+IK),13,16)
C---- FORM MASS ARRAY ( AGAIN )
  DO 50 I=1,MBT
    II = 13*( I - 1 ) + 1
    XM(11) = A(1,3)
    IF( 13.NE.3 ) GO TO 50
    XM(11+1) = A(1,3)
    XM(11+2) = A(1,4)
  50 CONTINUE
  DMI = 1.0
  TPI = 8.0*DATAN( DMI )
C---- GET MODAL DISP
  REWIND 1
  READ(1) (( D(I,J),I=1,MBS), J=1,NFQ )
  IF( IK.LE.0 ) GO TO 59
C---- TRANSFORM TO EQ DIRECTION COOR SYSTEM
  DO 200 J=1,NFQ
    II = 1
    DO 200 I=1,MBT
      X = D(II,J)
      Y = D(II+1,J)
      D(II,J) = X*BC(1) + Y*BC(2)
      D(II+1,J) = -X*BC(2) + Y*BC(1)
    200 II = II + 3
C
  59 IF( DABS(GRAV).LT.1.0D-10 ) GO TO 56
C---- ASSEMBLE GEOM STIFFNESS MATRIX
  DO 40 I=1,MBS
    DO 40 J=1,MBS
  40 S(I,J) = 0.0
  XMT = 0.0
  X8MT = 0.0
  DO 52 I=1,MBT
    H = A(1,2)
    XMT = XMT + A(1,3)
    X8MT = X8MT + A(1,4)
  KK = ( I - 1 ) * I3
C
  DO 51 J=1,13
    IF( J.NE.3 ) POEL = XMT*GRAV/H
    IF( J.EQ.3 ) POEL = X8MT*GRAV/H

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```

      NN = KK + J
      B(NN,NN) = B(NN,NN) + PDEL
      IF( I.GE.MBT ) GO TO 51
      B(NN,NN+13) = -PDEL
      B(NN+13,NN) = -PDEL
      B(NN+13,NN+13) = B(NN+13,NN+13) + PDEL
51 CONTINUE
52 CONTINUE
C---- CALC P-DELTA FORCES
      DO 38 I=1,MBS
      DO 38 J=1,NFQ
38 Z(I,J) = 0.0
      DO 46 I=1,MBS
      K1 = I - 13
      K2 = I + 13
      IF( K1.LE.0 ) K1 = 1
      IF( K2.GT.MBS ) K2 = MBS
      DO 44 J=1,NFQ
      XX = 0.0
      DO 42 K=K1,K2
42 XX = XX + B(I,K)*D(K,J)
44 Z(I,J) = XX
46 CONTINUE
C---- CALC STORY INTERIA FORCES
56 DO 60 I=1,NFQ
      WW = ( TP1/W(I) )**2
      DO 60 J=1,MBS
60 D(J,I) = D(J,I)*M(J)*WW
      IF( DABS(GRAV) LT 1.0D-10 ) GO TO 64
C---- ADD P-DELTA FORCES TO INTERIA FORCES
      DO 62 I=1,NFQ
      DO 62 J=1,MBS
62 D(J,I) = D(J,I) + Z(J,I)
C---- CALC STORY SHEARS
64 N = MBS - 13
      DO 66 I=1,NFQ
      IF(N.EQ.0)GO TO 66
      DO 65 J=1,N
65 D(J+13,I) = D(J+13,I) + D(J,I)
66 CONTINUE
      WRITE(6,1003)
      IF( NMD.LE.0 ) GO TO 67
C---- PRINT OUT (INDIV MODAL SHEARS
      WRITE(6,1300)
      WRITE(6,1600)
      CALL PROUT(D,MBS,NMD,SN,MST,RLAB(1+1K),13,18)
C---- COMBINE MODAL SHEARS
67 CALL COMBO(D,R,DBC,CCC,KOD,MBS,NFQ)
C---- PRINT OUT COMBINED RESULTS
      WRITE(6,1400)
      DO 68 I=1,4
      IF( KOD(I) LE 0 ) GO TO 68
      WRITE(6,1100) KOD(I),NAM(I)
68 CONTINUE
      CALL PROUT(R,MBS,NJM,SN,MST,RLAB(1+1K),13,18)
C
C---- CALC STORY OVERTURNING MOMENTS
      IF( I3.EQ.3 ) GO TO 75
C---- PLANAR ANALYSIS
      DO 71 I=1,NFQ
      D(1,I) = D(1,I)*A(1,2)
      IF(MBT.EQ.1)GO TO 71
      DO 70 J=2,MBT
70 D(J,I) = D(J,I)*A(J,2) + D(J-1,I)
71 CONTINUE
      GO TO 95
C---- 3D ANALYSIS
75 DO 80 I=1,NFQ
      D(3,I) = 0.
      DO 80 K=1,2
80 D(K,I) = D(K,I)*A(1,2)

```

```

      IF(MBT.EQ.1)GO TO 90
      IX = 4
      JY = 5
      IT = 6
      DO 85 J=2,MBT
      H = A(J,2)
      D(IX,1) = D(IX,1)*H + D(IX-3,1)
      D(JY,1) = D(JY,1)*H + D(JY-3,1)
      D(IT,1) = 0.0
      IX = IX + 3
      JY = JY + 3
85  IT = IT + 3
90  CONTINUE
95  WRITE(6,1004)
      IF( NMD.LE.0 ) GO TO 97
C---- PRINT OUT INDIV MODAL OTM
      WRITE(6,1300)
      WRITE(6,1600)
      CALL PROUT(D,MBS,NMD,SN,MBT,RLAB(1+IK),13,18)
C---- COMBINE MODAL OTM
97  CALL COMBO(D,R,DSC,COC,KOD,MBS,NFQ)
C---- PRINT OUT COMBINED RESULTS
      WRITE(6,1400)
      DO 98 I=1,4
      IF( KOD(I).LE.0 ) GO TO 99
      WRITE(6,1100) KOD(I),NAM(I)
98  CONTINUE
      CALL PROUT(R,MBS,NUM,SN,MBT,RLAB(1+IK),13,18)
C
      REWIND 1
      READ (1) (( D(I,J),I=1,MBS ), J=1,NFQ )
C
      IK = 3
      WRITE(6,1200)
500 CONTINUE
C
      WRITE(6,1500)
      RETURN
1000 FORMAT( 1H ,//,1H ,11(1H-),/, 112H RESPONSE SPECTRUM ANALYSIS TYP
1E 6, SOLUTION FOR BUILDING STORY DEFLECTIONS, DRIFTS, SHEARS, OVER
2TURNING MOMENTS ,/,1H ,11(1H-),// )
1001 FORMAT( ///,1H ,17(1H-),/,17H STORY DEFLECTIONS ,/,1H ,17(1H-),/ )
1002 FORMAT( ///,1H ,18(1H-),/,18H STORY DRIFT RATIOS ,/,1H ,18(1H-),/ )
1003 FORMAT( ///,1H ,12(1H-),/,12H STORY SHEARS ,/,1H ,12(1H-),/ )
1004 FORMAT( ///,1H ,25(1H-),/,25H STORY OVERTURNING MOMENTS ,/,1H ,
1 25(1H-),/ )
1100 FORMAT( 20X,22H OUTPUT COLUMN NUMBER ,1,10H CONTAINS ,A4,
1 8H RESULTS )
1200 FORMAT( 5(/) )
1300 FORMAT( ///,24H --- MODAL RESPONSES ---,/ )
1400 FORMAT( ///, 25H --- COMBINED RESULTS ---,/ )
1500 FORMAT( /,1H ,22(1H-),/,23H END OF OPTION 8 OUTPUT ,/,1H ,22(1H-))
1600 FORMAT( /,20X,38H COLUMN NUMBER REFERS TO MODE NUMBER ,/ )
      END
      SUBROUTINE OPT8(SN,A,AA,BB,R,MBS,MBT,13,18)
C-----
C  ROUTINE TO CALC RESPONSE ENVELOPES FOR, DISPLACEMENTS, DRIFTS,
C  SHEARS, AND OVERTURNING MOMENTS FOR OPTION NAT = 8
C-----
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      DIMENSION A(MBT,8),R(MBS,4),AA(MBS,1),BB(MBS,1),RLAB(8),SN(MBT)
      COMMON /DYN/ NTIME,DT,NPC,DAMP
      COMMON /JUNK/ SHED(7),KOD(5),IFIL(58)
      COMMON /BUNK/ BC(2),AFIL(258)
      CHARACTER*4 RLAB,SN,SHED
      DATA RLAB /' X ',' Y ','ROTN',' R ',' B ','ROTN'/
C
C---- A = STORY LEVEL INPUT DATA TABLE
C  R(1,1) = TIME OF MAX RESPONSE
C  R(1,2) = MAX RESPONSE

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C   R(1,3) = TIME OF MIN RESPONSE
C   R(1,4) = MIN RESPONSE
C   KOD = TIME HISTORY OUTPUT TABLE
C   AA(1,J) = DISP OF DOF 1 AT TIME STEP J
C   BB(1,J) = INTERIA FORCE AT DOF 1 AT TIME STEP J
WRITE(6,1000)
REWIND 1
WRITE(1) (( AA(1,J+5),I=1,MBS ), J=1,NTIME )
1      (( BB(1,J),I=1,MBS ), J=1,NTIME )
C
IK = 0
MM = 1
IF( KOD(5).EQ.1 ) IK = 3
IF( KOD(5).EQ.2 ) MM = 2
DO 500 M=1,MM
C
IF( IK.LE.0 ) GO TO 14
C---- TRANSFORM TO EQ DIRECTION COOR SYSTEM
DO 100 J=1,NTIME
II = 1
DO 100 I=1,MST
X = AA(II,J+5)
Y = AA(II+1,J+5)
AA(II,J+5) = X*BC(1) + Y*BC(2)
AA(II+1,J+5) = -X*BC(2) + Y*BC(1)
X = BB(II,J)
Y = BB(II+1,J)
BB(II,J) = X*BC(1) + Y*BC(2)
BB(II+1,J) = -X*BC(2) + Y*BC(1)
100 II = II + 3
C---- ENVELOPE STORY DISPLACEMENTS
C
14 CALL ENVLB(AA,R,MBS,NTIME,DT,5)
C
C---- PRINT DISPLACEMENT ENVELOPES
C
WRITE(6,1001)
WRITE(6,1400)
WRITE(6,1200)
C
CALL PROUT(R,MBS,4,SN,MST,RLAB(1+IK),13,18)
C
C---- PRINT OUT FLOOR TIME HISTORY ( IF REQUESTED )
C
IF( KOD(1).EQ.0 ) GO TO 10
WRITE(6,1300)
WRITE(6,1100)
C
CALL PROUT(AA(1,6),MBS,NTIME,SN,MST,RLAB(1+IK),13,18)
C
C---- COMPUTE STORY DRIFTS ETC
C
10 N = MST - 1
DO 20 II=1,NTIME
I=II-5
IF(N.EQ.0)GO TO 16
DO 15 J=1,N
JJ = 13*( J - 1 ) + 1
AA(JJ,1) = ( AA(JJ,1) - AA(JJ+13,1) )/A(J,2)
IF( 13.NE.3 ) GO TO 15
AA(JJ+1,1) = ( AA(JJ+1,1) - AA(JJ+4,1) )/A(J,2)
AA(JJ+2,1) = AA(JJ+2,1) - AA(JJ+5,1)
15 CONTINUE
16 JJ = 13*( MST - 1 ) + 1
AA(JJ,1) = AA(JJ,1)/A(MST,2)
IF( 13.EQ.3 ) AA(JJ+1,1) = AA(JJ+1,1)/A(MST,2)
20 CONTINUE
C
CALL ENVLB(AA,R,MBS,NTIME,DT,5)
WRITE(6,1002)
WRITE(6,1400)

```

```

WRITE(6,1200)
CALL PROUT(R,MBS,4,SN,MST,RLAB(1+IK),13,18)
IF( MOD(2),EQ.0 ) GO TO 30
WRITE(6,1300)
WRITE(6,1100)
CALL PROUT(AA(1,6),MBS,NTIME,SN,MST,RLAB(1+IK),13,18)
C
C---- STORY SHEARS ETC
C
30 N = MBS - 13
IF(N.EQ.0)GO TO 38
DO 35 I=1,NTIME
DO 35 J=1,N
35 BB(J+13,1) = BB(J+13,1) + BB(J,1)
38 CONTINUE
CALL ENVL8(BB,R,MBS,NTIME,DT,0)
WRITE(6,1003)
WRITE(6,1400)
WRITE(6,1200)
CALL PROUT(R,MBS,4,SN,MST,RLAB(1+IK),13,18)
IF( MOD(3),EQ.0 ) GO TO 40
WRITE(6,1300)
WRITE(6,1100)
CALL PROUT(BB,MBS,NTIME,SN,MST,RLAB(1+IK),13,18)
C
C---- COMPUTE STORY OVERTURNING MOMENTS ETC
C
40 IF( 13.EQ.3 ) GO TO 48
C---- PLANAR ANALYSIS
DO 48 I=1,NTIME
BB(1,1) = BB(1,1)*A(1,2)
IF(MST.EQ.1)GO TO 46
DO 45 J=2,MST
45 BB(J,1) = BB(J,1)*A(J,2) + BB(J-1,1)
48 CONTINUE
GO TO 65
C---- 3D ANALYSIS
48 DO 60 I=1,NTIME
DO 50 K=1,2
50 BB(K,1) = BB(K,1)*A(1,2)
IF(MST.EQ.1)GO TO 60
IX = 4
IY = 5
IT = 6
DO 55 J=2,MST
H = A(J,2)
BB(IX,1) = BB(IX,1)*H + BB(IX-3,1)
BB(IY,1) = BB(IY,1)*H + BB(IY-3,1)
IX = IX + 3
BB(IT,1) = 0.0
IY = IY + 3
55 IT = IT + 3
60 CONTINUE
C
65 CALL ENVL8(BB,R,MBS,NTIME,DT,0)
WRITE(6,1004)
WRITE(6,1400)
WRITE(6,1200)
CALL PROUT(R,MBS,4,SN,MST,RLAB(1+IK),13,18)
IF( MOD(4),EQ.0 ) GO TO 68
WRITE(6,1300)
WRITE(6,1100)
CALL PROUT(BB,MBS,NTIME,SN,MST,RLAB(1+IK),13,18)
C
68 REWIND 1
READ(1) (( AA(I,J+5),I=1,MBS ), J=1,NTIME ),
1 (( BB(I,J),I=1,MBS ), J=1,NTIME )
IK = 3
WRITE(6,1600)
500 CONTINUE
C

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```

WRITE(6,1500)
RETURN
1000 FORMAT( 1H ,//,1H ,100(1H-),/,107H TIME HISTORY ANALYSIS TYPE B , B
1010 LUTION FOR BUILDING STORY DEFLECTIONS , DRIFTS , SHEARS , OVERTURNIN
20 MOMENTS ,/,1H ,100(1H-),// )
1001 FORMAT( ///,1H ,17(1H-),/,108H STORY DEFLECTIONS ,/,1H ,17(1H-), /)
1002 FORMAT( ///,1H ,18(1H-),/,109H STORY DRIFT RATIOS ,/,1H ,18(1H-),/)
1003 FORMAT( ///,1H ,12(1H-),/,13H STORY SHEARS ,/,1H ,12(1H-),/ )
1004 FORMAT( ///,1H ,25(1H-),/,20H STORY OVERTURNING MOMENTS ,/,1H ,
1 25(1H-),/ )
1100 FORMAT( /,20X,40H OUTPUT COLUMN NUMBER REFERS TO TIME STEP NUMBER
1 / )
1200 FORMAT( /,20X,50H OUTPUT COLUMN 1 CONTAINS TIME OF MAXIMUM RESPON
1SE,/
2 20X,40H OUTPUT COLUMN 2 CONTAINS MAXIMUM RESPONSE VALUES,/
3 20X,50H OUTPUT COLUMN 3 CONTAINS TIME OF MINIMUM RESPONSE ,/
4 20X,40H OUTPUT COLUMN 4 CONTAINS MINIMUM RESPONSE VALUES,/ )
1300 FORMAT( //,30H --- TIME HISTORY RESPONSE ---,/ )
1400 FORMAT( //,37H --- TIME HISTORY ENVELOPE VALUES ---,/ )
1500 FORMAT( /,1H ,22(1H-),/,23H END OF OPTION B OUTPUT ,/,1H ,22(1H-))
1600 FORMAT( 5(/) )
END
SUBROUTINE DBCOQC(A,CGC,WW,NFG,DP,TIM)
C-----
C ROUTINE TO FORM THE DBC AND CGC MATRICES
C-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION A(NFG,NFG),CGC(NFG,NFG),WW(NFG)
DM1 = 1.0
TPI = 8.0*DATAN( DM1 )
C
C---- FORM THE DBC MATRIX
C
DO 100 I=1,NFG
WI = TPI/WW(I)
BI = DP + 2.0/(TIM*WI)
WII = WI*DBSQRT( 1.0 - BI*BI )
DO 100 J=1,NFG
WJ = TPI/WW(J)
BJ = DP + 2.0/(TIM*WJ)
WJJ = WJ*DBSQRT( 1.0 - BJ*BJ )
A(I,J) = 1.0/( 1.0 + ( ( WII - WJJ )/( BI*WI + BJ*WJ ) )**2 )
100 CONTINUE
C
DO 200 I=1,NFG
DO 200 J=1,NFG
200 A(J,I) = A(I,J)
C
WRITE(6,2000)
IL=0
180 IF=IL+1
IL=IF+19
IF(IL.GE.NFG)IL=NFG
DO 185 I=1,NFG
185 WRITE(6,1100) I,( A(I,J),J=IF,IL)
WRITE(6,1200)
IF(IL.NE.NFG)GO TO 180
C
C---- FORM THE CGC MATRIX
C
F = DP*DP
DO 60 I=1,NFG
W1=TPI/WW(I)
DO 50 J=1,I
IF(J.NE.I)GO TO 20
CGC(I,I)=1.0
GO TO 50
20 W2=TPI/WW(J)
R=W2/W1
R1=8.0*F*(1.0+R)*R**1.5

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R2=1.0-R*R
R2=R2*R2
R3=1.0+R
R3=4.0*F*R*R3*R3
CQC(I,J)=R1/(R2+R3)
50 CONTINUE
60 CONTINUE
DO 70 J=2,NFQ
JJ=J-1
DO 70 I=1,JJ
70 CQC(I,J)=CQC(J,I)
WRITE(6,1000)
IL=0
80 IF=IL+1
IL=IF+10
IF(IL.GE.NFQ)IL=NFQ
DO 85 I=1,NFQ
85 WRITE(6,1100) I,(CQC(I,J),J=IF,IL)
WRITE(6,1200)
IF(IL.NE.NFQ)GO TO 80
RETURN
1000 FORMAT(///41H CQC MODAL CROSS-CORRELATION COEFFICIENTS//)
1100 FORMAT(15,20F6.3)
1200 FORMAT(//3H )
2000 FORMAT(///42H DSC MODAL CROSS-CORRELATION COEFFICIENTS//)
END
SUBROUTINE PROUT(F,NBS,NFQ,A,NBT,RLAB,13,18)
-----
C ROUTINE TO OUTPUT GROSS STORY RESPONSE QUANTITIES
-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION F(NBS,NFQ),A(NBT),RLAB(3)
CHARACTER*4 RLAB,A
C
DO 800 I=1,NFQ,8
IH = I + 7
IF( IH.GT.NFQ ) IH = NFQ
WRITE(6,2003) ( J,J=1,IH )
DO 800 N=1,NBT
LN = NBT + 1 - N
NN = 13*( N - 1 )
WRITE(6,2002)
DO 800 J=1,13
800 WRITE(6,2004) LN,A(N),RLAB(J+18),(F(NN+J,K),K=1,IH)
RETURN
2002 FORMAT( 1H )
2003 FORMAT(///, 18H LEVEL ID DIRN ,8I13 )
2004 FORMAT( 15,3X,A4,2X,A4,2X,8F13.4 )
END
SUBROUTINE CODE(P,A,NF)
-----
C ROUTINE TO PERFORM STRESS RATIO CALC
-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION P(10),A(12)
C---- P = MEMBER FORCES
C A = ALLOWABLE FORCE QUANTITIES
C
IF( NF.NE.10 ) GO TO 10
C---- COLUMN ELEMENT
P(0) = 0.0
P(10) = 0.0
IF( A(10).LE.0.0 ) RETURN
X = DABS( P(4)/A(10) )
P(0) = X + DABS( P(2)/A(11) ) + DABS( P(5)/A(12) )
P(10) = X + DABS( P(3)/A(11) ) + DABS( P(8)/A(12) )
RETURN
10 IF( NF.NE.5 ) GO TO 20
C---- BEAM ELEMENT

```

```

P(4) = 0.0
P(5) = 0.0
IF( A(10) .LE. 0.0 ) RETURN
P(4) = DABS( P(2)/A(10) )
P(5) = DABS( P(3)/A(10) )
RETURN
20 IF( NF.NE.2 ) RETURN
C---- TRUSS ELEMENT
P(2) = 0.0
IF( DABS(A(3)) .LT. 1.0D-10 ) RETURN
P(2) = DABS( P(1)/A(3) )
RETURN
END
SUBROUTINE COMBO(A,R,DBC,CC,COD,MBS,NFQ)
-----
C ROUTINE TO PERFORM MODAL COMBINATIONS OF GROSS STORY RESPONSES
-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION A(MBS,1),R(MBS,4),DBC(NFQ,NFQ),CC(NFQ,NFQ),COD(4)
C
C A = MODAL RESPONSES
C R = COMBINED MODAL RESPONSES
C
I1 = COD(1)
IF( I1 .LE. 0 ) GO TO 25
C---- SRSS COMBO
DO 20 I=1,MBS
X = 0.0
DO 10 J=1,NFQ
10 X = X + A(I,J)**2
20 R(I,I1) = DSQRT( X )
C
25 I1 = COD(2)
C---- DSC COMBO
IF( I1 .LE. 0 ) GO TO 45
DO 40 K=1,MBS
X = 0.0
DO 30 I=1,NFQ
Y = A(K,I)
DO 30 J=1,NFQ
30 X = X + Y*DBC(I,J)*A(K,J)
40 R(K,I1) = DSQRT( X )
C
45 I1 = COD(3)
IF( I1 .LE. 0 ) GO TO 80
C---- CQC COMBO
DO 50 K=1,MBS
X = 0.0
DO 55 I=1,NFQ
Y = A(K,I)
DO 55 J=1,NFQ
55 X = X + Y*CC(I,J)*A(K,J)
50 R(K,I1) = DSQRT( X )
C
80 I1 = COD(4)
IF( I1 .LE. 0 ) RETURN
C---- ABS COMBO
DO 70 I=1,MBS
X = 0.0
DO 65 J=1,NFQ
65 X = X + DABS( A(I,J) )
70 R(I,I1) = X
RETURN
END

```



```

SUBROUTINE TYP0(A,F,HH,AA,H,BH,MBS,MST,NFQ,13)
-----
C  ROUTINE TO GENERATE TYPE 0 MODE SHAPES - EMPIRICAL RULE
-----
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  DIMENSION A(MST,1),F(MBS,MBS),HH(MST),AA(NFQ),H(NFQ),BH(NFQ)
C
C---- A = STORY DATA
C  F = MODE SHAPES
C  HH,AA,H,BH = LOCAL WORK ARRAYS ( LOCATED IN B )
C
C  SUM UP STORY HEIGHTS
  SUMH = 0.0
  DO 12 I=1,MST
C  HH IS STORY HEIGHT ABOVE BASE
    SUMH = SUMH + A(MST-I+1,2)
  12 HH(I) = SUMH
    AT=1.0
    AA(1)=1.0
    PI=3.1415927
    Z=PI-1.0
    SUM=0.0
    I = 0
    DO 300 IK=1,NFQ,13
      IF( IK.GT.NFQ ) GO TO 300
      I = I + 1
      IF( I.GT.1 ) GO TO 62
C
C  FIRST MODE SHAPE LINEAR
C
    SUM = SUMH
    DO 60 J=1,MST
      JJ = 13*( J - 1 ) + 1
      XX = SUM/SUMH
      F(JJ,1) = XX
      IF( 13.NE.3 ) GO TO 60
      F(JJ+1,2) = XX
      F(JJ+2,3) = XX
  60 SUM = SUM - A(J,2)
      SUM = 0.0
      GO TO 300
C
C  HIGHER MODES
C
  62 I1=I-1
    Q=I1
    SUM=SUM+1/Q
    AA(1)=1.0+Z*SUM
    AT=AT+AA(1)
C
C  HA IS SUMMATION OF H(I)
C
    HA=0.0
    DO 140 J=1,I
      H(J)=AA(J)*SUMH/AT
      M=I-J
      IF(M.EQ.0) GO TO 140
      HA=HA+H(J)
C
C  BH(M) IS THE NODE HEIGHT FROM BASE
C
    BH(M)=SUMH-HA
  140 CONTINUE
C
  DO 100 M=1,MST
    JJ = ( MST - M ) * 13 + 1
    IF(HH(M).LT.BH(1)) GO TO 90
    IF(HH(M).GE.BH(11)) GO TO 90
    I1=I-2
    K=1

```

```

      DO 70 L=K,111
      IF(HH(M) .GE. BH(L) .AND. HH(M) .LT. BH(L+1)) GO TO 95
70  CONTINUE
      GO TO 100
80  XX=(HH(M)-BH(11))/H(1)
      X=1/2.0
      IL=X
      IF((X-IL) .EQ. 0.0) XX = - XX
      GO TO 96
90  XX=DBIN(PI*(HH(M)/H(1)))**1.3569)
      GO TO 96
95  XX=DBIN(PI*(HH(M)-BH(L))/H(1-L))
      Y=L/2.0
      LI=Y
      IF(DABS(Y-LI) .GT. 1.00-10) XX = -XX
      K=L
96  F(JJ,IK) = XX
      IF( 13.NE.3 ) GO TO 100
      F(JJ+1,IK+1) = XX
      F(JJ+2,IK+2) = XX
100 CONTINUE
300 CONTINUE
C
      RETURN
      END
      SUBROUTINE TYP12(A,F,HH,MBS,MBT,NFQ,13,NSD,KOD)
-----
C  ROUTINE TO GENERATE TYPE 1 OR TYPE 2 MODE SHAPES
C      TYPE 1 - UNIFORM SHEAR BEAM RULE
C      TYPE 2 - READ IN SHAPES
-----
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      DIMENSION A(MBT,1),F(MBS,MBS),HH(MBT)
C
C---- A = STORY DATA
C      F = MODE SHAPES
C      HH = LOCAL WORK ARRAY
C
C      SUM UP STORY HEIGHTS
      SUMH = 0.0
      DO 12 I=1,MBT
C      HH IS STORY HEIGHT ABOVE BASE
      SUMH = SUMH + A(MBT-I+1,2)
12  HH(1) = SUMH
      IF( KOD.EQ.2 ) GO TO 490
C
C---- GENERATE UNIFORM SHEAR BEAM MODE SHAPES
C
      T = 1.0
      DO 40 J=1,NFQ,13
      IF( J.GT.NFQ ) GO TO 40
      SUM = SUMH
      DO 30 I=1,MBT
      II = 13*( I - 1 ) + 1
      U = 3.1415927*SUM/SUMH
      X = DBIN( T*U/2.0 )
      F(II,J) = X
      IF( 13.NE.3 ) GO TO 30
      F(II+1,J+1) = X
      F(II+2,J+2) = X
30  SUM = SUM - A(1,2)
      T = T * 2.0
40  CONTINUE
      RETURN
C
C---- READ IN MODE SHAPES
C
490 MODE = 1
      WRITE(6,3002)
500 READ(5,3000) MCD,LB,X,Y,T

```

```

WRITE(6,3001) MOD, LB, X, Y, T
IF( LB.NE.MBT ) GO TO 600
IF( MOD.NE.MODE ) GO TO 600
JJ = ( MBT - LB ) * 13 + 1
F(JJ,MOD) = X
IF( NBD.EQ.2 ) F(JJ,MOD) = Y
IF( I3.NE.3 ) GO TO 502
F(JJ+1,MOD) = Y
F(JJ+2,MOD) = T
502 I1 = JJ
LT = LB
READ(5,3000) MOD, LB, X, Y, T
WRITE(6,3001) MOD, LB, X, Y, T
IF( MOD.NE.MODE ) GO TO 600
JJ = ( MBT - LB ) * 13 + 1
F(JJ,MOD) = X
IF( NBD.EQ.2 ) F(JJ,MOD) = Y
IF( I3.NE.3 ) GO TO 504
F(JJ+1,MOD) = Y
F(JJ+2,MOD) = T
504 IF( (LB+1).EQ.LT ) GO TO 550
C
C---- INTER MODAL VALUES
LLB = LB + 1
LLT = LT - 1
DH = HH(LT) - HH(LB)
DX = F(I1,MOD) - F(JJ,MOD)
IF( I3.NE.3 ) GO TO 506
DY = F(I1+1,MOD) - F(JJ+1,MOD)
DT = F(I1+2,MOD) - F(JJ+2,MOD)
506 DO 520 I=LLB,LLT
DDH = ( HH(I) - HH(LB) ) / DH
IK = ( MBT - I ) * 13 + 1
F(IK,MOD) = F(JJ,MOD) + DX * DDH
IF( I3.NE.3 ) GO TO 520
F(IK+1,MOD) = F(JJ+1,MOD) + DY * DDH
F(IK+2,MOD) = F(JJ+2,MOD) + DT * DDH
520 CONTINUE
C
550 IF( LB.NE.1 ) GO TO 502
MODE = MODE + 1
IF( MODE.LE.NFQ ) GO TO 500
C
RETURN
600 WRITE(6,3005)
STOP
3000 FORMAT( 2I5,3F10.0 )
3001 FORMAT( 20X,15,16,3F12.4 )
3002 FORMAT( //,25X,16H MODE INPUT DATA ,
1 //,22X,11H MODE LEVEL 5X,3H X ,9X,3H Y ,6X,4HROTN,/ )
3005 FORMAT( //,10X,14H *INPUT ERROR* )
END
SUBROUTINE ENVL8(A,R,MBS,NTIME,DT,IK)
C-----
C ROUTINE TO FIND ENVELOPE VALUES
C-----
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION A(MBS,NTIME),R(MBS,4)
C
DO 200 I=1,MBS
I1 = 0
X1 = 0.0
I2 = 0
X2 = 0.0
DO 100 J=1,NTIME
Y = A(I,J+IK)
IF( Y.GT.X1 ) GO TO 20
IF( Y.LT.X2 ) GO TO 30
GO TO 100
C---- NEW MAXIMUM

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```

20 I1 = J
   X1 = Y
   GO TO 100
C---- NEW MINIMUM
30 I2 = J
   X2 = Y
100 CONTINUE
   T = DBLE( I1 )
   R( I1,1 ) = DT*T
   R( I1,2 ) = X1
   T = DBLE( I2 )
   R( I1,3 ) = DT*T
   R( I1,4 ) = X2
200 CONTINUE
C
   RETURN
   END
   SUBROUTINE DYNA (BN,A,AA,BB,PA,X,T, XM,S,R,MBS,MST,GRAY)
C-----
C   ROUTINE TO EVALUATE TIME DEPENDENT LATERAL DISPLACEMENTS AND
C   LATERAL INTERIA FORCES ( FOR OPTION NAT = B )
C-----
   IMPLICIT REAL*8 (A-H)
   IMPLICIT REAL*8 (O-Z)
   DIMENSION A(MST,8),PA(2,1),X(1),T(1),XM(1),AA(MBS,1),BB(MBS,1)
   DIMENSION R(MBS,4),B(MBS,MBS),BN(MST)
   COMMON/GEN/ NST,NDF,NTF,MLD,NAT,NFQ,NSD,BHED(9),FHED(7),NBS
1   ,RLAB(3),IB,IS,O(6)
   COMMON/BUNK/ SC(2),AFIL(258)
   COMMON/DYN/NTIME,DT,NPC,DAMP
   CHARACTER*4 BN,RLAB,BHED,FHED
C
C---- A = STORY DATA
C   AA(I,J+5) = DISP OF DOF I AT TIME STEP J ( 5 STAT CASES IN FRONT )
C   BB(I,J) = STORY INTERIA FORCE AT DOF I AT TIME STEP J
C   PA = EG GROUND TIME-ACC HISTORY
C   X(I) = MODAL AMP AT TIME STEP I
C   T = MODE SHAPE
C   XM = MASS ARRAY
C   B = GEOM STIFFNESS MATRIX
C   *NOTE B SHARES STORAGE WITH PA,X,T,XM
C   *PROGRAMMING NOTE B IS SPARSE POSSIBLE TO REDUCE STORAGE REQD.
C   R = ARRAY TO COLLECT MAX + MIN STORY RESPONSES ( OPTB )
C   *NOTE R SHARES STORAGE WITH PA,X,T,XM
C
   DO 100 I=1,MBS
   DO 100 K=1,NTIME
100 AA(I,K+5) = 0.0
C
   IF( NPC.LT.0 ) GO TO 105
C---- TIME AND ACC POINTS INPUT
   READ(5,1000) (PA(1,I),PA(2,I),I=1,NPC)
   WRITE(6,2000) (PA(1,I),PA(2,I),I=1,NPC)
   GO TO 118
C---- ACC POINTS INPUT
105 NPC = IABS( NPC )
   READ(5,1001) DDT
   WRITE(6,2001) DDT
   TIM = 0.0
   DO 115 I=1,NPC
   PA(1,I) = TIM
115 TIM = TIM + DDT
   READ(5,1002) ( PA(2,I),I=1,NPC )
   WRITE(6,2002) ( PA(1,I),PA(2,I),I=1,NPC )
C
C   CHECK GROUND ACCELERATION DATA
C
118 DO 120 I=2,NPC
   IF (PA(1,I).GT.PA(1,I-1)) GO TO 120
   WRITE (6,3001) PA(1,I-1),PA(1,I)
   STOP

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```

120 CONTINUE
    TIME=NTIME
    TIME=TIME*DT
    ATIME=PA(1,NPC)-PA(1,1)
    IF(ATIME.GE.TIME) GO TO 150
    WRITE (6,3000)
    STOP
150 REWIND 1
    IF( NAT.GT.4 ) GO TO 170
C
C---- ANALYSIS TYPE 4
C
    DO 160 L=1,NFG
    READ (1) W,DAMP,(T(K),K=1,MBS)
C
    CALL RESP (PA,X,W,NTIME,NPC,DT,DAMP)
C
    DO 155 I=1,MBS
    DO 155 J=1,NTIME
155 AA(I,J+5) = AA(I,J+5) + T(I)*X(J)
160 CONTINUE
    RETURN
C
C---- ANALYSIS TYPE 8 OR 9
C
170 DO 172 I=1,MBS
    DO 172 J=1,NTIME
172 BB(I,J) = 0.0
C---- CREATE MASS ARRAY XM FROM ARRAY A
    DO 175 I=1,MST
    I = I3*( I - 1 ) + 1
    XM(I) = A(I,3)
    IF( I3.NE.3 ) GO TO 175
    XM(I+1) = A(I,3)
    XM(I+2) = A(I,4)
175 CONTINUE
    DM1 = 1.0
    TP1 = 8.0*DATAN( DM1 )
    DO 300 L=1,NFG
    READ (1) W,DAMP,(T(K),K=1,MBS)
    VW = ( TP1/W )**2
C
    CALL RESP (PA,X,W,NTIME,NPC,DT,DAMP)
C
    DO 200 I=1,MBS
    XOM = VW*XM(I)
    DO 200 J=1,NTIME
    Z = T(I)*X(J)
    AA(I,J+5) = AA(I,J+5) + Z
200 BB(I,J) = BB(I,J) + XOM*Z
300 CONTINUE
    IF( DABS(GRAV).LT.1.0D-10 ) GO TO 360
C---- ASSEMBLE GEOM STIFFNESS MATRIX
    DO 310 I=1,MBS
    DO 310 J=1,MBS
310 B(I,J) = 0.0
    XMT = 0.0
    XMMT = 0.0
    DO 320 I=1,MST
    H = A(I,2)
    XMT = XMT + A(I,3)
    XMMT = XMMT + A(I,4)
    KK = ( I - 1 ) * I3
C
    DO 315 J=1,I3
    IF( J.NE.3 ) PDEL = XMT*GRAV/H
    IF( J.EQ.3 ) PDEL = XMMT*GRAV/H
    NN = KK + J
    B(NN,NN) = B(NN,NN) + PDEL
    IF( I.GE.MST ) GO TO 315
    B(NN,NN+I3) = -PDEL

```

```

      B(NN+13,NN) = -PDEL
      B(NN+13,NN+13) = B(NN+13,NN+13) + PDEL
315 CONTINUE
320 CONTINUE
C---- CALC AND ADD P-DELTA FORCES TO BB
      IB = 3
      IF( 13.EQ.3 ) IB = 7
      DO 350 J=1,NTIME
      DO 350 I=1,MBS
      K1 = I - IB
      K2 = I + IB
      IF( K1.LE.0 ) K1 = 1
      IF( K2.GT.MBS ) K2 = MBS
      Z = 0.0
      DO 330 K=K1,K2
330 Z = Z + B(I,K)*AA(K,J+5)
350 BB(I,J) = BB(I,J) + Z
C
360 CALL OPTB(SN,A,AA,BB,R,MBS,MST,13,IB)
C
      RETURN
1000 FORMAT(2F10.0)
1001 FORMAT( F10.0 )
1002 FORMAT( 8F9.0 )
2000 FORMAT (///26H GROUND ACCELERATION CARDS ,//,
1          11X,4HTIME,3X,12HACCELERATION ,/, (2F15.4) )
2001 FORMAT( //, 10X,42H ACCELERATION RECORD INPUT TIME INTERVAL = ,
1          F10.5, / )
2002 FORMAT( ///, 26H GROUND ACCELERATION CARDS ,/, ( 3X,12F10.4 ) )
3000 FORMAT (/,44H GROUND ACCELERATION TIME SPAN IS LESS THAN
1 32H SPECIFIED BUILDING RESPONSE TIME )
3001 FORMAT (//,32H INCONSISTENT ACCELERATION DATA ,//
1 34H TIMES MUST INCREASE SEQUENTIALLY ,//
2 16H ERROR AT TIMES ,F12.5/10X,F12.6)
      END
      SUBROUTINE MODGEN(SN,A,DD,F,XM,RR,W,S,MBS,MST,NFO,13,IB,NBO)
C-----
C      SUBROUTINE TO GENERATE APPROX MODE SHAPES
C-----
      IMPLICIT REAL*8 (A-H)
      IMPLICIT REAL*8 (O-Z)
      DIMENSION A(MST,1),F(MBS,MBS),XM(MBS),W(NFO),S(MBS,MBS),RR(MBS,2),
1  RLAB(3),DD(MBS,2),SN(MST)
      CHARACTER*4 RLAB,SN
      DATA RLAB /' X ',' Y ',' ROTN' /
C
C---- A = STORY DATA
C      DD = DIBP FROM STAT LOADS ( LOCATED IN ARRAY A STORAGE )
C      F = MODE SHAPES
C      XM = MASS ARRAY
C      RR = LAT STATIC LOADS ( LOCATED IN ARRAY XM AND IQ STORAGE )
C      W = PERIOD ARRAY
C      S = FLEXIBILITY MATRIX ( USED AS SCRATCH IN TYP0 AND TYP12 )
C
      WRITE(6,3004)
      DO 10 I=1,MBS
      DO 10 J=1,MBS
      S(I,J) = 0.0
10 F(I,J) = 0.0
C
      J=NFO
      IF(NFO.GT.7)J=7
      READ(5,1000)KOD,(W(I),I=1,J)
      IF(NFO.GT.7)READ(5,1001)(W(I),I=8,NFO)
      WRITE(6,2000) KOD
      WRITE(6,2001)(I,W(I),I=1,NFO)
C
C-----DUMMY WRITE TAPE 2
      REWIND 2
      WRITE(2) ( ( F(I,J),I=1,MBS), J=1,5 )
      REWIND 2

```

```

C
C---- GENERATE EMPIRICAL MODE SHAPES
C
  IF( KOD.EQ.0 ) CALL TYP0( A,F,B(1,1),B(1,2),B(1,3),B(1,4),MBS,
  1 MBT,NFQ,13)
C
C---- GENERATE SHEAR BEAM TYPE OR READ IN MODE SHAPES
C
  IF( KOD.NE.0 ) CALL TYP12(A,F,B(1,1),MBS,MBT,NFQ,13,NSD,KOD)
C
C---- ORDER PERIODS AND MODE SHAPES ACCORDING TO DECREASING PERIOD VAL.
C
  DO 560 I=1,NFQ
    WM = W(I)
    K = 0
    DO 560 J=1,NFQ
      IF( W(J).LT.WM ) GO TO 560
      WM = W(J)
      K = J
    560 CONTINUE
    IF( K.LE.0 ) GO TO 580
C
    W(K) = W(I)
    W(I) = WM
    DO 570 J=1,MBS
      VM = F(J,K)
      F(J,K) = F(J,I)
    570 F(J,I) = VM
    580 CONTINUE
C
C---- MASS ARRAY
C
  DO 105 I=1,MBT
    I1 = 13*( I - 1 ) + 1
    XM(I1) = A(1,3)
    IF( 13.NE.3 ) GO TO 105
    XM(I1+1) = A(1,3)
    XM(I1+2) = A(1,4)
  105 CONTINUE
C---- NORMALIZE MODE SHAPES
  DO 120 J=1,NFQ
    BUM = 0.0
    DO 110 I=1,MBS
      BUM = BUM + F(I,J)*F(I,J)*XM(I)
    110 CONTINUE
    Y = 1.0/DSQRT( BUM )
    DO 130 I=1,MBS
      130 F(I,J) = F(I,J)*Y
    120 CONTINUE
C
  WRITE(6,3005)
C
C---- SOLVE FOR DISP FROM LAT STATIC FORCES
C
C---- CALCULATE APPROX FLEXIBILITY MATRIX
  DM1 = 1.0
  TP1 = 8.0*DATAN( DM1 )
  DO 703 I=1,MBS
    DO 702 J=1,MBS
      XX = 0.0
      DO 701 K=1,NFQ
        WFR = TP1/W(K)
        WFR = WFR*WFR
      701 XX = XX + F(I,K)*F(J,K)/WFR
      702 B(I,J) = XX
    703 CONTINUE
C---- ASSEMBLE LAT LOAD VECTOR
  DO 710 I=1,MBT
    IF( NSD.NE.0 ) GO TO 707
C---- 3-D ANAL.
    I1 = 13*( I - 1 ) + 1

```

```

RR(11,1) = A(1,9)
RR(11+1,1) = A(1,10)
RR(11+2,1) = A(1,11)
RR(11,2) = A(1,12)
RR(11+1,2) = A(1,13)
RR(11+2,2) = A(1,14)
GO TO 710
707 IF( NBD.NE.1 ) GO TO 708
C---- X DIRECTION ANAL.
RR(1,1) = A(1,9)
RR(1,2) = A(1,12)
GO TO 710
C---- Y DIRECTION ANAL.
708 RR(1,1) = A(1,10)
RR(1,2) = A(1,13)
710 CONTINUE
C---- SOLVE FOR DISP
DO 706 I=1,MBS
DO 705 J=1,2
XX = 0.0
DO 704 K=1,MBS
704 XX = XX + 8(1,K)*RR(K,J)
705 DD(I,J) = XX
706 CONTINUE
C---- PRINT OUT DISP
WRITE(6,3001)
WRITE(6,3003)
CALL PROUT(DD,MBS,2,BN,MGT,RLAB,13,18)
C---- CALC DRIFTS
N = MBS - 13
DO 720 I=1,2
DO 720 J=1,N
720 DD(J,I) = DD(J,I) - DD(J+13,I)
C---- PRINT OUT DRIFTS
WRITE(6,3002)
WRITE(6,3003)
CALL PROUT(DD,MBS,2,BN,MGT,RLAB,13,18)
RETURN
1000 FORMAT( 15,5X, 7F10.0)
1001 FORMAT((8F10.0))
2000 FORMAT( //,20X,23H MODE GENERATION CODE = ,12,//
1 20X,22H EQ.0 - EMPIRICAL RULE ,/
2 20X,23H EQ.1 - BHEAR BEAM RULE ,/
3 20X,22H EQ.2 - SHAPES READ IN ,/ )
2001 FORMAT(//40H APPROX PERIOD VALUES IN ORDER OF INPUT SEQUENCE ,//
18H NUMBER,5X,7H PERIOD,/, (18,F12.2))
3001 FORMAT( ///,1H ,17(1H-),/,18H STORY DEFLECTIONS ,/,1H ,17(1H-), /)
3002 FORMAT( ///,1H ,12(1H-),/,13H STORY DRIFTS ,/,1H ,12(1H-), /)
3003 FORMAT( 20X,65H OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATER
1AL LOAD CASE A ,/,20X,65H OUTPUT COLUMN 2 CONTAINS RESULTS FROM ST
2ATIC LATERAL LOAD CASE B ,/ )
3004 FORMAT( 1H ,//,1H ,37(1H-),/,38H GENERATION OF APPROXIMATE MODE SH
1APES ,/,1H ,37(1H-),// )
3005 FORMAT( //,1H ,28(1H-),/,29H END OF MODE SHAPE GENERATION ,/,1H ,
128(1H-),// )
END

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```

SUBROUTINE DIAG (IO,L,VANG,DL,BNA,CBA,NTRU,XL1,TP)
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  DIMENSION TP(3,NTRU)
C
  COMMON/STIF/ ABA(12,12),BA(8,12),T(8,12)
C
C  DIAGONAL STIFFNESS AND FORCE MATRICES
C
C  TRANSFORMATION MATRIX
  CALL TRANS(4,VANG,0.D0,DL,BNA,CBA,XL1,0.D0,0.D0,0.D0)
C
C  MEMBER STIFFNESS
  COMM=TP(1,L)*TP(2,L)/DL
C
C  FORCE-FRAME DISPLACEMENT MATRIX
  DO 10 I=1,8
10 BA(1,I)=COMM*T(1,I)
C
  IF(IO.EQ.2) RETURN
C
C  STIFFNESS MATRIX
  DO 120 I=1,8
  DO 120 J=1,8
  ABA(I,J)=T(1,I)*BA(1,J)
120 ABA(J,I)=ABA(I,J)
  RETURN
C
  END
  SUBROUTINE MEMORY(M)
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  WRITE (6,1000) M
  STOP
1000 FORMAT (20H ** INCREASE MTOT BY 15.3H **)
  END
  SUBROUTINE TRANS(KK,XLR,A,B,BNA,CBA,XL1,YL1,XL2,YL2)
  IMPLICIT REAL*8 (A-H)
  IMPLICIT REAL*8 (O-Z)
  COMMON/STIF/ ABA(12,12),BA(8,12),T(8,12)
  COMMON/JUNK/ HLD,N,ND,MM,MW,LM(12),FIL(53)
  COMMON/BUNK/ P(12,3),TF(8,12),TT(12,12),AFIL(8)
C
C  FORM TRANSFORMATION MATRICES
C
  DO 10 I=1,6
  DO 10 J=1,12
10 TF(I,J)=0.
C
  GO TO (100,200,300,400,500)KK
C
C  COLUMN TRANSFORMATION
C
100 D1= 1./XLR
  TF(2,2)=D1
  TF(3,2)=D1
  TF(2,8)=-D1
  TF(3,8)=-D1
  TF(5,1)=-D1
  TF(6,1)=-D1
  TF(5,7)=D1
  TF(6,7)=D1
  TF(1,3)=1.
  TF(4,8)=1.
  TF(1,9)=-1.
  TF(4,12)=-1.
  TF(3,4)=A/XLR
  TF(8,5)=A/XLR
  TF(2,4)=1.+A/XLR
  TF(5,5)=1.+A/XLR
  TF(2,10)=B/XLR

```

```

      TF(5,11)=B/XLR
      TF(3,10)=1.-B/XLR
      TF(8,11)=1.-B/XLR
      DO 150 I=1,12
      DO 150 J=1,12
150  TT(I,J)=0.
      TT(1,1)=BNA
      TT(2,2)=BNA
      TT(1,2)=-CSA
      TT(2,1)= CSA
      TT(3,3)=1.
      DO 155 I=3,9,3
      DO 152 I=1,3
      DO 152 J=1,3
152  TT(I+1,I+J)=TT(I,J)
155  CONTINUE
      TT(1,3)=-YL1*BNA-XL1*CSA
      TT(2,3)=-YL1*CSA+XL1*BNA
      TT(7,9)=TT(1,3)
      TT(8,9)=TT(2,3)
      DO 190 I=1,6
      DO 190 I1=1,10,3
      I2=I1+2
      DO 180 J=11,12
      XX=0.
      DO 170 K=11,12
170  XX=XX+TF(I,K)*TT(K,J)
180  T(I,J)=XX
190  CONTINUE
      RETURN
C
C   BEAM LOCAL TRANSFORMATION
200  D1=-1./XLR
      TF(1,2)=-1.
      TF(1,5)=1.
      TF(2,1)=1.+A/XLR
      TF(3,1)=A/XLR
      TF(2,4)=B/XLR
      TF(3,4)=1.+B/XLR
      TF(2,3)=-D1
      TF(3,3)=-D1
      TF(2,6)=D1
      TF(3,6)=D1
      DO 210 I=1,3
      DO 210 J=1,3
210  TT(I,J)=0.
      TT(1,1)=BNA
      TT(2,2)=BNA
      TT(1,2)=-CSA
      TT(2,1)= CSA
      TT(3,3)=1.
      DO 230 J=1,3
      DO 230 I1=1,4,3
      I2=I1-1
      DO 230 J1=1,3
      XX=0.
      DO 220 K=1,3
220  XX=XX+TF(J,I2+K)*TT(K,J1)
      I=J1+12
230  T(J,I)=XX
      RETURN
C
C   PANEL TRANSFORMATION
C
300  D1=1./XLR
      D2=1./A
C
      IF(KK.EQ.5) GO TO 305
C
      TF(1,4)=-D1
      TF(2,4)=-D1

```

```

TF(1,1)=D1
TF(2,1)=D1
TF(2,5)=-D2
TF(2,6)=D2
TF(1,2)=-D2
TF(1,3)=D2
TF(3,5)=-0.5
TF(3,6)=-0.5
TF(3,2)=0.5
TF(3,3)=0.5

```

C

```

KN=3
GO TO 315

```

C

```

305 TF(1,1)=D1
TF(1,4)=-D1
TF(1,2)=-D2/2.
TF(1,3)=D2/2.
TF(1,5) = -D2/2.
TF(1,6) = D2/2.

```

C

```

KN=1

```

C

```

315 DO 310 I=1,6
      DO 310 J=1,10
310   TT(I,J)=0.
      TT(1,1)=CSA
      TT(1,2)=SNA
      TT(1,3)= B
      TT(2,4)=1.
      TT(3,5)=1
      TT(4,6)=CSA
      TT(4,7)=SNA
      TT(4,8)= B
      TT(5,9)=1.
      TT(6,10)=1.
      DO 330 I1=1,4,3
        I2=I1-1
        JJ=0
        IF(I1.EQ.4) JJ=5
        DO 330 J1=1,5
          XX=0.
          DO 320 K=1,3
320   XX=XX+TF(J,I2+K)*TT(K,J1)
          I=J1+JJ
330   T(J,I)=XX
      RETURN

```

C

C DIAGONAL TRANSFORMATION

C

```

400 T(1,1)=DCOS(XLR)*CSA
T(1,2)=DCOS(XLR)*SNA
T(1,3)= DCOS(XLR)*XL1
T(1,4)=DSIN(XLR)
T(1,5)=-T(1,1)
T(1,6)=-T(1,2)
T(1,7)=-T(1,3)
T(1,8)=-T(1,4)
RETURN
END
SUBROUTINE STIFF (IO,B,R,NN,NS)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION B(1)
COMMON/JUNK/NLD,N,ND,MM,MN,LM(12),IFIL(53)
COMMON/BUNK/ P(12,3),TT(8),AFIL(216)
COMMON/STIF/EB(12,12),BA(8,12),T(8,12)
COMMON/FTAPES/ NTS,NTE,NTBL,NSKS
NSKS=3
NTS=11
NTE=12

```

```

NTBL=13
NLD=3
MM=2*MM
MM6=MM+6
LB=(MM*(MM+1))/2
LC=MM*MM
NE=MM+NLD-MM
LE=MM*NE
NMM=MM-MM
LSL=(MM*(MM+1))/2+MM*NLD
NNL=MM+NLD
N1=1
N2=N1+MAX0(LB,LE)
N3=N2+LC
N4=N1+LSL
N3=MAX0(N3,N4)
N4=N3+MAX0(LB,LE)
N5=N4-MM6*6
N6=N5-MM*3
N7=N6+NNL
N8=N7+MM
IF (IO.GT.0) GO TO 50
IO=N8-N1
RETURN
50 GO TO (100,200,300,400,500) , IO
C
C   IO=1  ZERO ARRAYS
C
100 NL=N8-1
    DO 110 I=N1,NL
110 B(I)=0.0
    REWIND NTSL
    REWIND NTB
    REWIND NTE
    WRITE (NTS) (B(I),I=1,LS)
    WRITE (NTE) (B(I),I=1,LE)
    WRITE (NTSL) (B(I),I=1,LSL)
    RETURN
C
C   IO=2  SHIFT STORAGE
C
200 REWIND NTB
    READ (NTB) (B(I),I=1,LS)
    NL=N8-N1
    DO 210 I=N2,NL
210 B(I)=0.0
    RETURN
C
C   IO=3  REDUCE EQN,8  WRITE 88 EQNS ON TAPE 3 (NBK8)
C
300 MM6=MM+6
    CALL SHRINK (B(N1),LS,B(N8),MM,NNL,B(N7),B(N2),B(N3),B(N3),B(N1),
1      B(N1),NE,LSL,B(N4),B(N5),MM6,MM,N8)
    RETURN
C
C   IO=4  WRITE LAT STIF ON TAPE 2
C
400 NFR=MM-MM-3
    NT2=2
    NF=N1
    NL=(NFR*(NFR+1))/2
    M=LSL-NMM
    L=M-NMM
    K=L-NMM
    WRITE (NT2) N,NFR,(B(I),I=NF,NL),(B(K+1),I=1,NFR),
1      (B(L+1),I=1,NFR),(B(M+1),I=1,NFR)
    RETURN
C
C   IO=5  ADD ELEMENT STIFF TO FRAME STIFFNESS
C
500 MM6=MM+6

```

```

CALL ADDSM (B(N1),B(N2),B(N3),B(N4),B(N5),LB,MM,MN6,MN)
RETURN
C
END
SUBROUTINE ADDSM (S,C,SB,EF,PF,LB,MM,MN6,MN)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION B(LB),C(MM,MM),SB(LB),EF(MN6,8),PF(MN,3)
COMMON/STIF/ EB(12,12),BFIL(192)
COMMON/JUNK/ NLD,N,ND,LD,JD,LM(12),IFIL(53)
COMMON/BUNK/ P(12,3),TT(8),AFIL(216)
DIMENSION KM(12)
C
DO 100 I=1,ND
  II=LM(I)
  DO 50 J=1,3
    II=II-MM
    IF (II) 20,20,50
  20 KM(I)=J
  GO TO 100
  50 KM(I)=3
100 CONTINUE
C
C ADD ELEMENT STIFF TO FRAME STIFFNESS
C
MJ=MN+3*(N-1)
DO 320 I=1,ND
  II=LM(I)
  IF (II) 320,320,110
110 KI=KM(I)
  DO 290 J=1,ND
    JJ=LM(J)
    IF (JJ.LT.II) GO TO 290
    KJ=KM(J)
    MI=3*(N-1)
    GO TO (120,150,210),KI
120 GO TO (130,140,200),KJ
130 L=(JJ*(JJ-1))/2+II
    S(L)=S(L)+EB(I,J)
    GO TO 290
140 C(II,JJ-MM)=C(II,JJ-MM)+EB(I,J)
    GO TO 290
150 GO TO (290,180,200),KJ
180 JM=JJ-MM
    L=(JM*(JM-1))/2+II-MM
    SB(L)=SB(L)+EB(I,J)
    GO TO 290
200 MI=0
210 EF(II-MI,JJ-MJ)=EF(II-MI,JJ-MJ)+EB(I,J)
290 CONTINUE
    GO TO (300,300,320),KI
300 DO 310 L=1,3
310 PF(II,L)=PF(II,L)+P(I,L)
320 CONTINUE
C
RETURN
END
SUBROUTINE SHRINK (S,LS,KH,MM,NML,SD,C,SB,E,EB,SL,NE,LSL,EF,PF,
1 MN6,MN,NG)
C
C PERFORMS BLOCK BY BLOCK STATIC CONDENSATION ON SUBASSEMBLAGE
C EQUATIONS
C
C -----
C | | | NBS=3*NUMBER OF STORIES
C | S C E | MM=3*NUMBER OF COLUMN LINES
C | | | E=(MM*NBS)
C | SB EB | B=(MM*(MM+1))/2
C | | | EB=(MM*NBS)
C | | SL | C=MM*MM
C | | | BL=(NBS*(NBS+1))/2

```

```

C -----          SS=(MM*(MM+1))/2
C
C MAXIMUM STORAGE GOVERNED BY THAT REQUIRED FOR ANY THREE BLOCKS
C
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION B(LB),KH(NNL),C(MM,MM),SB(LB),SD(MM)
1      ,E(MM,NE),EB(MM,NE),SL(LSL),EF(MM,0),PF(MN,3)
COMMON/JUNK/NLD,N,ND,LD,JD,LM(12),FIL(53)
COMMON/BUNK/ P(12,3),TT(8),AFIL(216)
COMMON/FTAPEB/NTS,NTE,NTSL,NBKS
C
NLD=3
MN=2*MM
MNP=MM+1
MNP=MM+1
NNN=MM+3*N+3
NN=NNL-NLD
NNM=NN-MN
C
C DETERMINE PROFILE OF (B,C,SS)
C
JB=0
DO 50 J=1,MM
KH(J)=1
DO 40 I=1,J
IF (B(JB+I)) 50,40,50
40 KH(J)=I+1
50 JB=JB+J
DO 70 J=1,MM
KH(J+MM)=1
DO 60 I=1,MM
IF (C(I,J)) 70,80,70
80 KH(J+MM)=I+1
70 CONTINUE
C
C REDUCTION OF B
C
SD(1)=B(1)
JB=1
DO 300 J=2,MM
SD(J)=0.0
JM=J-1
IF (J,SD,2) GO TO 260
IB=1
DO 250 I=2,JM
IM=I-1
SB=0.0
KF=MAX0(KH(I),KH(J))
IF (KF.GT.IM) GO TO 250
C
C REDUCE B BY S,S
C
DO 200 K=KF,IM
200 SB=SB+(IB-K)*B(JB+K)
S(JB+I)=B(JB+I)-SB
250 IB=IB+I
C
C RED COL BY SELF
C
260 SB=0.0
KF=KH(J)
IF (KF.GT.JM) GO TO 290
KD=(KF*(KF+1))/2
DO 280 K=KF,JM
IF (B(KD)) 270,280,270
270 T=B(JB+K)/B(KD)
SB=SB+T*B(JB+K)
S(JB+K)=T
280 KD=KD+K+1
S(JB+J)=B(JB+J)-SB

```

```

290 BD(J)=B(JB+J)
300 JB=JB+J
C
C   REDUCTION OF C,SB
C
   JB=0
   DO 500 J=MMF,MM
   JJ=J-MM
   JM=J-1
   IB=1
   DO 450 I=2,JM
   II=I-MM
   IM=I-1
   KL=MINO(IM,MM)
   KF=MAXO(KH(I),KH(J))
   IF (KF.GT.KL) GO TO 450
   SB=0.0
   IF (I.GT.MM) GO TO 430
C
C   RED C BY S,C
C
   DO 420 K=KF,KL
420 SB=SB+B(IB+K)*C(K,JJ)
   C(I,JJ)=C(I,JJ)-SB
   GO TO 450
C
C   RED SB BY C,C
C
430 DO 440 K=KF,KL
440 SB=SB+C(K,II)*C(K,JJ)
   SB(JB+I)=SB(JB+I)-SB
450 IB=IB+I
C
C
C   RED COL BY SELF
   SB=0.0
   KF=KH(J)
   IF (KF.GT.MM) GO TO 500
   DO 460 K=KF,MM
   IF (BD(K)) 455,460,455
455 T=C(K,JJ)/BD(K)
   SB=SB+T*C(K,JJ)
   C(K,JJ)=T
460 CONTINUE
   SB(JB+JJ)=SB(JB+JJ)-SB
500 JB=JB+JJ
   REWIND NTS
   WRITE (NTS) SB
   WRITE (NBKS) S,C
C
C   OVERWRITE SB WITH (E,EB)
C
   REWIND NTE
   READ (NTE) E
   L=3*(N-1)
   DO 810 I=1,MM
   DO 810 J=1,6
810 E(I,J+L)=E(I,J+L)+EF(I,J)
   DO 820 I=1,MM
   DO 820 J=1,3
820 E(I,J+MM)=E(I,J+MM)+PF(I,J)
C
C   DETERMINE PROFILE OF (E,EB)
C
   DO 90 J=MMF,NML
   JJ=J-MM
   KH(J)=1
   DO 90 I=1,MM
   IF (E(I,JJ)) 90,90,90
90 KH(J)=I+1
90 CONTINUE

```

```

C
C   REDUCE E BY B,E
C
  JB=0
  DO 540 J=MNP,NNL
  JJ=J-MN
  IB=1
  DO 530 I=2,MM
  IM=I-1
  KF=MAXD(KH(I),KH(J))
  BB=0.0
  IF (KF.GT.IM) GO TO 530
  DO 520 K=KF,IM
520  BB=BB-B(IB+K)*E(K,JJ)
  E(I,JJ)=E(I,JJ)-BB
530  IB=IB+1
540  CONTINUE
  DO 830 I=1,MM
  DO 830 J=1,NE
830  EB(I,J)=0.0
  L=3*(N-1)
  DO 840 I=1,MM
  DO 840 J=1,8
840  EB(I,J+L)=EB(I,J+L)+EF(I-MM,J)
  DO 845 I=1,MM
  DO 845 J=1,NLD
845  EB(I,J+MM)=EB(I,J+MM)+PF(I-MM,J)
C
C   RED EB BY C,E
C
  DO 570 J=MNP,NNL
  JJ=J-MN
  DO 560 I=MNP,MN
  II=I-MM
  KF=MAXD(KH(I),KH(J))
  BB=0.0
  IF (KF.GT.MM) GO TO 560
  DO 550 K=KF,MM
550  BB=BB+C(K,II)*E(K,JJ)
560  EB(II,JJ)=EB(II,JJ)-BB
570  CONTINUE
  REWIND NTE
  REWIND NTSL
  WRITE (NTE) EB
C
C   OVERWRITE B BY BL
C
  READ (NTSL) BL
  L=3*(N-1)
  K=(L*(L+1))/2
  DO 860 J=1,8
  DO 850 I=1,J
850  BL(K+L+I)=BL(K+L+I)+EF(I-MN,J)
860  K=K+L+J
C
C   RED BL BY E,E
C
  JB=0
  DO 700 J=MNP,NNL
  JJ=J-MN
  JM=J-1
  JM=MINO(JM,MM)
  IF (MNP.GT.JM) GO TO 810
  DO 600 I=MNP,JM
  KF=MAXD(KH(I),KH(J))
  II=I-MN
  BB=0.0
  IF (KF.GT.MM) GO TO 600
  DO 580 K=KF,MM
580  BB=BB+E(K,II)*E(K,JJ)
600  BL(JB+I)=BL(JB+I)-BB

```



```
C
C   REDUCE COLS BY BELF
C
610  SS=0.0
     KF=KH(J)
     IF (KF.GT.MM) GO TO 660
     DO 650 K=KF,MM
     IF (SD(K)) 640,650,640
640  T=E(K,JJ)/SD(K)
     SS=SS+T*E(K,JJ)
     E(K,JJ)=T
650  CONTINUE
660  JA=MIN0(JJ,MM)
     IF (J.GT.MN) GO TO 700
     BL(JB+JA) = BL(JB+JA) - SS
700  JB = JB + JA
     REWIND NTBL
     WRITE(NBK8) E,KH
     WRITE(NTBL) BL
C
C   RETURN
C
C   END
C
C   FUNCTION TABA (NPC,SF,T,PA)
C   IMPLICIT REAL*8 (A-H)
C   IMPLICIT REAL*8 (O-Z)
C   DIMENSION PA(2,NPC)
C
C   SPECTRUM INTERPOLATION
C
DO 100 I=2,NPC
T1=PA(1,I-1)
T2=PA(1,I)
IF (T.LE.T2) GO TO 200
100 CONTINUE
200 R1=(T2-T)/(T2-T1)
R2=(T-T1)/(T2-T1)
TABA=SF*(PA(2,I-1)*R1+PA(2,I)*R2)
RETURN
END
```

```

SUBROUTINE LAT(BN,A,BB,RR,B,R,D,AA,MBS,NFS,MTF,HED,MBT,GRAV,ICHEK
1 ,RRR,NPT,ITYPE)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION BB(MBS,MBS),RR(MBS,5),A(MBT,14),S(NFS,NFS),R(NFS,3)
1 ,D(MBT,MTF,2),AA(MTF,5),HED(MTF,4),BN(MBT)
2 ,RRR(MBS,2)
COMMON/GEN/ NBT,NDF,NTF,NLD,NAT,NFO,NSD,BHED(9),FHED(7),NBS
1 ,RLAB(3),IB,IZ,T(6)
COMMON /BUNK/ AI(3,3),AJ(3,3),AR(3,3),AB(3,3),AFIL(224)
CHARACTER*4 BN,HED,BHED,FHED,RLAB
C
C COMPUTE STRUCTURE LATERAL STIFFNESS , SOLVE STATIC LOAD CASES
C
IF( ICHEK.NE.0 ) GO TO 105
REWIND 2
DO 50 I=1,MBS
DO 40 J=1,5
40 RR(I,J)=0
DO 50 J=1,MBS
50 BB(I,J)=0
DO 100 I=1,NBT
II=I3*(I-1)
BS(II+1,II+1)=A(I,7+IB)
IF(NSD.EQ.0) BS(II+2,II+2)=A(I,8)
DO 100 J=1,13
DO 100 L=1,2
LL=5+3*L+J+IB
100 RR(II+J,L+3)=A(I,LL)
C
105 WRITE(NPT,3000)
IFP=0
DO 500 K=1,NTF
READ (5,1000) IF,IFC,X1,Y1,ANG,(HED(K,J),J=1,4)
WRITE (NPT,2000) K,IF,IFC,X1,Y1,ANG,(HED(K,J),J=1,4)
IF( ICHEK.NE.0 ) GO TO 500
IF(IF.EQ.IFP) GO TO 150
READ (2)NT,NFR,((S(I,J),I=1,J),J=1,NFR),((R(I,L),I=1,NFR),L=1,3)
DO 145 I=1,NFR
DO 145 J=1,NFR
145 S(J,I)=S(I,J)
IFP=IF
150 DM1 = 1.0
ANG=ANG*DATAN(DM1)/45
DO 190 I=1,3
DO 190 J=1,3
190 AI(I,J)=0
C
AI(1,1)=DCOS(ANG)
AI(1,2)= DSIN(ANG)
AI(2,1)=-AI(1,2)
AI(2,2)=AI(1,1)
AI(3,3)=1.
DO 195 I=1,3
DO 195 J=1,3
195 AJ(J,I)=AI(I,J)
C
DO 200 N=NT,NBT
XM=X1-A(N,5)
YM=Y1-A(N,6)
D(N,K,1)=-YM*DCOS(ANG)-XM*DSIN(ANG)
200 D(N,K,2)= YM*DSIN(ANG)-XM*DCOS(ANG)
C
DO 400 M=NT,NBT
I2=3*(M-NT)
AI(1,3)=D( N,K,1)
AI(2,3)=D( N,K,2)
C
DO 400 M=NT,NBT
I2=3*(M-NT)
IR=I3*(M-1)

```

```

      AJ(3,1)=D(M,K,1)
      AJ(3,2)=D(M,K,2)
C
      DO 225 I1=1,3
      DO 225 J1=1,13
      JJ=J1+18
      AR(11,JJ)=0
      DO 225 KK=1,3
225 AR(11,JJ)=AR(11,JJ)+8(12+11,J2+KK)*A1(KK,JJ)
C
      DO 275 I1=1,13
      I1=I1+18
C
      IF(N.NE.NT) GO TO 260
      DO 250 L=1,3
      DO 250 KK=1,3
250 RR(IR+11,L)=RR(IR+11,L)+AJ(11,KK)*R(12+KK,L)
C
260 DO 275 J1=1,13
      JJ=J1+18
      AB(11,JJ)=0
      DO 275 KK=1,3
275 AB(11,JJ)=AB(11,JJ)+AJ(11,KK)*AR(KK,JJ)
C
      NN=13*(NT-1)
C
      DO 300 I=1,13
      I1=13*(M-NT)+I
      DO 300 J=1,13
      JJ=13*(N-NT)+J
300 BB(NN+11,NN+JJ)=BB(NN+11,NN+JJ)+AB(1+18,J+18)
400 CONTINUE
C
      AA(K,1)=IF
      AA(K,2)=IFC
      AA(K,3)=A1(1,1)
      AA(K,4)=A1(1,2)
      AA(K,5)=NT
500 CONTINUE
      IF(1CHEK.NE.0) RETURN
C
C---- MOD OF LAT STIFFNESS FOR P-DELTA EFFECTS
C
      IF( NAT.GT.9 ) REWIND 1
      IF( NAT.GT.9 ) WRITE(1) BB
      IF( DABS(GRAV).LT.1.0E-10 ) GO TO 655
      IPD=0
501 XMT=0.0
      XMMT = 0.0
      DO 650 I=1,NST
      H = A(1,2)
      XMT = XMT + A(1,3)
      XMMT = XMMT + A(1,4)
      MM = ( I - 1 ) * 13
C
      DO 600 J=1,13
      IF( J.NE.3 ) PDEL = XMT*GRAV/H
      IF( J.EQ.3 ) PDEL = XMMT*GRAV/H
      NN = MM + J
      BB(NN,NN) = BB(NN,NN) - PDEL
      IF( 1.0E.NST ) GO TO 600
      BB(NN,NN+13) = BB(NN,NN+13) + PDEL
      BB(NN+13,NN) = BB(NN+13,NN) + PDEL
      BB(NN+13,NN+13) = BB(NN+13,NN+13) - PDEL
600 CONTINUE
650 CONTINUE
      IF(IPD.EQ.1)GO TO 730
C
C---- END OF P-DELTA MODS
C
655 NT2 = 2

```

```

REWIND NT2
WRITE (NT2) BS,MM
IF(NAT.EQ.1) RETURN
IF(DABS(GRAV).LT.1.0D-10)GO TO 657
DO 656 I=1,NBS
DO 656 J=1,2
656 RRR(I,J)=RR(I,J+3)
657 CONTINUE
C DO 658 I = 1,NBS
C IF ( BS(I,1) .LE. 0.0 ) THEN
C WRITE (6,*) ' MATRIX BS '
C WRITE (6,*) 'BS('',1,'',',',1,') = ',BS(I,1)
C GOTO 659
C ELSE
C WRITE (6,*) 'BS('',1,'',',',1,') = ',BS(I,1)
C ENDF
C 658 CONTINUE
C GOTO 660
C 659 WRITE (6,1101)
C WRITE (6,1102)
C STOP
C 1101 FORMAT (T5,'*****')
C 1102 FORMAT (T5,'ZERO ON DIAGONAL OF STRUCTURE STIFFNESS MTX.')
C 660 CONTINUE
CALL SOLVE(BS,NBS,RR,5)
C
C PRINT STRUCTURE DISPLACEMENTS
C
IF ( ITYPE .EQ. 0 ) THEN
WRITE(6,1001)
WRITE(6,1003)
CALL PROUT( RR,NBS,5,SN,NST,RLAB,13,18 )
ENDIF
C
WRITE (2) RR
WRITE (2) AA,D,HED
IF(DABS(GRAV).LT.1.0D-10)GO TO 750
DO 725 I=1,NBS
DO 725 J=1,NBS
725 BS(I,J)=0.0
IPD=1
GO TO 501
C
C-----CALCULATE P-DELTA FORCES
C
730 CONTINUE
DO 740 I=1,NBS
K1=I-13
K2=I+13
IF(K1.LE.0)K1=1
IF(K2.GT.NBS)K2=NBS
DO 735 J=1,2
XX=0.
DO 732 K=K1,K2
732 XX=XX+BS(I,K)*RR(K,J+3)
735 RRR(I,J)=RRR(I,J)-XX
740 CONTINUE
750 CONTINUE
C
C---- CALC DRIFTS
N = NST - 1
DO 722 I=1,5
IF(NST.EQ.1)GO TO 721
DO 720 J=1,N
JJ = 13*( J - 1 ) + 1
RR(JJ,1) = ( RR(JJ,1) - RR(JJ-13,1) )/A(J,2)
IF( 13.NE.3 ) GO TO 720
RR(JJ+1,1) = ( RR(JJ+1,1) - RR(JJ-4,1) )/A(J,2)
RR(JJ+2,1) = RR(JJ+2,1) - RR(JJ+5,1)
720 CONTINUE
721 JJ = 13*( NST - 1 ) + 1

```

```

      RR(JJ,1) = RR(JJ,1)/A(NST,2)
      IF( 13.EQ.3 ) RR(JJ+1,1) = RR(JJ+1,1)/A(NST,2)
722 CONTINUE
C---- PRINT OUT DRIFTS
      IF ( ITYPE .EQ. 0 ) THEN
        WRITE(6,1002)
        WRITE(6,1003)
        CALL PROUT( RR,NBS,5,8N,NST,RLAB,13,18 )
      ENDIF
C
C-----CALCULATE TOTAL RESISTING FORCES FOR STATIC LAT.LOAD CASES INCL.
C----- P-DELTA
      IF(DABB(GRAV) .LT. 1.0D-10)GO TO 790
      DO 760 I=1,NBS
      DO 760 J=1,5
        IF(J.LT.4)RR(I,J)=0
      760 IF(J.GE.4)RR(I,J)=RRR(I,J-3)
C-----CALCULATE CUMULATIVE SHEAR FORCES
      IF(NST.EQ.1)GO TO 786
C
      N=13*(NST-1)
      DO 765 I=1,N
      DO 765 J=4,5
      765 RR(I+13,J)=RR(I+13,J)+RRR(I,J)
      786 WRITE(6,1004)
        WRITE(6,1006)
        WRITE(6,1003)
        CALL PROUT(RR,NBS,5,8N,NST,RLAB,13,18)
C
C-----CALCULATE CUMULATIVE OVERTURNING FORCES
C
      IF(13.NE.3)GO TO 772
      DO 770 I=1,NBT
      II=I*3
      DO 770 J=4,5
      770 RR(II,J)=0.0
      772 DO 780 J=4,5
        XM=0.
        YM=0.
      DO 775 I=1,NBT
      II=(I-1)*13+1
      RR(II,J)=XM+RR(II,J)*A(I,2)
      IF(13.EQ.3)RR(II+1,J)=YM+RR(II+1,J)*A(I,2)
      XM=RR(II,J)
      775 IF(13.EQ.3)YM=RR(II+1,J)
      780 CONTINUE
        WRITE(6,1005)
        WRITE(6,1006)
        WRITE(6,1003)
        CALL PROUT(RR,NBS,5,8N,NST,RLAB,13,18)
      790 CONTINUE
C
      RETURN
1000 FORMAT (2I5,3F10.0,4A4)
2000 FORMAT (10,15,19,8X, 3F12.2,10X,4A4)
1001 FORMAT( ///,1H ,17(1H-),/,18H STORY DEFLECTIONS ,/,1H ,17(1H-), /)
1002 FORMAT( ///,1H ,18(1H-),/,19H STORY DRIFT RATIOS ,/,1H ,18(1H-),/)
1003 FORMAT( /,20X,85H OUTPUT COLUMNS 1,2,3 CONTAIN RESULTS FROM VERTIC
1AL LOAD CASES 1,II,III, RESPECTIVELY ,/20X,
2 84H OUTPUT COLUMNS 4,5 CONTAIN RESULTS FROM STATIC LATERAL LOAD C
3ASES A,B, RESPECTIVELY ,// )
1004 FORMAT(///1H ,12(1H-),/,13H STORY SHEARS/1H ,12(1H-),/)
1005 FORMAT(///1H ,25(1H-),/,26H STORY OVERTURNING MOMENTS,/,1H ,
1 25(1H-),//)
1006 FORMAT(/90H NOTE THAT THE FORCE QUANTITIES BELOW FOR LOAD CASES A
1AND B INCLUDE P-DELTA EFFECTS. /
180H HOWEVER, P-DELTA FORCES ARE NOT CALCULATED FOR LOAD CASES 1,II
1 AND III. //)
3000 FORMAT ( // 20H1FRAME POSITION DATA ,//
1 23H FRAME 1D FORCE CODE ,10X,2HX1,10X,2HY1,8X,3HANG )
      END

```

```

SUBROUTINE SOLVE(A,N,B,NL)
C
C SOLUTION OF SYMMETRICAL LINEAR EQUATIONS- E L WILSON
C
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION A(N,N),B(N,NL)
C
M=0
C REDUCTION OF M TH EQUATION
C
50 M=M+1
MM=M+1
WRITE (6,*) 'B(' ,M, ',' ,M, ') = ' ,A(M,M)
IF ( A(M,M) .LE. 0.0 ) THEN
WRITE (6,1000)
WRITE (6,1001)
ENDIF
1000 FORMAT (T5, '*****')
1001 FORMAT (T5, 'ZERO OR MINUS ON DIAGONAL')
DO 80 L=1,NL
80 B(M,L)=B(M,L)/A(M,M)
IF (M-N) 70,130,70
70 DO 80 J=MM,N
80 A(M,J)=A(M,J)/A(M,M)
C
C SUBSTITUTION INTO REMAINING EQUATIONS
C
DO 120 I=MM,N
IF (A(I,M)) 90,120,90
90 DO 100 J=I,N
A(I,J)=A(I,J)-A(I,M)*A(M,J)
100 A(J,I)=A(I,J)
DO 110 L=1,NL
110 B(I,L)=B(I,L)-A(I,M)*B(M,L)
120 CONTINUE
GO TO 50
C
C BACK SUBSTITUTION
C
130 M=M-1
IF (M.EQ.0) GO TO 150
MM=M+1
DO 140 L=1,NL
DO 140 J=MM,N
140 B(M,L)=B(M,L)-A(M,J)*B(J,L)
GO TO 130
C
150 RETURN
END
SUBROUTINE EARTH(SN,A,F,W,WM,IQ,S,PA,Z,MBS,MBT,NMD,R,DBC,CCQ,NQ,
1 GRAV)
IMPLICIT REAL*8 (A-H)
IMPLICIT REAL*8 (O-Z)
DIMENSION F(MBS,MBS),B(MBS,MBS),WM(1),W(1),IQ(1),A(MBT,4),PA(2,1)
2 ,SN(MBT),R(MBS,4),DBC(NQ,NQ),CCQ(NQ,NQ),Z(MBS,NQ),RR(3)
COMMON/GEN/ NST,NDF,NTF,NLD,NAT,NFQ,NBD,BHED(9),FHED(7),NBS
1 ,RLAS(3),IB,IS,T(5)
COMMON/JUNK/ BHED(7),KDD(5),IFIL(53)
COMMON/BUNK/ BC(2),AFIL(258)
COMMON /DYN/ NTIME,DT,NPC,DAMP
CHARACTER*4 SN,RLAS,BHED,BHED,FHED
C
C COMPUTE MODE SHAPES AND FREQUENCIES
C
DM1 = 1.0
TPI = 8.0*DATAN(DM1)
TM = 0.0
TMM = 0.0
DO 100 I=1,NST
TM = TM - A(I,3)

```

```

    TMM = TMM + A(1,4)
    I1=I3*(I-1)+1
    XM(I1)=A(1,3)
    XM(I1+1)=A(1,3)
100 XM(I1+2)=A(1,4)
    IF(NAT.LT.0)GO TO 510
    REWIND 2
    READ(2)B
    IF(NAT.EQ.0)GO TO 700
C
    DO 150 I=1,NBS
    IF(XM(I).GT.0.) GO TO 150
    WRITE (6,3002)
    STOP
150 XM(I)=1.0/DSQRT(XM(I))
    DO 200 I=1,NBS
    DO 200 J=1,NBS
200 B(I,J)=B(I,J)*XM(I)*XM(J)
C
    CALL EIGEN(B,NBS,0,F,NR,W,IQ)
C
    DO 250 I=1,NBS
    W(I)=B(I,1)
    DO 250 J=1,NBS
250 F(I,J)=F(I,J)*XM(I)
    DO 300 I=1,NFQ
    WM=W(I)
    DO 270 J=1,NBS
    IF(W(J).GT.WM) GO TO 270
    WM=W(J)
    K=J
270 CONTINUE
C
    W(K)=W(I)
    W(I)=TP1/DSQRT(WM)
    DO 300 J=1,NBS
    WM=F(J,K)
    F(J,K)=F(J,I)
300 F(J,I)=WM
    WRITE(6,1005) ( I,W(I),I=1,NFQ )
    GO TO 520
C
C---- GENERATE APPROX MODE SHAPES
C
510 CALL MODGEN(BN,A,A(1,0),F,XM,XM,W,B,NBS,MST,NFQ,13,18,NBD)
    NAT = IABS( NAT )
C
    PRINT MODES,PERIODS
520 WRITE(6,4000)
    DO 522 I=1,NFQ
    X = 1.0/W(I)
    Y = TP1/W(I)
522 WRITE(6,4001) I,W(I),X,Y
    DO 600 I=1,NFQ,8
    IH=I+7
    IF(IH.GT.NFQ) IH=NFQ
    WRITE (6,2003) (J,J=1,IH)
    DO 600 N=1,NST
    LN=NST+1-N
    NN=I3*(N-1)
    WRITE (6,2002)
    DO 600 J=1,13
600 WRITE (6,2004) LN,BN(N),RLAB(J+18),( F(NN+J,K),K=1,IH)
C---- CALC GLOBAL EFFECTIVE MODAL MASS ( NORMALIZED )
    DO 523 I=1,NFQ
    DO 523 J=1,3
523 R(I,J) = 0.0
    IF( NBD.LE.0 ) GO TO 535
C---- PLANAR ANAL
    DO 530 J=1,NFQ
    X = 0.0
    DO 525 I=1,NST

```

```

525 X = X + F(I,J)*A(I,3)
      IF( NBD.EQ.1 ) R(J,1) = X*X/TM
      IF( NBD.NE.1 ) R(J,2) = X*X/TM
530 CONTINUE
      GO TO 548
C---- 3-D ANAL
535 DO 545 J=1,NFQ
      X = 0.0
      Y = 0.0
      ZZ = 0.0
      DO 540 I=1,NBT
          II = 3*( I - 1 ) + 1
          X = X + F(II,J)*A(I,3)
          Y = Y + F(II+1,J)*A(I,3)
540 ZZ = ZZ + F(II+2,J)*A(I,4)
          R(J,1) = X*X/TM
          R(J,2) = Y*Y/TM
545 R(J,3) = ZZ*ZZ/TM
548 WRITE(6,4002)
      WRITE(6,4003) ( I, ( R(I,J),J=1,3 ), I=1,NFQ )
      DO 549 J=1,3
          RR(J)=0.
      DO 549 I=1,NFQ
549 RR(J)=RR(J)+R(I,J)
      WRITE(6,4004)(RR(I),I=1,3)
      IF(NAT.EQ.1) RETURN
C
C DYNAMIC ANALYSIS
C
      IF( (NAT.NE.4) .AND. (NAT.NE.8) .AND. (NAT.NE.9) ) GO TO 440
C
C GROUND MOTION CONTROL DATA
      READ(5,1001) NPC,NTIME,BF,F1,DT,KOD,BHED
      IF(NBD.NE.0)KOD(5)=0
      WRITE(6,2005) BHED,NPC,NTIME,BF,F1,DT,KOD
      GO TO 445
C
440 IF( (NAT.NE.3) .AND. (NAT.NE.5) .AND. (NAT.NE.7) ) GO TO 700
C
C RESPONSE SPECTRUM DATA
      READ(5,1000) NPC,NMD,BF,F1,DP,SB,KOD,BHED,( PA(1,1),PA(2,1),I=1,
1 NPC )
      IF( NMD.GT.NFQ ) NMD = NFQ
      IF( SB.LE.0.0 ) SB = 1.0E+03
      IF(NBD.NE.0)KOD(5)=0
      WRITE(6,2000) BHED,NPC,NMD,BF,F1,DP,SB,KOD,( PA(1,1),PA(2,1),I=1,
1 NPC )
      WRITE(6,4005)
      DX = 1.0
      DO 441 I=1,NFQ
          BAG=TABA(NPC,DX,W(I),PA)
441 WRITE(6,4008)I,W(I),BAG
      CALL DSCCOC( DSC,COC,W,NFQ,DP,SB )
C---- IF DSC AND/OR COC COMBO NOT RECD THEN SET FLAG SUCH THAT
C CALCS SKIPPED IN TYPE 3 ANAL ( SEE ROUTINE STRESS )
      IF( KOD(2).LE.0 ) DSC(1,1) = -1.0
      IF( KOD(3).LE.0 ) COC(1,1) = -1.0
C
C MODAL PARTICIPATION FACTORS
C
445 F1=FI*DATAN(DM1)/45.
      SC(1)=DBIN(F1)
      SC(2)=DCOB(F1)
      IFLG = 0
      IF( NAT.EQ.4 ) IFLG = 1
      IF( NAT.EQ.8 ) IFLG = 1
      IF( NAT.EQ.9 ) IFLG = 1
      DO 500 I=1,NFQ
          RUM=0.
      DO 450 J=1,NBT
          JJ=13*(J-1)+1

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```

FR=F(JJ,1)*BC(1+18)
IF(NBD.EQ.0) FR=FR+F(JJ+1,1)*BC(2)
450 RLM=RLM+FR*A(J,3)
    WM=(TP1/W(1))**2
    IF( IFLG.EQ.0 ) YM = RLM*TAB1( NPC,BF,W(1),PA )/WM
    IF( IFLG.NE.0 ) YM = RLM*BF
    DO 500 J=1,NBS
500 F(J,1)=F(J,1)*YM
C
C--- RESPONSE SPECTRUM OPTION 8
C
    IF( (NAT.EQ.6) .OR. (NAT.EQ.7) ) CALL OPT8( F,R,XM,W,DBC,COG,KOD,BN,
1 A,BC,B,Z,MBS,MST,NFQ,NMD,13,18,GRAY )
    IF( NAT.EQ.6 ) RETURN
C
C SAVE MODE SHAPES ON TAPE 1 NAT=4
C
    IF( (NAT.NE.4) .AND. (NAT.NE.8) .AND. (NAT.NE.9) ) GO TO 550
    REWIND 1
    WRITE(6,3000)
    DO 800 K=1,NFQ
    READ(5,1002) I,DAMP
    IF(DAMP.LE.1.0) GO TO 720
    DAMP=1.0
    WRITE(6,3001) I
720 WRITE(6,2008) I,DAMP
    WRITE(1) W(K),DAMP,(F(I,K),I=1,NBS)
800 CONTINUE
C
550 DO 650 K=1,NFQ
    I=NFQ+1-K
    DO 650 J=1,NBS
650 F(J,I+5)=F(J,I)
C
700 READ(2) ((F(I,J),I=1,NBS),J=1,5)
C
    RETURN
C
1000 FORMAT( 2I5,2F10.0,2F5.0,5I11 ,7A4,/, ( 2F10.0 ) )
1001 FORMAT( 2I5,3F10.0,5I11,7A4 )
1002 FORMAT (15,F10.2)
1005 FORMAT( //,10X,13H PERIODS,/, ( 10X,15,F22.17 ) )
2000 FORMAT(//22H ACCELERATION SPECTRUM ,5X, 7A4,//
1 25H NUMBER OF PERIOD CARDS = ,18, /
2 25H NUMBER OF LOWEST MODES = ,18, /
2 25H ACCEL., UNITS/SEC/SEC = ,F10.3, /
3 25H ANGLE OF EQ INCIDENCE = ,F10.3, /
* 25H DBC / COG DAMPING COE. = ,F10.3, /
* 25H DBC TIME DURATION S = ,F10.1, /
* 25H OUTPUT CODE = ,2X,4I2, /
* 25H COOR. SYSTEM CODE = ,8X,12, //
4 26H PERIOD ACCELERATION ,//,(F10.3,5X,F10.3))
2002 FORMAT (1H )
2003 FORMAT (/// 12H MODE SHAPES,/,18H LEVEL 1D DIRN ,8I13)
2004 FORMAT (15,3X,A4,2X,A4,2X,BF13.8)
2005 FORMAT (//,23H RESPONSE ANALYSIS DATA ,///
. 31H ACCELERATION HISTORY HEADING... ,7A4, //
1 30H NUMBER OF ACCELERATION CARDS ,13 , /
2 30H NUMBER OF OUTPUT TIMES ,13 , /
3 30H ACCELERATION SCALE FACTOR ,F10.4, /
4 30H ANGLE OF EQ INCIDENCE ,F10.4, /
5 30H TIME INCREMENT FOR OUTPUT ,F10.4, /
6 30H OUTPUT CODE ,2X,4I2, /
7 30H COOR. SYSTEM CODE ,8X,12, // )
2006 FORMAT(14,F12.3)
3000 FORMAT( /// 16H MODE DAMPING )
3001 FORMAT (30H DAMPING MUST BE LESS THAN 1.0 , /
1 16H VALUE FOR MODE ,13, 6H RESET )
3002 FORMAT (/// 22H NEGATIVE OR ZERO MASS ,//,21H EXECUTION TERMINATED
1)
4000 FORMAT(//,1H ,13X,4#MODE,10X,7#NATURAL,3X,8#FREQUENCY,4X,8#CIRCULAR

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```
1 ,/,13X,6NUMBER,10X, 6PERIOD,7X,4H(HZ),4X,6FREQUENCY,/ )
4001 FORMAT( 10X,17,6X,F12.6,2F12.4 )
4002 FORMAT( ////,14X,4MODE,6X,53GLOBAL EFFECTIVE MODAL MASS (AS RATIO
OF TOTAL MASS) ,
1 ,/,13X,6NUMBER,12X,1HX,11X,1HY,11X,2HZZ,/ )
4003 FORMAT( 10X,17,6X,3F12.3 )
4004 FORMAT(/14X,6TOTALS,3X,3F12.3)
4005 FORMAT(///26H MODAL SPECTRAL AMPLITUDES,/,5H MODE,7X,6PERIOD,4X,
2 SHAMPLITUDE )
4006 FORMAT(15,F12.2,F12.3)
END
SUBROUTINE SECOND(T)
REAL*8 T
integer*2 hour, minute, secnd, hundredth
c
call gettim (hour, minute, secnd, hundredth)
c GETTIM is a FORTRAN-callable subroutine in Microsoft FORTRAN version 5.00
c returning the system time with arguments in INTEGER*2
T = ((dbie(hour)*3600.)+(dbie(minute)*60.)+dbie(secnd)+
1 (dbie(hundredth)/100.))
return
END
```

ภาคผนวก ค.

การป้อนข้อมูลสำหรับโปรแกรม CU-NTABS

1. บรรทัดป้อนข้อมูลควบคุม (715, 3x, 311, 14, F10.0, 4A4)

คอลัมน์	ข้อมูล
1 - 5	จำนวนชั้นทั้งหมดของอาคาร (ไม่รวมพื้นและฐานราก)
6 - 10	จำนวนโครงข้อแข็งที่มีคุณสมบัติต่างกัน กรณีวิเคราะห์โครงสร้าง 2 มิติ ป้อนเลข 1
11 - 15	จำนวนโครงข้อแข็งทั้งหมด กรณีวิเคราะห์โครงสร้าง 2 มิติ ป้อนเลข 1
16 - 20	จำนวนชุดของแรงกระทำต่อโครงสร้าง กรณีวิเคราะห์โครงสร้าง 2 มิติพิจารณาความไม่เชิงเส้นทางเรขาคณิต ป้อนเลข 1 (ชุดของแรงกระทำต่อโครงสร้าง เกิดจากการประกอบกันขึ้นจากแรงกระทำพื้นฐาน 5 แรง, คูห้ข้อ 5 บรรทัดกำหนดแรงกระทำ)
21 - 25	รหัสลักษณะปัญหา กรณีวิเคราะห์ปัญหาสถิตศาสตร์ ป้อนเลข 0
26 - 30	จำนวนความถี่ (Number of Frequencies) ที่ใช้ในการคำนวณ กรณีวิเคราะห์ปัญหาสถิตศาสตร์ ป้อนเลข 0
31 - 35	ดีกรีความอิสระ (Degree of Freedom) ที่ต้องการในแต่ละชั้น ป้อนเลข 1 สำหรับโครงข้อแข็ง 2 มิติ ที่มีความสมมาตรในระนาบ X , ป้อนเลข 2 สำหรับโครงข้อแข็ง 2 มิติ ที่มีความสมมาตรในระนาบ Y
36 - 38	ว่าง

- 39 รหัสการคำนวณอัตราส่วนความเค้นในองค์อาคาร (Element Stress Ratio) ป้อนเลข 0 สำหรับการวิเคราะห์ความไม่เชิงเส้นทางเรขาคณิตของโครงสร้าง
- 40 รหัสปฏิบัติการ
 ป้อนเลข 0 สำหรับการวิเคราะห์ปัญหาจนเสร็จสิ้น
 ป้อนเลข 1 สำหรับตรวจการป้อนข้อมูลเท่านั้น
- 41 รหัสการวิเคราะห์
 ป้อนเลข 0 สำหรับการวิเคราะห์เชิงเส้น
 ป้อนเลข 1 สำหรับการวิเคราะห์ไม่เชิงเส้นทางเรขาคณิต
- 42 - 45 จำนวนรอบที่มากที่สุดที่ต้องการให้โปรแกรมทำงาน หากการคำนวณไม่สามารถให้ผลต่างของการเปลี่ยนตำแหน่งในแต่ละรอบอยู่ในขอบเขตของความคลาดเคลื่อนที่ยอมรับ
- 46 - 55 ความคลาดเคลื่อนที่ยอมรับ
- 56 - 71 ข้อความที่ต้องการให้พิมพ์ออกมาพร้อมกับผลการคำนวณ

2. บรรทัดป้อนข้อมูลชั้น

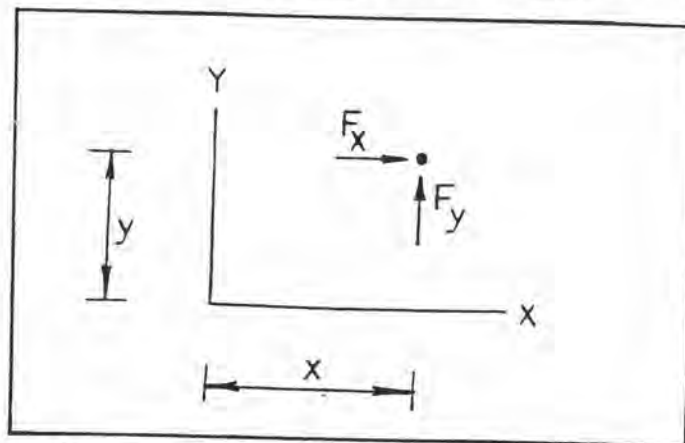
2 บรรทัดสำหรับ 1 ชั้น ข้อมูลต้องเริ่มจากชั้นบนลงล่างตามลำดับ

2.1 บรรทัดหนึ่ง (1X,A4,5X,F10.0)

คอลัมน์	ข้อมูล
2 - 5	ตัวอักษร 4 ตัวหรือน้อยกว่าสำหรับแสดงชื่อความประจำแต่ละชั้น
6 - 10	ว่าง
11 - 20	ความสูงของชั้น (ระยะระหว่างพื้นชั้นบน (หรือหลังคา) และพื้นชั้นล่าง)

2.2 บรรทัดสอง (8F10.0)

คอลัมน์	ข้อมูล
1 - 10	F_{xA} : ขนาดของแรงกระทำด้านข้างกรณี A
11 - 20	F_{yA} : ขนาดของแรงกระทำด้านข้างกรณี A
21 - 30	X_A : พิกัดตำแหน่งของแรงกระทำด้านข้างกรณี A แนว X
31 - 40	Y_A : พิกัดตำแหน่งของแรงกระทำด้านข้างกรณี A แนว Y
41 - 50	F_{xB} : ขนาดของแรงกระทำด้านข้างกรณี B
51 - 60	F_{yB} : ขนาดของแรงกระทำด้านข้างกรณี B
61 - 70	X_B : พิกัดตำแหน่งของแรงกระทำด้านข้างกรณี B แนว X
71 - 80	Y_B : พิกัดตำแหน่งของแรงกระทำด้านข้างกรณี B แนว Y



รูป ค. 1 ทิศทางบวกของแรงกระทำด้านข้าง

3. ข้อมูลโครงการอาคาร

3.1 บรรทัดป้อนข้อมูลโครงข้อแข็ง (915,7A4)

คอลัมน์	ข้อมูล
1 - 5	เลขประจำโครงข้อแข็ง
6 - 10	จำนวนชั้น (ไม่รวมพื้นและฐานราก) ของโครงข้อแข็งนี้
11 - 15	จำนวนเสาของโครงข้อแข็ง
16 - 20	จำนวนช่วงเสา (BAY) ของโครงข้อแข็ง
21 - 25	จำนวนชุดของคุณสมบัติที่ต่างกันของเสา
26 - 30	จำนวนชุดของคุณสมบัติที่ต่างกันของคาน จำนวนชุดของคุณสมบัติของคานจะเป็นตัวกำหนดจำนวนบรรทัดข้อมูลที่ต้องป้อนให้โปรแกรมในหัวข้อ 3.4
31 - 35	จำนวนชุดที่ต่างกันของแรงยึดแน่นปลาย (Fixed End Forces) ที่ประยุกต์ใช้เป็นน้ำหนักกระทำในแนวตั้งกับคาน ถ้าไม่มีแรงกระทำในแนวตั้งกระทำกับคาน ในปัญหาที่ต้องการวิเคราะห์ให้เว้นว่างในช่องนี้และยกเว้นหัวข้อ 3.5
36 - 40	จำนวนของผนังต้านแรงเฉือนในโครงข้อแข็งนี้ ถ้าไม่มีผนังต้านแรงเฉือนในโครงข้อแข็งนี้ ให้เว้นว่างในช่องนี้และยกเว้นหัวข้อ 3.8
41 - 45	ว่าง
46 - 73	ข้อความบรรยายโครงข้อแข็งนี้

3.2 บรรทัดป้อนพิกัดตำแหน่งแนวเสา (15, 2F10.0)

1 บรรทัดสำหรับ 1 แนวเสา

คอลัมน์	ข้อมูล
1 - 5	เลขประจำเสา
6 - 15	ระยะทางแกน X ถึงตำแหน่งเสา วัดจากจุดอ้างอิงของโครงข้อแข็งโลคอล (Local Frame Reference)
16 - 25	ระยะทางแกน Y ถึงตำแหน่งเสา วัดจากจุดอ้างอิงของโครงข้อแข็งโลคอล

3.3 บรรทัดป้อนคุณสมบัติเสา (15, F15.0, F10.0, 20X, F10.0)

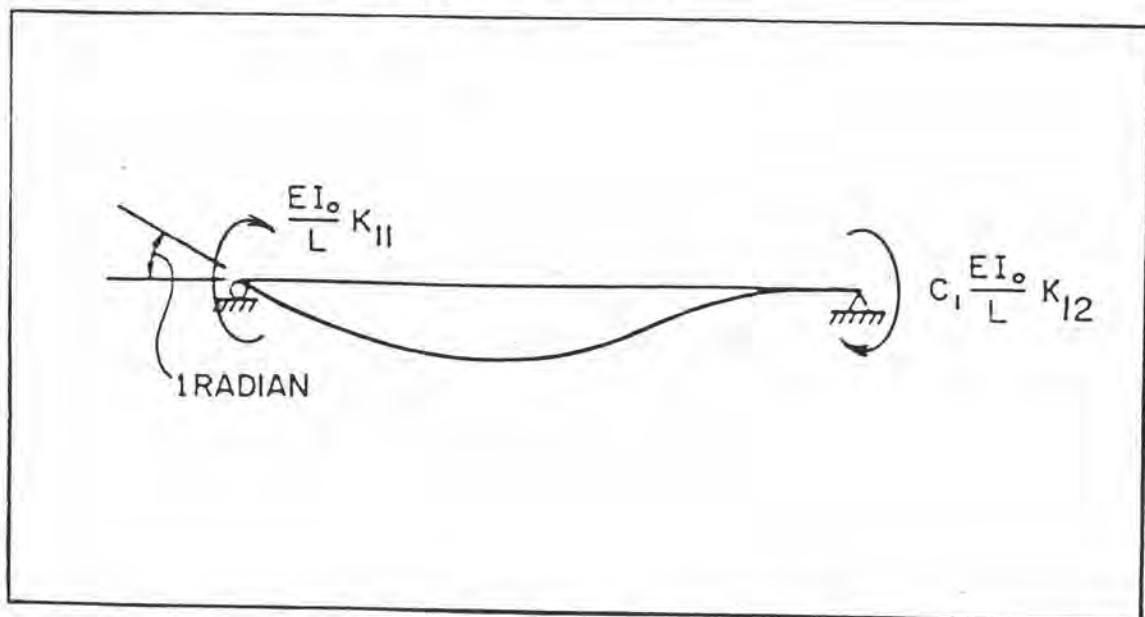
1 บรรทัดสำหรับ 1 ชุดคุณสมบัติเสา

คอลัมน์	ข้อมูล
1 - 5	เลขประจำชุดคุณสมบัติเสา ต้องป้อนเริ่มจาก 1 ขึ้นไปตามลำดับ
6 - 20	โมดูลัสความยืดหยุ่น (Elastic Modulus)
21 - 30	พื้นที่หน้าตัดรับแรงตามแนวแกน
31 - 50	ว่าง
51 - 60	อินเนอร์เชียรับแรงคด (Flexural Inertia)

3.4 บรรทัดป้อนคุณสมบัติแกน (I5, F15.0, 15X, F10.0, 3F5.0)

1 บรรทัดสำหรับ 1 ชุดคุณสมบัติแกน

คอลัมน์	ข้อมูล
1 - 5	เลขประจำชุดคุณสมบัติแกน ต้องป้อนเริ่มจาก 1 ขึ้นไปตามลำดับ
6 - 20	โมดูลัสความยืดหยุ่น
21 - 35	ว่าง
36 - 45	อินเนอร์เซียร์รับแรงคด
46 - 50	K_{11} , สติฟเนสแฟคเตอร์ (Stiffness Factor) โดยทั่วไป เท่ากับ 4 จากรูป ค.2 ประกอบ
51 - 55	K_{22} , สติฟเนสแฟคเตอร์ (Stiffness Factor) โดยทั่วไป เท่ากับ 4 จากรูป ค.2 ประกอบ
56 - 60	K_{12} , สติฟเนสแฟคเตอร์ (Stiffness Factor) โดยทั่วไป เท่ากับ 2 จากรูป ค.2 ประกอบ

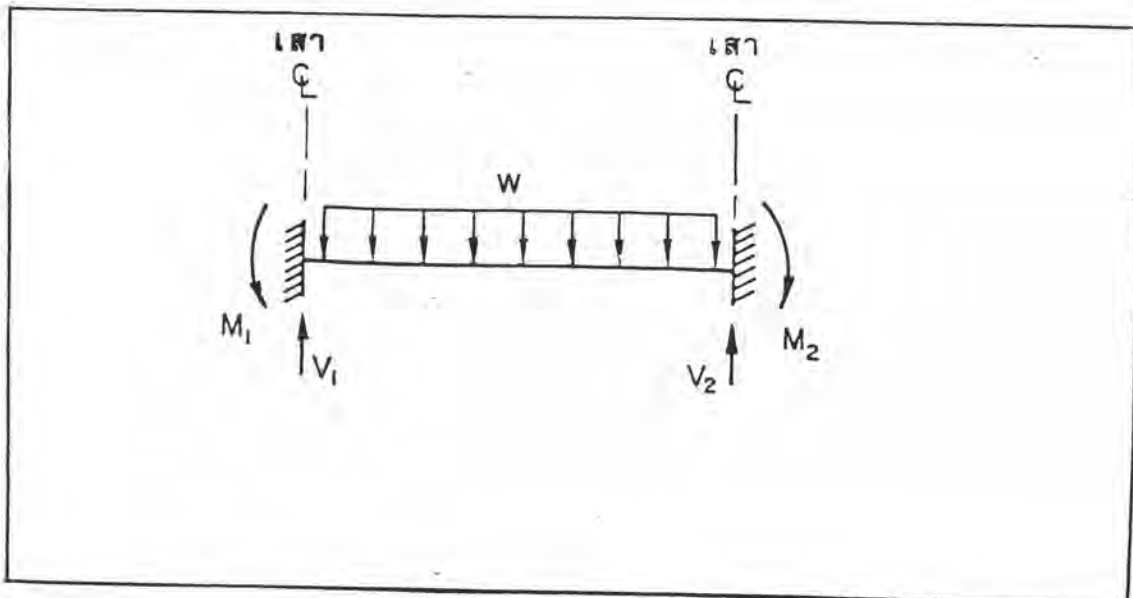


รูป ค.2 สติฟเนสแฟคเตอร์ของแกน

3.5 บรรทัดป้อนแรงยึดแน่นที่ปลายของคาน (215, 5F10.0)

1 บรรทัดสำหรับ 1 ชุดที่แตกต่างกันของแรงกระทำในแนวตั้งบนคาน

คอลัมน์	ข้อมูล
1 - 5	เลขประจำชุดของแรงกระทำใน แนวตั้งเริ่มจาก 1 ขึ้นไป ตามลำดับ
6 - 10	รหัสตำแหน่งแรงกระทำ ป้อนเลข 0 สำหรับแรงยึดแน่นปลายกระทำที่ขอบเสา ป้อนเลข 1 สำหรับแรงยึดแน่นปลายกระทำที่จุดกึ่งกลาง (Center Line) ของเสา
11 - 20	แรงปฏิกิริยาของแรงยึดแน่นปลายแรงดัด M_1 . รูป ค. 3 ประกอบ
21 - 30	แรงปฏิกิริยาของแรงยึดแน่นปลายแรงเฉือน V_1
31 - 40	แรงปฏิกิริยาของแรงยึดแน่นปลายแรงดัด M_2
41 - 50	แรงปฏิกิริยาของแรงยึดแน่นปลายแรงเฉือน V_2
51 - 60	แรงกระทำแผ่สม่ำเสมอตลอดความยาว, w , ทิศทางลงใน แนวตั้ง



รูป ค. 3 แรงยึดแน่นปลายที่คาน

3.6 บรรทัดป้อนข้อมูลคาน (815)

1 บรรทัดสำหรับ 1 คาน ต้องป้อนข้อมูลจากคานชั้นบนลงสู่ชั้นล่างตามลำดับ (ยกเว้นใช้การสร้างคุณสมบัติซ้ำในคอลัมน์ 21-25) และต้องป้อนคานทุกช่วงเสาในแต่ละชั้น

คอลัมน์	ข้อมูล
1 - 5	เลขประจำช่วง เสาของคานนี้
6 - 10	เลขประจำแนว เสาที่ปลาย I
11 - 15	เลขประจำแนว เสาที่ปลาย J
16 - 20	เลขประจำชุดคุณสมบัติคานของคานนี้ คานที่มีสติฟเนสเป็นศูนย์ (คือไม่มีคาน) สามารถป้อนข้อมูลเลขประจำชุดคุณสมบัติคานเป็น 0 แต่ถ้าเป็นคานที่มีค่าสติฟเนส เลขประจำชุดคุณสมบัติคานต้องสอดคล้องกับชุดคุณสมบัติคานที่ได้ป้อนไปแล้วในหัวข้อ 3.4
21 - 25	จำนวนคานที่อยู่ชั้นล่างลงไปตามลำดับจากชั้นนี้ ที่ต้องการสร้างให้มีคุณสมบัติและแรงกระทำในแนวตั้งเหมือนกัน การสร้างคานให้มีคุณสมบัติและแรงกระทำในแนวตั้งซ้ำกันสามารถใช้ได้สำหรับคานที่อยู่ในช่วง เสาเดียวกันเท่านั้น สำหรับช่วง เสาต่อไปต้องเริ่มป้อนข้อมูลจากบรรทัดป้อนตำแหน่งคานบรรทัดใหม่
26 - 30	เลขประจำชุดของแรงยึดแน่นปลายที่ใช้เป็นแรงกระทำในแนวตั้งชุดที่ I
31 - 35	เลขประจำชุดของแรงยึดแน่นปลายที่ใช้เป็นแรงกระทำในแนวตั้งชุดที่ II
36 - 40	เลขประจำชุดของแรงยึดแน่นปลายที่ใช้เป็นแรงกระทำในแนวตั้งชุดที่ III

3.7 บรรทัดป้อนข้อมูลเสา (415)

1 บรรทัดสำหรับ 1 เสา ป้อนข้อมูลจากเสาในชั้นบนลงชั้นล่างตามลำดับ (ยกเว้นใช้การสร้างคุณสมบัติซ้ำในคอลัมน์ 16-20)

คอลัมน์	ข้อมูล
1 - 5	เลขประจำแนวเสา
6 - 10	เลขประจำชุดคุณสมบัติของเสาแนวนี้ เสาที่มีสติฟเนสเป็นศูนย์ (คือไม่มีเสา) สามารถป้อนข้อมูลเลขประจำชุดคุณสมบัติเสาเป็น 0 แต่ถ้าเป็นเสาที่มีค่าสติฟเนส เลขประจำชุดคุณสมบัติของเสาต้องสอดคล้องกับชุดคุณสมบัติเสาที่ได้ป้อนไปแล้วในหัวข้อ 3.3
11 - 15	เลขประจำแนวเสาที่กำหนดทิศทางแกนหลัก (Direction of Major Axis)
16 - 20	จำนวนเสาที่อยู่ชั้นล่างลงไปจากชั้นนี้ ที่ต้องการสร้างให้มีคุณสมบัติเหมือนกัน การสร้างเสาให้มีคุณสมบัติซ้ำกันสามารถใช้ได้กับเสาที่อยู่ในแนวเสาเดียวกันเท่านั้น สำหรับแนวเสาต่อไป ต้องเริ่มป้อนข้อมูลจากบรรทัดป้อนข้อมูลเสาบรรทัดใหม่

3.8 บรรทัดป้อนข้อมูลผนังต้านแรงเฉือน (315,5F10.0)

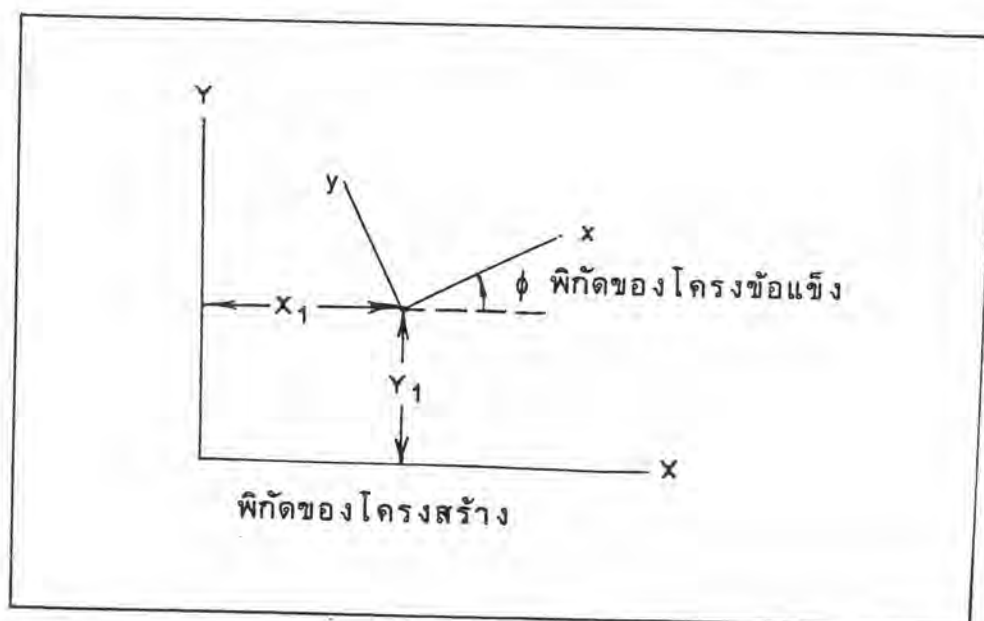
1 บรรทัดสำหรับ 1 ผนัง ไม่จำเป็นต้องเรียงลำดับ ไม่มีการสร้างคุณสมบัติซ้ำ

คอลัมน์	ข้อมูล
1 - 5	เลขชั้นที่อยู่ในตำแหน่งบนของผนังต้านแรงเฉือน เลขชั้นของ ชั้นฐาน (Foundation) กำหนดให้เป็นศูนย์ และชั้นบนสุดต้องมี เลขชั้นเท่ากับจำนวนชั้นทั้งหมดในอาคาร
6 - 10	แนวเสาที่ปลายด้าน I ของผนังต้านแรงเฉือนนี้
11 - 15	แนวเสาที่ปลายด้าน J ของผนังต้านแรงเฉือนนี้
16 - 25	โมดูลัสยึดหยุน
26 - 35	พื้นที่หน้าตัด
36 - 45	อินเนอร์เชียรับแรงดัด ถ้าอินเนอร์เชียรับแรงดัดไม่เท่ากับศูนย์ โปรแกรมจะสร้างหุ่นจำลอง (Model) ให้เป็นผนังรับแรงดัด (Flexural Panel) แต่ถ้าอินเนอร์เชียรับแรงดัดเท่ากับ 0 โปรแกรมจะสร้างหุ่นจำลองให้เป็นผนังรับแรงเฉือน (Pure Shear Panel)
46 - 55	พื้นที่รับแรงเฉือน (Effective Shear Area)
56 - 65	โมดูลัสเฉือน (Shear Modulus)

4. บรรทัดป้อนตำแหน่งโครงข้อแข็ง (215, 3F10.0, 4A4)

1 บรรทัดสำหรับ 1 โครงข้อแข็ง

คอลัมน์	ข้อมูล
1 - 5	เลขประจำโครงข้อแข็งนี้
6 - 10	รหัสการคำนวณแรงภายในโครงข้อแข็ง ป้อนเลข 0 เพื่อคำนวณแรงภายในโครงข้อแข็งและแสดงในแฟ้ม ผลการคำนวณ (Output File) ป้อนเลข 1 สำหรับไม่ต้องการคำนวณแรงภายใน
11 - 20	ระยะ x_1 , ดูรูป ค.4 ประกอบ
21 - 30	ระยะ y_1 , ดูรูป ค.4 ประกอบ
31 - 40	มุม ϕ ในหน่วยองศาและจุดทศนิยม ทิศทางทวนเข็มนาฬิกาจาก x ถึง x_1 , ดูรูป ค.4 ประกอบ
41 - 56	ข้อความที่ต้องการให้พิมพ์ออกมาพร้อมผลการคำนวณของโครง ข้อแข็งนี้



รูป ค.4 ความสัมพันธ์ระหว่าง พิกัดของโครงสร้าง (Global Coordinate) และพิกัดของโครงข้อแข็ง (Local Coordinate)

5. บรรทัดข้อมูลแรงกระทำ (5F10.0)

แรงกระทำทั้งหมดต่อโครงสร้างเกิดจากการรวมกันของแรงกระทำในแนวดิ่ง
I, II, III และแรงกระทำในแนวราบ A, B

คอลัมน์	ข้อมูล
1 - 10	ตัวคูณสำหรับแรงกระทำในแนวดิ่ง I
11 - 20	ตัวคูณสำหรับแรงกระทำในแนวดิ่ง II
21 - 30	ตัวคูณสำหรับแรงกระทำในแนวดิ่ง III
31 - 40	ตัวคูณสำหรับแรงกระทำในแนวราบ A
41 - 50	ตัวคูณสำหรับแรงกระทำในแนวราบ B

ภาคผนวก ง .

แฟ้มป้อนข้อมูลและแฟ้ม ผลการคำนวณ

ตัวอย่าง 1 : เสายืน

กรณี เสาย 1 ชิ้นส่วน


```
1 1 1 1 0 0 1 00001 5 0.001 test1.inp
Top      200.0
      28.6
1 1 2 1 2 1 1 0 0 One-Col. Frame
1
2      1.08
1      2000000.0      24.7      476.0
2      0.01      0.01      0.01
1      0.01      0.01 4.0 4.0 2.0
1 1      59100.0
1 1 2 1 0 1
1 1 2 0
2 2 1 0
1 0      0.0      0.0      0.0 One-Col.
      1.0      1.0
0
```

PROGRAM CU-NTABS
 INPUT FILE : t1t1.inp
 OUTPUT FILE : t1t1g.out

t1t1.inp
 TOTAL NUMBER OF STORIES-- 1
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 6 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM 001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
1	Top	200.00	72.63	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
1	Top	200.00	72.63	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
1	29.60	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL ID DIRN 1 2

1	Top	X	29.6000	.0000
1	Top	Y	.0000	.0000
1	Top	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
1	Top	X	5920.0000	.0000
1	Top	Y	.0000	.0000
1	Top	ROTN	.0000	.0000

One-Col. Frame

FRAME ID NUMBER-----	1
NUMBER OF STORY LEVELS----	1
NUMBER OF COLUMN LINES----	2
NUMBER OF BAYS-----	1
NUMBER OF DIFF. COL. PROP-	2
NUMBER OF DIFF. BEAM PROP-	1
NUMBER OF DIFF. FEF-----	1
NUMBER OF PANEL ELEMENTS--	0
NUMBER OF BRACING ELEMENTS	0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	1.06	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00
2	.01	.01	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	59100.000	.000	.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	1	1	2	1	0	1	0	0

GENERATED BEAM LOCATIONS

OSTORY 1

1 1

GENERATED BEAM LOADS ... LOAD CASE 1

OSTORY 1

1 1

GENERATED BEAM LOADS ...LOAD CASE I I

0STORY 1

1 0

GENERATED BEAM LOADS ...LOAD CASE I I I

0STORY 1

1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KOOL	GEN
1	1	1	2	0
2	1	2	1	0

GENERATED COLUMN LOCATIONS

0STORY 1 2

1 1 2

BEAM PROPERTIES AND LOADS

BAY NUMBERS	I	LEVEL	E	BA	TORS I	FLEX I	K11	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
1	01	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		

COLUMN PROPERTIES

COLUMN LINE NO.	1	LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
1	200000.00	24.70	.00	.00	.00	476.00	.00	.00	.00	.00	.00
COLUMN LINE NO.	2	LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
1	.01	.01	.00	.00	.00	.01	.00	.00	.00	.00	.00

0...FRAME TYPE 1...

TIME REQUIRED TO FORM STIFFNESS = .00

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG
1	1	0	.00	.00	.00

One-Cd

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3 ... DOUBLE SUM COMBINATION

SPECTRUM-4 ... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
1	X	74.0010593
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	One-Col	FRAME TYPE	1
	LEVEL NO	1	LEVEL ID	Top

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-.0000033	4379382.6061368	-59000.9999996	29.5999994
2	1	-.0000038	.0000044	-.0000004	.0000002

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	.0000033	-.0000038

CONVERGE IN ITERATION NO. 3

TOTAL TIME 3.73 SEC.

ตัวอย่าง 1 : เส้น

กรรม แบ่งเสาเป็น 2 ชั้นส่วน

```
2 1 1 1 0 0 1 00001 5 0.001 ts1s2.inp
Top 100.0
29.4
Mid 100.0

1 2 2 1 2 1 1 0 0 One-Col. Frame
1
2 1.06
1 2000000.0 24.7 476.0
2 0.01 0.01 0.01
1 0.01 0.01 4.0 4.0 2.0
1 1 58750.0
1 1 2 1 0 1
1 1 2 1 0 0
1 1 2 1
2 2 1 1
1 0 0.0 0.0 0.0 One-Col.
1.0 1.0
0
```

PROGRAM CU-NTAB9
 INPUT FILE : ts1a2.inp
 OUTPUT FILE : ts1a2g.out

ts1a2.inp

TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	Top	100.00	63.00	.00	.00	.00	.00	.00
1	Mid	100.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	Top	200.00	63.00	.00
1	Mid	100.00	63.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
2	29.40	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	Top	X	29.4000	.0000
2	Top	Y	.0000	.0000
2	Top	ROTN	.0000	.0000
1	Mid	X	29.4000	.0000
1	Mid	Y	.0000	.0000
1	Mid	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	Top	X	2940.0000	.0000
2	Top	Y	.0000	.0000
2	Top	ROTN	.0000	.0000
1	Mid	X	5980.0000	.0000
1	Mid	Y	.0000	.0000
1	Mid	ROTN	.0000	.0000

One-Col. Frame

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 2
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 2
 NUMBER OF DIFF. BEAM PROP- 1
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	1.06	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00
2	.01	.01	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	58750.000	.000	.000	.000

BEAM LOCATIONS

I	BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0	0
1	1	1	2	1	0	0	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1
 2 1
 1 1

GENERATED BEAM LOADS ...LOAD CASE I

OSTORY 1
 2 1
 1 0

GENERATED BEAM LOADS ...LOAD CASE II

OSTORY 1
 2 0
 1 0

GENERATED BEAM LOADS ...LOAD CASE III

OSTORY 1
 2 0
 1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	2	1	2	1
2	2	2	1	1

GENERATED COLUMN LOCATIONS

OSTORY 1 2
 2 1 2
 1 1 2

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
2	.01	.00	.00	.01	4.00	-4.00	2.00	.00	.00	1	0	0
1	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO. 1

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
2	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00
1	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00

COLUMN LINE NO. 2

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
2	.01	.01	.00	.00	.00	.01	.00	.00	.00
1	.01	.01	.00	.00	.00	.01	.00	.00	.00

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 1.87

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	One-Col

LOAD CONDITION DEFINITION CARDS

LOAD		11	111	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	1130.2859877
2	Y	.0000000
2	ROTN	.0000000
1	X	331.0490366
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	One-Col	FRAME TYPE
	LEVEL NO	1	LEVEL ID Mid

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	*****86409005	6039022	-58749.9999981	29.4000047
2	1	.0004594	.0001317	-.0000019	.0000122

BEAM FORCES	BAY LOAD	I MOMENT	J MOMENT
	1 1	-.0008672	.0008748

MEMBER FORCES	FRAME ID	One-Col	FRAME TYPE
	LEVEL NO	2	LEVEL ID Top

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-.000234846958934	.7040213	-58749.9999909	29.4000584
2	1	-.0002443	.0004154	-.0000091	.0000744

BEAM FORCES	BAY LOAD	I MOMENT	J MOMENT
	1 1	.0002348	-.0002443

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.30 SEC.

ตัวอย่าง 1 : เส้น

กรณี แบ่งเสาเป็น 4 ชั้นส่วน

```

4 1 1 1 0 0 1 00001 5 0.001 tats4.inp
F4      50.0
 29.4
F3      50.0
F2      50.0
F1      50.0

1 4 2 1 2 1 1 0 0 One-Col Frame
1
2 1.06
1 2000000.0 24.7 476.0
2 0.01 0.01 0.01
1 0.01 0.01 4.0 4.0 2.0
1 1 59725.0
1 1 2 1 0 1
1 1 2 1 2 0
1 1 2 3
2 2 1 3
1 0 0.0 0.0 0.0 One-Col
 1.0 1.0
0

```

PROGRAM CU-NTAB
 INPUT FILE : TS184.INP
 OUTPUT FILE : TS184G.OUT

ts184.inp

TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

- EQ.0-STATIC LOADS ONLY
- EQ.1-MODE SHAPES AND FREQUENCIES ONLY
- EQ.2-STATIC AND MODE SHAPE ANALYSES
- EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
- EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
- EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
- EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
- EQ.7-TYPE 3 AND 8 ANALYSES
- EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
- EQ.9-TYPE 4 AND 8 ANALYSES
- EQ.10-SLAM RESTART
- EQ.11-SLAM-2 RESTART
- EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	F4	50.00	60.55	.00	.00	.00	.00	.00
3	F3	50.00	.00	.00	.00	.00	.00	.00
2	F2	50.00	.00	.00	.00	.00	.00	.00
1	F1	50.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	F4	200.00	60.55	.00
3	F3	150.00	60.55	.00
2	F2	100.00	60.55	.00
1	F1	50.00	60.55	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
4	28.40	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	F4	X	29.4000	.0000
4	F4	Y	.0000	.0000
4	F4	ROTN	.0000	.0000
3	F3	X	29.4000	.0000
3	F3	Y	.0000	.0000
3	F3	ROTN	.0000	.0000
2	F2	X	29.4000	.0000
2	F2	Y	.0000	.0000
2	F2	ROTN	.0000	.0000
1	F1	X	29.4000	.0000
1	F1	Y	.0000	.0000
1	F1	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	F4	X	1470.0000	.0000
4	F4	Y	.0000	.0000
4	F4	ROTN	.0000	.0000
3	F3	X	2940.0000	.0000
3	F3	Y	.0000	.0000
3	F3	ROTN	.0000	.0000
2	F2	X	4410.0000	.0000
2	F2	Y	.0000	.0000
2	F2	ROTN	.0000	.0000
1	F1	X	5880.0000	.0000
1	F1	Y	.0000	.0000
1	F1	ROTN	.0000	.0000

One-Col. Frame

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 2
 NUMBER OF DIFF. BEAM PROP- 1
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1 .00 .00
 2 1.06 .00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00
2	.01	.01	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	58725.000	.000	.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	0	1	0	0
1	3	1	2	1	2	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1

4	1
3	1
2	1
1	1

GENERATED BEAM LOADS ...LOAD CASE I

OSTORY 1

4	1
3	0
2	0
1	0

GENERATED BEAM LOADS ...LOAD CASE II

OSTORY 1

4	0
3	0
2	0
1	0

GENERATED BEAM LOADS ...LOAD CASE III

OSTORY 1

4	0
3	0
2	0
1	0

COLUMN LOCATIONS

LINE	LEV	CID	KCOL	GEN
1	4	1	2	3
2	4	2	1	3

GENERATED COLUMN LOCATIONS

DBTORY 1 2
 4 1 2
 3 1 2
 2 1 2
 1 1 2

BEAM PROPERTIES AND LOADS

BAY NUMBERS	↑										VERT1	VERT2	VERT3
LEVEL	E	SA	TORS I	FLEX I	K11	KJJ	KIJ	WI	WJ				
4	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0	
3	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00	0	0	0	
2	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00	0	0	0	
1	.01	.00	.00	.01	4.00	4.00	2.00	.00	.00	0	0	0	

COLUMN PROPERTIES

COLUMN LINE NO.	↑									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB	
4	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00	
3	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00	
2	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00	
1	2000000.00	24.70	.00	.00	.00	476.00	.00	.00	.00	

COLUMN LINE NO.	↑									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB	
4	.01	.01	.00	.00	.00	.01	.00	.00	.00	
3	.01	.01	.00	.00	.00	.01	.00	.00	.00	
2	.01	.01	.00	.00	.00	.01	.00	.00	.00	
1	.01	.01	.00	.00	.00	.01	.00	.00	.00	

0... FRAME TYPE 1
 TIME REQUIRED TO FORM STIFFNESS = 3.79

1 FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	One-Col

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	4453.1940256
4	Y	.0000000
4	ROTN	.0000000
3	X	2749.0318885
3	Y	.0000000

```

3  ROTN      .0000000
2  X        1304.3121317
2  Y        .0000000
2  ROTN      .0000000
1  X        338.9800980
1  Y        .0000000
1  ROTN      .0000000
    
```

```

MEMBER FORCES ..... FRAME ID One-Col.      FRAME TYPE 1
                      LEVEL NO 1            LEVEL ID F1
    
```

```

COLUMN FORCES
LINE  LOAD      TOP MOMENT      BOT MOMENT      AXIAL FORCE      SHEAR FORCE
1  1  *****
2  1  - .0009917      .0014145      - .0000252      .0001795
    
```

```

BEAM FORCES
BAY  LOAD      I MOMENT      J MOMENT
1  1  - .0002927      .0002884
    
```

```

MEMBER FORCES ..... FRAME ID One-Col.      FRAME TYPE 1
                      LEVEL NO 2            LEVEL ID F2
    
```

```

COLUMN FORCES
LINE  LOAD      TOP MOMENT      BOT MOMENT      AXIAL FORCE      SHEAR FORCE
1  1  *****
2  1  - .0000595      .0012791      - .0000193      .0003974
    
```

```

BEAM FORCES
BAY  LOAD      I MOMENT      J MOMENT
1  1  - .0007270      .0007138
    
```

```

MEMBER FORCES ..... FRAME ID One-Col.      FRAME TYPE 1
                      LEVEL NO 3            LEVEL ID F3
    
```

```

COLUMN FORCES
LINE  LOAD      TOP MOMENT      BOT MOMENT      AXIAL FORCE      SHEAR FORCE
1  1  *****
2  1  .0009405      .0007733      - .0000089      .0002327
    
```

```

BEAM FORCES
BAY  LOAD      I MOMENT      J MOMENT
1  1  - .0015453      .0015672
    
```

```

MEMBER FORCES ..... FRAME ID One-Col.      FRAME TYPE 1
                      LEVEL NO 4            LEVEL ID F4
    
```

```

COLUMN FORCES
LINE  LOAD      TOP MOMENT      BOT MOMENT      AXIAL FORCE      SHEAR FORCE
1  1  - .0003725*****
2  1  - .0004020      .0008288      - .0000275      .0009420
    
```

```

BEAM FORCES
BAY  LOAD      I MOMENT      J MOMENT
1  1  .0003728      - .0004020
    
```

CONVERGE IN ITERATION NO. 3

TOTAL TIME 14.38 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 1000$ หน่วย

```

2 1 1 1 0 0 1 00001 5 0.001 T8E4813 .IMP
TOP      60.0
1.0     0.0     0.0     0.0
MID      60.0

1 2 2 1 1 2 1          TWO-STORY FRAME
1      0.0     0.0
2     120.0    0.0
1     30000.0  11.77 0.0 0.0          310.1     0.0 0.0 0.0
1     30000.0          310.1 4.0 4.0 2.0
2           0.1          0.1 4.0 4.0 2.0
1 1           1000.0          1000.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0     0.0     0.0     0.0 TWO-STORY FRAME
1.0     0.0     0.0     1.0     0.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTAB9
 INPUT FILE : tse4813.inp
 OUTPUT FILE : tse4813g.out

TSE4813.INP

TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 6 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-SLAM RESTART

EQ.11-SLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	TOP	80.00	.00	.00	.00	.00	.00	.00
1	MID	80.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	TOP	120.00	.00	.00
1	MID	80.00	.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MM-A	FX-B	FY-B	MM-B	XA	YA	XB	YB
2	1.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	1.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	1.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	60.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	120.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 2
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	1000.000	.000	1000.000	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0
1	1	1	2	2	0	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1
 2 1
 1 2

GENERATED BEAM LOADS ...LOAD CASE I

OSTORY 1
 2 1
 1 0

GENERATED BEAM LOADS ...LOAD CASE II

OSTORY 1
 2 0
 1 0

GENERATED BEAM LOADS ...LOAD CASE III

OSTORY 1
 2 0
 1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	2	1	2	1
2	2	1	1	1

GENERATED COLUMN LOCATIONS

OSTORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS	1											
LEVEL	E	SA	TORS I	FLEX I	K11	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.	1											
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB			
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00			
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00			

COLUMN LINE NO.	2											
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB			
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00			
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00			

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 1.87

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.0141583
2	Y	.0000000
2	ROTN	.0000000
1	X	.0059583
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID TWO-STORY FRAME FRAME TYPE 1
 LEVEL NO 1 LEVEL ID MID

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-5.9846735	41.9436127	-999.4830780	.5000646
2	1	5.9846740	-41.9422584	-1000.5369220	- .4999354

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-.0000001	-.0000001

MEMBER FORCES FRAME ID TWO-STORY FRAME FRAME TYPE 1
 LEVEL NO 2 LEVEL ID TOP

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	32.2154188	5.9846735	-999.4830780	.5000750
2	1	-32.2152216	-5.9846740	-1000.5369220	- .4999250

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-32.2154188	-32.2152216

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.03 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 2000$ หน่วย

```
2 1 1 1 0 0 1 00001 5 0.001 T8E4814.INP
TOP 60.0
2.0 0.0 0.0 0.0
MID 60.0

1 2 2 1 1 2 1 TWO-STORY FRAME
1 0.0 0.0
2 120.0 0.0
1 30000.0 11.77 0.0 0.0 310.1 0.0 0.0 0.0
1 30000.0 310.1 4.0 4.0 2.0
2 0.1 0.1 4.0 4.0 2.0
1 1 2000.0 2000.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0 0.0 0.0 0.0 TWO-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0
0
```

PROGRAM CU-NTAB8
 INPUT FILE : tse4s14.inp
 OUTPUT FILE : tse4s14g.out

TSE4S14.INP
 TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-BLAM RESTART
 EQ.11-BLAM-2 RESTART
 EQ.-1,-8,-9 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	TOP	60.00	.00	.00	.00	.00	.00	.00
1	MID	60.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	TOP	120.00	.00	.00
1	MID	60.00	.00	.00

STRUCTURE LATERAL LOADS ... CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
2	2.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	2.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	2.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	120.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	240.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER-----	1
NUMBER OF STORY LEVELS----	2
NUMBER OF COLUMN LINES----	2
NUMBER OF BAYS-----	1
NUMBER OF DIFF. COL. PROP-	1
NUMBER OF DIFF. BEAM PROP-	2
NUMBER OF DIFF. FEF-----	1
NUMBER OF PANEL ELEMENTS--	0
NUMBER OF BRACING ELEMENTS	0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	2000.000	.000	2000.000	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0
1	1	1	2	2	0	0	0	0

GENERATED BEAM LOCATIONS

0STORY 1
 2 1
 1 2

GENERATED BEAM LOADS ...LOAD CASE I

0STORY 1
 2 1
 1 0

GENERATED BEAM LOADS ...LOAD CASE II

0STORY 1
 2 0
 1 0

GENERATED BEAM LOADS ...LOAD CASE III

0STORY 1
 2 0
 1 0

COLUMN LOCATIONS

D LINE	LEV	CID	KCOL	GEN
1	2	1	2	1
2	2	1	1	1

GENERATED COLUMN LOCATIONS

0STORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS	1											
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.	1										
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

COLUMN LINE NO.	2										
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 1.87

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.0386308
2	Y	.0000000
2	ROTN	.0000000
1	X	.0181628
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
	LEVEL NO	1	1
	LEVEL ID	MID	

COLUMN FORCES	LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	1	1	-17.4004488	109.7308181	-1999.5410681	1.0004780
	2	1	17.4004894	-109.7208555	-2001.4689319	-.9995220

BEAM FORCES	BAY	LOAD	I MOMENT	J MOMENT
	1	1	-.0000002	-.0000002

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
	LEVEL NO	2	1
	LEVEL ID	TOP	

COLUMN FORCES	LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	1	1	87.5368888	17.4004490	-1999.5410681	1.0005586
	2	1	-87.5351546	-17.4004896	-2001.4589319	-.9994414

BEAM FORCES	BAY	LOAD	I MOMENT	J MOMENT
	1	1	-87.5368888	-87.5351546

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.03 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 3000$ หน่วย

```

2 1 1 1 0 0 1 00001 5 0.001 T9E4815.INP
TOP      60.0
3.0      0.0      0.0      0.0
MID      60.0

1 2 2 1 1 2 1          TWO-STORY FRAME
1      0.0      0.0
2     120.0      0.0
1     30000.0    11.77 0.0 0.0      310.1      0.0 0.0 0.0
1     30000.0      310.1 4.0 4.0 2.0
2      0.1      0.1 4.0 4.0 2.0
1 1      3000.0      3000.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0      0.0      0.0 TWO-STORY FRAME
1.0      0.0      0.0      1.0      0.0 0.0 0.0 0.0 0.0 0.0
0

```


PROGRAM CU-NTAB8
 INPUT FILE : ts04s15.inp
 OUTPUT FILE : ts04s15g.out

TSE4S15.INP
 TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES--- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	TOP	60.00	.00	.00	.00	.00	.00	.00
1	MID	60.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	TOP	120.00	.00	.00
1	MID	60.00	.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MM-A	FX-B	FY-B	MM-B	XA	YA	XB	YB
2	3.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	3.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	3.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	180.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	380.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 2
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	3000.000	.000	3000.000	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0
1	1	1	2	2	0	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1
 2 1
 1 2

GENERATED BEAM LOADS ... LOAD CASE I

OSTORY 1
 2 1
 1 0

GENERATED BEAM LOADS ... LOAD CASE II

OSTORY 1
 2 0
 1 0

GENERATED BEAM LOADS ... LOAD CASE III

OSTORY 1
 2 0
 1 0

COLUMN LOCATIONS

0	LINE	LEV	CID	KCOL	GEN
	1	2	1	2	1
	2	2	1	1	1

GENERATED COLUMN LOCATIONS

OSTORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.		1									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
COLUMN LINE NO.		2									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 2.03

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	AND	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.0012848
2	Y	.0000000
2	ROTN	.0000000
1	X	.0379455
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	1		1
	LEVEL ID	MID	

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-43.9321917	247.7974578	-2996.5852405	1.5028519
2	1	43.9328230	-247.7403304	-3003.4347595	-1.4973481

BAY	LOAD	I MOMENT	J MOMENT
1	1	-.0000005	-.0000005

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	2		1
	LEVEL ID	TOP	

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	206.0899343	43.9321922	-2996.5852405	1.5031226
2	1	-206.0812072	-43.9328235	-3003.4347595	-1.4968774

BAY	LOAD	I MOMENT	J MOMENT
1	1	-206.0899343	-206.0812072

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.74 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 3500$ หน่วย

```

2 1 1 1 0 0 1 00001 5 0.001 T8E4818 .INP
TOP      60.0
      3.5 0.0 0.0 0.0
MID      60.0

1 2 2 1 1 2 1          TWO-STORY FRAME
1      0.0 0.0
2     120.0 0.0
1     30000.0 11.77 0.0 0.0 310.1 0.0 0.0 0.0
1     30000.0 310.1 4.0 4.0 2.0
2      0.1 0.1 4.0 4.0 2.0
1 1      3500.0 3500.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0 0.0 0.0 0.0 TWO-STORY FRAME
      1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTABS
 INPUT FILE : tse4818.inp
 OUTPUT FILE : tse4818g.out

TSE4818.INP
 TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

- EQ. 0-STATIC LOADS ONLY
- EQ. 1-MODE SHAPES AND FREQUENCIES ONLY
- EQ. 2-STATIC AND MODE SHAPE ANALYSES
- EQ. 3-TYPE 2 AND RESPONSE SPECTRUM ANAL
- EQ. 4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
- EQ. 5-THIS OPTION IS NOT AVAILABLE FOR USE
- EQ. 6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
- EQ. 7-TYPE 3 AND 8 ANALYSES
- EQ. 8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
- EQ. 9-TYPE 4 AND 8 ANALYSES
- EQ. 10-SLAM RESTART
- EQ. 11-SLAM-2 RESTART
- EQ. -1,-2,-3 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR ²	X(M)	Y(M)	K-X	K-Y
2	TOP	60.00	.00	.00	.00	.00	.00	.00
1	MID	60.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR ²
2	TOP	120.00	.00	.00
1	MID	60.00	.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MM-A	FX-B	FY-B	MM-B	XA	YA	XB	YB
2	3.50	.00	.00	.00	.00	.00	0	0	0	0
1	.00	.00	.00	.00	.00	.00	0	0	0	0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	3.5000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	3.5000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	210.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	420.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER-----	1
NUMBER OF STORY LEVELS----	2
NUMBER OF COLUMN LINES----	2
NUMBER OF BAYS-----	1
NUMBER OF DIFF. COL. PROP-	1
NUMBER OF DIFF. BEAM PROP-	2
NUMBER OF DIFF. FEF-----	1
NUMBER OF PANEL ELEMENTS--	0
NUMBER OF BRACING ELEMENTS	0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	3500.000	.000	3500.000	.000

BEAM LOCATIONS

I	BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0	0
1	1	1	2	2	0	0	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1
 2 1
 1 2

GENERATED BEAM LOADS ... LOAD CASE I

OSTORY 1
 2 1
 1 0

GENERATED BEAM LOADS ... LOAD CASE II

OSTORY 1
 2 0
 1 0

GENERATED BEAM LOADS ... LOAD CASE III

OSTORY 1
 2 0
 1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KOOL	GEN
1	2	1	2	1
2	2	1	1	1

GENERATED COLUMN LOCATIONS

OSTORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS	1											
LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.	1										
LEVEL	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
COLUMN LINE NO.	2										
LEVEL	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 2.04

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.1496361
2	Y	.0000000
2	ROTN	.0000000
1	X	.0019621
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
	LEVEL NO	1	1
			LEVEL ID MID

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-74.5190010	396.5340987	-3494.3786472	1.7571028
2	1	74.5204327	-396.3800195	-3505.6211528	-1.7428972

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-.0000008	-.0000008

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
	LEVEL NO	2	1
			LEVEL ID TOP

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	337.2810853	74.5190019	-3494.3786472	1.7583986
2	1	-337.2572516	-74.5204336	-3505.6211528	-1.7418014

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-337.2810853	-337.2572516

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.41 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 4000$ หน่วย

```
2 1 1 1 0 0 1 00001 5 0.001 TBE4811.INP
TOP      60.0
4.0      0.0      0.0      0.0
MID      60.0

1 2 2 1 1 2 1 TWO-STORY FRAME
1      0.0      0.0
2      120.0     0.0
1      30000.0   11.77 0.0 0.0      310.1      0.0 0.0 0.0
1      30000.0      310.1 4.0 4.0 2.0
2      0.1      0.1 4.0 4.0 2.0
1 1      4000.0      4000.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0      0.0      0.0      0.0 TWO-STORY FRAME
1.0      0.0      0.0      1.0      0.0 0.0 0.0 0.0 0.0 0.0
0
```

PROGRAM CU-HTAB8
 INPUT FILE : tee4e11.inp
 OUTPUT FILE : tee4e11g.out

TSE4E11.INP
 TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

- EQ.0-STATIC LOADS ONLY
- EQ.1-MODE SHAPES AND FREQUENCIES ONLY
- EQ.2-STATIC AND MODE SHAPE ANALYSES
- EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
- EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
- EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
- EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
- EQ.7-TYPE 3 AND 8 ANALYSES
- EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
- EQ.9-TYPE 4 AND 8 ANALYSES
- EQ.10-SLAM RESTART
- EQ.11-SLAM-2 RESTART
- EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	TOP	60.00	.00	.00	.00	.00	.00	.00
1	MID	60.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	TOP	120.00	.00	.00
1	MID	60.00	.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
2	4.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	4.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	4.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	240.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	480.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 2
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	4000.000	.000	4000.000	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0
1	1	1	2	2	0	0	0	0

GENERATED BEAM LOCATIONS

OSTORY 1
 2 1
 1 2

GENERATED BEAM LOADS...LOAD CASE I

OSTORY 1
 2 1
 1 0

GENERATED BEAM LOADS...LOAD CASE II

OSTORY 1
 2 0
 1 0

GENERATED BEAM LOADS...LOAD CASE III

OSTORY 1
 2 0
 1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	2	1	2	1
2	2	1	1	1

GENERATED COLUMN LOCATIONS

OSTORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS	1											
LEVEL	E	SA	TORS I	FLEX I	K11	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.	1										
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
COLUMN LINE NO.	2										
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

D...FRAME TYPE 1

TIME REQUIRED TO FORM STIFFNESS = 1.93

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	AND	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.2877338
2	Y	.0000000
2	ROTN	.0000000
1	X	.1187397
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	1		LEVEL ID MID

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-148.3877378	743.8357200	-3989.2069238	2.0261783
2	1	148.3940293	-743.0637533	-4010.7930762	-1.9738217

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-.0000016	-.0000016

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	2		LEVEL ID TOP

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	647.6293666	148.3877392	-3989.2069238	2.0310936
2	1	-647.5397745	-148.3940310	-4010.7930762	-1.9589064

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-647.6293666	-647.5397745

CONVERGE IN ITERATION NO. 3

TOTAL TIME 7.31 SEC.

ตัวอย่าง 2 : โครงข้อแข็งพอร์ทอล

กรณีแรง $P = 4200$ หน่วย

```

2 1 1 1 0 0 1 00001 5 0.001 TBE4816 .IMP
TOP      60.0
4.2      0.0      0.0      0.0
MID      60.0

1 2 2 1 1 2 1          TWO-STORY FRAME
1      0.0      0.0
2     120.0      0.0
1     30000.0    11.77 0.0 0.0      310.1      0.0 0.0 0.0
1     30000.0      310.1 4.0 4.0 2.0
2       0.1      0.1 4.0 4.0 2.0
1 1      4200.0      4200.0
1 1 2 1 0 1
1 1 2 2 0
1 1 2 1
2 1 1 1
1 0      0.0      0.0      0.0 TWO-STORY FRAME
1.0      0.0      0.0      1.0      0.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTAB
 INPUT FILE : tse4s16.inp
 OUTPUT FILE : tse4s16g.out

TSE4S16.INP
 TOTAL NUMBER OF STORIES-- 2
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-BLAM RESTART
 EQ.11-BLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
2	TOP	60.00	.00	.00	.00	.00	.00	.00
1	MID	60.00	.00	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
2	TOP	120.00	.00	.00
1	MID	60.00	.00	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
2	4.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	4.2000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	4.2000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
2	TOP	X	252.0000	.0000
2	TOP	Y	.0000	.0000
2	TOP	ROTN	.0000	.0000
1	MID	X	504.0000	.0000
1	MID	Y	.0000	.0000
1	MID	ROTN	.0000	.0000

TWO-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 2
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	120.00	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ J	MIN J	RIGID TOP	RIGID BOT
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00
2	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	4200.000	.000	4200.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	2	1	2	1	0	1	0	0
1	1	1	2	2	0	0	0	0

GENERATED BEAM LOCATIONS

STORY 1
 2 1
 1 2

GENERATED BEAM LOADS...LOAD CASE I

STORY 1
 2 1
 1 0

GENERATED BEAM LOADS...LOAD CASE II

STORY 1
 2 0
 1 0

GENERATED BEAM LOADS...LOAD CASE III

STORY 1
 2 0
 1 0

COLUMN LOCATIONS

0	LINE	LEV	CID	KCOL	GEN
	1	2	1	2	1
	2	2	1	1	1

GENERATED COLUMN LOCATIONS

STORY 1 2
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
2	30000.00	.00	.00	310.10	4.00	4.00	2.00	.00	.00	1	0	0
1	.10	.00	.00	.10	4.00	4.00	2.00	.00	.00	0	0	0

COLUMN PROPERTIES

COLUMN LINE NO.		1									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
COLUMN LINE NO.		2									
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB		
2	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		
1	30000.00	11.77	.00	.00	.00	310.10	.00	.00	.00		

0...FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 1.87

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	TWO-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
2	X	.4157481
2	Y	.0000000
2	ROTN	.0000000
1	X	.1713002
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	1		1
			LEVEL ID
			MID

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-217.4718493	1063.5377749	-4184.4132924	2.1548839
2	1	217.4858104	-1062.3418814	-4215.5887078	-2.0454181

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-.0000024	-.0000024

MEMBER FORCES	FRAME ID	TWO-STORY FRAME	FRAME TYPE
LEVEL NO	2		1
			LEVEL ID
			TOP

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	935.2988069	217.4718517	-4184.4132924	2.1648551
2	1	-935.1083059	-217.4858128	-4215.5887078	-2.0350449

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-935.2988069	-935.1083059

CONVERGE IN ITERATION NO. 3

TOTAL TIME 6.98 SEC.

ตัวอย่าง 3 : โครงข้อแข็ง 4 ชั้น

กรณีแรง $P = 100,000$ ปอนด์

```

4 1 1 1 0 0 1 00001 5 0.001 TBEBB01.INP
FOUR 144.0
16.7
THRE 144.0
TWO 144.0
ONE 144.0

```

```

1 4 2 1 1 2 1 FOUR-STORY FRAME
1 0.0 0.0
2 360.0 0.0
1 30000.0 17.66 0.0 0.0 343.7 0.0 0.0 0.0
1 30000.0 889.9 4.0 4.0 2.0
2 30000.0 984.0 4.0 4.0 2.0
1 1 100.0 100.0
1 1 2 1 1 1
1 1 2 2 1 1
1 1 2 3
2 1 1 3
1 0 0.0 0.0 0.0 FOUR-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0
0

```


PROGRAM CU-NTABS
 INPUT FILE : tse0e01.inp
 OUTPUT FILE : tse0e01g.out

TSE0E01.INP
 TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 6 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-0,-9 SAME AS 1,0,9 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	FOUR	144.00	10.19	.00	.00	.00	.00	.00
3	THRE	144.00	10.19	.00	.00	.00	.00	.00
2	TWO	144.00	10.19	.00	.00	.00	.00	.00
1	ONE	144.00	10.19	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	FOUR	576.00	10.19	.00
3	THRE	432.00	20.38	.00
2	TWO	288.00	30.57	.00
1	ONE	144.00	40.76	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
4	18.70	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	16.7000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	16.7000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	16.7000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	16.7000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	2404.8000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	4809.6000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	7214.4000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	9619.2000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

FOUR-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1	.00	.00							
2	360.00	.00							

COLUMN ID	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

BEAM ID	E	BA	TORS I	FLEX I	K11	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	889.00	4.00	4.00	2.00	.00	.00
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	100.000	.000	100.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	1	1	0	0
1	2	1	2	2	1	1	0	0

GENERATED BEAM LOCATIONS

OSTORY 1

4	1
3	1
2	2
1	2

GENERATED BEAM LOADS...LOAD CASE I

OSTORY 1

4	1
3	1
2	1
1	1

GENERATED BEAM LOADS...LOAD CASE II

OSTORY 1

4	0
3	0
2	0
1	0

GENERATED BEAM LOADS...LOAD CASE III

OSTORY 1

4	0
3	0
2	0
1	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	4	1	2	3
2	4	1	1	3

GENERATED COLUMN LOCATIONS

DBSTORY 1 2
 4 1 1
 3 1 1
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
4	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
3	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0
1	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0

COLUMN PROPERTIES

COLUMN LINE NO 1

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

COLUMN LINE NO 2

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

0...FRAME TYPE 1...
 TIME REQUIRED TO FORM STIFFNESS = 3.70

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG
1	1	0	.00	.00	.00

FOUR-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	2.1933002
4	Y	.0000000
4	ROTN	.0000000
3	X	1.6595535
3	Y	.0000000

3	ROTN	.0000000
2	X	1.0327302
2	Y	.0000000
2	ROTN	.0000000
1	X	.4146378
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES ----- FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 1 LEVEL ID ONE

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	514.8054844	854.4935810	-375.0754134	8.4290179
2	1	-515.3118357	-851.8995984	-424.9245866	-8.2709821

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-1226.6879010	-1226.5991549

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 2 LEVEL ID TWO

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	876.3819581	711.8824188	-291.8900996	8.4306268
2	1	-876.1235145	-711.2875192	-318.1099004	-8.2693732

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-1341.1596136	-1340.9132238

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 3 LEVEL ID THREE

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	863.0518405	864.7975554	-189.3403020	8.3989894
2	1	-862.8901283	-864.7898093	-210.6598980	-8.3030106

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-1211.5182379	-1211.4658005

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 4 LEVEL ID FOUR

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	707.2929032	648.4643974	-96.0708076	8.3844433
2	1	-707.2163551	-648.5758722	-103.9291924	-8.3355587

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-707.2929032	-707.2163551

CONVERGE IN ITERATION NO. 3

TOTAL TIME 15.27 SEC.

ตัวอย่าง 3 : โครงข้อแข็ง 4 ชั้น

กรรมแรง $P = 200,000$ ปอนด์

```

4 1 1 1 0 0 1 00001 5 0.001 TBE9S02.INP
FOUR 144.0
33.3
THRE 144.0
TWO 144.0
ONE 144.0

```

```

1 4 2 1 1 2 1 FOUR-STORY FRAME
1 0.0 0.0
2 360.0 0.0
1 30000.0 17.66 0.0 0.0 343.7 0.0 0.0 0.0
1 30000.0 889.9 4.0 4.0 2.0
2 30000.0 984.0 4.0 4.0 2.0
1 1 200.0
1 1 2 1 1 1
1 1 2 2 1 1
1 1 2 3
2 1 1 3
1 0 0.0 0.0 0.0 FOUR-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTABS
 INPUT FILE : tee02.inp
 OUTPUT FILE : tee02g.out

TEE02.INP

TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 8 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-BLAM RESTART

EQ.11-BLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	FOUR	144.00	10.19	.00	.00	.00	.00	.00
3	THRE	144.00	10.19	.00	.00	.00	.00	.00
2	TWO	144.00	10.19	.00	.00	.00	.00	.00
1	ONE	144.00	10.19	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	FOUR	576.00	10.19	.00
3	THRE	432.00	20.38	.00
2	TWO	288.00	30.57	.00
1	ONE	144.00	40.76	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MM-A	FX-B	FY-B	MM-B	XA	YA	XB	YB
4	33.30	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	33.3000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	33.3000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	33.3000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	33.3000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	4795.2000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	9590.4000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	14385.6000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	19180.8000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

FOUR-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1	.00	.00							
2	360.00	.00							

COLUMN ID	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

BEAM ID	E	EA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	200.000	.000	200.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	1	1	0	0
1	2	1	2	2	1	1	0	0

GENERATED BEAM LOCATIONS

OSTORY 1

4	1
3	1
2	2
1	2

GENERATED BEAM LOADS...LOAD CASE I

OSTORY 1

4	1
3	1
2	1
1	1

GENERATED BEAM LOADS...LOAD CASE II

OSTORY 1

4	0
3	0
2	0
1	0

GENERATED BEAM LOADS...LOAD CASE III

OSTORY 1

4	0
3	0
2	0
1	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KOOL	GEN
1	4	1	2	3
2	4	1	1	3

GENERATED COLUMN LOCATIONS

0STORY 1 2

4 1 1
 3 1 1
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
4	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
3	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0
1	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0

COLUMN PROPERTIES

COLUMN LINE NO		1								
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB	
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	

COLUMN LINE NO		2								
LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB	
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	

0...FRAME TYPE 1...

TIME REQUIRED TO FORM STIFFNESS = 3.79

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	FOUR-STORY FRAME

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	4.9566110
4	Y	.0000000
4	ROTN	.0000000
3	X	3.8169595
3	Y	.0000000

ตัวอย่าง 3 : โครงข้อแข็ง 4 ชั้น

กรณีแรง $P = 300,000$ ปอนด์

```

4 1 1 1 0 0 1 00001 5 0.001 TSE8803.INP
FOUR 144.0
50.0
THRE 144.0
TWO 144.0
ONE 144.0

```

```

1 4 2 1 1 2 1 FOUR-STORY FRAME
1 0.0 0.0
2 300.0 0.0
1 30000.0 17.86 0.0 0.0 343.7 0.0 0.0 0.0
1 30000.0 889.9 4.0 4.0 2.0
2 30000.0 984.0 4.0 4.0 2.0
1 1 300.0 300.0
1 1 2 1 1 1
1 1 2 2 1 1
1 1 2 3
2 1 1 3
1 0 0.0 0.0 0.0 0.0 FOUR-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTABS
 INPUT FILE : t00803.inp
 OUTPUT FILE : t00803g.out

T00803.INP

TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 8 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-BLAM RESTART

EQ.11-BLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	FOUR	144.00	10.19	.00	.00	.00	.00	.00
3	THRE	144.00	10.19	.00	.00	.00	.00	.00
2	TWO	144.00	10.19	.00	.00	.00	.00	.00
1	ONE	144.00	10.19	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	FOUR	576.00	10.19	.00
3	THRE	432.00	20.38	.00
2	TWO	288.00	30.57	.00
1	ONE	144.00	40.76	.00

STRUCTURE LATERAL LOADS . . . CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
4	50.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	50.0000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	50.0000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	50.0000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	50.0000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	7200.0000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	14400.0000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	21600.0000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	28800.0000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

FOUR-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1	.00	.00								
2	300.00	.00								
COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT	
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00	
BEAM ID	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J	
1	30000.00	.00	.00	989.90	4.00	4.00	2.00	.00	.00	
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	
FEB ID	CCDE	ML	VL	MR	VR	W				
1	1	.000	300.000	.000	300.000	.000				

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	1	1	0	0
1	2	1	2	2	1	1	0	0

GENERATED BEAM LOCATIONS

STORY 1

4	1
3	1
2	2
1	2

GENERATED BEAM LOADS...LOAD CASE I

STORY 1

4	1
3	1
2	1
1	1

GENERATED BEAM LOADS...LOAD CASE II

STORY 1

4	0
3	0
2	0
1	0

GENERATED BEAM LOADS...LOAD CASE III

STORY 1

4	0
3	0
2	0
1	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	4	1	2	3
2	4	1	1	3

GENERATED COLUMN LOCATIONS

OSTORY 1 2

4 1 1
 3 1 1
 2 1 1
 1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
4	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
3	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
2	30000.00	.00	.00	884.00	4.00	4.00	2.00	.00	.00	1	0	0
1	30000.00	.00	.00	884.00	4.00	4.00	2.00	.00	.00	1	0	0

COLUMN PROPERTIES

COLUMN LINE NO 1

LEVEL	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

COLUMN LINE NO 2

LEVEL	E	A	MAJ BA	MIN BA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

0... FRAME TYPE 1

TIME REQUIRED TO FORM STIFFNESS = 3.70

IFRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG
1	1	0	.00	.00	.00

FOUR-STORY FRAM

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	8.6341524
4	Y	.0000000
4	ROTN	.0000000
3	X	6.7949526
3	Y	.0000000

ตัวอย่าง 3 : โครงข้อแข็ง 4 ชั้น

กรณีแรง $P = 400,000$ ปอนด์

```

4 1 1 1 0 0 1 00001 5 0.001 TBE804.INP
FOUR 144.0
66.7 0.0 0.0 0.0
THRE 144.0

TWO 144.0

ONE 144.0

```

```

1 4 2 1 1 2 1 FOUR-STORY FRAME
1 0.0 0.0
2 360.0 0.0
1 30000.0 17.66 0.0 0.0 343.7 0.0 0.0 0.0
1 30000.0 889.9 4.0 4.0 2.0
2 30000.0 984.0 4.0 4.0 2.0
1 1 400.0 400.0
1 1 2 1 1 1
1 1 2 2 1 1
1 1 2 3
2 1 1 3
1 0 0.0 0.0 0.0 0.0 FOUR-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTABS
 INPUT FILE : ts0804.inp
 OUTPUT FILE : ts0804g.out

TSE804.INP
 TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL.
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 6 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM 001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	FOUR	144.00	10.19	.00	.00	.00	.00	.00
3	THRE	144.00	10.19	.00	.00	.00	.00	.00
2	TWO	144.00	10.19	.00	.00	.00	.00	.00
1	ONE	144.00	10.19	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	FOUR	576.00	10.19	.00
3	THRE	432.00	20.38	.00
2	TWO	288.00	30.57	.00
1	ONE	144.00	40.76	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
4	86.70	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	88.7000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	88.7000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	88.7000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	88.7000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	9004.8000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	19209.8000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	28814.4000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	38419.2000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

FOUR-STORY FRAME

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1 .00 .00
 2 360.00 .00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	400.000	.000	400.000	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	1	1	0	0
1	2	1	2	2	1	1	0	0

GENERATED BEAM LOCATIONS

STORY 1
 4 1
 3 1
 2 2
 1 2

GENERATED BEAM LOADS ...LOAD CASE I

STORY 1
 4 1
 3 1
 2 1
 1 1

GENERATED BEAM LOADS ...LOAD CASE II

STORY 1
 4 0
 3 0
 2 0
 1 0

GENERATED BEAM LOADS ...LOAD CASE III

STORY 1
 4 0
 3 0
 2 0
 1 0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	4	1	2	3
2	4	1	1	3

GENERATED COLUMN LOCATIONS

OSTORY 1 2

4 1 1
3 1 1
2 1 1
1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	SA	TORS I	FLEX I	K11	KJJ	KIJ	W1	WJ	VERT 1	VERT 2	VERT 3
4	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
3	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0
1	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0

COLUMN PROPERTIES

COLUMN LINE NO. 1

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

COLUMN LINE NO. 2

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

0...FRAME TYPE 1...

TIME REQUIRED TO FORM STIFFNESS = 3.78

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	FOUR-STORY FRAM

LOAD CONDITION DEFINITION CARDS

DLOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	13.8325415
4	Y	.0000000
4	ROTN	.0000000
3	X	11.1532463
3	Y	.0000000

3	ROTN	.0000000
2	X	7.4073071
2	Y	.0000000
2	ROTN	.0000000
1	X	3.0245057
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 1 LEVEL ID ONE

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	3852.4079450	5937.9712908	-1446.6823765	36.9088897
2	1	-3871.8744077	-5720.9648583	-1753.3176235	-29.7911103

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-8887.8655033	-8884.9739304

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 2 LEVEL ID TWO

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	5046.4137091	5035.4575583	-1096.0513749	36.8534432
2	1	-5028.5524660	-5013.0995227	-1303.9486251	-30.0485568

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-8757.2546595	-8747.0891553

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 3 LEVEL ID THREE

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	4087.8619811	3710.8409503	-744.8745494	34.7847037
2	1	-4081.2641035	-3718.5356893	-855.3254506	-31.9152963

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-8552.2761228	-8550.4889406

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 4 LEVEL ID FOUR

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	3408.1133815	2464.6141617	-381.0710576	33.8925394
2	1	-3408.3058999	-2469.2027370	-418.9289424	-33.0074606

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-3408.1133815	-3408.3058999

CONVERGE IN ITERATION NO. 3

TOTAL TIME 14.72 SEC.

ตัวอย่าง 3 : โครงข้อแข็ง 4 ชั้น

กรรมแรง $P = 500,000$ ปอนด์

```

4 1 1 1 0 0 1 00001 5 0.001 T8E8805.INP
FOUR 144.0
83.3
THRE 144.0
TWO 144.0
ONE 144.0

```

```

1 4 2 1 1 2 1 FOUR-STORY FRAME
1 0.0 0.0
2 380.0 0.0
1 30000.0 17.66 0.0 0.0 343.7 0.0 0.0 0.0
1 30000.0 889.9 4.0 4.0 2.0
2 30000.0 984.0 4.0 4.0 2.0
1 1 500.0 500.0
1 1 2 1 1 1
1 1 2 2 1 1
1 1 2 3
2 1 1 3
1 0 0.0 0.0 0.0 FOUR-STORY FRAME
1.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0 0.0
0

```

PROGRAM CU-NTABS
 INPUT FILE : tsa005.inp
 OUTPUT FILE : tsa005g.out

TSE005.INP
 TOTAL NUMBER OF STORIES-- 4
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ. 0-STATIC LOADS ONLY
 EQ. 1-MODE SHAPES AND FREQUENCIES ONLY
 EQ. 2-STATIC AND MODE SHAPE ANALYSES
 EQ. 3-TYPE 2 AND RESPONSE SPECTRUM ANAL.
 EQ. 4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ. 5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ. 6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ. 7-TYPE 3 AND 8 ANALYSES
 EQ. 8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ. 9-TYPE 4 AND 8 ANALYSES
 EQ. 10-SLAM RESTART
 EQ. 11-SLAM-2 RESTART
 EQ. -1,-6,-9 SAME AS 1,6,9 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
4	FOUR	144.00	10.19	.00	.00	.00	.00	.00
3	THRE	144.00	10.19	.00	.00	.00	.00	.00
2	TWO	144.00	10.19	.00	.00	.00	.00	.00
1	ONE	144.00	10.19	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
4	FOUR	576.00	10.19	.00
3	THRE	432.00	20.38	.00
2	TWO	288.00	30.57	.00
1	ONE	144.00	40.76	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MDM-A	FX-B	FY-B	MDM-B	XA	YA	XB	YB
4	83.30	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	.00	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	83.3000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	83.3000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	83.3000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	83.3000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
4	FOUR	X	11995.2000	.0000
4	FOUR	Y	.0000	.0000
4	FOUR	ROTN	.0000	.0000
3	THRE	X	23990.4000	.0000
3	THRE	Y	.0000	.0000
3	THRE	ROTN	.0000	.0000
2	TWO	X	35985.6000	.0000
2	TWO	Y	.0000	.0000
2	TWO	ROTN	.0000	.0000
1	ONE	X	47980.8000	.0000
1	ONE	Y	.0000	.0000
1	ONE	ROTN	.0000	.0000

FOUR-STORY FRAME
 FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 4
 NUMBER OF COLUMN LINES---- 2
 NUMBER OF BAYS----- 1
 NUMBER OF DIFF. COL. PROP- 1
 NUMBER OF DIFF. BEAM PROP- 2
 NUMBER OF DIFF. FEF----- 1
 NUMBER OF PANEL ELEMENTS-- 0
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE X Y

1 .00 .00
 2 300.00 .00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	30000.00	17.66	.00	.00	.00	343.70	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00
2	30000.00	.00	.00	994.00	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	500.000	.000	500.000	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	4	1	2	1	1	1	0	0
1	2	1	2	2	1	1	0	0

GENERATED BEAM LOCATIONS

OSTORY 1

4	1
3	1
2	2
1	2

GENERATED BEAM LOADS ...LOAD CASE I

OSTORY 1

4	1
3	1
2	1
1	1

GENERATED BEAM LOADS ...LOAD CASE II

OSTORY 1

4	0
3	0
2	0
1	0

GENERATED BEAM LOADS ...LOAD CASE III

OSTORY 1

4	0
3	0
2	0
1	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	4	1	2	3
2	4	1	1	3

GENERATED COLUMN LOCATIONS

DBSTORY 1 2

4 1 1
3 1 1
2 1 1
1 1 1

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	SA	TORS I	FLEX I	K11	K1J	K1J	W1	WJ	VERT 1	VERT 2	VERT 3
4	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
3	30000.00	.00	.00	889.90	4.00	4.00	2.00	.00	.00	1	0	0
2	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0
1	30000.00	.00	.00	984.00	4.00	4.00	2.00	.00	.00	1	0	0

COLUMN PROPERTIES

COLUMN LINE NO. 1

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00

COLUMN LINE NO. 2

LEVEL	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	DT	DB
4	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
3	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
2	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00
1	30000.00	17.86	.00	.00	.00	343.70	.00	.00	.00

D... FRAME TYPE 1 ...

TIME REQUIRED TO FORM STIFFNESS = 3.79

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG
1	1	0	.00	.00	.00

FOUR-STORY FRAM

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
4	X	21.9468295
4	Y	.0000000
4	ROTN	.0000000
3	X	18.2114779
3	Y	.0000000

3	ROTN	.0000000
2	X	12.4848685
2	Y	.0000000
2	ROTN	.0000000
1	X	5.1888202
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 1 LEVEL ID ONE

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	6665.5364552	9799.4871994	-1759.6770236	51.2007839
2	1	-6712.6198312	-9485.2373595	-2240.3229764	-32.0992161

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-15085.3779812	-15079.3062454

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 2 LEVEL ID TWO

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8623.5301748	8419.8415260	-1343.4878131	49.9887131
2	1	-8569.2867551	-8366.8864141	-1656.5321869	-33.3112869

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-14045.8279772	-14019.6172757

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 3 LEVEL ID THREE

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	6285.0287250	5422.2977023	-921.4273890	44.7220707
2	1	-6270.5617528	-5450.3305206	-1078.5728170	-38.5779293

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-9499.5595553	-9495.6148216

MEMBER FORCES FRAME ID FOUR-STORY FRAM FRAME TYPE 1
 LEVEL NO 4 LEVEL ID FOUR

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	4647.1894434	3214.5308303	-474.1917557	42.2947730
2	1	-4643.7785148	-3225.0528688	-525.8082443	-41.0052270

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-4647.1894434	-4643.7785148

CONVERGE IN ITERATION NO. 3

TOTAL TIME 15.22 SEC.

ตัวอย่าง 4 : โครงข้อแข็งประกอบผนังต้านแรงเฉือน 25 ชั้น 3 ช่วงเสา

$$\text{กรณี } \alpha = 0.5$$

```

25 1 1 1 0 0 1 00001 5 0.001 T810805.IMP
F25 4.0
.2.56
F24 4.0
5.12
F23 4.0
5.12
F22 4.0
5.12
F21 4.0
5.12
F20 4.0
5.12
F19 4.0
5.12
F18 4.0
5.12
F17 4.0
5.12
F16 4.0
5.12
F15 4.0
5.12
F14 4.0
5.12
F13 4.0
5.12
F12 4.0
5.12
F11 4.0
5.12
F10 4.0
4.48
F09 4.0
3.84
F08 4.0
3.84
F07 4.0
3.84
F06 4.0
3.84
F05 4.0
3.20
F04 4.0
2.56
F03 4.0
2.56
F02 4.0
1.60
F01 4.0
1.60
1 25 4 3 5 1 2 25 25-STORY, 3-BAY BUILDING
1 0.0 0.0
2 8.0 0.0
3 11.5 0.0
4 18.5 0.0
1 3042000.0 0.16 0.0021333
2 3042000.0 0.36 0.0108000
3 3042000.0 0.5625 0.0263672
4 3042000.0 0.81 0.0546750
5 3042000.0 0.60 0.0125000
1 3042000.0 0.0052083 4.0 4.0 2.0
1 1 38.4 55.2
2 1 55.2 38.4
1 1 2 1 24 1
2 2 3 1 24
3 3 4 1 24 2
1 1 2 4
1 2 2 4
1 3 2 5
1 4 2 8

```


PROGRAM DU-NTABS
 INPUT FILE : ts10s05.inp
 OUTPUT FILE : ts10s05g.out

TS10S05.INP

TOTAL NUMBER OF STORIES-- 25
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 8 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-BLAM RESTART

EQ.11-BLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0

STORY TRANSLATION CODE--- 1

LAT FORCE GENERATION CODE 0 0

STRESS CHECK KEY----- 0

DATA CHECK KEY----- 0

TYPE OF SOLUTION----- 1

MAXIMUM NO. OF CYCLES---- 5

CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
25	F25	4.00	19.08	.00	.00	.00	.00	.00
24	F24	4.00	19.08	.00	.00	.00	.00	.00
23	F23	4.00	19.08	.00	.00	.00	.00	.00
22	F22	4.00	19.08	.00	.00	.00	.00	.00
21	F21	4.00	19.08	.00	.00	.00	.00	.00
20	F20	4.00	19.08	.00	.00	.00	.00	.00
19	F19	4.00	19.08	.00	.00	.00	.00	.00
18	F18	4.00	19.08	.00	.00	.00	.00	.00
17	F17	4.00	19.08	.00	.00	.00	.00	.00
16	F16	4.00	19.08	.00	.00	.00	.00	.00
15	F15	4.00	19.08	.00	.00	.00	.00	.00
14	F14	4.00	19.08	.00	.00	.00	.00	.00
13	F13	4.00	19.08	.00	.00	.00	.00	.00
12	F12	4.00	19.08	.00	.00	.00	.00	.00
11	F11	4.00	19.08	.00	.00	.00	.00	.00
10	F10	4.00	19.08	.00	.00	.00	.00	.00
9	F09	4.00	19.08	.00	.00	.00	.00	.00
8	F08	4.00	19.08	.00	.00	.00	.00	.00
7	F07	4.00	19.08	.00	.00	.00	.00	.00
6	F06	4.00	19.08	.00	.00	.00	.00	.00
5	F05	4.00	19.08	.00	.00	.00	.00	.00
4	F04	4.00	19.08	.00	.00	.00	.00	.00
3	F03	4.00	19.08	.00	.00	.00	.00	.00
2	F02	4.00	19.08	.00	.00	.00	.00	.00
1	F01	4.00	19.08	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
25	F25	100.00	19.08	.00

24	F24	96.00	39.17	.00
23	F23	92.00	57.25	.00
22	F22	88.00	76.33	.00
21	F21	84.00	95.41	.00
20	F20	80.00	114.50	.00
19	F19	76.00	133.58	.00
18	F18	72.00	152.66	.00
17	F17	68.00	171.74	.00
16	F16	64.00	190.83	.00
15	F15	60.00	209.91	.00
14	F14	56.00	228.99	.00
13	F13	52.00	248.07	.00
12	F12	48.00	267.16	.00
11	F11	44.00	286.24	.00
10	F10	40.00	305.32	.00
9	F09	36.00	324.40	.00
8	F08	32.00	343.49	.00
7	F07	28.00	362.57	.00
6	F06	24.00	381.65	.00
5	F05	20.00	400.73	.00
4	F04	16.00	419.82	.00
3	F03	12.00	438.90	.00
2	F02	8.00	457.98	.00
1	F01	4.00	477.06	.00

STRUCTURE LATERAL LOADS...CASES A AND B

LEVEL NO.	FX-A	FY-A	MM-A	FX-B	FY-B	MM-B	XA	YA	XB	YB
25	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
24	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
23	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
22	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
21	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
20	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
19	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
18	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
17	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
16	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
15	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
14	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
13	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
12	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
11	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
10	4.48	.00	.00	.00	.00	.00	.0	.0	.0	.0
9	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
8	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
7	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
6	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
5	3.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
4	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0

STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL ID	DIRN	1	2
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29	F25	X	2.5800	.0000
29	F25	Y	.0000	.0000
29	F25	ROTN	.0000	.0000
24	F24	X	7.8800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	12.8000	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	17.9200	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	23.0400	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	28.1600	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	33.2800	.0000
19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	38.4000	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	43.5200	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	48.6400	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	53.7600	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	58.8800	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	64.0000	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	69.1200	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	74.2400	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	79.3600	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	84.4800	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	89.6000	.0000
8	F08	Y	.0000	.0000

8	F08	ROTN	.0000	.0000
7	F07	X	90.2400	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	94.0800	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	97.2800	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	99.8400	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	102.4000	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	104.0000	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000
1	F01	X	105.6000	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
25	F25	X	10.2400	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	40.9600	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	92.1600	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	163.8400	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	256.0000	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	368.8400	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	501.7600	.0000

19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	655.3600	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	829.4400	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	1024.0000	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	1239.0400	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	1474.5600	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	1730.5600	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	2007.0400	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	2304.0000	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	2618.8800	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	2949.1200	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	3294.7200	.0000
8	F08	Y	.0000	.0000
8	F08	ROTN	.0000	.0000
7	F07	X	3655.8800	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	4032.0000	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	4421.1200	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	4820.4800	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	5230.0800	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	5646.0800	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000

1	F01	X	6069.4800	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

25-STORY,3-BAY BUILDING

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 25
 NUMBER OF COLUMN LINES---- 4
 NUMBER OF BAYS----- 3
 NUMBER OF DIFF. COL. PROP- 5
 NUMBER OF DIFF. BEAM PROP- 1
 NUMBER OF DIFF. FEF----- 2
 NUMBER OF PANEL ELEMENTS-- 25
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	8.00	.00
3	11.50	.00
4	19.50	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
2	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
3	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.80	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	38.400	.000	55.200	.000
2	1	.000	55.200	.000	38.400	.000

BEAM LOCATIONS

/ BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	25	1	2	1	24	1	0	0
2	25	2	3	1	24	0	0	0
3	25	3	4	1	24	2	0	0

GENERATED BEAM LOCATIONS

STORY	1	2	3
25	1	1	1
24	1	1	1
23	1	1	1
22	1	1	1
21	1	1	1
20	1	1	1
19	1	1	1
18	1	1	1
17	1	1	1
16	1	1	1
15	1	1	1
14	1	1	1
13	1	1	1
12	1	1	1
11	1	1	1
10	1	1	1
9	1	1	1
8	1	1	1

7	1	1	1
6	1	1	1
5	1	1	1
4	1	1	1
3	1	1	1
2	1	1	1
1	1	1	1

GENERATED BEAM LOADS...LOAD CASE I

OSTORY	1	2	3
25	1	0	2
24	1	0	2
23	1	0	2
22	1	0	2
21	1	0	2
20	1	0	2
19	1	0	2
18	1	0	2
17	1	0	2
16	1	0	2
15	1	0	2
14	1	0	2
13	1	0	2
12	1	0	2
11	1	0	2
10	1	0	2
9	1	0	2
8	1	0	2
7	1	0	2
6	1	0	2
5	1	0	2
4	1	0	2
3	1	0	2
2	1	0	2
1	1	0	2

GENERATED BEAM LOADS...LOAD CASE II

OSTORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

STORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KCOL	GEN
1	25	1	2	4
1	20	2	2	4
1	15	3	2	5
1	9	4	2	8
2	25	5	3	24
3	25	5	4	24
4	25	1	3	4
4	20	2	3	4
4	15	3	3	5
4	9	4	3	8

GENERATED COLUMN LOCATIONS

STORY	1	2	3	4
25	1	5	5	1
24	1	5	5	1
23	1	5	5	1
22	1	5	5	1
21	1	5	5	1
20	2	5	5	2
19	2	5	5	2
18	2	5	5	2
17	2	5	5	2
16	2	5	5	2
15	3	5	5	3
14	3	5	5	3
13	3	5	5	3
12	3	5	5	3
11	3	5	5	3
10	3	5	5	3
9	4	5	5	4
8	4	5	5	4

7	4	5	5	4
8	4	5	5	4
5	4	5	5	4
4	4	5	5	4
3	4	5	5	4
2	4	5	5	4
1	4	5	5	4

PANEL CARDS

LEVEL	COL I	COL J	E	A	I	SA	G
25	2	3	3042000.00	1.05	1.07	.00	.00
24	2	3	3042000.00	1.05	1.07	.00	.00
23	2	3	3042000.00	1.05	1.07	.00	.00
22	2	3	3042000.00	1.05	1.07	.00	.00
21	2	3	3042000.00	1.05	1.07	.00	.00
20	2	3	3042000.00	1.05	1.07	.00	.00
19	2	3	3042000.00	1.05	1.07	.00	.00
18	2	3	3042000.00	1.05	1.07	.00	.00
17	2	3	3042000.00	1.05	1.07	.00	.00
16	2	3	3042000.00	1.05	1.07	.00	.00
15	2	3	3042000.00	1.05	1.07	.00	.00
14	2	3	3042000.00	1.05	1.07	.00	.00
13	2	3	3042000.00	1.05	1.07	.00	.00
12	2	3	3042000.00	1.05	1.07	.00	.00
11	2	3	3042000.00	1.05	1.07	.00	.00
10	2	3	3042000.00	1.05	1.07	.00	.00
9	2	3	3042000.00	1.05	1.07	.00	.00
8	2	3	3042000.00	1.05	1.07	.00	.00
7	2	3	3042000.00	1.05	1.07	.00	.00
6	2	3	3042000.00	1.05	1.07	.00	.00
5	2	3	3042000.00	1.05	1.07	.00	.00
4	2	3	3042000.00	1.05	1.07	.00	.00
3	2	3	3042000.00	1.05	1.07	.00	.00
2	2	3	3042000.00	1.05	1.07	.00	.00
1	2	3	3042000.00	1.05	1.07	.00	.00

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
25	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
24	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
23	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
22	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
21	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
20	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
19	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
18	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
17	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
16	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
15	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
14	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
13	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
12	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
11	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
10	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
9	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
8	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
7	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
6	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
5	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
4	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
3	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
2	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
BAY NUMBERS		2										
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3

25	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
24	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
23	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
22	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
21	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
20	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
19	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
18	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
17	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
16	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
15	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
14	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
13	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
12	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
11	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
10	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
9	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
8	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
7	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
6	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
3	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
2	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
1	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00

0...FRAME TYPE 1 ...
 TIME REQUIRED TO FORM STIFFNESS = 76.12

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	25-B,3-B BUILD

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	.50	.00	.00	.50	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
25	X	.1294520
25	Y	.0000000
25	ROTN	.0000000
24	X	.1246610
24	Y	.0000000
24	ROTN	.0000000
23	X	.1198007
23	Y	.0000000
23	ROTN	.0000000
22	X	.1146365
22	Y	.0000000
22	ROTN	.0000000
21	X	.1097403
21	Y	.0000000
21	ROTN	.0000000
20	X	.1044931

20	Y	.0000000
20	ROTN	.0000000
19	X	.0990931
19	Y	.0000000
19	ROTN	.0000000
18	X	.0935183
18	Y	.0000000
18	ROTN	.0000000
17	X	.0877606
17	Y	.0000000
17	ROTN	.0000000
16	X	.0818295
16	Y	.0000000
16	ROTN	.0000000
15	X	.0757323
15	Y	.0000000
15	ROTN	.0000000
14	X	.0694972
14	Y	.0000000
14	ROTN	.0000000
13	X	.0631419
13	Y	.0000000
13	ROTN	.0000000
12	X	.0567034
12	Y	.0000000
12	ROTN	.0000000
11	X	.0502251
11	Y	.0000000
11	ROTN	.0000000
10	X	.0437820
10	Y	.0000000
10	ROTN	.0000000
9	X	.0373783
9	Y	.0000000
9	ROTN	.0000000
8	X	.0311599
8	Y	.0000000
8	ROTN	.0000000
7	X	.0251734
7	Y	.0000000
7	ROTN	.0000000
6	X	.0195275
6	Y	.0000000
6	ROTN	.0000000
5	X	.0143286
5	Y	.0000000
5	ROTN	.0000000
4	X	.0097024
4	Y	.0000000
4	ROTN	.0000000
3	X	.0057897
3	Y	.0000000
3	ROTN	.0000000
2	X	.0027480
2	Y	.0000000
2	ROTN	.0000000
1	X	.0007522
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID 25-8,3-8 BUILD.
LEVEL NO 1

FRAME TYPE 1
LEVEL ID F01

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-10.6781815	18.0530037	-380.2214248	1.7727032
2	1	-1.3828925	4.8548454	-102.2760744	.7988046
3	1	-1.2950894	4.8100589	-640.3981239	.7083145
4	1	10.8144251	-18.0509746	-567.2915156	-1.7524576

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-4.5913058	-4.4811012
2	1	.5042466	.5130438
3	1	-4.6052671	-4.7183361

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-178.8080667	370.2877619	-649.8319610	47.7677200

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 2

FRAME TYPE 1
LEVEL ID F02

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-7.3877593	15.2674873	-362.1554757	1.7892406
2	1	.4746329	5.3595470	-128.0688115	1.3948471
3	1	.6017819	5.3873127	-585.1730332	1.2053109
4	1	7.2876172	-15.3327613	-546.9160654	-1.7434110

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-8.2343456	-8.0642128
2	1	1.2782750	1.2871521
3	1	-8.3082810	-8.4846734

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-140.8965353	325.8118079	-624.0866142	45.8673901

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 3

FRAME TYPE 1
LEVEL ID F03

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-3.7739619	15.8221039	-344.9927955	2.8996881
2	1	2.1648119	6.3113048	-150.4371190	2.0096303
3	1	2.3589728	8.4093468	-533.3976854	1.7859614
4	1	3.5955409	-15.7522908	-525.8189461	-2.8394857

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-11.2935289	-11.0812439
2	1	1.8738901	1.9017024
3	1	-11.4232867	-11.6647783

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-110.3811298	280.4621277	-598.3554539	42.0652342

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 4

FRAME TYPE 1
LEVEL ID F04

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-.8663063	15.0674888	-328.5871418	3.2288880
2	1	3.5940208	7.0025419	-188.9215159	2.4839090
3	1	3.8120419	7.1846114	-485.5221748	2.2892466
4	1	.8313758	-15.2603193	-503.5309390	-3.1647038

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-13.7721489	-13.4932739
2	1	2.3685873	2.4050643
3	1	-13.8708853	-14.2616160

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
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2 1 -82.8936448 240.2271809 -572.6382294 38.7732542

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 5 LEVEL ID F05

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	1.8824255	14.8384532	-312.7953194	3.7184550
2	1	-4.7586048	7.5306857	-183.9750797	2.9597895
3	1	5.0248249	7.7535791	-441.0921898	2.8844541
4	1	-1.9743304	-14.8929918	-480.8019004	-3.8607572

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-15.7458318	-15.4293655
2	1	2.7652478	2.8100253
3	1	-16.0197185	-16.3509215

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-58.5086317	203.9052435	-546.9346308	35.7165436

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 6 LEVEL ID F06

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	3.7882280	14.0634080	-297.4922190	4.0712510
2	1	5.7056926	7.9045129	-195.8837451	3.1479827
3	1	6.0183123	8.1848664	-399.8441004	3.0311080
4	1	-4.1113431	-14.3765911	-457.5555706	-4.0272880

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.2898943	-16.9231530
2	1	3.0793404	3.1320531
3	1	-17.8242946	-17.9884489

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-37.2130958	170.9724670	-521.2443648	32.7623694

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 7 LEVEL ID F07

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	5.7102774	13.5016883	-282.5683500	4.4041466
2	1	6.4388956	8.1381200	-204.6679347	3.3548673
3	1	6.7991912	8.4739295	-361.6945573	3.3077522
4	1	-8.1220287	-13.8771058	-433.9039776	-4.3873329

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-18.3858883	-18.0241649
2	1	3.3101957	3.3711322
3	1	-18.8328651	-19.2142885

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-19.4019884	140.8635384	-495.5871805	29.6658999

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 8 LEVEL ID F08

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
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1	1	6.4267790	12.8755909	-267.9176041	4.3748220
2	1	7.0386369	8.2770736	-210.7912537	3.5138109
3	1	7.4401810	8.6625316	-326.2403788	3.5376593
4	1	-6.8367261	-13.0922579	-409.9480849	-4.3690162

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-19.2021852	-18.8021398
2	1	3.4965517	3.5627943
3	1	-19.7204940	-20.1432409

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-2.7002255	115.1314438	-469.9026785	27.4048903

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
LEVEL NO 9 LEVEL ID F09

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	10.5822129	12.7754062	-253.4681447	5.4401736
2	1	7.3857736	8.2669511	-213.7389101	3.5757427
3	1	7.8592039	8.7176287	-293.9768824	3.6866971
4	1	-11.2352459	-13.3065146	-385.7651193	-5.5354411

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-19.5180183	-19.2015065
2	1	3.5829294	3.6880802
3	1	-20.2079959	-20.5488229

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	6.5185624	86.4130751	-444.2511434	23.0419442

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
LEVEL NO 10 LEVEL ID F10

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	9.0090697	8.9569054	-239.1080853	4.1096161
2	1	7.7420003	8.2528035	-214.9382358	3.6556751
3	1	8.0695398	8.6817119	-263.4751765	3.7673217
4	1	-9.3358010	-9.3135770	-361.4705170	-4.0854584

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-18.7452532	-18.5412478
2	1	3.8240190	3.6800280
3	1	-20.0657995	-20.2758940

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	24.0491853	73.5908523	-418.6099856	23.7419270

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
LEVEL NO 11 LEVEL ID F11

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	10.0308007	10.7361835	-224.8188990	4.8294942
2	1	7.9972723	8.1752284	-214.7772991	3.6980981
3	1	8.0947189	8.3362317	-234.2644489	3.7292236
4	1	-10.1453882	-10.9398929	-337.2278303	-4.7264433

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-20.0039409	-19.7673624

2	1	3.8687051	3.8741388
3	1	-19.8378271	-20.0759011

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		31.0042088	51.4941417	-392.9115268	20.1397390

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 12 LEVEL ID F12

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	10.1822948	9.9731402	-210.5903109	-4.6927901
2	1	8.1661971	8.1013950	-211.9801847	3.7235759
3	1	8.0875370	8.0889714	-207.6310553	3.8978512
4	1	-10.0536446	-9.9305129	-313.0386143	-4.4890471

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-19.8940189	-19.7825843
2	1	3.6562405	3.8298923
3	1	-19.4151498	-19.6406980

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		39.3222943	34.8832246	-387.1599349	17.9567337

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 13 LEVEL ID F13

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	10.5036117	9.8317241	-196.3598863	4.7877651
2	1	8.2123508	7.9401467	-207.0886978	3.7047880
3	1	7.9327081	7.7177205	-183.0359351	3.6179852
4	1	-10.1874372	-9.5870535	-288.9566333	-4.4785063

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-19.8114313	-19.5894492
2	1	3.8113633	3.5574724
3	1	-18.8578114	-19.0889548

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		44.2381039	19.6855777	-341.3589575	15.4309652

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 14 LEVEL ID F14

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	9.9398001	9.3078196	-182.0849963	-4.5226071
2	1	8.2288950	7.7857451	-200.2741037	3.6799632
3	1	7.7890786	7.3677309	-180.3121516	3.5294974
4	1	-9.4721934	-8.8915175	-265.0157750	-4.1673884

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-18.5897715	-19.3138446
2	1	3.5862233	3.4833928
3	1	-18.2328021	-18.4693366

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		48.4783201	7.8890905	-315.5129734	13.5405636

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 15 LEVEL ID F15

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	12.2862188	9.8299714	-167.7454233	5.2175933
2	1	8.0542208	7.5205282	-191.0614889	3.5958627
3	1	7.4939271	6.9803307	-139.9393478	3.4004289
4	1	-11.5243088	-8.9971532	-241.2280077	-4.7543428

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-18.8921665	-18.7971911
2	1	3.4542843	3.3613751
3	1	-17.3850879	-17.4785499

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	48.8189719	-5.3640332	-299.8257322	9.9117701

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 16 LEVEL ID F16

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.7730420	6.6058479	-153.2553430	3.6111159
2	1	7.9243213	7.2788861	-180.8003651	3.5251585
3	1	7.0110450	6.5207857	-120.5727570	3.2014191
4	1	-7.8301958	-5.9542412	-217.6700530	-3.1143156

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.9480504	-18.2335456
2	1	3.2789643	3.1087928
3	1	-15.9389009	-15.6786791

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	53.2777551	-8.1979650	-263.7014819	10.8679883

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 17 LEVEL ID F17

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	9.4333793	9.1750094	-138.5780425	4.4466142
2	1	7.8434636	7.0302600	-189.5800929	3.4669784
3	1	6.5089085	5.9210631	-102.0486282	2.9311757
4	1	-8.0054112	-7.8464834	-194.5181055	-3.6745432

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.8521307	-18.0298482
2	1	3.2383044	3.0052988
3	1	-14.8895107	-14.7324774

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	49.8520538	-19.2796186	-237.6751309	7.2409858

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 18 LEVEL ID F18

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	9.2978296	8.4187514	-123.8632899	4.2509187
2	1	7.7278315	6.9480903	-156.0175982	3.4444821
3	1	8.0490079	5.3753034	-85.7537902	2.7326855

4	1	-7.4402344	-6.7270663	-171.6153569	-3.2948855
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BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.4269432	-17.8542587
2	1	3.1118268	2.8272482
3	1	-12.7828647	-13.5934401

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	47.4235757	-24.2978568	-211.5499648	5.4770276

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 19 LEVEL ID F19

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.2751222	8.1290137	-109.0484276	3.9489981
2	1	7.8581241	6.8146004	-141.0851234	3.4215074
3	1	5.6340237	4.9066086	-70.7526118	2.5365145
4	1	-6.3447308	-6.1532057	-148.9933188	-2.9167569

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.3118910	-17.3980869
2	1	3.0706351	2.7296318
3	1	-12.8545385	-12.7705722

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	44.0352041	-27.7367116	-185.3405183	3.8162204

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 20 LEVEL ID F20

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	11.8138234	9.0367688	-94.1871749	5.0854940
2	1	7.3457768	6.6693278	-123.6377929	3.3368634
3	1	5.1355462	4.4908829	-58.1342845	2.3281252
4	1	-8.4756831	-6.4258413	-126.8901800	-3.5544776

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-15.9345086	-16.5513517
2	1	2.9112827	2.5543679
3	1	-11.5910129	-11.1448092

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	33.4114236	-33.4523923	-159.0506677	- .2249627

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 21 LEVEL ID F21

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	5.7032507	4.1208852	-79.0479074	2.3522882
2	1	6.7373642	6.2942923	-105.0572443	3.1189184
3	1	4.1977718	3.9010987	-45.7248306	1.9847354
4	1	-3.6090814	-2.6891461	-104.5482022	-1.4324046

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-12.5343731	-16.0223202
2	1	2.4519714	2.0247835
3	1	-9.1872741	-7.8104211

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	2	1	36.3934729	-25.0904457	-132.7218155	2.8518511

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 22	LEVEL ID F22

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.7089985	8.8311224	-83.2924941	3.3043928
2	1	8.6328840	5.8328846	-88.7108003	3.0034414
3	1	3.5472037	2.9447188	-32.8126747	1.5811781
4	1	-3.7958986	-4.0013596	-83.2509903	-1.8431888

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-13.1531409	-15.3228826
2	1	2.5527174	2.0306746
3	1	-8.2819439	-7.0881747

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	2	1	27.2568143	-29.8035745	-106.3330408	-1.7722122

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 23	LEVEL ID F23

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.8174013	8.4441444	-47.8519070	3.2062473
2	1	8.7180080	8.1373011	-88.8867538	3.1278346
3	1	3.0973802	2.8840856	-22.3215275	1.4176616
4	1	-3.3119142	-3.2904760	-82.1324755	-1.5734873

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-12.9825557	-15.2250305
2	1	2.5102514	1.9089426
3	1	-7.3772958	-6.2611944

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	2	1	18.1145187	-29.4192851	-79.8072461	-2.9252324

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 24	LEVEL ID F24

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.1472853	8.3451545	-31.8754453	3.0842570
2	1	8.1806733	5.8987711	-47.3010293	2.8873862
3	1	2.7117581	2.3709830	-13.4973123	1.2542798
4	1	-2.8157808	-2.9492801	-41.2278643	-1.3911700

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-13.6472238	-15.8288006
2	1	2.2712481	1.7455350
3	1	-8.9402803	-8.0595478

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
	2	1	7.8288990	-26.8785115	-53.1985488	-4.8770841

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 25	LEVEL ID F25

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	9.2099887	7.4999385	-16.4349234	4.1577970
2	1	8.9766897	7.1766792	-22.6631937	4.0113173
3	1	2.9021146	2.4829672	-7.7100901	1.3370357
4	1	-3.9893440	-3.2437670	-20.4026882	-1.7788405

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-9.2099887	-12.9106244
2	1	3.9339348	2.7600473
3	1	-6.8521619	-3.9893440

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-12.3653433	-27.5277122	-26.4891146	-10.0049911

CONVERGE IN ITERATION NO. 3

TOTAL TIME 280.51 SEC.

ตัวอย่าง 4 : โครงข้อแข็งประกอบผนังต้านแรงเฉือน 25 ชั้น 3 ช่วงเสา

กรณี $\alpha = 1.0$

25	1	1	1	0	0	1	00001	5	0.001	TS10801.INP
F25									4.0	
	2.56									
F24									4.0	
	5.12									
F23									4.0	
	5.12									
F22									4.0	
	5.12									
F21									4.0	
	5.12									
F20									4.0	
	5.12									
F19									4.0	
	5.12									
F18									4.0	
	5.12									
F17									4.0	
	5.12									
F16									4.0	
	5.12									
F15									4.0	
	5.12									
F14									4.0	
	5.12									
F13									4.0	
	5.12									
F12									4.0	
	5.12									
F11									4.0	
	5.12									
F10									4.0	
	4.48									
F09									4.0	
	3.84									
F08									4.0	
	3.84									
F07									4.0	
	3.84									
F06									4.0	
	3.84									
F05									4.0	
	3.20									
F04									4.0	
	2.56									
F03									4.0	
	2.56									
F02									4.0	
	1.60									
F01									4.0	
	1.60									

1	25	4	3	5	1	2	25	25-STORY, 3-BAY BUILDING
1		0.0		0.0				
2		0.0		0.0				
3		11.5		0.0				
4		19.5		0.0				
1		3042000.0		0.16			0.0021333	
2		3042000.0		0.36			0.0108000	
3		3042000.0		0.5625			0.0263672	
4		3042000.0		0.81			0.0548750	
5		3042000.0		0.60			0.0126000	
1		3042000.0				0.0052083	4.0	4.0
							2.0	
1	1			38.4			55.2	
2	1			55.2			38.4	
1	1	2	1	24	1			
2	2	3	1	24				
3	3	4	1	24	2			
1	1	2	4					
1	2	2	4					
1	3	2	5					
1	4	2	8					

PROGRAM CU-NTAB8
 INPUT FILE : ts10e01.inp
 OUTPUT FILE : ts10e01g.out

TS10E01.INP

TOTAL NUMBER OF STORIES-- 25
 NUMBER OF DIFF FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 6 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-SLAM RESTART

EQ.11-SLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0

STORY TRANSLATION CODE--- 1

LAT FORCE GENERATION CODE 0 0

STRESS CHECK KEY----- 0

DATA CHECK KEY----- 0

TYPE OF SOLUTION----- 1

MAXIMUM NO OF CYCLES---- 5

CONVERGENCE TOLERANCE OF EQUILIBRIUM 001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
25	F25	4.00	19.08	.00	.00	.00	.00	.00
24	F24	4.00	19.08	.00	.00	.00	.00	.00
23	F23	4.00	19.08	.00	.00	.00	.00	.00
22	F22	4.00	19.08	.00	.00	.00	.00	.00
21	F21	4.00	19.08	.00	.00	.00	.00	.00
20	F20	4.00	19.08	.00	.00	.00	.00	.00
19	F19	4.00	19.08	.00	.00	.00	.00	.00
18	F18	4.00	19.08	.00	.00	.00	.00	.00
17	F17	4.00	19.08	.00	.00	.00	.00	.00
16	F16	4.00	19.08	.00	.00	.00	.00	.00
15	F15	4.00	19.08	.00	.00	.00	.00	.00
14	F14	4.00	19.08	.00	.00	.00	.00	.00
13	F13	4.00	19.08	.00	.00	.00	.00	.00
12	F12	4.00	19.08	.00	.00	.00	.00	.00
11	F11	4.00	19.08	.00	.00	.00	.00	.00
10	F10	4.00	19.08	.00	.00	.00	.00	.00
9	F09	4.00	19.08	.00	.00	.00	.00	.00
8	F08	4.00	19.08	.00	.00	.00	.00	.00
7	F07	4.00	19.08	.00	.00	.00	.00	.00
6	F06	4.00	19.08	.00	.00	.00	.00	.00
5	F05	4.00	19.08	.00	.00	.00	.00	.00
4	F04	4.00	19.08	.00	.00	.00	.00	.00
3	F03	4.00	19.08	.00	.00	.00	.00	.00
2	F02	4.00	19.08	.00	.00	.00	.00	.00
1	F01	4.00	19.08	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
25	F25	100.00	19.08	.00

24	F24	96.00	38.17	.00
23	F23	92.00	57.25	.00
22	F22	88.00	76.33	.00
21	F21	84.00	95.41	.00
20	F20	80.00	114.50	.00
19	F19	76.00	133.58	.00
18	F18	72.00	152.66	.00
17	F17	68.00	171.74	.00
16	F16	64.00	190.83	.00
15	F15	60.00	209.91	.00
14	F14	56.00	228.99	.00
13	F13	52.00	248.07	.00
12	F12	48.00	267.16	.00
11	F11	44.00	286.24	.00
10	F10	40.00	305.32	.00
9	F09	36.00	324.40	.00
8	F08	32.00	343.49	.00
7	F07	28.00	362.57	.00
6	F06	24.00	381.65	.00
5	F05	20.00	400.73	.00
4	F04	16.00	419.82	.00
3	F03	12.00	438.90	.00
2	F02	8.00	457.98	.00
1	F01	4.00	477.06	.00

STRUCTURE LATERAL LOADS - CASES A AND B

LEVEL NO	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
25	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
24	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
23	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
22	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
21	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
20	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
19	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
18	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
17	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
16	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
15	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
14	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
13	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
12	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
11	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
10	4.48	.00	.00	.00	.00	.00	.0	.0	.0	.0
9	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
8	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
7	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
6	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
5	3.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
4	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	1.80	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	1.80	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

25	F25	X	2.5600	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	7.6800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	12.8000	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	17.9200	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	23.0400	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	28.1600	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	33.2800	.0000
19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	38.4000	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	43.5200	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	48.6400	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	53.7600	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	58.8800	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	64.0000	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	69.1200	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	74.2400	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	79.3600	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	84.4800	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	89.6000	.0000
8	F08	Y	.0000	.0000

8	F08	ROTN	.0000	.0000
7	F07	X	90.2400	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	94.0800	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	97.2800	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	99.8400	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	102.4000	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	104.0000	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000
1	F01	X	105.6000	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
25	F25	X	10.2400	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	40.9600	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	92.1600	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	163.8400	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	256.0000	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	368.6400	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	501.7600	.0000

19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	655.3600	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	829.4400	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	1024.0000	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	1239.0400	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	1474.5600	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	1730.5600	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	2007.0400	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	2304.0000	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	2618.8800	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	2949.1200	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	3294.7200	.0000
8	F08	Y	.0000	.0000
8	F08	ROTN	.0000	.0000
7	F07	X	3655.6800	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	4032.0000	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	4421.1200	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	4820.4800	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	5230.0800	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	5646.0800	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000

```

T  F01  X      8068.4800      .0000
+  F01  Y       0000      .0000
1  F01  ROTN     .0000      .0000
    
```

25-STORY, 3-BAY BUILDING

```

FRAME ID NUMBER----- 1
NUMBER OF STORY LEVELS---- 25
NUMBER OF COLUMN LINES---- 4
NUMBER OF BAYS----- 3
NUMBER OF DIFF. COL. PROP- 5
NUMBER OF DIFF. BEAM PROP- 1
NUMBER OF DIFF. FEF----- 2
NUMBER OF PANEL ELEMENTS-- 25
NUMBER OF BRACING ELEMENTS 0
    
```

COLUMN LINE COORDINATES

```

LINE      X      Y
1         00      00
2         8 00      00
3        11 50      00
4        19 50      00
    
```

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
2	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
3	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.80	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	38.400	.000	55.200	.000
2	1	.000	55.200	.000	38.400	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	25	1	2	1	24	1	0	0
2	25	2	3	1	24	0	0	0
3	25	3	4	1	24	2	0	0

GENERATED BEAM LOCATIONS

OSTORY	1	2	3
25	1	1	1
24	1	1	1
23	1	1	1
22	1	1	1
21	1	1	1
20	1	1	1
19	1	1	1
18	1	1	1
17	1	1	1
16	1	1	1
15	1	1	1
14	1	1	1
13	1	1	1
12	1	1	1
11	1	1	1
10	1	1	1
9	1	1	1
8	1	1	1

7	1	1	1
6	1	1	1
5	1	1	1
4	1	1	1
3	1	1	1
2	1	1	1
1	1	1	1

GENERATED BEAM LOADS ... LOAD CASE 1

OSTORY	1	2	3
25	1	0	2
24	1	0	2
23	1	0	2
22	1	0	2
21	1	0	2
20	1	0	2
19	1	0	2
18	1	0	2
17	1	0	2
16	1	0	2
15	1	0	2
14	1	0	2
13	1	0	2
12	1	0	2
11	1	0	2
10	1	0	2
9	1	0	2
8	1	0	2
7	1	0	2
6	1	0	2
5	1	0	2
4	1	0	2
3	1	0	2
2	1	0	2
1	1	0	2

GENERATED BEAM LOADS ... LOAD CASE 11

OSTORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

GENERATED BEAM LOADS ... LOAD CASE III

STORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KOOL	GEN
1	25	1	2	4
1	20	2	2	4
1	15	3	2	5
1	9	4	2	8
2	25	5	3	24
3	25	5	4	24
4	25	1	3	4
4	20	2	3	4
4	15	3	3	5
4	9	4	3	8

GENERATED COLUMN LOCATIONS

STORY	1	2	3	4
25	1	5	5	1
24	1	5	5	1
23	1	5	5	1
22	1	5	5	1
21	1	5	5	1
20	2	5	5	2
19	2	5	5	2
18	2	5	5	2
17	2	5	5	2
16	2	5	5	2
15	3	5	5	3
14	3	5	5	3
13	3	5	5	3
12	3	5	5	3
11	3	5	5	3
10	3	5	5	3
9	4	5	5	4
8	4	5	5	4

7	4	5	5	4
6	4	5	5	4
5	4	5	5	4
4	4	5	5	4
3	4	5	5	4
2	4	5	5	4
1	4	5	5	4

PANEL CARDS

LEVEL	COL I	COL J	E	A	I	BA	G
25	2	3	3042000.00	1.05	1.07	.00	.00
24	2	3	3042000.00	1.05	1.07	.00	.00
23	2	3	3042000.00	1.05	1.07	.00	.00
22	2	3	3042000.00	1.05	1.07	.00	.00
21	2	3	3042000.00	1.05	1.07	.00	.00
20	2	3	3042000.00	1.05	1.07	.00	.00
19	2	3	3042000.00	1.05	1.07	.00	.00
18	2	3	3042000.00	1.05	1.07	.00	.00
17	2	3	3042000.00	1.05	1.07	.00	.00
16	2	3	3042000.00	1.05	1.07	.00	.00
15	2	3	3042000.00	1.05	1.07	.00	.00
14	2	3	3042000.00	1.05	1.07	.00	.00
13	2	3	3042000.00	1.05	1.07	.00	.00
12	2	3	3042000.00	1.05	1.07	.00	.00
11	2	3	3042000.00	1.05	1.07	.00	.00
10	2	3	3042000.00	1.05	1.07	.00	.00
9	2	3	3042000.00	1.05	1.07	.00	.00
8	2	3	3042000.00	1.05	1.07	.00	.00
7	2	3	3042000.00	1.05	1.07	.00	.00
6	2	3	3042000.00	1.05	1.07	.00	.00
5	2	3	3042000.00	1.05	1.07	.00	.00
4	2	3	3042000.00	1.05	1.07	.00	.00
3	2	3	3042000.00	1.05	1.07	.00	.00
2	2	3	3042000.00	1.05	1.07	.00	.00
1	2	3	3042000.00	1.05	1.07	.00	.00

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
25	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
24	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
23	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
22	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
21	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
20	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
19	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
18	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
17	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
16	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
15	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
14	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
13	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
12	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
11	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
10	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
9	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
8	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
7	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
6	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
5	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
4	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
3	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
2	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
BAY NUMBERS		2										
LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3

25	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
24	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
23	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
22	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
21	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
20	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
19	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
18	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
17	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
16	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
15	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
14	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
13	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
12	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
11	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
10	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
9	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
8	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
7	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
6	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
3	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
2	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
1	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00

0. FRAME TYPE 1
 TIME REQUIRED TO FORM STIFFNESS = 75.47

1. FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	25-S,3-B BUILD

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.00	.00	.00	1.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
25	X	.2740243
25	Y	.0000000
25	ROTN	.0000000
24	X	.2638885
24	Y	.0000000
24	ROTN	.0000000
23	X	.2535621
23	Y	.0000000
23	ROTN	.0000000
22	X	.2430379
22	Y	.0000000
22	ROTN	.0000000
21	X	.2322344
21	Y	.0000000
21	ROTN	.0000000
20	X	.2211108

20	Y	.0000000
20	ROTN	.0000000
19	X	.2098631
19	Y	.0000000
19	ROTN	.0000000
18	X	.1978400
18	Y	.0000000
18	ROTN	.0000000
17	X	.1858371
17	Y	.0000000
17	ROTN	.0000000
16	X	.1730611
16	Y	.0000000
16	ROTN	.0000000
15	X	.1601324
15	Y	.0000000
15	ROTN	.0000000
14	X	.1469108
14	Y	.0000000
14	ROTN	.0000000
13	X	.1334351
13	Y	.0000000
13	ROTN	.0000000
12	X	.1197840
12	Y	.0000000
12	ROTN	.0000000
11	X	.1060514
11	Y	.0000000
11	ROTN	.0000000
10	X	.0923556
10	Y	.0000000
10	ROTN	.0000000
9	X	.0788339
9	Y	.0000000
9	ROTN	.0000000
8	X	.0656640
8	Y	.0000000
8	ROTN	.0000000
7	X	.0530077
7	Y	.0000000
7	ROTN	.0000000
6	X	.0410775
6	Y	.0000000
6	ROTN	.0000000
5	X	.0301057
5	Y	.0000000
5	ROTN	.0000000
4	X	.0203574
4	Y	.0000000
4	ROTN	.0000000
3	X	.0121279
3	Y	.0000000
3	ROTN	.0000000
2	X	.0057442
2	Y	.0000000
2	ROTN	.0000000
1	X	.0015673
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID 25-S,3-B BUILD.
LEVEL NO 1

FRAME TYPE 1
LEVEL ID F01

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-22.4128719	37.3957962	-749.5722588	3.4520222
2	1	-2.9271731	9.8490490	-179.9384365	1.6099627
3	1	-2.6342145	9.4086333	-1305.3917443	1.1821061
4	1	22.2423919	-37.3356654	-1145.4336522	-3.3244971

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-9.5901100	-9.3808896
2	1	1.0771751	1.0941020
3	1	-9.6098671	-9.9445885

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-381.0635009	767.2261623	-1299.8639082	96.0314112

MEMBER FORCES FRAME ID 25-S,3-B BUILD.
LEVEL NO 2

FRAME TYPE 1
LEVEL ID F02

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-15.5747877	32.0029820	-713.5411337	3.3619620
2	1	.9672076	11.2108876	-232.5848553	2.8018565
3	1	1.3005457	11.1499796	-1193.8988891	1.8659505
4	1	15.2969667	-32.0869783	-1104.6018455	-3.0440669

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-17.2834802	-16.9067250
2	1	2.6948041	2.7346481
3	1	-17.3930195	-17.7631745

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-301.9608334	678.8797002	-1248.1732764	92.9263621

MEMBER FORCES FRAME ID 25-S,3-B BUILD.
LEVEL NO 3

FRAME TYPE 1
LEVEL ID F03

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-8.0820798	32.8392479	-679.4124069	5.1097540
2	1	4.5803340	13.2447133	-279.1190523	4.0058116
3	1	4.9596940	13.3578257	-1088.5514280	2.8421386
4	1	7.6742681	-33.0601412	-1061.8073213	-4.6519084

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-23.7376999	-23.2493452
2	1	3.9502715	4.0085955
3	1	-23.9710599	-24.4790050

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-237.5456301	588.3465883	-1196.7107935	65.7903640

MEMBER FORCES FRAME ID 25-S,3-B BUILD.
LEVEL NO 4

FRAME TYPE 1
LEVEL ID F04

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-1.9621093	31.7997797	-646.8957875	6.1285271
2	1	7.5391265	14.7387397	-318.3702185	4.9144578
3	1	8.0107859	15.0027704	-990.5167945	3.7155137
4	1	1.4681268	-32.1532731	-1017.3510631	-5.5782079

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-29.0108895	-28.4229290
2	1	4.9978161	5.0739038
3	1	-29.3749757	-29.9883918

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
-------	------	------------	------------	-------------	-------------

2 1 -179.1950293 506.6332609 -1145.2781364 79.5032987

MEMBER FORCES FRAME ID 25-S,3-B BUILD. FRAME TYPE 1
LEVEL NO 5 LEVEL ID F05

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	3.4125104	30.9729988	-615.6650149	7.0959523
2	1	10.0141144	15.8859864	-351.0512327	5.6194852
3	1	10.5683645	16.2903061	-899.0844188	-4.5230269
4	1	-4.0149336	-31.4585186	-971.5306422	-6.5001650

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-33.2296326	-32.5610099
2	1	5.8417343	5.9343854
3	1	-33.7389493	-34.4383593

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-127.1857295	432.0145696	-1093.8886934	73.5413643

MEMBER FORCES FRAME ID 25-S,3-B BUILD. FRAME TYPE 1
LEVEL NO 6 LEVEL ID F06

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	7.8342138	29.8171222	-585.4888451	7.8068665
2	1	12.0318890	16.7051612	-377.5290748	6.1487388
3	1	12.6693284	17.2381893	-813.8858858	5.2444330
4	1	-8.5337904	-30.4234256	-924.6084786	-7.2031478

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-36.5030519	-35.7690904
2	1	6.5128287	6.6210943
3	1	-37.1688271	-37.9388136

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-81.5561421	363.7013414	-1042.4879156	67.6768061

MEMBER FORCES FRAME ID 25-S,3-B BUILD. FRAME TYPE 1
LEVEL NO 7 LEVEL ID F07

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	11.9744721	28.6688381	-556.1228629	8.5021530
2	1	13.5986473	17.2242947	-397.8377037	6.5191573
3	1	14.3289863	17.8784044	-734.8860902	5.8599946
4	1	-12.8081254	-29.4050233	-876.8200235	-7.9381114

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-38.9124058	-38.1457815
2	1	7.0081758	7.1324527
3	1	-39.7809275	-40.5879937

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-43.2119958	300.7187835	-991.1333196	61.4205740

MEMBER FORCES FRAME ID 25-S,3-B BUILD. FRAME TYPE 1
LEVEL NO 8 LEVEL ID F08

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
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    LM(1)=LM(2)-1
    LM( 9)=LM(3)+3
    LM(8)=LM( 9)-1
    LM(7)=LM(8)-1
    CALL STIFF(5,8,R,NN,NB)
500 CONTINUE
C
C   2. FORM BEAM MATRICES
C
    IF (NB.EQ.0) GO TO 610
    NF=3
    ND=6
    DO 600 M=1,NB
    MB=LB(N,M,3)
    IF (MB.EQ.NBP) GO TO 600
    KI=LB(N,M,1)
    KJ=LB(N,M,2)
    B1=CLN(KJ,1)-CLN(KI,1)
    B2=CLN(KJ,2)-CLN(KI,2)
    B3=B1*B1+B2*B2
    B3=DSQRT (B3)
    CSA=B1/B3
    SNA=B2/B3
    XL=B3
    XLR=XL-BP(8,MB)-BP(9,MB)
    DO 550 L=1,NLD
    DO 520 I=1,6
520 P(I,L)=0.
    J=LDB(N,M,L)
    IF (J) 550,550,530
530 V=FEF(5,J)*XLR/2.
    YM=V*XLR/6.
    P(1,L)=-FEF(1,J)-YM
    P(2,L)=-FEF(2,J)-Y
    P(3,L)= FEF(3,J)-YM
    P(4,L)=-FEF(4,J)-Y
    IF (IFEF(J)) 550,540,550
540 P(1,L)=P(1,L)+P(2,L)*BP(8,MB)
    P(3,L)=P(3,L)-P(4,L)*BP(9,MB)
550 CONTINUE
C
    CALL BEAM (1,MB,XL,SNA,CSA,NBP,BP)
C
    LM(3)=3*KI
    LM(2)=LM(3)-1
    LM(1)=LM(2)-1
    LM( 6)=3*KJ
    LM( 5)=LM( 6)-1
    LM(4)=LM( 5)-1
    CALL STIFF(5,8,R,NN,NB)
600 CONTINUE
C
C   FORM PANEL STIFFNESS
C
    IF(NPAN.EQ.0) GO TO 610
    DO 720 I=1,10
    DO 720 J=1,3
720 P(I,J)=0.
    NF=3
    ND=10
    DO 800 L=1,NPAN
    NP=NB-LP(1,L)+1
    IF (NP.NE.N) GO TO 800
    XL=BD(N+K,2)
    KI=LP(2,L)
    KJ=LP(3,L)
    B1=CLN(KJ,1)-CLN(KI,1)
    B2=CLN(KJ,2)-CLN(KI,2)
    B3=B1*B1+B2*B2
    B3=DSQRT (B3)
    CSA=B1/B3

```

1	1	13.5111006	26.0379338	-527.3551338	8.4438699
2	1	14.8917007	17.5389384	-412.7115588	6.8018114
3	1	15.6964172	18.2995085	-661.3502853	6.4064226
4	1	-14.3363398	-27.7598683	-928.3789084	-7.9030020

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-40.8846004	-39.8353285
2	1	7.4095277	7.5439092
3	1	-41.6703138	-42.5658300

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-7.2232021	246.4979549	-939.6041138	56.8450819

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 9 LEVEL ID F09

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	22.3478481	27.1734999	-499.0201249	10.7373303
2	1	15.6041006	17.5341001	-420.9845453	6.8984729
3	1	16.5889165	18.4299874	-594.4450485	6.7975360
4	1	-23.6958551	-28.2294902	-779.4493904	-10.4150258

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-41.3871184	-40.7151843
2	1	7.5985370	7.7703721
3	1	-42.7266276	-43.4477179

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	12.7699979	189.7789243	-888.5008928	47.7116217

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 10 LEVEL ID F10

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	19.0772603	19.0392703	-470.8829128	7.9373387
2	1	16.4031911	17.5125467	-425.5962192	7.0402297
3	1	17.0577522	18.3873389	-531.2248421	7.0604962
4	1	-19.7310315	-19.7518828	-730.2775972	-7.4020800

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-41.8637747	-41.4302378
2	1	7.6889573	7.7598111
3	1	-42.4782915	-42.9234572

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	60.3239118	158.1162151	-837.2184267	49.2798605

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 11 LEVEL ID F11

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	21.2430587	22.7865144	-442.8948843	9.4909443
2	1	16.9401237	17.3400894	-427.3504258	7.1068270
3	1	17.1343101	17.6609282	-470.7311513	7.0870499
4	1	-21.4731951	-23.1924257	-681.2023786	-8.8340027

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-42.4022204	-41.8997071

2	1	7.7830302	7.7840625		
3	1	-42.0401884	-42.5455456		
PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	66.6884146	110.9586750	-785.8213799	41.7211597

MEMBER FORCES	FRAME ID	25-8,3-B BUILD.	FRAME TYPE	1
	LEVEL NO	12	LEVEL ID	F12

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	21.5213429	21.1591617	-415.0324053	9.2452543
2	1	17.2940593	17.1765532	-423.5077368	7.1636841
3	1	17.0987412	17.1118158	-415.7127607	7.1249316
4	1	-21.3027403	-21.0723505	-632.2291619	-8.4232300

BEAM FORCES					
BAY	LOAD	I MOMENT	J MOMENT		
1	1	-42.3678110	-41.8784677		
2	1	7.7587757	7.7037251		
3	1	-41.1815631	-41.8607373		

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	83.3453140	75.3903319	-734.3179353	37.1628819

MEMBER FORCES	FRAME ID	25-8,3-B BUILD.	FRAME TYPE	1
	LEVEL NO	13	LEVEL ID	F13

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	22.2434187	20.8464681	-387.1629401	9.4511736
2	1	17.3861703	16.8256326	-415.1972803	7.1359778
3	1	16.8277189	16.3810968	-385.0497520	7.0563730
4	1	-21.6100281	-20.3579970	-583.4738744	-8.5007441

BEAM FORCES					
BAY	LOAD	I MOMENT	J MOMENT		
1	1	-41.9643437	-41.4933603		
2	1	7.6610944	7.5526128		
3	1	-40.0305586	-40.4781172		

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	93.9603195	42.7823425	-682.7181532	31.8557122

MEMBER FORCES	FRAME ID	25-8,3-B BUILD.	FRAME TYPE	1
	LEVEL NO	14	LEVEL ID	F14

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	21.0442083	19.7209250	-359.1951531	8.9811708
2	1	17.4094937	16.4480956	-402.7817428	7.1070109
3	1	16.4955999	15.6502268	-318.4087543	6.9837517
4	1	-20.1066298	-18.8690890	-535.0101649	-7.9415042

BEAM FORCES					
BAY	LOAD	I MOMENT	J MOMENT		
1	1	-41.4339367	-40.8908504		
2	1	7.5642897	7.3975797		
3	1	-38.7298407	-39.2331839		

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	103.0689302	16.9808073	-631.0241949	27.8865410

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 15 LEVEL ID F15

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	26.0012562	20.3897284	-331.0857515	10.5033748
2	1	17.0392351	15.9170689	-385.1834581	6.9858896
3	1	15.9210861	14.8366610	-276.8182548	6.7744470
4	1	-24.4740578	-19.1265541	-486.8647888	-9.2908694

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-39.9781273	-39.7553450
2	1	7.3261299	7.1391924
3	1	-36.9517137	-37.1507376

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	98.5794239	-11.0192262	-579.2497488	20.2253985

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 16 LEVEL ID F16

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	18.5384485	13.9788711	-302.8524355	7.1505993
2	1	16.7418441	15.3899799	-365.3225413	6.8521137
3	1	14.9184040	13.8914353	-237.4217702	6.4350672
4	1	-16.6493822	-12.6766798	-439.2019804	-5.9119307

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-37.9184922	-38.5240494
2	1	6.9480906	6.8022906
3	1	-33.9349627	-33.3744309

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	113.2584627	-17.2787496	-527.4012726	22.2902665

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 17 LEVEL ID F17

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	19.9154586	19.3800439	-273.8077532	8.9630218
2	1	16.5442027	14.8343146	-343.3758260	6.7650529
3	1	13.8789962	12.4142682	-199.8796090	5.9448930
4	1	-17.0590565	-16.7250488	-392.3893082	-7.2123543

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-37.6845611	-38.0401052
2	1	6.8594030	6.3908608
3	1	-31.7603312	-31.4252620

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	105.4869327	-40.9703152	-475.3485056	14.6348548

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 18 LEVEL ID F18

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	19.5996064	17.7491025	-244.8708385	8.5901387
2	1	16.2778892	14.6374995	-318.4180883	6.7634898
3	1	12.9240482	11.4904742	-187.1247418	5.5937743

4	1	-15.8831929	-14.3662058	-346.0901070	-6.5085141
---	---	-------------	-------------	--------------	------------

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-36.7161674	-37.1968553
2	1	6.5857258	6.0150589
3	1	-29.4548725	-29.0492287

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	100.8612676	-51.7139480	-423.0982263	10.9460618

MEMBER FORCES	FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 19	LEVEL ID F19

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	17.4250085	17.1185610	-215.7099643	7.9978025
2	1	16.1082888	14.3334403	-286.4768970	6.7636720
3	1	12.0641988	10.5157874	-137.1566717	5.2395878
4	1	-13.5630245	-13.1660356	-300.3770944	-5.7944190

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-36.4303540	-36.8125630
2	1	6.4948623	5.8111638
3	1	-27.5265048	-27.3481026

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	93.3642568	-59.0437014	-370.6793726	7.4844953

MEMBER FORCES	FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 20	LEVEL ID F20

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	24.8327201	19.0053475	-186.4403290	10.4259324
2	1	15.4364137	14.0096119	-251.2709105	6.6423795
3	1	11.0186133	9.8511422	-112.2714375	4.8461227
4	1	-18.1579273	-13.7860781	-255.1177685	-7.2556149

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-33.4923500	-34.7905066
2	1	6.1554180	5.4401992
3	1	-24.6704134	-23.9125906

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	70.7390494	-71.1377887	-318.0995545	-1.0100725

MEMBER FORCES	FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 21	LEVEL ID F21

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	11.9354649	9.6596300	-156.6758880	4.7133454
2	1	14.1211369	13.1886767	-215.5275009	6.2305868
3	1	9.0451825	8.4118009	-87.6348569	4.1199334
4	1	-7.7510632	-5.7546633	-210.6198930	-2.7907127

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-28.2449060	-31.4811872
2	1	5.1716399	4.3164499
3	1	-19.7732344	-18.4005502

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		77.0165306	-53.3222279	-265.4420631	5.1854002

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 22	LEVEL ID F22

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	14.0408520	14.3094511	-125.3914477	6.7489078
2	1	13.8680065	12.1864105	-180.7257757	6.0259845
3	1	7.7005066	6.4116021	-62.3197616	3.3597086
4	1	-8.2178997	-8.6494869	-167.6981600	-3.7639130

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-27.5082188	-32.0558015
2	1	5.3828558	4.3378668
3	1	-17.9364420	-15.3785111

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		57.6228496	-83.2394451	-212.6548451	-1.9785324

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 23	LEVEL ID F23

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	13.8218977	13.4673668	-84.4369502	8.5738452
2	1	14.0158911	12.8049392	-140.4845517	6.3355318
3	1	6.7811025	5.8980686	-41.9310478	3.0594689
4	1	-7.2140707	-7.1605114	-125.1338008	-3.2644338

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-27.0875268	-31.8029668
2	1	5.2866932	4.0834141
3	1	-16.1099822	-13.6693058

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		38.2733907	-62.3267446	-159.6136495	-6.4332943

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 24	LEVEL ID F24

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	12.8282993	13.2456291	-63.3957819	6.3551861
2	1	12.8929638	12.5005825	-98.5490292	6.0998634
3	1	5.9568799	5.2454657	-25.0471585	2.7380816
4	1	-6.1676007	-6.4552351	-83.0113898	-2.9418605

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-28.4774147	-32.6148878
2	1	4.7847106	3.7330140
3	1	-15.2387299	-13.3036059

PANEL FORCES						
I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		16.1368211	-56.8514982	-106.3966625	-10.4527613

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 25	LEVEL ID F25

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	19.2058358	15.6491154	-32.6322722	8.6308694
2	1	18.6661078	14.9369935	-45.9817114	8.2840085
3	1	8.5190103	5.5488360	-14.5644913	2.9799756
4	1	-8.7279943	-7.1360052	-41.0435978	-3.8617712

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-19.2058358	-26.9359864
2	1	8.2898788	5.9017778
3	1	-12.4207881	-8.7279943

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-26.0886590	-58.1597097	-52.9779273	-21.1966276

CONVERGE IN ITERATION NO. 3

TOTAL TIME 284.29 SEC

ตัวอย่าง 4 : โครงข้อแข็งประกอบผนังต้านแรงเฉือน 25 ชั้น 3 ช่วงเสา

$$\text{กรณี } \alpha = 1.5$$

25	1	1	1	0	0	1	00001	5	0.001	7810802	IMP
F25											
	2.56										
F24											
	5.12										
F23											
	5.12										
F22											
	5.12										
F21											
	5.12										
F20											
	5.12										
F19											
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F10											
	4.48										
F09											
	3.84										
F08											
	3.84										
F07											
	3.84										
F06											
	3.84										
F05											
	3.20										
F04											
	2.56										
F03											
	2.56										
F02											
	1.60										
F01											
	1.60										
1	25	4	3	6	1	2	25			25-STORY, 3-BAY BUILDING	
1		0.0		0.0							
2		8.0		0.0							
3		11.5		0.0							
4		10.5		0.0							
1		3042000.0		0.16						0.0021333	
2		3042000.0		0.36						0.0108000	
3		3042000.0		0.5625						0.0263672	
4		3042000.0		0.81						0.0546750	
5		3042000.0		0.80						0.0125000	
1		3042000.0					0.0052083	4.0	4.0	2.0	
1	1			38.4					55.2		
2	1			55.2					38.4		
1	1	2	1	24	1						
2	2	3	1	24							
3	3	4	1	24	2						
1	1	2	4								
1	2	2	4								
1	3	2	5								
1	4	2	6								

PROGRAM CU-NTAB8
 INPUT FILE : ts10s02.inp
 OUTPUT FILE : ts10s02g.out

TB10S02.INP

TOTAL NUMBER OF STORIES--- 25
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY

EQ.1-MODE SHAPES AND FREQUENCIES ONLY

EQ.2-STATIC AND MODE SHAPE ANALYSES

EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL

EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)

EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE

EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)

EQ.7-TYPE 3 AND 8 ANALYSES

EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)

EQ.9-TYPE 4 AND 8 ANALYSES

EQ.10-SLAM RESTART

EQ.11-SLAM-2 RESTART

EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0

STORY TRANSLATION CODE--- 1

LAT FORCE GENERATION CODE 0 0

BTRESS CHECK KEY----- 0

DATA CHECK KEY----- 0

TYPE OF SOLUTION----- 1

MAXIMUM NO. OF CYCLES---- 5

CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
25	F25	4.00	19.08	.00	.00	.00	.00	.00
24	F24	4.00	19.08	.00	.00	.00	.00	.00
23	F23	4.00	19.08	.00	.00	.00	.00	.00
22	F22	4.00	19.08	.00	.00	.00	.00	.00
21	F21	4.00	19.08	.00	.00	.00	.00	.00
20	F20	4.00	19.08	.00	.00	.00	.00	.00
19	F19	4.00	19.08	.00	.00	.00	.00	.00
18	F18	4.00	19.08	.00	.00	.00	.00	.00
17	F17	4.00	19.08	.00	.00	.00	.00	.00
16	F16	4.00	19.08	.00	.00	.00	.00	.00
15	F15	4.00	19.08	.00	.00	.00	.00	.00
14	F14	4.00	19.08	.00	.00	.00	.00	.00
13	F13	4.00	19.08	.00	.00	.00	.00	.00
12	F12	4.00	19.08	.00	.00	.00	.00	.00
11	F11	4.00	19.08	.00	.00	.00	.00	.00
10	F10	4.00	19.08	.00	.00	.00	.00	.00
9	F09	4.00	19.08	.00	.00	.00	.00	.00
8	F08	4.00	19.08	.00	.00	.00	.00	.00
7	F07	4.00	19.08	.00	.00	.00	.00	.00
6	F06	4.00	19.08	.00	.00	.00	.00	.00
5	F05	4.00	19.08	.00	.00	.00	.00	.00
4	F04	4.00	19.08	.00	.00	.00	.00	.00
3	F03	4.00	19.08	.00	.00	.00	.00	.00
2	F02	4.00	19.08	.00	.00	.00	.00	.00
1	F01	4.00	19.08	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
25	F25	100.00	19.08	.00

24	F24	98.00	38.17	.00
23	F23	92.00	57.25	.00
22	F22	88.00	76.33	.00
21	F21	84.00	95.41	.00
20	F20	80.00	114.50	.00
19	F19	76.00	133.58	.00
18	F18	72.00	152.66	.00
17	F17	68.00	171.74	.00
16	F16	64.00	190.83	.00
15	F15	60.00	209.91	.00
14	F14	56.00	228.99	.00
13	F13	52.00	248.07	.00
12	F12	48.00	267.16	.00
11	F11	44.00	286.24	.00
10	F10	40.00	305.32	.00
9	F09	36.00	324.40	.00
8	F08	32.00	343.49	.00
7	F07	28.00	362.57	.00
6	F06	24.00	381.65	.00
5	F05	20.00	400.73	.00
4	F04	16.00	419.82	.00
3	F03	12.00	438.90	.00
2	F02	8.00	457.98	.00
1	F01	4.00	477.06	.00

STRUCTURE LATERAL LOADS . . . CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
25	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
24	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
23	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
22	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
21	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
20	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
19	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
18	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
17	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
16	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
15	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
14	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
13	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
12	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
11	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
10	4.48	.00	.00	.00	.00	.00	.0	.0	.0	.0
9	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
8	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
7	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
6	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
5	3.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
4	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL ID	DIRN	1	2
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25	F25	X	2.5800	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	7.8800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	12.8000	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	17.9200	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	23.0400	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	28.1600	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	33.2800	.0000
19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	38.4000	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	43.5200	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	48.6400	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	53.7600	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	58.8800	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	64.0000	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	69.1200	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	74.2400	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	79.3600	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	84.4800	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	89.6000	.0000
8	F08	Y	.0000	.0000

8	F08	ROTN	.0000	.0000
7	F07	X	90.2400	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	94.0800	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	97.2800	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	99.8400	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	102.4000	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	104.0000	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000
1	F01	X	105.6000	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
25	F25	X	10.2400	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	40.9800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	92.1800	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	183.8400	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	256.0000	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	388.6400	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	501.7600	.0000

19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	655.3600	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	829.4400	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	1024.0000	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	1239.0400	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	1474.5600	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	1730.5600	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	2007.0400	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	2304.0000	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	2618.8800	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	2949.1200	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	3294.7200	.0000
8	F08	Y	.0000	.0000
8	F08	ROTN	.0000	.0000
7	F07	X	3655.8800	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	4032.0000	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	4421.1200	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	4820.4800	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	5230.0800	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	5646.0800	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000

1	F01	X	6068.4800	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

25-STORY,3-BAY BUILDING

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 25
 NUMBER OF COLUMN LINES---- 4
 NUMBER OF BAYS----- 3
 NUMBER OF DIFF. COL. PROP- 5
 NUMBER OF DIFF. BEAM PROP- 1
 NUMBER OF DIFF. FEF----- 2
 NUMBER OF PANEL ELEMENTS-- 25
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	8.00	.00
3	11.50	.00
4	19.50	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	3042000.00	.18	.00	.00	.00	.00	.00	.00	.00
2	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
3	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.60	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	38.400	.000	55.200	.000
2	1	.000	55.200	.000	38.400	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	25	1	2	1	24	1	0	0
2	25	2	3	1	24	0	0	0
3	25	3	4	1	24	2	0	0

GENERATED BEAM LOCATIONS

STORY	1	2	3
25	1	1	1
24	1	1	1
23	1	1	1
22	1	1	1
21	1	1	1
20	1	1	1
19	1	1	1
18	1	1	1
17	1	1	1
16	1	1	1
15	1	1	1
14	1	1	1
13	1	1	1
12	1	1	1
11	1	1	1
10	1	1	1
9	1	1	1
8	1	1	1

7	1	1	1
6	1	1	1
5	1	1	1
4	1	1	1
3	1	1	1
2	1	1	1
1	1	1	1

GENERATED BEAM LOADS ...LOAD CASE I

STORY	1	2	3
25	1	0	2
24	1	0	2
23	1	0	2
22	1	0	2
21	1	0	2
20	1	0	2
19	1	0	2
18	1	0	2
17	1	0	2
16	1	0	2
15	1	0	2
14	1	0	2
13	1	0	2
12	1	0	2
11	1	0	2
10	1	0	2
9	1	0	2
8	1	0	2
7	1	0	2
6	1	0	2
5	1	0	2
4	1	0	2
3	1	0	2
2	1	0	2
1	1	0	2

GENERATED BEAM LOADS ...LOAD CASE II

STORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

STORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

COLUMN LOCATIONS

D LINE	LEV	CID	KCOL	GEN
1	25	1	2	4
1	20	2	2	4
1	15	3	2	5
1	9	4	2	8
2	25	5	3	24
3	25	5	4	24
4	25	1	3	4
4	20	2	3	4
4	15	3	3	5
4	9	4	3	8

GENERATED COLUMN LOCATIONS

STORY	1	2	3	4
25	1	5	5	1
24	1	5	5	1
23	1	5	5	1
22	1	5	5	1
21	1	5	5	1
20	2	5	5	2
19	2	5	5	2
18	2	5	5	2
17	2	5	5	2
16	2	5	5	2
15	3	5	5	3
14	3	5	5	3
13	3	5	5	3
12	3	5	5	3
11	3	5	5	3
10	3	5	5	3
9	4	5	5	4
8	4	5	5	4

```

7  4  5  5  4
8  4  5  5  4
5  4  5  5  4
4  4  5  5  4
3  4  5  5  4
2  4  5  5  4
1  4  5  5  4

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PANEL CARDS

LEVEL	COL I	COL J	E	A	I	BA	G
25	2	3	3042000.00	1.05	1.07	.00	.00
24	2	3	3042000.00	1.05	1.07	.00	.00
23	2	3	3042000.00	1.05	1.07	.00	.00
22	2	3	3042000.00	1.05	1.07	.00	.00
21	2	3	3042000.00	1.05	1.07	.00	.00
20	2	3	3042000.00	1.05	1.07	.00	.00
19	2	3	3042000.00	1.05	1.07	.00	.00
18	2	3	3042000.00	1.05	1.07	.00	.00
17	2	3	3042000.00	1.05	1.07	.00	.00
16	2	3	3042000.00	1.05	1.07	.00	.00
15	2	3	3042000.00	1.05	1.07	.00	.00
14	2	3	3042000.00	1.05	1.07	.00	.00
13	2	3	3042000.00	1.05	1.07	.00	.00
12	2	3	3042000.00	1.05	1.07	.00	.00
11	2	3	3042000.00	1.05	1.07	.00	.00
10	2	3	3042000.00	1.05	1.07	.00	.00
9	2	3	3042000.00	1.05	1.07	.00	.00
8	2	3	3042000.00	1.05	1.07	.00	.00
7	2	3	3042000.00	1.05	1.07	.00	.00
6	2	3	3042000.00	1.05	1.07	.00	.00
5	2	3	3042000.00	1.05	1.07	.00	.00
4	2	3	3042000.00	1.05	1.07	.00	.00
3	2	3	3042000.00	1.05	1.07	.00	.00
2	2	3	3042000.00	1.05	1.07	.00	.00
1	2	3	3042000.00	1.05	1.07	.00	.00

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1

LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
25	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
24	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
23	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
22	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
21	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
20	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
19	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
18	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
17	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
16	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
15	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
14	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
13	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
12	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
11	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
10	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
9	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
8	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
7	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
6	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
5	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
4	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
3	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
2	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0

BAY NUMBERS 2

LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
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25	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
24	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
23	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
22	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
21	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
20	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
19	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
18	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
17	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
16	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
15	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
14	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
13	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
12	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
11	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
10	3042000.00	.66	.00	.00	.00	.03	.00	.00	.00
9	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
8	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
7	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
6	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
3	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
2	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
1	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00

0...FRAME TYPE 1
 TIME REQUIRED TO FORM STIFFNESS = 74.64

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	25-B,3-B BUILD

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	1.50	.00	.00	1.50	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
25	X	.4385313
25	Y	.0000000
25	ROTN	.0000000
24	X	.4203223
24	Y	.0000000
24	ROTN	.0000000
23	X	.4038798
23	Y	.0000000
23	ROTN	.0000000
22	X	.3870875
22	Y	.0000000
22	ROTN	.0000000
21	X	.3698502
21	Y	.0000000
21	ROTN	.0000000
20	X	.3521023

2 1 -291.5218277 803.8918894 -1717.9147123 122.4993441

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 5 LEVEL ID F05

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	5.1903126	49.3160572	-906.7555591	10.1229553
2	1	15.8488918	25.2192397	-498.0565442	8.3425786
3	1	16.7197134	25.7465215	-1377.1469899	5.2953635
4	1	-8.1294859	-49.9929514	-1474.0378145	-6.3350351

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-52.7653065	-51.7025368
2	1	9.2855520	9.4303548
3	1	-53.4642990	-54.5757183

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-208.0733883	688.7293263	-1640.8030923	113.8240414

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 6 LEVEL ID F06

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	12.2436768	47.5749939	-862.2140395	11.1990917
2	1	19.0688743	26.5880930	-542.2848485	9.0521435
3	1	20.0687671	27.3142310	-1244.8370304	6.4235692
4	1	-13.3187291	-48.4482304	-1402.9328125	-9.3304362

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-58.0565481	-56.8876539
2	1	10.3648890	10.5324805
3	1	-58.9825100	-60.2077114

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-134.5132924	582.2170010	-1583.7314690	105.1147271

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 7 LEVEL ID F07

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	18.8961496	45.8128713	-618.9820648	12.2908193
2	1	21.8158813	27.4342907	-577.2720006	9.5248365
3	1	22.7228273	28.3812824	-1121.9127462	7.4559489
4	1	-20.1662509	-46.8889824	-1330.4340349	-10.4518854

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-61.9714123	-60.7487833
2	1	11.1847074	11.3558657
3	1	-63.1874218	-64.4525132

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-72.3998913	483.1477103	-1486.8991535	95.8364910

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 8 LEVEL ID F08

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
------	------	------------	------------	-------------	-------------

1	1	21.3881738	43.0852628	-776.7220892	12.2010852
2	1	23.7073999	27.9894146	-603.9989913	9.8770577
3	1	24.9192596	29.0889297	-1007.0924048	8.4298182
4	1	-22.6145884	-44.2962623	-1256.8815430	-10.3977311

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-84.8889747	-83.5103052
2	1	11.8153827	12.0205851
3	1	-86.2698229	-87.8972253

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-14.0381890	397.2147990	-1409.7049716	88.6942625

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
LEVEL NO 9 LEVEL ID F09

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	35.5789723	43.5008008	-735.1692492	15.9140392
2	1	24.8750070	27.9875236	-620.4153095	9.8616039
3	1	26.3524673	29.3207992	-902.7273912	9.1835935
4	1	-37.6049687	-45.0728389	-1182.5381870	-14.4670930

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-66.0420417	-64.9688786
2	1	12.1268874	12.3872845
3	1	-67.9830871	-69.1311828

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	18.5893481	306.6258706	-1332.7498631	74.3138380

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
LEVEL NO 10 LEVEL ID F10

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	30.3990744	30.4630684	-893.9455892	11.4762220
2	1	26.1532217	27.8889843	-631.0769705	10.1295291
3	1	27.1340693	29.2433354	-804.1526322	9.7811885
4	1	-31.3905011	-31.5261941	-1107.7989057	-9.7573184

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-66.7964684	-66.1031054
2	1	12.2702090	12.3904437
3	1	-67.8732703	-68.3838275

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	78.1500223	255.7406980	-1255.8259023	76.9556832

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
LEVEL NO 11 LEVEL ID F11

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	33.8548518	36.3973940	-852.9580380	13.9975900
2	1	27.0039800	27.8795748	-637.2142276	10.1914349
3	1	27.2938189	28.1587574	-709.9058787	9.8987833
4	1	-34.2017481	-37.0033264	-1033.1917885	-12.1586129

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-67.6411604	-66.8378730

2	1	12.4259411	12.4428499
3	1	-67.0478209	-67.8551180

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	105.9386334	180.0089243	-1178.7300912	85.0245348

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 12 LEVEL ID F12

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	34.2991888	33.7865086	-812.1679152	13.8886127
2	1	27.5626276	27.4079519	-634.4190542	10.2679649
3	1	27.2864743	27.3111541	-624.4093103	10.2245500
4	1	-33.9688721	-33.8533699	-959.7289014	-11.6548525

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-87.5883092	-86.7812200
2	1	12.3846171	12.3044433
3	1	-85.7388598	-86.5049732

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	132.9005760	122.8889013	-1101.4748188	57.8641501

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 13 LEVEL ID F13

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	35.4497224	33.2671204	-571.3613563	14.0877996
2	1	27.7009435	26.8339753	-624.4526111	10.2332044
3	1	26.8648837	26.1879423	-545.9155070	10.2853086
4	1	-34.4978845	-32.5361011	-884.5984223	-11.9412685

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-86.8975568	-86.1454382
2	1	12.2313681	12.0673577
3	1	-83.9518237	-84.8692924

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	150.1879429	70.0282224	-1024.0721033	49.4723442

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 14 LEVEL ID F14

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	33.5308281	31.4478344	-530.3917307	13.3930997
2	1	27.7285579	26.2131266	-607.8276535	10.2170340
3	1	26.3588870	25.0198023	-473.9258728	10.2868875
4	1	-32.1200982	-30.1718079	-810.9207828	-11.2131420

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-86.0233152	-85.1585903
2	1	12.0753119	11.8233610
3	1	-81.9164126	-82.7224981

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	164.8970402	28.2583417	-946.5341804	43.1989575

4	1	-25.6175510	-23.0897575	-523.9631209	-9.8011234
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BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-58.2193648	-58.9839231
2	1	10.4900546	9.8313424
3	1	-47.3723823	-46.7185170

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	180.9051895	-82.8064483	-634.6453400	16.4101698

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 19 LEVEL ID F19

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	27.6149441	27.1246598	-319.5329901	12.1778795
2	1	25.4995202	22.8897303	-437.0437748	9.8861062
3	1	19.4409145	18.9800827	-198.4043599	8.1645204
4	1	-21.8194285	-21.2009860	-454.6017573	-8.6110845

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-57.6962951	-57.9881226
2	1	10.3388339	9.3109382
3	1	-44.3590280	-44.0738825

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	148.9831120	-94.5725889	-556.0171179	10.9803217

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 20 LEVEL ID F20

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	39.2848816	30.0814511	-276.3932923	16.0794650
2	1	24.4121717	22.1477884	-383.6452557	9.8881200
3	1	17.7905603	15.8071732	-161.8862318	7.6112061
4	1	-29.2733850	-22.2542541	-385.9476687	-11.1195311

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-52.9801021	-55.0380970
2	1	9.7953006	8.7200503
3	1	-40.1570480	-38.8097473

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	112.7205332	-113.8388403	-477.1475515	-2.4584075

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 21 LEVEL ID F21

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	19.7983553	13.8952405	-232.2953172	7.0926878
2	1	22.2735819	20.6286247	-329.3873965	9.3140501
3	1	14.8644832	13.6484374	-125.6541308	6.5201991
4	1	-12.5240823	-9.3363623	-318.5018193	-4.0519043

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-41.3558254	-40.6487364
2	1	8.2096182	6.9251835
3	1	-32.8893335	-26.5903177

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	122.6673679	-85.2764791	-398.1613383	7.5810687

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 22	LEVEL ID F22

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	22.1139936	22.5572701	-186.0708624	10.3659662
2	1	21.8192871	19.1655382	-276.8653674	9.0539501
3	1	12.5741871	10.4988668	-87.9011125	5.3894143
4	1	-13.3843480	-14.0662554	-253.5669879	-5.7690348

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-43.2933558	-50.4865861
2	1	8.5429789	6.9737744
3	1	-29.2898942	-25.1037673

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	81.6865316	-100.9951780	-318.9956699	-3.6993342

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 23	LEVEL ID F23

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	21.7251262	21.1793823	-140.1907277	10.1375807
2	1	22.0094533	20.1034001	-215.3034400	9.8243378
3	1	11.1617399	9.7419228	-58.3166885	4.9810852
4	1	-11.8171317	-11.7184193	-189.1677815	-5.0899833

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-42.5317308	-49.9898091
2	1	8.3798575	6.5734946
3	1	-26.4536589	-22.4398391

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	60.8639438	-99.3756339	-239.4193624	-10.6330405

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 24	LEVEL ID F24

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	20.1443582	20.8086046	-94.1559201	9.8508963
2	1	20.2373056	19.6006983	-148.1108897	9.3506653
3	1	9.8361442	8.7184244	-34.2827026	4.4977171
4	1	-10.1562882	-10.6227074	-125.4560942	-4.6790396

BEAM FORCES			
BAY	LOAD	I MOMENT	J MOMENT
1	1	-44.7143632	-51.2147623
2	1	7.5861553	6.0081500
3	1	-26.1519739	-21.9657202

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	25.6917847	-90.5002397	-159.5943933	-16.8581545

MEMBER FORCES		FRAME ID 25-8,3-B BUILD.	FRAME TYPE 1
		LEVEL NO 25	LEVEL ID F25

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	30.1366023	24.5700050	-48.5470608	13.4799238
2	1	29.2030853	23.3913012	-70.4169754	12.8632448
3	1	10.9855751	9.3078797	-20.4018548	4.9906389
4	1	-14.4244482	-11.7994320	-61.9676325	-6.3048576

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-30.1366023	-42.2869110
2	1	13.0838257	9.5310363
3	1	-20.5166115	-14.4244482

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-41.4255886	-92.4810417	-79.4664765	-33.7986833

CONVERGE IN ITERATION NO. 3

TOTAL TIME 279.79 SEC.

ตัวอย่าง 4 : โครงข้อแข็งประกอบผนังต้านแรงเฉือน 25 ชั้น 3 ช่วงเสา

$$\text{กรณี } \alpha = 2.0$$

25	1	1	1	0	0	1	00001	5	0.001	T810LD3.INP
F25				4.0						
	2.56									
F24				4.0						
	5.12									
F23				4.0						
	5.12									
F22				4.0						
	5.12									
F21				4.0						
	5.12									
F20				4.0						
	5.12									
F19				4.0						
	5.12									
F18				4.0						
	5.12									
F17				4.0						
	5.12									
F16				4.0						
	5.12									
F15				4.0						
	5.12									
F14				4.0						
	5.12									
F13				4.0						
	5.12									
F12				4.0						
	5.12									
F11				4.0						
	5.12									
F10				4.0						
	4.48									
F09				4.0						
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F08				4.0						
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F06				4.0						
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F05				4.0						
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F04				4.0						
	2.56									
F03				4.0						
	2.56									
F02				4.0						
	1.60									
F01				4.0						
	1.60									

1	25	4	3	5	1	2	25	25-STORY, 3-BAY BUILDING
1		0.0		0.0				
2		8.0		0.0				
3		11.5		0.0				
4		19.5		0.0				
1		3042000.0		0.18			0.0021333	
2		3042000.0		0.36			0.0108000	
3		3042000.0		0.5625			0.0263672	
4		3042000.0		0.81			0.0546750	
5		3042000.0		0.60			0.0125000	
1		3042000.0			0.0052083	4.0	4.0	2.0
1	1			38.4			55.2	
2	1			55.2			38.4	
1	1	2	1	24	1			
2	2	3	1	24				
3	3	4	1	24	2			
1	1	2	4					
1	2	2	4					
1	3	2	5					
1	4	2	8					

PROGRAM CU-NTAB8
 INPUT FILE : t*10*03.inp
 OUTPUT FILE : t*10*03g.out

TS10L03.INP
 TOTAL NUMBER OF STORIES-- 25
 NUMBER OF DIFF. FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL.
 EQ.4-TYPE 2 AND TIME HISTORY ANAL. (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL. (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.9-TIME HISTORY ANAL. (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.8-TYPE 4 AND 8 ANALYSES
 EQ.10-SLAM RESTART
 EQ.11-SLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF SOLUTION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
25	F25	4.00	19.08	.00	.00	.00	.00	.00
24	F24	4.00	19.08	.00	.00	.00	.00	.00
23	F23	4.00	19.08	.00	.00	.00	.00	.00
22	F22	4.00	19.08	.00	.00	.00	.00	.00
21	F21	4.00	19.08	.00	.00	.00	.00	.00
20	F20	4.00	19.08	.00	.00	.00	.00	.00
19	F19	4.00	19.08	.00	.00	.00	.00	.00
18	F18	4.00	19.08	.00	.00	.00	.00	.00
17	F17	4.00	19.08	.00	.00	.00	.00	.00
16	F16	4.00	19.08	.00	.00	.00	.00	.00
15	F15	4.00	19.08	.00	.00	.00	.00	.00
14	F14	4.00	19.08	.00	.00	.00	.00	.00
13	F13	4.00	19.08	.00	.00	.00	.00	.00
12	F12	4.00	19.08	.00	.00	.00	.00	.00
11	F11	4.00	19.08	.00	.00	.00	.00	.00
10	F10	4.00	19.08	.00	.00	.00	.00	.00
9	F09	4.00	19.08	.00	.00	.00	.00	.00
8	F08	4.00	19.08	.00	.00	.00	.00	.00
7	F07	4.00	19.08	.00	.00	.00	.00	.00
6	F06	4.00	19.08	.00	.00	.00	.00	.00
5	F05	4.00	19.08	.00	.00	.00	.00	.00
4	F04	4.00	19.08	.00	.00	.00	.00	.00
3	F03	4.00	19.08	.00	.00	.00	.00	.00
2	F02	4.00	19.08	.00	.00	.00	.00	.00
1	F01	4.00	19.08	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
25	F25	100.00	19.08	.00

24	F24	96.00	39.17	.00
23	F23	92.00	57.25	.00
22	F22	88.00	76.33	.00
21	F21	84.00	95.41	.00
20	F20	80.00	114.50	.00
19	F19	76.00	133.58	.00
18	F18	72.00	152.66	.00
17	F17	68.00	171.74	.00
16	F16	64.00	190.83	.00
15	F15	60.00	209.91	.00
14	F14	56.00	228.99	.00
13	F13	52.00	248.07	.00
12	F12	48.00	267.16	.00
11	F11	44.00	286.24	.00
10	F10	40.00	305.32	.00
9	F09	36.00	324.40	.00
8	F08	32.00	343.49	.00
7	F07	28.00	362.57	.00
6	F06	24.00	381.65	.00
5	F05	20.00	400.73	.00
4	F04	16.00	419.82	.00
3	F03	12.00	438.90	.00
2	F02	8.00	457.98	.00
1	F01	4.00	477.06	.00

BSTRUCTURE LATERAL LOADS CASES A AND B

LEVEL NO	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
25	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
24	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
23	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
22	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
21	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
20	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
19	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
18	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
17	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
16	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
15	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
14	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
13	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
12	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
11	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
10	4.48	.00	.00	.00	.00	.00	.0	.0	.0	.0
9	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
8	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
7	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
6	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
5	3.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
4	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	1.80	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	1.80	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL ID DIRN 1 2

25	F25	X	2.5600	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	7.6800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	12.8000	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	17.9200	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	23.0400	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	28.1600	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	33.2800	.0000
19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	38.4000	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	43.5200	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	48.6400	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	53.7600	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	58.8800	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	64.0000	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	69.1200	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	74.2400	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	79.3600	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	84.4800	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	89.6000	.0000
8	F08	Y	.0000	.0000

8	F08	ROTN	.0000	.0000
7	F07	X	90.2400	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	94.0800	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	97.2800	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	99.8400	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	102.4000	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	104.0000	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000
1	F01	X	105.6000	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
25	F25	X	10.2400	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	40.9600	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	92.1600	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	163.8400	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	256.0000	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	368.6400	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	501.7600	.0000

19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	655.3600	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	929.4400	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	1024.0000	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	1239.0400	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	1474.5600	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	1730.5600	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	2007.0400	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	2304.0000	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	2618.8800	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	2949.1200	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	3284.7200	.0000
8	F08	Y	.0000	.0000
8	F08	ROTN	.0000	.0000
7	F07	X	3655.6800	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	4032.0000	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	4421.1200	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	4820.4800	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	5230.0800	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	5646.0800	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000

1	F01	X	6068.4600	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

25-STORY, 3-BAY BUILDING

FRAME ID NUMBER-----	1
NUMBER OF STORY LEVELS----	25
NUMBER OF COLUMN LINES----	4
NUMBER OF BAYS-----	3
NUMBER OF DIFF. COL. PROP-	5
NUMBER OF DIFF. BEAM PROP-	1
NUMBER OF DIFF. FEF-----	2
NUMBER OF PANEL ELEMENTS--	25
NUMBER OF BRACING ELEMENTS	0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	9.00	.00
3	11.50	.00
4	19.50	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
2	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
3	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.60	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	38.400	.000	55.200	.000
2	1	.000	55.200	.000	38.400	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	25	1	2	1	24	1	0	0
2	25	2	3	1	24	0	0	0
3	25	3	4	1	24	2	0	0

GENERATED BEAM LOCATIONS

STORY	1	2	3
25	1	1	1
24	1	1	1
23	1	1	1
22	1	1	1
21	1	1	1
20	1	1	1
19	1	1	1
18	1	1	1
17	1	1	1
16	1	1	1
15	1	1	1
14	1	1	1
13	1	1	1
12	1	1	1
11	1	1	1
10	1	1	1
9	1	1	1
8	1	1	1

7	1	1	1
6	1	1	1
5	1	1	1
4	1	1	1
3	1	1	1
2	1	1	1
1	1	1	1

GENERATED BEAM LOADS . . . LOAD CASE I

OSTORY	1	2	3
25	1	0	2
24	1	0	2
23	1	0	2
22	1	0	2
21	1	0	2
20	1	0	2
19	1	0	2
18	1	0	2
17	1	0	2
16	1	0	2
15	1	0	2
14	1	0	2
13	1	0	2
12	1	0	2
11	1	0	2
10	1	0	2
9	1	0	2
8	1	0	2
7	1	0	2
6	1	0	2
5	1	0	2
4	1	0	2
3	1	0	2
2	1	0	2
1	1	0	2

GENERATED BEAM LOADS . . . LOAD CASE II

OSTORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

STORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

COLUMN LOCATIONS

0 LINE	LEV	CID	KOOL	GEN
1	25	1	2	4
1	20	2	2	4
1	15	3	2	5
1	9	4	2	8
2	25	5	3	24
3	25	5	4	24
4	25	1	3	4
4	20	2	3	4
4	15	3	3	5
4	9	4	3	8

GENERATED COLUMN LOCATIONS

STORY	1	2	3	4
25	1	5	5	1
24	1	5	5	1
23	1	5	5	1
22	1	5	5	1
21	1	5	5	1
20	2	5	5	2
19	2	5	5	2
18	2	5	5	2
17	2	5	5	2
16	2	5	5	2
15	3	5	5	3
14	3	5	5	3
13	3	5	5	3
12	3	5	5	3
11	3	5	5	3
10	3	5	5	3
9	4	5	5	4
8	4	5	5	4

7	4	5	5	4
6	4	5	5	4
5	4	5	5	4
4	4	5	5	4
3	4	5	5	4
2	4	5	5	4
1	4	5	5	4

PANEL CARDS

LEVEL	COL I	COL J	E	A	I	BA	G
25	2	3	3042000.00	1.05	1.07	.00	.00
24	2	3	3042000.00	1.05	1.07	.00	.00
23	2	3	3042000.00	1.05	1.07	.00	.00
22	2	3	3042000.00	1.05	1.07	.00	.00
21	2	3	3042000.00	1.05	1.07	.00	.00
20	2	3	3042000.00	1.05	1.07	.00	.00
19	2	3	3042000.00	1.05	1.07	.00	.00
18	2	3	3042000.00	1.05	1.07	.00	.00
17	2	3	3042000.00	1.05	1.07	.00	.00
16	2	3	3042000.00	1.05	1.07	.00	.00
15	2	3	3042000.00	1.05	1.07	.00	.00
14	2	3	3042000.00	1.05	1.07	.00	.00
13	2	3	3042000.00	1.05	1.07	.00	.00
12	2	3	3042000.00	1.05	1.07	.00	.00
11	2	3	3042000.00	1.05	1.07	.00	.00
10	2	3	3042000.00	1.05	1.07	.00	.00
9	2	3	3042000.00	1.05	1.07	.00	.00
8	2	3	3042000.00	1.05	1.07	.00	.00
7	2	3	3042000.00	1.05	1.07	.00	.00
6	2	3	3042000.00	1.05	1.07	.00	.00
5	2	3	3042000.00	1.05	1.07	.00	.00
4	2	3	3042000.00	1.05	1.07	.00	.00
3	2	3	3042000.00	1.05	1.07	.00	.00
2	2	3	3042000.00	1.05	1.07	.00	.00
1	2	3	3042000.00	1.05	1.07	.00	.00

BEAM PROPERTIES AND LOADS

BAY NUMBERS		1										
LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3
25	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
24	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
23	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
22	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
21	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
20	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
19	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
18	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
17	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
16	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
15	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
14	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
13	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
12	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
11	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
10	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
9	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
8	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
7	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
6	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
5	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
4	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
3	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
2	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0

BAY NUMBERS		2										
LEVEL	E	BA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT1	VERT2	VERT3

25	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
24	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
23	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
22	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
21	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
20	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
19	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
18	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
17	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
16	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
15	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
14	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
13	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
12	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
11	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
10	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
9	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
8	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
7	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
6	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
3	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
2	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
1	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00

0... FRAME TYPE 1 ...
 TIME REQUIRED TO FORM STIFFNESS = 75.13

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	25-8.3-B BUILD

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	2.00	.00	.00	2.00	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
25	X	.6205304
25	Y	.0000000
25	ROTN	.0000000
24	X	.5974482
24	Y	.0000000
24	ROTN	.0000000
23	X	.5740344
23	Y	.0000000
23	ROTN	.0000000
22	X	.5501238
22	Y	.0000000
22	ROTN	.0000000
21	X	.5255801
21	Y	.0000000
21	ROTN	.0000000
20	X	.5003098

20	Y	.0000000
20	ROTN	.0000000
19	X	.4743028
19	Y	.0000000
19	ROTN	.0000000
18	X	.4474410
18	Y	.0000000
18	ROTN	.0000000
17	X	.4197126
17	Y	.0000000
17	ROTN	.0000000
16	X	.3911330
16	Y	.0000000
16	ROTN	.0000000
15	X	.3617490
15	Y	.0000000
15	ROTN	.0000000
14	X	.3316988
14	Y	.0000000
14	ROTN	.0000000
13	X	.3010736
13	Y	.0000000
13	ROTN	.0000000
12	X	.2700580
12	Y	.0000000
12	ROTN	.0000000
11	X	.2388712
11	Y	.0000000
11	ROTN	.0000000
10	X	.2077896
10	Y	.0000000
10	ROTN	.0000000
9	X	.1771328
9	Y	.0000000
9	ROTN	.0000000
8	X	.1473125
8	Y	.0000000
8	ROTN	.0000000
7	X	.1187029
7	Y	.0000000
7	ROTN	.0000000
6	X	.0917919
6	Y	.0000000
6	ROTN	.0000000
5	X	.0671082
5	Y	.0000000
5	ROTN	.0000000
4	X	.0452471
4	Y	.0000000
4	ROTN	.0000000
3	X	.0268628
3	Y	.0000000
3	ROTN	.0000000
2	X	.0126677
2	Y	.0000000
2	ROTN	.0000000
1	X	.0034333
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID 25-8,3-8 BUILD.
LEVEL NO 1

FRAME TYPE 1
LEVEL ID F01

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-49.895557	80.9502238	-1447.0418860	6.5216394
2	1	-6.6883186	20.9599636	-242.9252521	3.3844032
3	1	-5.4514128	19.6889256	-2727.7407495	1.2180999
4	1	49.2980972	-80.5285115	-2342.9593608	-5.7965905

BEAM FORCES				
BAY	LOAD	I MOMENT	J MOMENT	
1	1	-21.1142770	-20.6143017	
2	1	2.4823038	2.5139141	
3	1	-21.1145638	-21.8248551	

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-873.8825180	1860.0038118	-2599.3327515	194.2992594

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 2 LEVEL ID F02

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-34.9800589	71.0098327	-1375.4579594	5.9320450
2	1	1.9825329	24.8003184	-353.0688235	5.8806134
3	1	3.0880882	24.0520621	-2499.9045678	1.0137278
4	1	34.2137807	-70.9208523	-2260.8189335	-3.9574435

BEAM FORCES				
BAY	LOAD	I MOMENT	J MOMENT	
1	1	-38.3038874	-37.5126405	
2	1	6.0474829	6.1388872	
3	1	-38.4748768	-39.2981348	

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-700.5038871	1489.8206786	-2486.3517171	191.3181451

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 3 LEVEL ID F03

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-18.8058494	73.2839544	-1308.1350256	9.0272657
2	1	9.9977443	29.4828447	-454.4282991	8.2574482
3	1	11.1093859	29.2480013	-2280.9175301	1.9948122
4	1	17.0545876	-73.5119153	-2174.2952948	-8.2482793

BEAM FORCES				
BAY	LOAD	I MOMENT	J MOMENT	
1	1	-52.9500756	-51.8608149	
2	1	8.8643860	8.9982859	
3	1	-53.2909940	-54.4260492	

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-555.8278325	1308.8908509	-2393.4258508	179.2720547

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 4 LEVEL ID F04

COLUMN FORCES					
LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-5.0541975	71.5559249	-1244.4363889	10.9058871
2	1	18.7270852	32.9988846	-543.5812843	9.9331845
3	1	17.8780278	33.1853422	-2074.2182884	3.2325525
4	1	3.9275710	-72.0808188	-2084.0308642	-7.4598837

BEAM FORCES				
BAY	LOAD	I MOMENT	J MOMENT	
1	1	-85.0084511	-83.8892701	
2	1	11.2371187	11.4069953	
3	1	-85.5778651	-86.9555355	

PANEL FORCES					
I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-555.8278325	1308.8908509	-2393.4258508	179.2720547

2 1 -423.1879339 1137.8921669 -2290.5553762 188.1484538

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 5 LEVEL ID F05

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	7.0148528	70.0626486	-1183.7236021	12.7999065
2	1	22.3706514	35.7250852	-820.9875476	11.1300594
3	1	23.6055564	36.2928420	-1879.2857371	4.7037802
4	1	-8.3278309	-70.8631085	-1990.8639891	-8.9232018

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-74.7487793	-73.2419662
2	1	13.1873753	13.3702804
3	1	-75.5823677	-77.1582116

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-303.7626251	979.6007823	-2187.7391241	157.0028863

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 6 LEVEL ID F06

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	17.0533250	67.7339285	-1125.4224453	14.2518996
2	1	27.0137359	37.7039395	-688.7007950	11.9418302
3	1	28.3630898	38.6065309	-1698.1291553	6.2756956
4	1	-18.5309587	-68.8303807	-1894.7714167	-10.1478161

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-82.3809252	-80.7202979
2	1	14.7159915	14.9486904
3	1	-83.5054778	-85.2450341

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-197.9719373	831.6076419	-2084.9761978	145.5428653

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 7 LEVEL ID F07

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	26.5825106	85.3278002	-1099.0100981	15.7804804
2	1	30.8520971	38.9908704	-740.1371198	12.4312243
3	1	32.1494972	40.1938975	-1525.3094397	7.8238773
4	1	-28.2899078	-66.7140754	-1798.8778027	-11.8620280

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-88.0574217	-86.3179451
2	1	15.8690387	16.1313593
3	1	-89.5359253	-91.3617969

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-108.2031972	692.8771744	-1982.2857396	132.7822789

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 8 LEVEL ID F08

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
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1	1	30.1341052	81.4949110	-1014.0070190	15.8548544
2	1	33.8725950	39.7969092	-782.4185173	12.7711886
3	1	35.2944878	41.2550887	-1385.7028680	9.3693148
4	1	-31.8172432	-63.0718891	-1897.4853874	-11.5813051

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-92.2792786	-90.3457178
2	1	16.8105880	17.0903330
3	1	-94.0061888	-96.0370075

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-23.7549194	571.2235333	-1879.8062104	123.4234286

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
 LEVEL NO 9 LEVEL ID F09

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	50.5358015	82.1451734	-960.0351435	21.0130319
2	1	35.3804426	39.8825388	-810.3514527	12.7694905
3	1	37.3513077	41.6213877	-1220.5044772	10.6441811
4	1	-53.2441894	-64.2197643	-1598.9089879	-17.4608585

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-94.0318882	-92.5021489
2	1	17.2882007	17.6204241
3	1	-96.5168793	-98.1478762

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	23.7831880	442.1588228	-1776.9889387	103.2322908

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
 LEVEL NO 10 LEVEL ID F10

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	43.2189973	43.4962847	-908.5518979	14.7310419
2	1	37.2067680	39.8535056	-830.2273737	12.9020085
3	1	39.5124411	41.5451475	-1083.4108042	11.7108815
4	1	-44.5301883	-44.9038888	-1495.7788934	-10.8944801

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-95.1004138	-94.1109056
2	1	17.4765757	17.8257890
3	1	-98.2012959	-97.2133822

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	110.8288977	389.2098118	-1674.4332307	107.2014242

MEMBER FORCES FRAME ID 25-8,3-8 BUILD. FRAME TYPE 1
 LEVEL NO 11 LEVEL ID F11

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	48.1406507	51.8804185	-853.4033128	18.3739843
2	1	38.4104778	39.4275838	-843.7206651	12.9034482
3	1	38.7943201	40.0630858	-952.4375354	12.3135115
4	1	-48.8067818	-52.8831739	-1394.8000812	-14.4843081

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-96.2848278	-95.1389987

2	1	17.7022675	17.7285049
3	1	-95.4177084	-96.5684778

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	149.7785292	260.8890008	-1571.8384255	90.4045936

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 12	LEVEL ID F12

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	48.7783444	48.1441771	-800.5312911	17.9885956
2	1	39.1981648	39.0262534	-844.4985866	12.9717682
3	1	38.8027255	38.8978834	-833.9371045	12.9231610
4	1	-48.3319291	-47.9618961	-1294.0017879	-13.9844102

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-96.1519880	-95.0325092
2	1	17.8446940	17.5368933
3	1	-93.8427704	-94.7357484

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	189.0323384	178.2573002	-1468.8312298	80.3718731

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 13	LEVEL ID F13

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	50.4135649	47.3756236	-747.6293508	18.8502136
2	1	39.3835332	38.1886504	-835.0073169	12.9188876
3	1	38.2705883	37.3031516	-725.4813103	13.2680864
4	1	-49.1409143	-46.4038193	-1193.8544731	-14.8306416

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-95.1659203	-94.0940529
2	1	17.4280442	17.2052901
3	1	-91.1703220	-92.1943079

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	214.1119431	102.3885721	-1385.4275489	88.5321665

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 14	LEVEL ID F14

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	47.8747330	44.7523554	-894.4888474	17.7895445
2	1	39.4040593	37.2844755	-815.9264318	12.9251233
3	1	37.5858852	35.8944436	-828.4091726	13.5240304
4	1	-45.7864921	-43.0533937	-1093.9389943	-13.9344413

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-93.8827434	-92.8482921
2	1	17.2018858	16.8628983
3	1	-88.3304011	-88.4823084

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	235.3814085	42.0157150	-1282.0438539	59.8886452

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 15 LEVEL ID F15

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	59.8620613	46.2080104	-641.0032269	21.4519109
2	1	38.5453146	36.0423470	-784.8899789	12.7503434
3	1	38.3224234	33.9818187	-539.1044057	13.5009708
4	1	-55.7875846	-43.6958183	-994.9073058	-17.3964951

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-90.4907957	-89.9833735
2	1	18.8578888	16.2776640
3	1	-84.3799428	-84.8357810

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	227.6403567	-23.1468861	-1156.4950848	42.4200463

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 16 LEVEL ID F16

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	41.8445593	31.8287344	-586.7624980	14.0579285
2	1	37.7700882	34.7803701	-748.3892659	12.8398940
3	1	34.1409814	31.7798555	-457.0945537	13.1223633
4	1	-39.0445429	-29.0482182	-896.9553401	-10.1840983

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-85.5516213	-86.9279451
2	1	15.7704273	15.0710322
3	1	-77.7505997	-76.4551809

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	258.6657491	-39.5693430	-1054.7983422	47.2754852

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 17 LEVEL ID F17

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	44.8684862	43.7070820	-531.5224438	18.3461803
2	1	37.2041363	33.3874495	-706.9044291	12.5970925
3	1	31.8950295	28.5385661	-379.6011369	12.3981689
4	1	-39.1519259	-38.4106180	-800.8796201	-13.6883580

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-84.7463987	-85.5935949
2	1	15.5512440	14.6080532
3	1	-73.0391472	-72.2676680

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	240.6453608	-93.3468590	-950.8923702	30.0319663

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 18 LEVEL ID F18

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	44.0227775	39.8779105	-476.0149428	17.6753586
2	1	36.5028307	32.8382148	-853.8076080	12.8028073
3	1	29.8171168	26.5380645	-313.2890815	11.9188815

4	1	-36.5819678	-33.1158421	-705.8162682	-12.5309225
---	---	-------------	-------------	--------------	-------------

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-82.3910944	-83.4880844
2	1	14.9113408	13.7820077
3	1	-67.9863804	-67.0456216

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	229.2361203	-118.2786683	-846.1921018	21.8739174

MEMBER FORCES	FRAME ID 25-8,3-B BUILD	FRAME TYPE 1
		LEVEL NO 19	LEVEL ID F19

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	39.0538937	38.3583169	-419.9458401	18.5328381
2	1	36.0202821	32.0521129	-593.7865895	13.0304962
3	1	27.9545597	24.4072559	-253.4757529	11.3882252
4	1	-31.3221115	-30.4636538	-612.2372679	-11.3349324

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-81.5411100	-81.9524049
2	1	14.6876616	13.3126763
3	1	-63.7883546	-63.3789701

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	212.1514259	-135.1439048	-741.3545496	14.2732780

MEMBER FORCES	FRAME ID 25-8,3-B BUILD	FRAME TYPE 1
		LEVEL NO 20	LEVEL ID F20

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	55.4591351	42.4874183	-363.5825295	22.1226684
2	1	34.4504570	31.2444712	-521.7031764	13.0316814
3	1	25.6303542	22.5189186	-205.3772888	10.7019801
4	1	-42.1086305	-32.0568587	-519.5418023	-15.1633759

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-74.7857613	-77.8913512
2	1	13.9105636	12.4730643
3	1	-57.8544543	-55.6240441

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	160.2890722	-162.5429337	-636.1954052	-4.6999306

MEMBER FORCES	FRAME ID 25-8,3-B BUILD	FRAME TYPE 1
		LEVEL NO 21	LEVEL ID F21

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	26.4210078	19.3286262	-305.8421685	9.5047020
2	1	31.3494338	29.3303306	-448.3921630	12.3371524
3	1	21.2103668	19.7510358	-158.3293924	9.2400859
4	1	-18.0518155	-13.5154137	-428.5567800	-5.1843317

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-58.1503905	-69.8695214
2	1	11.6299921	9.9144575
3	1	-46.4546937	-38.4578748

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	174.3561225	-121.6663631	-530.6804860	9.8135181

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 22 LEVEL ID F22

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	31.0783502	31.7293828	-245.0448575	14.1983406
2	1	30.6307777	26.8900955	-377.3141166	12.0650209
3	1	18.3128992	15.3298694	-108.7726027	7.7432640
4	1	-19.4440289	-20.4058594	-341.1427439	-7.8692220

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-60.7973754	-70.8898953
2	1	12.0992057	10.0044424
3	1	-42.6593948	-36.5488350

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	130.1917645	-143.8968859	-425.3258793	-6.0360277

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 23 LEVEL ID F23

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	30.4684550	29.7190252	-184.7055664	13.9427290
2	1	30.8370141	28.1599120	-293.9865677	12.9918152
3	1	16.3792981	14.3420531	-70.8395488	7.2568704
4	1	-17.2610725	-17.1048061	-254.4417152	-7.0704580

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-59.6296900	-70.1096019
2	1	11.8528660	9.4425483
3	1	-38.7317932	-32.8454346

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	86.3766293	-141.3915917	-319.2248019	-15.6620139

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 24 LEVEL ID F24

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	28.2237280	29.1612350	-124.1229778	13.6198791
2	1	28.3407917	27.4197218	-202.4507981	12.7550699
3	1	14.4771289	12.9099466	-40.7398475	6.8082957
4	1	-14.9094205	-15.5843621	-168.6945617	-6.6359830

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-62.6413330	-71.7536070
2	1	10.7335129	8.6287974
3	1	-37.0047255	-32.2988136

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	38.5057185	-128.5598458	-212.7918148	-24.2591221

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 25 LEVEL ID F25

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	42.1909940	34.4178050	-84.1223453	18.7821200
2	1	40.7582714	32.6793024	-96.0732054	17.8049854
3	1	18.4725383	13.8987992	-25.0180134	7.4484633
4	1	-21.2466092	-17.3993871	-83.2318194	-9.1786958

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-42.1909940	-59.2302432
2	1	18.4719718	13.7338074
3	1	-30.2063457	-21.2466092

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-58.6995774	-131.2319432	-105.9548165	-48.0943118

CONVERGE IN ITERATION NO. 3

TOTAL TIME 280.77 SEC.

ตัวอย่าง 4 : โครงข้อแข็งประกอบผนังต้านแรงเฉือน 25 ชั้น 3 ช่วงเสา

$$\text{กรณี } \alpha = 2.5$$

28	1	1	1	0	0	1	00001	5	0.001	TS10804.INP
F25									4.0	
									2.56	
F24									4.0	
									5.12	
F23									4.0	
									5.12	
F22									4.0	
									5.12	
F21									4.0	
									5.12	
F20									4.0	
									5.12	
F19									4.0	
									5.12	
F18									4.0	
									5.12	
F17									4.0	
									5.12	
F16									4.0	
									5.12	
F15									4.0	
									5.12	
F14									4.0	
									5.12	
F13									4.0	
									5.12	
F12									4.0	
									5.12	
F11									4.0	
									5.12	
F10									4.0	
									4.48	
F09									4.0	
									3.84	
F08									4.0	
									3.84	
F07									4.0	
									3.84	
F06									4.0	
									3.84	
F05									4.0	
									3.20	
F04									4.0	
									2.56	
F03									4.0	
									2.56	
F02									4.0	
									1.60	
F01									4.0	
									1.60	

1	25	4	3	5	1	2	25	25-STORY, 3-BAY BUILDING	
1		0.0		0.0					
2		8.0		0.0					
3		11.5		0.0					
4		19.5		0.0					
1		3042000.0		0.16				0.0021333	
2		3042000.0		0.36				0.0108000	
3		3042000.0		0.5625				0.0263672	
4		3042000.0		0.81				0.0546750	
5		3042000.0		0.60				0.0125000	
1		3042000.0				0.0052083	4.0	4.0	2.0
1	1			38.4				55.2	
2	1			55.2				38.4	
1	1	2	1	24	1				
2	2	3	1	24					
3	3	4	1	24	2				
1	1	2	4						
1	2	2	4						
1	3	2	5						
1	4	2	6						

PROGRAM CU-NTABS
 INPUT FILE : ts10s04.inp
 OUTPUT FILE : ts10s04g.out

TS10S04.INP
 TOTAL NUMBER OF STORIES-- 25
 NUMBER OF DIFF FRAMES--- 1
 TOTAL NUMBER OF FRAMES--- 1
 NUMBER OF LOAD CONDITIONS 1
 TYPE OF ANALYSIS----- 0

EQ.0-STATIC LOADS ONLY
 EQ.1-MODE SHAPES AND FREQUENCIES ONLY
 EQ.2-STATIC AND MODE SHAPE ANALYSES
 EQ.3-TYPE 2 AND RESPONSE SPECTRUM ANAL
 EQ.4-TYPE 2 AND TIME HISTORY ANAL (INDIVIDUAL MEMBER RESPONSE ENVELOPES ONLY)
 EQ.5-THIS OPTION IS NOT AVAILABLE FOR USE
 EQ.6-RESPONSE SPECTRUM ANAL (GROSS BUILDING RESPONSE)
 EQ.7-TYPE 3 AND 8 ANALYSES
 EQ.8-TIME HISTORY ANAL (GROSS BUILDING RESPONSE/ENVELOPES OR STEP-BY-STEP RESPONSE)
 EQ.9-TYPE 4 AND 8 ANALYSES
 EQ.10-BLAM RESTART
 EQ.11-BLAM-2 RESTART
 EQ.-1,-6,-8 SAME AS 1,6,8 ABOVE EXCEPT APPROXIMATE PERIODS AND MODES USED

NUMBER OF FREQUENCIES---- 0
 STORY TRANSLATION CODE--- 1
 LAT FORCE GENERATION CODE 0 0
 STRESS CHECK KEY----- 0
 DATA CHECK KEY----- 0
 TYPE OF COLLISION----- 1
 MAXIMUM NO. OF CYCLES---- 5
 CONVERGENCE TOLERANCE OF EQUILIBRIUM .001000

STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2	X(M)	Y(M)	K-X	K-Y
25	F25	4.00	19.08	.00	.00	.00	.00	.00
24	F24	4.00	19.08	.00	.00	.00	.00	.00
23	F23	4.00	19.08	.00	.00	.00	.00	.00
22	F22	4.00	19.08	.00	.00	.00	.00	.00
21	F21	4.00	19.08	.00	.00	.00	.00	.00
20	F20	4.00	19.08	.00	.00	.00	.00	.00
19	F19	4.00	19.08	.00	.00	.00	.00	.00
18	F18	4.00	19.08	.00	.00	.00	.00	.00
17	F17	4.00	19.08	.00	.00	.00	.00	.00
16	F16	4.00	19.08	.00	.00	.00	.00	.00
15	F15	4.00	19.08	.00	.00	.00	.00	.00
14	F14	4.00	19.08	.00	.00	.00	.00	.00
13	F13	4.00	19.08	.00	.00	.00	.00	.00
12	F12	4.00	19.08	.00	.00	.00	.00	.00
11	F11	4.00	19.08	.00	.00	.00	.00	.00
10	F10	4.00	19.08	.00	.00	.00	.00	.00
9	F09	4.00	19.08	.00	.00	.00	.00	.00
8	F08	4.00	19.08	.00	.00	.00	.00	.00
7	F07	4.00	19.08	.00	.00	.00	.00	.00
6	F06	4.00	19.08	.00	.00	.00	.00	.00
5	F05	4.00	19.08	.00	.00	.00	.00	.00
4	F04	4.00	19.08	.00	.00	.00	.00	.00
3	F03	4.00	19.08	.00	.00	.00	.00	.00
2	F02	4.00	19.08	.00	.00	.00	.00	.00
1	F01	4.00	19.08	.00	.00	.00	.00	.00

CUMULATIVE STORY DATA

LEVEL NO.	ID	HEIGHT	MASS(M)	MR**2
25	F25	100.00	19.08	.00

24	F24	96.00	38.17	.00
23	F23	92.00	57.25	.00
22	F22	88.00	76.33	.00
21	F21	84.00	95.41	.00
20	F20	80.00	114.50	.00
19	F19	76.00	133.58	.00
18	F18	72.00	152.66	.00
17	F17	68.00	171.74	.00
16	F16	64.00	190.83	.00
15	F15	60.00	209.91	.00
14	F14	56.00	228.99	.00
13	F13	52.00	248.07	.00
12	F12	48.00	267.16	.00
11	F11	44.00	286.24	.00
10	F10	40.00	305.32	.00
9	F09	36.00	324.40	.00
8	F08	32.00	343.48	.00
7	F07	28.00	362.57	.00
6	F06	24.00	381.65	.00
5	F05	20.00	400.73	.00
4	F04	16.00	419.82	.00
3	F03	12.00	438.90	.00
2	F02	8.00	457.98	.00
1	F01	4.00	477.06	.00

STRUCTURE LATERAL LOADS - CASES A AND B

LEVEL NO.	FX-A	FY-A	MOM-A	FX-B	FY-B	MOM-B	XA	YA	XB	YB
25	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
24	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
23	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
22	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
21	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
20	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
19	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
18	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
17	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
16	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
15	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
14	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
13	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
12	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
11	5.12	.00	.00	.00	.00	.00	.0	.0	.0	.0
10	4.48	.00	.00	.00	.00	.00	.0	.0	.0	.0
9	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
8	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
7	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
6	3.84	.00	.00	.00	.00	.00	.0	.0	.0	.0
5	3.20	.00	.00	.00	.00	.00	.0	.0	.0	.0
4	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
3	2.56	.00	.00	.00	.00	.00	.0	.0	.0	.0
2	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0
1	1.60	.00	.00	.00	.00	.00	.0	.0	.0	.0

 STORY SHEARS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL ID DIRN 1 2

25	F25	X	2.5600	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	7.6800	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	12.8000	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	17.9200	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	23.0400	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	28.1600	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	33.2800	.0000
19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	38.4000	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	43.5200	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	48.6400	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	53.7600	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	58.8800	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	64.0000	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	69.1200	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	74.2400	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	79.3600	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	84.4800	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	89.6000	.0000
8	F08	Y	.0000	.0000

9	F08	ROTN	.0000	.0000
7	F07	X	90.2400	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	94.0900	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	97.2800	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	99.8400	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	102.4000	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	104.0000	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000
1	F01	X	105.6000	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

 STORY OVERTURNING MOMENTS

NOTE THAT THE FORCE QUANTITIES BELOW DO NOT INCLUDE P-DELTA EFFECTS.

OUTPUT COLUMN 1 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE A
 OUTPUT COLUMN 2 CONTAINS RESULTS FROM STATIC LATERAL LOAD CASE B

LEVEL	ID	DIRN	1	2
25	F25	X	10.2400	.0000
25	F25	Y	.0000	.0000
25	F25	ROTN	.0000	.0000
24	F24	X	40.9600	.0000
24	F24	Y	.0000	.0000
24	F24	ROTN	.0000	.0000
23	F23	X	92.1600	.0000
23	F23	Y	.0000	.0000
23	F23	ROTN	.0000	.0000
22	F22	X	183.8400	.0000
22	F22	Y	.0000	.0000
22	F22	ROTN	.0000	.0000
21	F21	X	256.0000	.0000
21	F21	Y	.0000	.0000
21	F21	ROTN	.0000	.0000
20	F20	X	368.6400	.0000
20	F20	Y	.0000	.0000
20	F20	ROTN	.0000	.0000
19	F19	X	501.7600	.0000

19	F19	Y	.0000	.0000
19	F19	ROTN	.0000	.0000
18	F18	X	865.3600	.0000
18	F18	Y	.0000	.0000
18	F18	ROTN	.0000	.0000
17	F17	X	829.4400	.0000
17	F17	Y	.0000	.0000
17	F17	ROTN	.0000	.0000
16	F16	X	1024.0000	.0000
16	F16	Y	.0000	.0000
16	F16	ROTN	.0000	.0000
15	F15	X	1239.0400	.0000
15	F15	Y	.0000	.0000
15	F15	ROTN	.0000	.0000
14	F14	X	1474.5600	.0000
14	F14	Y	.0000	.0000
14	F14	ROTN	.0000	.0000
13	F13	X	1730.5600	.0000
13	F13	Y	.0000	.0000
13	F13	ROTN	.0000	.0000
12	F12	X	2007.0400	.0000
12	F12	Y	.0000	.0000
12	F12	ROTN	.0000	.0000
11	F11	X	2304.0000	.0000
11	F11	Y	.0000	.0000
11	F11	ROTN	.0000	.0000
10	F10	X	2618.8800	.0000
10	F10	Y	.0000	.0000
10	F10	ROTN	.0000	.0000
9	F09	X	2949.1200	.0000
9	F09	Y	.0000	.0000
9	F09	ROTN	.0000	.0000
8	F08	X	3294.7200	.0000
8	F08	Y	.0000	.0000
8	F08	ROTN	.0000	.0000
7	F07	X	3655.8800	.0000
7	F07	Y	.0000	.0000
7	F07	ROTN	.0000	.0000
6	F06	X	4032.0000	.0000
6	F06	Y	.0000	.0000
6	F06	ROTN	.0000	.0000
5	F05	X	4421.1200	.0000
5	F05	Y	.0000	.0000
5	F05	ROTN	.0000	.0000
4	F04	X	4820.4800	.0000
4	F04	Y	.0000	.0000
4	F04	ROTN	.0000	.0000
3	F03	X	5230.0800	.0000
3	F03	Y	.0000	.0000
3	F03	ROTN	.0000	.0000
2	F02	X	5646.0800	.0000
2	F02	Y	.0000	.0000
2	F02	ROTN	.0000	.0000

1	F01	X	8088.4800	.0000
1	F01	Y	.0000	.0000
1	F01	ROTN	.0000	.0000

25-STORY, 3-BAY BUILDING

FRAME ID NUMBER----- 1
 NUMBER OF STORY LEVELS---- 25
 NUMBER OF COLUMN LINES---- 4
 NUMBER OF BAYS----- 3
 NUMBER OF DIFF. COL. PROP- 5
 NUMBER OF DIFF. BEAM PROP- 1
 NUMBER OF DIFF. FEF----- 2
 NUMBER OF PANEL ELEMENTS-- 25
 NUMBER OF BRACING ELEMENTS 0

COLUMN LINE COORDINATES

LINE	X	Y
1	.00	.00
2	8.00	.00
3	11.50	.00
4	19.50	.00

COLUMN ID	E	A	MAJ SA	MIN SA	TORS I	MAJ I	MIN I	RIGID TOP	RIGID BOT
1	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
2	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
3	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.60	.00	.00	.00	.01	.00	.00	.00

BEAM ID	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	RIGID I	RIGID J
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00

FEF ID	CODE	ML	VL	MR	VR	W
1	1	.000	38.400	.000	55.200	.000
2	1	.000	55.200	.000	38.400	.000

BEAM LOCATIONS

BAY	LEV	IC	JC	BID	GEN	VL1	VL2	VL3
1	25	1	2	1	24	1	0	0
2	25	2	3	1	24	0	0	0
3	25	3	4	1	24	2	0	0

GENERATED BEAM LOCATIONS

STORY	1	2	3
25	1	1	1
24	1	1	1
23	1	1	1
22	1	1	1
21	1	1	1
20	1	1	1
19	1	1	1
18	1	1	1
17	1	1	1
16	1	1	1
15	1	1	1
14	1	1	1
13	1	1	1
12	1	1	1
11	1	1	1
10	1	1	1
9	1	1	1
8	1	1	1

7	1	1	1
6	1	1	1
5	1	1	1
4	1	1	1
3	1	1	1
2	1	1	1
1	1	1	1

GENERATED BEAM LOADS ... LOAD CASE 1

OSTORY	1	2	3
25	1	0	2
24	1	0	2
23	1	0	2
22	1	0	2
21	1	0	2
20	1	0	2
19	1	0	2
18	1	0	2
17	1	0	2
16	1	0	2
15	1	0	2
14	1	0	2
13	1	0	2
12	1	0	2
11	1	0	2
10	1	0	2
9	1	0	2
8	1	0	2
7	1	0	2
6	1	0	2
5	1	0	2
4	1	0	2
3	1	0	2
2	1	0	2
1	1	0	2

GENERATED BEAM LOADS ... LOAD CASE 11

OSTORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

OSTORY	1	2	3
25	0	0	0
24	0	0	0
23	0	0	0
22	0	0	0
21	0	0	0
20	0	0	0
19	0	0	0
18	0	0	0
17	0	0	0
16	0	0	0
15	0	0	0
14	0	0	0
13	0	0	0
12	0	0	0
11	0	0	0
10	0	0	0
9	0	0	0
8	0	0	0
7	0	0	0
6	0	0	0
5	0	0	0
4	0	0	0
3	0	0	0
2	0	0	0
1	0	0	0

COLUMN LOCATIONS

D LINE	LEV	CID	KOOL	GEN
1	25	1	2	4
1	20	2	2	4
1	15	3	2	5
1	9	4	2	8
2	25	5	3	24
3	25	5	4	24
4	25	1	3	4
4	20	2	3	4
4	15	3	3	5
4	9	4	3	8

GENERATED COLUMN LOCATIONS

OSTORY	1	2	3	4
25	1	5	5	1
24	1	5	5	1
23	1	5	5	1
22	1	5	5	1
21	1	5	5	1
20	2	5	5	2
19	2	5	5	2
18	2	5	5	2
17	2	5	5	2
16	2	5	5	2
15	3	5	5	3
14	3	5	5	3
13	3	5	5	3
12	3	5	5	3
11	3	5	5	3
10	3	5	5	3
9	4	5	5	4
8	4	5	5	4

7	4	5	5	4
6	4	5	5	4
5	4	5	5	4
4	4	5	5	4
3	4	5	5	4
2	4	5	5	4
1	4	5	5	4

PANEL CARDS

LEVEL	COL I	COL J	E	A	I	SA	G
25	2	3	3042000.00	1.05	1.07	.00	.00
24	2	3	3042000.00	1.05	1.07	.00	.00
23	2	3	3042000.00	1.05	1.07	.00	.00
22	2	3	3042000.00	1.05	1.07	.00	.00
21	2	3	3042000.00	1.05	1.07	.00	.00
20	2	3	3042000.00	1.05	1.07	.00	.00
19	2	3	3042000.00	1.05	1.07	.00	.00
18	2	3	3042000.00	1.05	1.07	.00	.00
17	2	3	3042000.00	1.05	1.07	.00	.00
16	2	3	3042000.00	1.05	1.07	.00	.00
15	2	3	3042000.00	1.05	1.07	.00	.00
14	2	3	3042000.00	1.05	1.07	.00	.00
13	2	3	3042000.00	1.05	1.07	.00	.00
12	2	3	3042000.00	1.05	1.07	.00	.00
11	2	3	3042000.00	1.05	1.07	.00	.00
10	2	3	3042000.00	1.05	1.07	.00	.00
9	2	3	3042000.00	1.05	1.07	.00	.00
8	2	3	3042000.00	1.05	1.07	.00	.00
7	2	3	3042000.00	1.05	1.07	.00	.00
6	2	3	3042000.00	1.05	1.07	.00	.00
5	2	3	3042000.00	1.05	1.07	.00	.00
4	2	3	3042000.00	1.05	1.07	.00	.00
3	2	3	3042000.00	1.05	1.07	.00	.00
2	2	3	3042000.00	1.05	1.07	.00	.00
1	2	3	3042000.00	1.05	1.07	.00	.00

BEAM PROPERTIES AND LOADS

BAY NUMBERS 1		LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
25	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
24	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
23	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
22	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
21	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
20	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
19	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
18	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
17	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
16	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
15	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
14	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
13	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
12	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
11	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
10	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
9	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
8	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
7	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
6	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
5	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
4	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
3	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
2	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		
1	3042000.00	.00	.00	.01	4.00	4.00	2.00	.00	.00	1	0	0		

BAY NUMBERS 2		LEVEL	E	SA	TORS I	FLEX I	KII	KJJ	KIJ	WI	WJ	VERT 1	VERT 2	VERT 3
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25	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
24	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
23	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
22	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
21	3042000.00	.16	.00	.00	.00	.00	.00	.00	.00
20	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
19	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
18	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
17	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
16	3042000.00	.36	.00	.00	.00	.01	.00	.00	.00
15	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
14	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
13	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
12	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
11	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
10	3042000.00	.56	.00	.00	.00	.03	.00	.00	.00
9	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
8	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
7	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
6	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
5	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
4	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
3	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
2	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00
1	3042000.00	.81	.00	.00	.00	.05	.00	.00	.00

0...FRAME TYPE 1...

TIME REQUIRED TO FORM STIFFNESS = 75.09

1FRAME POSITION DATA

FRAME	ID	FORCE CODE	X1	Y1	ANG	
1	1	0	.00	.00	.00	25-6,3-B BUILD

LOAD CONDITION DEFINITION CARDS

LOAD	I	II	III	A	B	SPECTRUM-1	SPECTRUM-2	SPECTRUM-3	SPECTRUM-4	TIME HIST
1	2.50	.00	.00	2.50	.00	.00	.00	.00	.00	.00

SPECTRUM-1... ROOT MEAN SQUARE COMBINATION

SPECTRUM-2... SUM OF ABSOLUTE VALUES

SPECTRUM-3... DOUBLE SUM COMBINATION

SPECTRUM-4... COMPLETE QUADRATIC COMBINATION

FRAME DISPLACEMENT

LEVEL		
25	X	.8305843
25	Y	.0000000
25	ROTN	.0000000
24	X	.7996303
24	Y	.0000000
24	ROTN	.0000000
23	X	.7882330
23	Y	.0000000
23	ROTN	.0000000
22	X	.7361707
22	Y	.0000000
22	ROTN	.0000000
21	X	.7032612
21	Y	.0000000
21	ROTN	.0000000
20	X	.6693779

20	Y	.0000000
20	ROTN	.0000000
19	X	.6345062
19	Y	.0000000
19	ROTN	.0000000
18	X	.5984871
18	Y	.0000000
18	ROTN	.0000000
17	X	.5613041
17	Y	.0000000
17	ROTN	.0000000
16	X	.5229777
16	Y	.0000000
16	ROTN	.0000000
15	X	.4835709
15	Y	.0000000
15	ROTN	.0000000
14	X	.4432709
14	Y	.0000000
14	ROTN	.0000000
13	X	.4022025
13	Y	.0000000
13	ROTN	.0000000
12	X	.3606166
12	Y	.0000000
12	ROTN	.0000000
11	X	.3188118
11	Y	.0000000
11	ROTN	.0000000
10	X	.2771840
10	Y	.0000000
10	ROTN	.0000000
9	X	.2361066
9	Y	.0000000
9	ROTN	.0000000
8	X	.1961076
8	Y	.0000000
8	ROTN	.0000000
7	X	.1579427
7	Y	.0000000
7	ROTN	.0000000
6	X	.1219996
6	Y	.0000000
6	ROTN	.0000000
5	X	.0890771
5	Y	.0000000
5	ROTN	.0000000
4	X	.0599884
4	Y	.0000000
4	ROTN	.0000000
3	X	.0355382
3	Y	.0000000
3	ROTN	.0000000
2	X	.0167208
2	Y	.0000000
2	ROTN	.0000000
1	X	.0045158
1	Y	.0000000
1	ROTN	.0000000

MEMBER FORCES FRAME ID 25-S,3-B BUILD.
LEVEL NO 1

FRAME TYPE 1
LEVEL ID F01

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-66.2030286	105.9390716	-1769.3281110	7.9115395
2	1	-8.9838565	27.4885144	-215.7876478	-4.3825517
3	1	-6.9283208	25.2438564	-3497.5534095	.6303442
4	1	65.2294761	-105.0500889	-2968.1570310	-6.6042720

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-27.8445599	-27.1888487
2	1	3.3503276	3.3889585
3	1	-27.8150445	-28.4838936

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-1176.5634729	2169.1210896	-3249.1738000	244.4712712

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 2

FRAME TYPE 1
LEVEL ID F02

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-46.8287670	94.0475887	-1680.2072630	6.7280344
2	1	2.4835309	32.8221795	-356.8731828	7.7372262
3	1	-4.2488246	31.3544068	-3209.2524430	- .8913065
4	1	45.4851478	-93.7131697	-2865.1196887	-3.3149136

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-50.7182655	-49.8711344
2	1	8.0541709	8.1788183
3	1	-50.8650583	-51.9565383

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-948.7287661	1959.2578502	-3120.4474226	243.1110697

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 3

FRAME TYPE 1
LEVEL ID F03

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-25.1515383	87.3470324	-1596.7559379	10.5370712
2	1	13.1317725	39.1334327	-489.7285579	10.7624244
3	1	14.8002447	38.4374154	-2929.4612143	- .4719858
4	1	23.8060694	-97.4418862	-2756.2669891	-5.4422809

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-70.3063465	-68.8808215
2	1	11.8057283	11.9840944
3	1	-70.6366690	-72.1455019

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-756.1483180	1731.3872176	-2991.7893007	229.7301069

MEMBER FORCES FRAME ID 25-B,3-B BUILD.
LEVEL NO 4

FRAME TYPE 1
LEVEL ID F04

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-7.1907493	95.4579848	-1518.1518089	12.7930869
2	1	22.1309886	43.9231206	-808.9766688	12.7941683
3	1	23.7588184	43.8523299	-2663.2521172	.8388260
4	1	5.6638236	-95.9515713	-2642.4192178	-8.4332639

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-86.5229083	-84.7668889
2	1	14.9811837	15.2092520
3	1	-87.1137945	-88.9499428

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
-------	------	------------	------------	-------------	-------------

2 1 -578.4494583 1516.1681282 -2863.2001875 216.9425124

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 5 LEVEL ID F05

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	8.8834760	93.7197476	-1463.5630198	15.1456988
2	1	29.7148313	-47.8545186	-714.7103740	14.1411916
3	1	31.3794755	-48.1457141	-2410.8366911	2.3385950
4	1	-10.8229260	-94.8135661	-2524.4112519	-7.9384595

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-99.8869552	-97.6760400
2	1	17.5775609	17.8469245
3	1	-100.5878592	-102.8916341

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-417.5876702	1311.7344510	-2734.8786732	203.6358721

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 6 LEVEL ID F06

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	22.3344887	90.8033792	-1372.2333817	16.9901080
2	1	35.9828134	50.3838477	-806.3758762	14.9548757
3	1	37.7405197	51.3614592	-2172.1656187	-4.3971814
4	1	-24.2535354	-92.0887082	-2403.0013152	-9.3023221

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-110.0530876	-107.8323457
2	1	19.6699921	19.9758155
3	1	-111.3011488	-113.8267487

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-274.3681480	1118.3916882	-2606.2238081	189.5554885

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 7 LEVEL ID F07

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	35.1525097	87.7185989	-1303.4690608	19.0050615
2	1	40.9176052	52.1795402	-892.7920094	15.3418916
3	1	42.8254353	53.5850135	-1949.0189832	8.5891123
4	1	-37.3872211	-89.3732133	-2278.8853280	-11.2074948

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-117.8038756	-115.4741593
2	1	21.2353785	21.5756851
3	1	-118.4857174	-121.9284446

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-152.2251833	935.1120171	-2477.8346185	173.4563758

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 8 LEVEL ID F08

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
------	------	------------	------------	-------------	-------------

1	1	39.9959183	92.6513659	-1236.6288153	18.8350076
2	1	45.0263438	53.3211757	-945.0942507	15.5482312
3	1	47.0871181	55.0845970	-1740.0591504	8.8964318
4	1	-42.1308952	-84.5612236	-2152.7085578	-11.0850052

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-123.6005587	-121.0081454
2	1	22.5186488	22.8783295
3	1	-125.5733207	-128.2936555

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-37.1631986	773.5837945	-2349.5092259	161.6350214

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 9 LEVEL ID F09

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	87.5760334	83.6046404	-1171.2046533	26.1096580
2	1	47.3790147	53.4611547	-988.6278852	15.3461632
3	1	49.8448888	55.6278732	-1549.9430674	10.9038693
4	1	-70.9741861	-86.1629803	-2024.9751858	-19.0804113

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-126.0604094	-124.0079303
2	1	23.1522184	23.6000861
3	1	-129.0193796	-131.2010619

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	27.9988622	600.4879481	-2221.2494085	134.9595588

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 10 LEVEL ID F10

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	57.8544249	58.4843781	-1106.4831957	17.7275795
2	1	49.8382455	53.4788973	-1021.5594956	15.3430959
3	1	51.4870180	55.5744250	-1370.4880638	12.6931870
4	1	-59.4952784	-60.2268758	-1896.4476306	-10.4647445

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-127.4899358	-128.1601404
2	1	23.4378013	23.6279885
3	1	-128.7881419	-130.1255303

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	146.1628863	502.0559377	-2093.0416144	140.5710034

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
 LEVEL NO 11 LEVEL ID F11

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	64.4534424	89.6354106	-1042.1694427	22.6711269
2	1	51.4437631	52.8940936	-1046.0272454	15.1907103
3	1	51.9191653	53.6731374	-1189.1888937	13.9122078
4	1	-65.0417035	-70.6302518	-1768.0850215	-15.5086474

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-129.0585707	-127.5175489

2	1	23.7464076	23.7766958
3	1	-127.8640779	-129.4086939

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	199.4396542	355.6471865	-1964.5474967	118.3168074

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 12	LEVEL ID F12

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	65.3124016	64.6031283	-978.2412077	22.2550269
2	1	52.4908165	52.3273781	-1053.4593982	15.1945681
3	1	51.9952219	52.1682169	-1044.5843170	15.1236349
4	1	-64.7506466	-64.3669805	-1639.9268283	-15.1401012

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-128.8462382	-127.3430701
2	1	23.6715867	23.5355523
3	1	-125.6061084	-127.0743492

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	253.0716585	244.0184910	-1835.7882508	105.0862302

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 13	LEVEL ID F13

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	67.5081565	63.5338366	-914.2648712	23.2552992
2	1	52.7248952	51.1806669	-1047.0479327	15.0907059
3	1	51.3366804	50.0753343	-903.5618592	15.9590789
4	1	-65.9121840	-62.3237026	-1512.3417691	-16.3358370

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-127.4812768	-126.0427153
2	1	23.3783999	23.0992768
3	1	-122.3899097	-123.7659720

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	287.3931153	141.0199782	-1706.7835678	89.3586151

MEMBER FORCES	FRAME ID 25-B,3-B BUILD.	FRAME TYPE 1
	LEVEL NO 14	LEVEL ID F14

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	63.8287841	59.9731202	-849.9553702	22.2238180
2	1	52.7318318	49.9394302	-1027.6333630	15.1169038
3	1	50.4669117	47.9539526	-775.2852215	16.6452118
4	1	-61.4569967	-57.8537880	-1385.5722839	-15.6017559

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-125.7113376	-124.0555448
2	1	23.0758846	22.6472393
3	1	-118.6620451	-120.2120071

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	316.3373594	58.8981428	-1577.5537614	77.6118241

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 15 LEVEL ID F15

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	78.7835357	61.8825535	-785.1782305	27.2557895
2	1	51.5696599	48.2480284	-992.0034654	14.9598832
3	1	48.8026962	45.5478841	-882.9889304	16.9078648
4	1	-74.9211337	-58.7550104	-1259.7130274	-20.7272953

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-121.1089357	-120.4274994
2	1	22.3444607	21.8640784
3	1	-113.4289933	-114.0403806

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	308.1120745	-29.5580425	-1448.1183483	54.5485839

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 16 LEVEL ID F16

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	55.9262385	42.3254000	-719.3682849	17.4758429
2	1	50.4649694	46.5133788	-948.8557786	14.8988570
3	1	45.9432048	42.7802177	-557.9986799	16.8785885
4	1	-51.1549338	-39.1192489	-1135.2798056	-11.3840063

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-114.3151992	-118.1803148
2	1	21.1381372	20.2552438
3	1	-104.8891573	-102.9388196

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	347.7003682	-51.0844645	-1318.4876511	61.1644109

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 17 LEVEL ID F17

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	59.9103448	58.3889597	-852.1777242	23.3258272
2	1	49.8280790	44.5592082	-898.8558040	14.9342190
3	1	43.0101562	38.4907087	-459.2755386	15.9745564
4	1	-52.7803289	-51.7816859	-1013.3263835	-16.4260714

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-113.0835140	-114.2180731
2	1	20.8322309	19.6483831
3	1	-98.5285837	-97.4848866

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	323.3107852	-125.2091384	-1188.3847488	38.1388069

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 18 LEVEL ID F18

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	58.8915457	53.1731892	-584.5900478	22.5319011
2	1	48.8239206	43.7547832	-833.1310389	15.3499866
3	1	40.2858317	35.8700243	-375.7142966	15.5463898

4	1	-49.3827314	-44.7245578	-892.8249522	-15.2272306
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BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-109.7722627	-111.2218500
2	1	19.9807175	18.5172892
3	1	-91.8758275	-90.8009548

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	307.7253704	-159.0189193	-1057.7398888	27.3439940

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 19 LEVEL ID F19

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	52.0100070	51.0807189	-518.2143116	21.1242113
2	1	47.8123798	42.8372118	-758.0133152	15.8115471
3	1	37.8497014	33.0727086	-301.0641982	15.0195424
4	1	-42.3382693	-41.2182233	-774.0153544	-13.8181752

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-108.5186771	-109.0881403
2	1	18.8498544	17.9246831
3	1	-86.3681048	-85.8182211

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	284.4858870	-181.8084428	-926.6928225	17.3250145

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 20 LEVEL ID F20

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	73.7288638	56.5088702	-447.4128638	28.8582449
2	1	45.7789233	41.5081062	-886.8526972	16.0093122
3	1	34.7878992	30.5817203	-242.1979815	14.2283985
4	1	-57.0314215	-43.4799518	-656.4823137	-18.4044774

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-99.4075405	-103.2740028
2	1	18.8034838	18.8008280
3	1	-78.4808199	-75.4533789

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	214.6425021	-218.5141177	-795.2443438	-7.8009240

MEMBER FORCES FRAME ID 25-B,3-B BUILD. FRAME TYPE 1
LEVEL NO 21 LEVEL ID F21

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	34.8695504	25.8808789	-378.7478587	11.8711859
2	1	41.5473829	38.8915958	-573.8388467	15.2504387
3	1	28.8814348	26.9120927	-184.7822090	12.3832584
4	1	-24.4927487	-18.4219574	-541.2505388	-6.1437285

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-76.9041784	-92.8881787
2	1	15.5150883	13.3657198
3	1	-83.3113989	-52.3589742

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		233.3798248	-163.4904834	-663.6007487	11.8509580

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 22 LEVEL ID F22

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	-41.1265136	-42.0246280	-301.9454014	18.3035085
2	1	40.4874381	35.5238995	-483.6788006	15.0232811
3	1	25.1024289	21.0842425	-123.9282581	10.5220381
4	1	-26.5882031	-27.8862275	-430.7917425	-10.0892356

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-80.3913117	-93.7825107
2	1	15.1371539	13.5148543
3	1	-58.4778405	-50.0819710

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		174.0942284	-193.0710751	-531.6559996	-9.1184522

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 23 LEVEL ID F23

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	40.2335294	39.2847981	-227.7148292	18.0492638
2	1	40.8777725	37.1279207	-377.3879168	16.4290124
3	1	22.6135660	19.9607594	-78.8660068	9.9880093
4	1	-23.7255189	-23.4837878	-321.2217660	-9.2299678

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-78.7140821	-92.5785148
2	1	15.7881730	12.7719144
3	1	-53.3597139	-45.2380359

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		115.4415359	-189.4335751	-399.0296823	-21.8965574

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 24 LEVEL ID F24

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	37.2311704	38.4805527	-153.1282038	17.7259599
2	1	37.3885924	36.1125694	-260.1848289	16.3276168
3	1	20.0437009	17.9742335	-43.9228372	9.1604943
4	1	-20.6908048	-21.5105170	-212.8872973	-8.8541837

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-82.8221048	-94.6481985
2	1	14.3011807	11.6892454
3	1	-51.2140003	-44.6961839

PANEL FORCES

I	COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1		49.8513138	-171.8735778	-265.9890328	-32.8684588

MEMBER FORCES FRAME ID 25-8,3-B BUILD. FRAME TYPE 1
 LEVEL NO 25 LEVEL ID F25

COLUMN FORCES

LINE	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
1	1	55.6114007	45.3909344	-79.2849917	24.6370207
2	1	53.5508018	42.9804254	-123.2126151	23.1793009
3	1	23.1991505	19.5010540	-28.1508431	10.4572001
4	1	-29.4357093	-24.1053790	-104.9085243	-12.5734161

BEAM FORCES

BAY	LOAD	I MOMENT	J MOMENT
1	1	-55.6114007	-78.1086658
2	1	24.5578640	18.6333343
3	1	-41.8324848	-29.4357093

PANEL FORCES

I COL	LOAD	TOP MOMENT	BOT MOMENT	AXIAL FORCE	SHEAR FORCE
2	1	-78.3257206	-175.3826905	-132.4430259	-64.4470401

CONVERGE IN ITERATION NO. 3

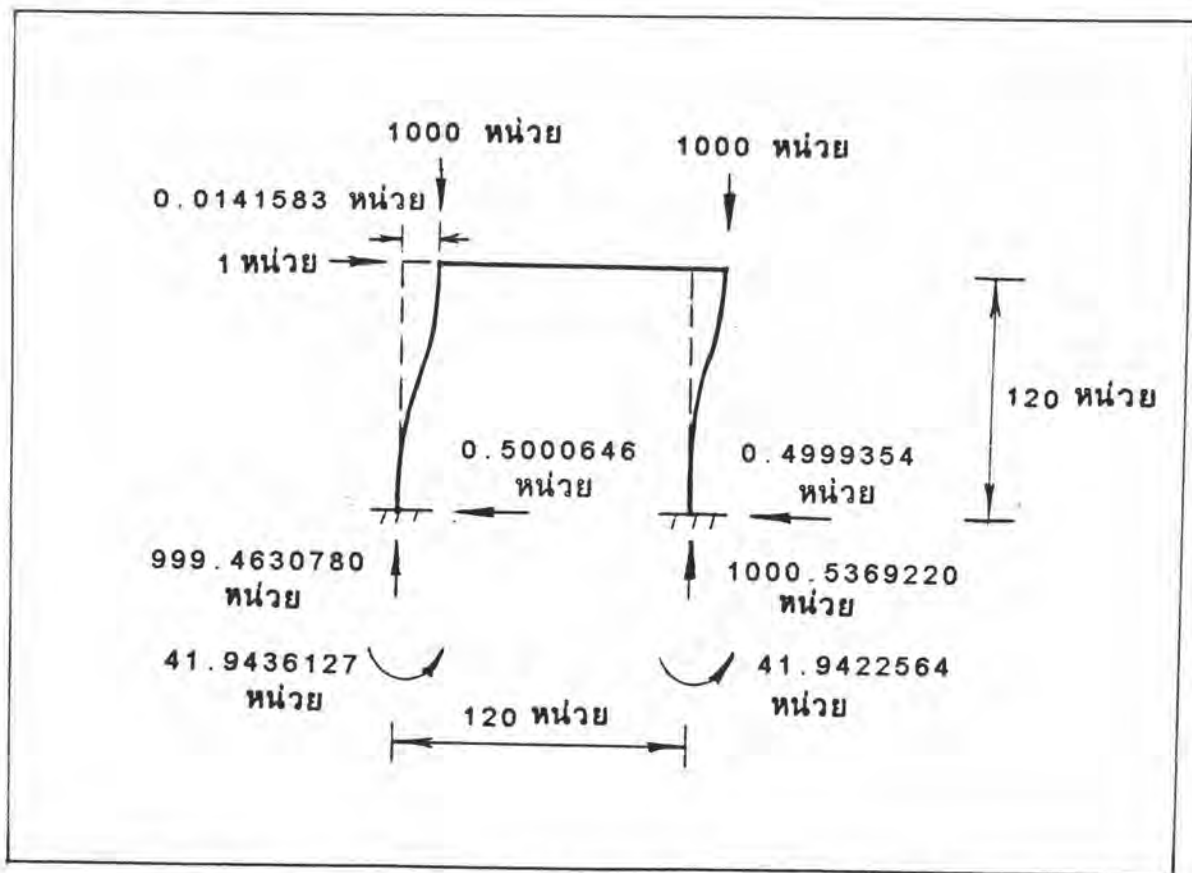
TOTAL TIME 280.73 SEC.



ภาคผนวก จ .

ตรวจสอบสมมูลย์ของโครงข้อแข็งพอร์ทอล

เลือกตรวจสอบสมมูลย์แรงภายในและภายนอกของโครงสร้างกรณี P เท่ากับ 1,000 หน่วย หลังจากเกิดการเปลี่ยนตำแหน่ง ไปทางขวาในแนวราบ เท่ากับ 0.0141583 หน่วย



รูป จ.1 สมมูลย์ของแรงที่กระทำกับโครงข้อแข็งพอร์ทอล

แรงในแนวดิ่ง

$$\begin{aligned}
 \text{ผลรวมแรงกระทำภายนอกในแนวดิ่ง} &= 1000.0000000 + 1000.0000000 \\
 &= 2000.0000000 \quad \text{หน่วยทิศทางลง} \\
 \text{ผลรวมแรงปฏิกิริยาที่ฐานรองรับในแนวดิ่ง} &= 999.4630780 + 1000.5369220 \\
 &= 2000.0000000 \quad \text{หน่วยทิศทางขึ้น}
 \end{aligned}$$

ฉนั้นแรงในแนวดิ่งอยู่ในสมดุลย์

แรงในแนวนราบ

$$\begin{aligned}
 \text{แรงกระทำภายนอกในแนวนราบ} &= 1.0000000 \quad \text{หน่วยทิศทางขวา} \\
 \text{ผลรวมแรงปฏิกิริยาที่ฐานรองรับในแนวนราบ} &= 0.5000646 + 0.4999354 \\
 &= 1.0000000 \quad \text{หน่วยทิศทางซ้าย}
 \end{aligned}$$

ฉนั้นแรงในแนวนราบอยู่ในสมดุลย์

แรงคัต

พิจารณาผลรวมแรงคัตที่ฐานรองรับด้านซ้ายของโครงข้อแข็งพอร์ทอล

1.) แรงคัตทิศทางตามเข็มนาฬิกาจากแรงกระทำด้านข้าง

$$\begin{aligned}
 &= 1.0000000 \times 120.0000000 \\
 &= 120.0000000 \quad \text{หน่วย}
 \end{aligned}$$

2.) แรงคัตทิศทางตามเข็มนาฬิกาจากแรงแนวดิ่งเสาดันซ้าย

$$\begin{aligned}
 &= 1000.0000000 \times 0.0141583 \\
 &= 14.1583000 \quad \text{หน่วย}
 \end{aligned}$$

3.) แรงคัตทิศทางตามเข็มนาฬิกาจากแรงแนวดิ่งเสาดันขวา

$$\begin{aligned}
 &= 1000.0000000 (120.0000000 + 0.0141583) \\
 &= 120,014.1583000 \quad \text{หน่วย}
 \end{aligned}$$

4.) แรงดัดทิศทางทวนเข็มนาฬิกาจากฐานรองรับด้านขวา

$$= 41.9422564 \quad \text{หน่วย}$$

5.) แรงดัดทิศทางทวนเข็มนาฬิกาจากแรงปฏิกิริยาในแนวตั้งจากฐานรองรับด้านขวา

$$= 1000.5369220 \times 120.0000000$$

$$= 120,064.4306400 \quad \text{หน่วย}$$

ผลรวมแรงดัดข้อ 1.) ถึง 5.) = 41.9437036 หน่วยทิศตามเข็มนาฬิกา

แรงดัดทวนเข็มนาฬิกาที่คำนวณได้โดยโปรแกรม CU-NTABS เท่ากับ 41.9436127 หน่วย มีความคลาดเคลื่อน 0.002% ซึ่งเกิดจากการตรวจสอบด้วยโปรแกรมนี้ ใช้ความละเอียดทศนิยม 7 ตำแหน่ง ในขณะที่โปรแกรม CU-NTABS ใช้ความละเอียดทศนิยม 15 ตำแหน่ง

ภาคผนวก ฉ

รายละเอียดโปรแกรมคำนวณไม่เชิงเส้นแบบนิวตัน-ราฟสัน

```

C*****
C
C
C          TP484.FOR *
C by Vicram Panichacarn
C First Written   June 23rd,1993
C Complete       October 20th,1994
C
C*****
C
C  MAIN PROGRAM
C
  CHARACTER*32 INPUTF,OUTPUT
  DOUBLE PRECISION SST(15,15),SSL(15,15),BSG(15,15),PEB(15,1),
  1  PRB(15,1),PDEL(15,1),QB(15,1),QDEL(15,1),
  2  BSGO,TI,TA,TE,TL,NORM,SML(6,6),SMG(6,6),PI,
  3  SMT(6,6),PRM(6,1),QM(6,1),QMB,QME,ZETA,TM(6,6),KA(6,6)
WRITE (*,*) '-----'
WRITE (*,*) ' Problem 4 -
WRITE (*,*) '-----'
WRITE (*,'(A1)') ' INPUT fn.ft <ret>'
READ (*,'(A32)') INPUTF
WRITE (*,'(A1)') ' OUTPUT fn.ft <ret>'
READ (*,'(A32)') OUTPUTF
OPEN (5,FILE=INPUTF,STATUS='OLD')
OPEN (6,FILE=OUTPUT,STATUS='UNKNOWN')
C-----READ CONSTANTS
  READ (5,205) TI,TA,TE,TL
C-----READ STRUCTURAL EXTERNAL APPLIED FORCE MATRIX
READ (5,200) IROWA,ICOLA
DO 302 I = 1,IROWA
  302 READ (5,205) (PEB(I,J),J=1,ICOLA)
  200 FORMAT (2I5)
  205 FORMAT (6D20.14)
C-----INITIALIZE STRUCTURAL DISPLACEMENT MATRIX
DO 320 I = 1,15
  320 QB(I,1) = 0.
C-----INITIALIZE STRUCTURAL LINEAR STIFFNESS MATRIX
DO 395 I = 1,15
  DO 390 J = 1,15
  390 SSL(I,J) = 0.
  395 CONTINUE
C-----EVALUATE STRUCTURAL LINEAR STIFFNESS MATRIX
  SSL(1,1) = (24*TE*TI)/(TL*TL*TL)
  SSL(1,4) = (-12*TE*TI)/(TL*TL*TL)
  SSL(1,6) = (-6*TE*TI)/(TL*TL)
  SSL(2,2) = (2*TA*TE)/TL
  SSL(2,5) = (-1*TA*TE)/TL
  SSL(3,3) = (8*TE*TI)/TL
  SSL(3,4) = (6*TE*TI)/(TL*TL)
  SSL(3,6) = (2*TE*TI)/TL
  SSL(4,1) = SSL(1,4)
  SSL(4,3) = SSL(3,4)
  SSL(4,4) = ((TA*TE)/TL)+((12*TE*TI)/(TL*TL*TL))
  SSL(4,6) = (6*TE*TI)/(TL*TL)
  SSL(4,7) = (-1*TA*TE)/TL
  SSL(5,2) = SSL(2,5)
  SSL(5,5) = ((TA*TE)/TL)+((12*TE*TI)/(TL*TL*TL))
  SSL(5,6) = (6*TE*TI)/(TL*TL)
  SSL(5,8) = (-12*TE*TI)/(TL*TL*TL)
  SSL(5,9) = (6*TE*TI)/(TL*TL)
  SSL(6,1) = SSL(1,6)
  SSL(6,3) = SSL(3,6)
  SSL(6,4) = SSL(4,6)
  SSL(6,5) = SSL(5,6)
  SSL(6,8) = (8*TE*TI)/TL
  SSL(6,8) = (-6*TE*TI)/(TL*TL)
  SSL(6,9) = (2*TE*TI)/TL
  SSL(7,4) = SSL(4,7)
  SSL(7,7) = (2*TA*TE)/TL
  SSL(7,10) = SSL(4,7)

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BBL(8,5) = BBL(5,8)
BBL(8,6) = BBL(6,8)
BBL(8,8) = (24*TE*T1)/(TL*TL*TL)
BBL(8,11) = BBL(5,8)
BBL(8,12) = BBL(5,9)
BBL(9,5) = BBL(5,9)
BBL(9,8) = BBL(6,9)
BBL(9,9) = (8*TE*T1)/TL
BBL(9,11) = BBL(8,8)
BBL(9,12) = BBL(8,9)
BBL(10,7) = BBL(7,10)
BBL(10,10) = BBL(4,4)
BBL(10,12) = BBL(4,6)
BBL(10,13) = BBL(1,4)
BBL(10,15) = (8*TE*T1)/(TL*TL)
BBL(11,8) = BBL(8,11)
BBL(11,9) = BBL(9,11)
BBL(11,11) = BBL(5,5)
BBL(11,12) = (-6*TE*T1)/(TL*TL)
BBL(11,14) = BBL(2,5)
BBL(12,8) = BBL(8,12)
BBL(12,9) = BBL(9,12)
BBL(12,10) = BBL(10,12)
BBL(12,11) = BBL(11,12)
BBL(12,12) = BBL(3,3)
BBL(12,13) = (-6*TE*T1)/(TL*TL)
BBL(12,15) = BBL(3,8)
BBL(13,10) = BBL(10,13)
BBL(13,12) = BBL(12,13)
BBL(13,13) = BBL(1,1)
BBL(14,11) = BBL(11,14)
BBL(14,14) = BBL(2,2)
BBL(15,10) = BBL(10,15)
BBL(15,12) = BBL(12,15)
BBL(15,15) = BBL(3,3)
C----BEGIN LOOP
IJ = 1
  330WRITE (6,*) 'LOOP NO. ',IJ
C----INITIALIZE STRUCTURAL GEOMETRICALLY STIFFNESS MATRIX
DO 310 I = 1,15
DO 305 J = 1,15
  305 BBS(I,J) = 0.
  310 CONTINUE
C----EVALUATE STRUCTURAL GEOMETRICALLY STIFFNESS MATRIX
BSCC = (TA*TE)/(30*TL*TL)
BSG(1,1) = BSCC*36*QB(5,1)
BSG(1,3) = BSCC*3*TL*(2*QB(2,1)-QB(5,1))
BSG(1,4) = BSCC*(-36)*(QB(5,1)-QB(2,1))
BSG(1,6) = BSCC*(-3)*TL*(QB(5,1)-QB(2,1))
BSG(3,1) = BSG(1,3)
BSG(3,3) = BSCC*4*TL*TL*QB(5,1)
BSG(3,4) = BSCC*3*TL*(QB(5,1)-QB(2,1))
BSG(3,6) = BSCC*(-1)*TL*TL*(QB(5,1)-QB(2,1))
BSG(4,1) = BSG(1,4)
BSG(4,3) = BSG(3,4)
BSG(4,4) = BSCC*36*(QB(5,1)-QB(2,1))
BSG(4,6) = BSCC*3*TL*(QB(5,1)-QB(2,1))
BSG(5,5) = BSCC*36*(QB(7,1)-QB(4,1))
BSG(5,8) = BSCC*3*TL*(QB(7,1)-QB(4,1))
BSG(5,8) = -1*BSG(5,5)
BSG(5,9) = BSG(5,8)
BSG(6,1) = BSG(1,8)
BSG(6,3) = BSG(3,8)
BSG(6,4) = BSG(4,8)
BSG(6,5) = BSG(5,8)
BSG(6,8) = BSCC*4*TL*TL*(QB(5,1)-QB(2,1)+QB(7,1)-QB(4,1))
BSG(6,8) = -1*BSG(5,9)
BSG(6,9) = BSCC*(-1)*TL*TL*(QB(7,1)-QB(4,1))
BSG(8,5) = BSG(5,8)
BSG(8,8) = BSG(6,8)
BSG(8,8) = BSCC*36*(QB(10,1)-QB(4,1))

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880(8,9) = 8000*(-3)*TL*(2*QB(7,1)-QB(4,1)-QB(10,1))
880(8,11) = 8000*(-36)*(QB(10,1)-QB(7,1))
880(8,12) = 8000*3*TL*(QB(10,1)-QB(7,1))
880(9,5) = 880(5,9)
880(9,6) = 880(6,9)
880(9,8) = 880(8,9)
880(9,9) = 8000*4*TL*TL*(QB(10,1)-QB(4,1))
880(9,11) = -1*880(8,12)
880(9,12) = 8000*(-1)*TL*TL*(QB(10,1)-QB(7,1))
880(10,10) = 8000*36*(QB(11,1)-QB(14,1))
880(10,12) = 8000*3*TL*(QB(11,1)-QB(14,1))
880(10,13) = 8000*(-36)*(QB(11,1)-QB(14,1))
880(10,15) = 8000*3*TL*(QB(11,1)-QB(14,1))
880(11,8) = 880(8,11)
880(11,9) = 880(9,11)
880(11,11) = 8000*36*(QB(10,1)-QB(7,1))
880(11,12) = 8000*(-3)*TL*(QB(10,1)-QB(7,1))
880(12,8) = 880(8,12)
880(12,9) = 880(9,12)
880(12,10) = 880(10,12)
880(12,11) = 880(11,12)
880(12,12) = 8000*4*TL*TL*(QB(10,1)-QB(7,1)+QB(11,1)-QB(14,1))
880(12,13) = -1*880(10,15)
880(12,15) = 8000*(-1)*TL*TL*(QB(11,1)-QB(14,1))
880(13,10) = 880(10,13)
880(13,12) = 880(12,13)
880(13,13) = 8000*36*QB(11,1)
880(13,15) = 8000*(-3)*TL*(QB(11,1)-2*QB(14,1))
880(15,10) = 880(10,15)
880(15,12) = 880(12,15)
880(15,13) = 880(13,15)
880(15,15) = 8000*4*TL*TL*QB(11,1)
C-----ADDITION FOR TOTAL STRUCTURAL STIFFNESS MATRIX
CALL PLUS (SSL,15,15,880,88T)
C-----FIND STRUCTURAL INTERNAL RESISTING FORCE
CALL MULTIP (88T,15,15,QB,15,1,PR8)
C-----FIND DELTA FORCE
DO 380 I = 1,15
  380PDEL(I,1) = PES(I,1) - PR8(I,1)
  NORM = PDEL(4,1)/PES(4,1)
WRITE (6,*) 'NORM ',NORM
C-----FIND DELTA DISPLACEMENT
CALL GAUSS (88T,15,15,PDEL,15,1,QDEL)
C-----FIND NEW STRUCTURAL DISPLACEMENT
CALL PLUS (QB,15,15,QDEL,QB)
IF ( NORM .LE. .1D-3) GOTO 385
IJ = IJ + 1
GOTO 330
C====DETERMINE MEMBER FORCES
385 CALL DISPLY (QB,15,1)
  II = 1
  PI = 3.141592654
415 IF ( II .EQ. 1 ) THEN
  DO 450 I = 1,6
450   QM(I,1) = QB(I,1)
      QME = QM(5,1)
      QMS = QM(2,1)
      IM = 2
      ZETA = PI/2.0
  ELSEIF (II .EQ. 2 ) THEN
  DO 455 I = 1,6
455   QM(I,1) = QB(I+6,1)
      QME = QM(4,1)
      QMS = QM(1,1)
      IM = 4
      ZETA = 0.0
  ELSE
  DO 460 I = 1,6
460   QM(I,1) = QB(I+9,1)
      QME = QM(2,1)
      QMS = QM(5,1)

```



```

      IM = 5
      ZETA = 1.5*PI
    ENDIF
C-----INITIALIZE MEMBER LINEAR STIFFNESS MATRIX
    DO 400 I = 1,6
      DO 400 J = 1,6
        400   BML(I,J) = 0.0
C-----EVALUATE MEMBER LINEAR STIFFNESS MATRIX
      BML(1,1) = TE*TA/TL
      BML(1,4) = (-1)*BML(1,1)
      BML(2,2) = (12*TE*T1)/(TL*TL*TL)
      BML(2,3) = (6*TE*T1)/(TL*TL)
      BML(2,5) = (-1)*BML(2,2)
      BML(2,6) = BML(2,3)
      BML(3,2) = BML(2,3)
      BML(3,3) = (4*TE*T1)/TL
      BML(3,5) = (-1)*BML(2,3)
      BML(3,6) = (2*TE*T1)/TL
      BML(4,1) = BML(1,4)
      BML(4,4) = BML(1,1)
      BML(5,2) = BML(2,5)
      BML(5,3) = BML(3,5)
      BML(5,5) = BML(2,2)
      BML(5,6) = (-1)*BML(2,3)
      BML(6,2) = BML(2,6)
      BML(6,3) = BML(3,6)
      BML(6,5) = BML(5,6)
      BML(6,6) = BML(3,3)
C-----INITIALIZE MEMBER GEOMETRICALLY STIFFNESS MATRIX
    DO 405 I = 1,6
      DO 405 J = 1,6
        405   SMG(I,J) = 0.0
C-----EVALUATE MEMBER GEOMETRICALLY STIFFNESS MATRIX
      SGCO = (TA*TE*(QME-QMS))/(30*TL*TL)
      SMG(2,2) = SGCO*36
      SMG(2,3) = SGCO*3*TL
      SMG(2,5) = (-1)*SMG(2,2)
      SMG(2,6) = SMG(2,3)
      SMG(3,2) = SMG(2,3)
      SMG(3,3) = SGCO*4*TL*TL
      SMG(3,5) = (-1)*SMG(2,3)
      SMG(3,6) = SGCO*(-1)*TL*TL
      SMG(5,2) = SMG(2,5)
      SMG(5,3) = SMG(3,5)
      SMG(5,5) = SMG(2,2)
      SMG(5,6) = (-1)*SMG(2,3)
      SMG(6,2) = SMG(2,6)
      SMG(6,3) = SMG(3,6)
      SMG(6,5) = SMG(5,6)
      SMG(6,6) = SMG(3,3)
C-----ADDITION FOR MEMBER TOTAL STIFFNESS MATRIX
      CALL PLUS(BML,6,6,SMG,6,6)
C-----INITIALIZE TRANSFORMATION MATRIX
    DO 410 I = 1,6
      DO 410 J = 1,6
        410   TM(I,J) = 0.0
C-----EVALUATE TRANSFORMATION MATRIX
      TM(1,1) = COS(ZETA)
      TM(1,2) = SIN(ZETA)
      TM(2,1) = (-1)*TM(1,2)
      TM(2,2) = TM(1,1)
      TM(3,3) = 1.0
      TM(4,4) = TM(1,1)
      TM(4,5) = TM(1,2)
      TM(5,4) = TM(2,1)
      TM(5,5) = TM(2,2)
      TM(6,6) = TM(3,3)
C-----k*s MATRIX
      CALL MULTIP(BMT,6,6,TM,6,6,KA)
C-----FIND MEMBER FORCES
      CALL MULTIP(KA,6,6,QM,6,1,PRM)

```

```

WRITE (6,*) ' ---- MEMBER FORCES OF MEMBER NO. ',IM,' ---- '
WRITE (6,*) '     NODE I AXIAL = ',PRM(1,1)
WRITE (6,*) '     NODE I SHEAR = ',PRM(2,1)
WRITE (6,*) '     NODE I MOMENT = ',PRM(3,1)
WRITE (6,*) '     NODE J AXIAL = ',PRM(4,1)
WRITE (6,*) '     NODE J SHEAR = ',PRM(5,1)
WRITE (6,*) '     NODE J MOMENT = ',PRM(6,1)
II = II + 1
IF ( II .EQ. 4 ) GO TO 420
GOTO 415
420 STOP
END
C
SUBROUTINE PLUS(VA, IROWVA, ICOLVA, VB, VC)
C
DOUBLE PRECISION VA(IROWVA, ICOLVA), VB(IROWVA, ICOLVA),
1 VC(IROWVA, ICOLVA)
DO 5 I = 1, IROWVA
DO 5 J = 1, ICOLVA
5 VC(I, J) = VA(I, J) + VB(I, J)
RETURN
END
C
SUBROUTINE MINUS(VA, IROWVA, ICOLVA, VB, VC)
C-----
CThis is a subprogram for matrix subtraction A - B = C
CVA(20,20) is local matrix A dimension 20 * 20
CVB(20,20) is local matrix B dimension 20 * 20
C VC(20,20) is local result matrix C dimension 20 * 20
C-----
DOUBLE PRECISION VA(20,20), VB(20,20), VC(20,20)
DO 20 I = 1, IROWVA
DO 15 J = 1, ICOLVA
15 VC(I, J) = VA(I, J) - VB(I, J)
20 CONTINUE
WRITE (*,*) 'SUBTRACTION COMPLETE'
RETURN
END
C
SUBROUTINE MULTIP(VA, IROWVA, ICOLVA, VB, IROWVB, ICOLVB, VC)
C-----
CThis is a subprogram for matrix multiplication VA * VB = VC
CIROWVA is number of row of matrix VA
CICOLVA is number of column of matrix VA
C IROWVB is number of row of matrix VB
CICOLVB is number of column of matrix VB
C-----
DOUBLE PRECISION VA(IROWVA, ICOLVA), VB(IROWVB, ICOLVB),
1 VC(IROWVA, ICOLVB)
IF ( ICOLVA.NE.IROWVB) GOTO 40
DO 35 I = 1, IROWVA
DO 30 J = 1, ICOLVB
VC(I, J) = 0.
DO 25 K = 1, IROWVB
25 VC(I, J) = VC(I, J) + (VA(I, K)*VB(K, J))
30 CONTINUE
35 CONTINUE
WRITE (*,*) 'MULTIPLICATION COMPLETE'
GOTO 45
40 WRITE (*,*) 'COLUMN 1ST .NE. ROW 2ND'
45RETURN
END
C
SUBROUTINE GAUSS(VA, IROWVA, ICOLVA, VB, IROWVB, ICOLVB, VX)
C-----
CThis is a subprogram for elimination of linear equation by
CGaussian Method : VA * VX = VB
CICOLVA is number of column of matrix VA
C-----
DOUBLE PRECISION VA(IROWVA, ICOLVA), VB(IROWVB, ICOLVB),
1 VX(IROWVB, ICOLVB), BUM

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C.... FORWARD REDUCTION .....
DO 60 J = 1,ICOLVA
DO 55 I = J+1,ICOLVA
CO = -VA(I,J)/VA(J,J)
VB(I,1) = VB(I,1)+(VB(J,1)*CO)
DO 50 K = J,ICOLVA
  50 VA(I,K) = VA(I,K)+(VA(J,K)*CO)
  55 CONTINUE
  60 CONTINUE

C.... BACK SUBSTITUTION .....
VX(ICOLVA,1) = VB(ICOLVA,1)/VA(ICOLVA,ICOLVA)
DO 70 K = ICOLVA-1,1,-1
SUM = 0.
DO 65 I = K+1,ICOLVA
  65 SUM = SUM+(VA(K,I)*VX(I,1))
  70 VX(K,1) = (VB(K,1)-SUM)/VA(K,K)
WRITE (*,*) 'ELIMINATION COMPLETE'
RETURN
END
C
SUBROUTINE DISPLY(VA,IROWA,ICOLVA)
C-----
CThis is a subprogram for displaying matrix on datafile or screen.
C-----
DOUBLE PRECISION VA(IROWA,ICOLVA)
WRITE (6,*) ' '
  DO 75 I = 1,IROWA
    75 WRITE (6,100) (VA(I,J),J=1,ICOLVA)
  100 FORMAT (6D20.14)
RETURN
END

```

เพิ่มป้อนข้อมูลและเพิ่มแสดงผลการคำนวณ

กรณีแรง $P = 1000$ หน่วย

LOOP NO. 1
NORM 1.00000000000000
LOOP NO. 2
NORM 1.115822992264838E-001
LOOP NO. 3
NORM -1.572163086072109E-005

.59895630998348D-02
- .16983229862570D+00
- .18058856339340D-03
.14242922007700D-01
- .33986459725139D+00
- .73011983582340D-04
.14158300678441D-01
- .33986843227288D+00
.31588484428679D-04
.14073879349182D-01
- .34002954038867D+00
- .71587776170637D-04
.59269808842467D-02
- .17001477019334D+00
- .15882311117136D-03

---- MEMBER FORCES OF MEMBER NO. 2 ----

NODE I AXIAL = 999.463079535329800
NODE I SHEAR = 5.019997889188185E-001
NODE I MOMENT = 8.043352791399367
NODE J AXIAL = -999.463079535329800
NODE J SHEAR = -5.019997889188185E-001
NODE J MOMENT = 32.325554617140170

---- MEMBER FORCES OF MEMBER NO. 4 ----

NODE I AXIAL = 4.979965226903457E-001
NODE I SHEAR = -5.369225877878022E-001
NODE I MOMENT = -1.104152177897729E-001
NODE J AXIAL = -4.979965226903457E-001
NODE J SHEAR = 5.369225877878022E-001
NODE J MOMENT = -32.104859818218450

---- MEMBER FORCES OF MEMBER NO. 5 ----

NODE I AXIAL = 1000.538928874776000
NODE I SHEAR = 4.979854461720258E-001
NODE I MOMENT = 32.104518359880320
NODE J AXIAL = -1000.538928874776000
NODE J SHEAR = -4.979854461720258E-001
NODE J MOMENT = 5.925660715081342

แฟ้มป้อนข้อมูลและแฟ้มแสดงผลการคำนวณ

กรณีแรง $P = 2000$ หน่วย

15	1	310.1	11.77	30000.0	60.0	387
		0.0				
		0.0				
		0.0				
		2.0				
		-2000.0				
		0.0				
		0.0				
		0.0				
		0.0				
		0.0				
		-2000.0				
		0.0				
		0.0				
		0.0				
		0.0				

LOOP NO. 1
 NORM 1.000000000000000
 LOOP NO. 2
 NORM 2.231848278331246E-001
 LOOP NO. 3
 NORM -1.17898229899709E-004

.16224454143889D-01
 -.33959916077236D+00
 -.43998587013333D-03
 .38800612370503D-01
 -.67919832154473D+00
 -.19790007794075D-03
 .38631162247854D-01
 -.87973743588464D+00
 .85834838396063D-04
 .38461712124804D-01
 -.68018995373140D+00
 -.19501362101515D-03
 .16101001813180D-01
 -.34009497886570D+00
 -.43645045798414D-03

---- MEMBER FORCES OF MEMBER NO. 2 ----

NODE I AXIAL = 1998.541086952879000
 NODE I SHEAR = 1.002778948193035
 NODE I MOMENT = 17.526733122493140
 NODE J AXIAL = -1998.541086952879000
 NODE J SHEAR = -1.002778948193035
 NODE J MOMENT = 87.759353321245540

---- MEMBER FORCES OF MEMBER NO. 4 ----

NODE I AXIAL = 9.972139729683733E-001
 NODE I SHEAR = -1.458938855057545
 NODE I MOMENT = -2.237887214961978E-001
 NODE J AXIAL = -9.972139729683733E-001
 NODE J SHEAR = 1.458938855057545
 NODE J MOMENT = -87.312093324835500

---- MEMBER FORCES OF MEMBER NO. 5 ----

NODE I AXIAL = 2001.458956110939000
 NODE I SHEAR = 9.971927085286314E-001
 NODE I MOMENT = 87.311410385863180
 NODE J AXIAL = -2001.458956110939000
 NODE J SHEAR = -9.971927085286314E-001
 NODE J MOMENT = 17.27410839883830

15 1

310.1

11.77

30000.0

60.0

390

0.0
0.0
0.0
3.0
-3000.0
0.0
0.0
0.0
0.0
0.0
-3000.0
0.0
0.0
0.0
0.0

LOOP NO. 1
 NORM 1.000000000000000
 LOOP NO. 2
 NORM 3.347469580997892E-001
 LOOP NO. 3
 NORM -8.810751589894251E-004

.38037573600512D-01
 .50918694791562D+00
 -.10440762626192D-02
 .91540918208438D-01
 -.10183738958312D+01
 -.46472755938725D-03
 .91286696694939D-01
 -.10196072233038D+01
 .20208720735621D-03
 .91032475181440D-01
 -.10207085170829D+01
 -.46032664887203D-03
 .37854623890007D-01
 -.51035425854147D+00
 -.10387975431772D-02

---- MEMBER FORCES OF MEMBER NO. 2 ----

NODE I AXIAL = 2996.585202246725000
 NODE I SHEAR = 1.503898211132425
 NODE I MOMENT = 44.132247290447940
 NODE J AXIAL = -2996.585202246725000
 NODE J SHEAR = -1.503898211132425
 NODE J MOMENT = 208.427718801684500

---- MEMBER FORCES OF MEMBER NO. 4 ----

NODE I AXIAL = 1.496093606941263
 NODE I SHEAR = -3.434811523588612
 NODE I MOMENT = -3.412086458550178E-001
 NODE J AXIAL = -1.496093606941263
 NODE J SHEAR = 3.434811523588612
 NODE J MOMENT = -205.745835130879800

---- MEMBER FORCES OF MEMBER NO. 5 ----

NODE I AXIAL = 3003.434852555189000
 NODE I SHEAR = 1.496063050276878
 NODE I MOMENT = 205.744810246548300
 NODE J AXIAL = -3003.434852555189000
 NODE J SHEAR = -1.496063050276878
 NODE J MOMENT = 43.734982136557730

เพิ่มป้อนข้อมูลและเพิ่มแสดงผลการคำนวณ

กรณีแรง $P = 3000$ หน่วย

เพิ่มป้อนข้อมูลและเพิ่มแสดงผลการคำนวณ

กรณีแรง $P = 4000$ หน่วย

15 1

310.1

11.77

30000.0

60.0

393

0.0
0.0
0.0
4.0
-4000.0
0.0
0.0
0.0
0.0
0.0
-4000.0
0.0
0.0
0.0
0.0

```

LOOP NO.      1
NORM         1.000000000000000
LOOP NO.      2
NORM        4.463292844464205E-001
LOOP NO.      3
NORM       -6.609929083135940E-003

```

```

.11887276360474D+00
-.67786003330427D+00
-.33050165016365D-02
.28808732360110D+00
-.13557200666088D+01
-.14564892512868D-02
.28775213338329D+00
-.13594785681884D+01
.63506152916819D-03
.28741894318559D+00
-.13630564839437D+01
-.14504701115114D-02
.11882039391346D+00
-.88152824197185D+00
-.32984244124165D-02

```

---- MEMBER FORCES OF MEMBER NO. 2 ----

```

NODE I AXIAL = 3989.206339524666000
NODE I SHEAR = 2.027392553089967
NODE I MOMENT = 148.594244108347000
NODE J AXIAL = -3989.206339524666000
NODE J SHEAR = -2.027392553089967
NODE J MOMENT = 648.080978987684400

```

---- MEMBER FORCES OF MEMBER NO. 4 ----

```

NODE I AXIAL = 1.972594431166230
NODE I SHEAR = -10.793704251498290
NODE I MOMENT = -4.664873087285185E-001
NODE J AXIAL = -1.972594431166230
NODE J SHEAR = 10.793704251498290
NODE J MOMENT = -647.148710003471400

```

---- MEMBER FORCES OF MEMBER NO. 5 ----

```

NODE I AXIAL = 4010.793834268770000
NODE I SHEAR = 1.972555476214682
NODE I MOMENT = 647.147050538432800
NODE J AXIAL = -4010.793834268770000
NODE J SHEAR = -1.972555476214682
NODE J MOMENT = 148.214056581340500

```

ประวัติผู้เขียน



นายวิกรม พนิชการ เกิดวันเสาร์ที่ 23 ธันวาคม 2510 จังหวัดนครสวรรค์
สำเร็จการศึกษาวิศวกรรมศาสตรบัณฑิต(โยธา) จากภาควิชาวิศวกรรมโยธา คณะ
วิศวกรรมศาสตร์ มหาวิทยาลัยเชียงใหม่ ในปีพ.ศ. 2532