

CHAPTER I

INTRODUCTION

Carbon dioxide (CO₂) is part of the greenhouse gases (GHGs) which continue to cause damaging effect to the global environment. CO₂ is produced from fossil fuels during post combustion, pre-combustion, oxyfuel, and industrial processes. CO₂ is not the most severe GHG, but it's the highest emitted which makes it the most unavoidable anthropogenic GHG (Kangwanwatana *et al.*, 2013). Capture of CO₂ through absorption is known as one of the most reliable and economical processes (Singh *et al.*, 2009). More so, with the advent of CO₂ enhanced oil recovery (EOR), several research studies are underway to develop oil reserves more economically (Nonthanasin *et al.*, 2013).

Most commonly used solvents are the conventional amines covering primary alkanolamines; monoethanolamine (MEA) and diglycolamine (DGA), secondary alkanolamines; diethanolamine (DEA) and diisopropanolamine (DIPA) and tertiary alkanolamines; methyldiethanolamine (MDEA) and triethanolamine (TEA). Other amines classified as a sterically hindered amine like 2-amino-2-methyl-1-propanol (AMP) and cyclic diamine, piperazine (PZ) are also available commercially.

In recent times, amine solvents have been promoted for CO₂ capture to utilize the merit of high reaction rate of CO₂ with the promoting agent(s), which can be blended with the merits of the high loading capacity of tertiary amines or hindered amines and the relatively low cost of regeneration of the promoting solvent (Balsora, and Mondal, 2011). The highly reactive cyclic diamine PZ and the reactive MEA have both been used as potential promoters (activators), and research on this combination is available in literature and commercial application (Yang *et al.*, 2010; Bruder *et al.*, 2011; Samanta and Bandyopadhyay, 2009; Austgen *et al.*, 1991; Mandal *et al.*, 2001; Dash and Bandyopadhyay, 2013; Bishnoi, 2000)

The success recorded by blending two solvents to enhance CO₂ capture, is gradually leading to ternary and quaternary amine blends (Haghtalab *et al.*, 2014; Esmaeili and Roozbehani, 2014). This research work is then focused on the equilibrium solubility of CO₂ in the novel ternary blend of AMP based solvent promoted with PZ – MEA blends. This was experimentally studied and investigated consider-

ing the absorption temperature range 25 – 60 °C, CO₂ partial pressure range 2 – 100 kPa. At 40 °C and 93.93 kPa CO₂ partial pressure, the concentrations of PZ and MEA promoters were varied between 0.5 M – 1 M and 2 – 4 M, respectively, while the AMP concentration was kept constantly at 2 M. This high concentration of the AMP-PZ-MEA ternary blend was chosen for experimental investigation because it leads to an increase in the absorption working capacity (aWC). Several researchers (Freeman *et al.*, 2010b; Bruder and Svendsen, 2012; Aboudheira *et al.*, 2003; Dugas and Rochelle, 2009; Yang *et al.*, 2010) have successfully studied CO₂ solubility in high concentrations of MEA, PZ, and blends of MEA-PZ and AMP-PZ which showed higher absorption working than their respective low concentrated solutions. The various concentrations of the ternary blend indicated higher equilibrium CO₂ loading (6.9 – 19 %) and absorption working capacity (aWC) between 13.8 – 48.3 % compared to the standard 5 M MEA. The very high concentrations (6 – 7 M) of the AMP – PZ – MEA ternary blend also showed high absorption working capacity (5.4 – 16.2 %) than the optimal AMP – PZ binary blend (3 M AMP – 1.5 M PZ). Higher absorption working capacity will most often translate to lower amine circulation rate in the CO₂ capture plant, which will reduce the energy of regeneration. The absorption working capacity is usually seen as more relevant parameter compared to the CO₂ loading. It represents the amount of CO₂ the amine solution can carry in the absorption section, which leads to more capture of CO₂ and hence reduced amine circulation rate. This reduced circulation rate is mostly beneficial in the regeneration section. Absorption working capacity can be calculated by multiplying the equilibrium CO₂ loading of the amine solution (α_{CO_2}) by its molar concentration (Equation 1.1).

$$aWC = \alpha_{CO_2} \left(\frac{\text{mol } CO_2}{\text{mol amine}} \right) \times \text{Amine Conc} \left(\frac{\text{mol amine}}{\text{L of solution}} \right) \quad 1.1$$

The influence of MEA and PZ concentrations, H₂O/PZ molar ratio, and possibility of precipitation were also studied, and the solvent combination of 2 M AMP – 0.5 M PZ – 3 M MEA was finally selected for further equilibrium CO₂ loading analysis considering its high H₂O/PZ molar ratio (very minimal possibility of forming solid precipitates). The results were reported as a function of CO₂ partial pres-

tures at the investigated temperatures. In addition, the energy penalty during regeneration was predicted using a validated ProMax[®] 3.2 CO₂ capture plant simulation. The simulation results showed 10 – 24.7 % energy reductions compared to 5 M MEA and 5 – 15 % reductions compared to 3 M AMP – 1.5 M PZ.