PREDICTION OF GASOLINE EMISSION

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วัตถุประสงค์ของงานวิจัยนี้ เพื่อศึกษาการปลดปล่อยของไอน้ำมันจากถังเก็บ และ ประเมินแบบจำลองที่สามารถใช้คาดคะเนการปลดปล่อยนี้ ในการทดลองนี้ใช้น้ำมันไร้สารตะกั่ว มีค่าออกเทน 95 ถังเก็บจำลองทำด้วยแก้วมีเส้นผ่านสูนย์กลางภายนอก 8±0.5 เซนติเมตร ความสูง 10±0.5 เซนติเมตร และปริมาตร 410±15 มิลลิเมตร ถังเก็บมีท่อระบายซึ่งมีเส้นผ่านสูนย์กลางภาย ใน 0.5 เซนติเมตร และเปลี่ยนความสูงได้จาก 15, 30 และ 45 เซนติเมตร ผลจากการทดลองแสดง ให้เห็นถึงปริมาณการปลดปล่อยของน้ำมันเพิ่มขึ้นเมื่อเพิ่มอุณหภูมิและความสูงของท่อระบายลด ลง ปริมาตรน้ำมันเริ่มต้นในถังเก็บมีผลกระทบน้อยมากต่อการปลดปล่อยของน้ำมัน พื้นฐานของ แบบจำลองที่เสนอในงานวิจัยนี้ประกอบด้วย การแพร่ของไอน้ำมัน, การขยายตัวของน้ำมัน และ การขยายตัวของใอของน้ำมัน การคาดคะเนจากแบบจำลองในงานวิจัยนี้ให้ผลที่สอดคล้องด้วยดี กับข้อมูลที่ได้จากการทดลองเมื่อเปรียบเทียบกับแบบจำลองอื่นที่ได้รับการยอมรับ

ABSTRACT

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The purpose of this study was to investigate the emission of gasoline vapor from storage tanks and to evaluate the best model that can be used to predict this emission. Unleaded gasoline with 95 octane number was used in this experiment. In this experimental study, a simulated storage tank was made of glass with 8±0.5 cm outside diameter, 10±0.5 cm in height and 410±15 ml in volume. It had a release vent tube having 0.5 cm inside diameter and variable height from 15, 30 and 45cm. The experimental results showed that the amount of gasoline emission increased with increasing temperature and decreasing vent height. Initial gasoline volume had very little effect on the gasoline emission rate. The model proposed in this work was derived by recognizing that the emission consists of diffusion, liquid expansion and vapor expansion of gasoline. The predictions from the model gave exceptionally good agreement with the experimental data in comparison with two well-known published models.

V

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LIST OF SYMBOLS

A = vent cross-sectional area

D =tank diameter

 D_G = molar diffusivity of gasoline to air

 D_W = molar diffusivity of water to air

 H_{VO} = vapor space outage

I = daily total solar insolation factor

 J_{AZ} = molar flux of component A in z direction

 K_E = vapor space expansion factor

 K_S = vented vapor saturation factor

 L_D = loss from diffusion

 L_{LE} = losses from liquid expansion

 L_{VE} = loss from vapor expansion

 L_S = standing storage loss

 M_A = molecular weight of air

 M_V = vapor molecular weight

 M_G = molecular weight of gasoline

 M_W = molecular weight of water

 P_A = atmospheric pressure

 P_{BP} = breather vent pressure setting

 P_{BV} = breather vent vacuum setting

 P_{VA} = true vapor pressure

 P_{VN} = vapor pressure at minimum liquid temperature

 P_{VX} = vapor pressure at maximum liquid temperature

 ΔP_B = breather vent pressure setting range

 ΔP_V = daily vapor pressure range

R = the ideal gas constant

 T_{AA} = daily average ambient temperature

 T_{AN} = daily minimum ambient temperature

 T_{AX} = daily maximum ambient temperature

 T_B = liquid bulk temperature

 T_{L4} = daily average liquid surface temperature

 ΔT_A = daily ambient temperature range

 ΔT_V = daily temperature range

 V_L = volume of liquid gasoline

 V_V = vapor space volume

 W_V = vapor density

 $y_{gasoline final}$ = final vapor mole fraction of gasoline

 $y_{gasoline initial}$ = initial vapor mole fraction of gasoline

 Δz = vent height

 α = thermal expansion coefficient

 α_A = tank paint solar absorbance

 α_L = liquid expansion coefficient

 α_V = vapor expansion coefficient

 Σv_A group contribution value for air

 Σv_W = group contribution value for water