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สถาบันวิทยบริการ
จุฬาลงกรณ์มหาวิทยาลัย

ภาคผนวก ก

การคำนวณ Sensitivity

สำหรับค่า Sensitivity คือความไวต่อการเปลี่ยนแปลงตัวแปรซึ่งเทอมของ Sensitivity ที่ใช้ในวิทยานิพนธ์เล่มนี้เป็นแบบ normalized differential sensitivity, S_{xx} ซึ่งอยู่ในรูปของสมการไร้มิติ สามารถแสดงได้ดังต่อไปนี้

$$S_{xx} = \frac{\Delta F / F_0}{\Delta x / x_0} \Big|_{\Delta x \rightarrow 0} \quad (1) \quad [29]$$

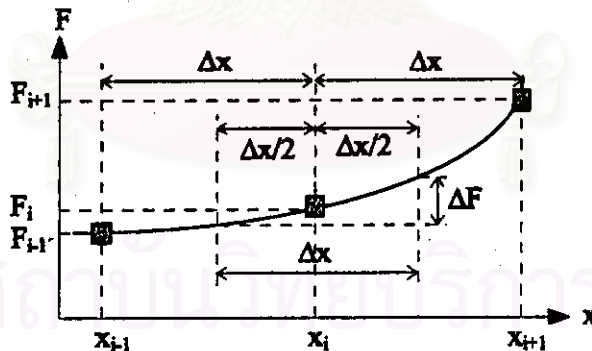
โดยเทอมของ

F_0 คือ function ของกำลังงานสูญเสียหรือ Net indicated power ที่ตัวแปร $x = x_0$

x_0 คือ ตัวแปรการออกแบบจาก baseline engine data

ΔF คือ ผลต่าง function ของกำลังงานสูญเสีย หรือ Net indicated power ในช่วงตัวแปร Δx

Δx คือ ช่วงตัวแปรที่เข้าใกล้ 0 ซึ่งในวิทยานิพนธ์เล่มนี้จะประมาณเป็นช่วงที่ครอบคลุมจุดที่พิจารณา โดยจะแสดงได้ดังรูปต่อไปนี้



รูป ก.1 แสดงตัวแปรต่างๆในการคำนวณหาค่า sensitivity

F_i คือ function ของกำลังงานสูญเสียหรือ Net indicated power ที่ตัวแปร $x = x_i$ ซึ่งเป็นตัวแปรที่พิจารณา

F_{i-1} คือ function ของกำลังงานสูญเสียหรือ Net indicated power ที่ตัวแปร $x = x_{i-1}$

F_{i+1} คือ function ของกำลังงานสูญเสียหรือ Net indicated power ที่ตัวแปร $x = x_{i+1}$

ซึ่ง ค่า sensitivity เป็นบวก หมายถึงเมื่อเปลี่ยนแปลงตัวแปร x จะทำให้ค่า F มากขึ้น

ค่า sensitivity เป็นลบ หมายถึงเมื่อเปลี่ยนแปลงตัวแปร x จะทำให้ค่า F ลดลง

สำหรับผลในการคำนวณค่า Sensitivity ของตัวแปรต่างๆสามารถแสดงได้ดังตาราง ก1
 ตาราง ก.1 แสดงผลการคำนวณค่า Sensitivity ของตัวแปรต่างๆที่ความเร็ว 2600 รอบต่อนาที

ตัวแปรที่เกี่ยวข้องกับองค์ประกอบทางทอร์โมไดนามิกส์						
ตัวแปรทางออกแบบ	Sensitivity					
- Spark advance (degree crank angle)	-30 0.832	-28 0.891	-26 0.953	-24 0.901	-22 0.965	-20 0.871
- Combustion duration (degree crank angle)	36 -1.297	37.6 -1.373	39.2 -1.411	40.2 -1.429	42.4 -1.42	44 -1.401
- Compression ratio	8.5 1.259	8.9 1.259	9.3 1.25	9.7 1.241	10.1 1.232	10.5 1.232
- Connecting rod length (m)	0.12 0.072	0.128 0.066	0.136 0.059	0.144 0.053	0.152 0.046	0.16 0.053
ตัวแปรที่เกี่ยวข้องกับองค์ประกอบในฐานของเครื่องยนต์						
ก) Connecting rod bearing						
- Radius bearing at big-end (m)	0.021 2.281	0.022 2.523	0.023 2.736	0.024 2.979	0.025 3.232	0.026 3.497
- Radius clearance at big-end (mm)	0.0315 -1.225	0.0329 -1.129	0.0343 -1.034	0.0357 -0.954	0.0371 -0.884	0.0385 -0.821
- Bearing width at big-end (m)	0.02 0.992	0.0208 0.992	0.0216 0.992	0.0224 0.992	0.0232 0.992	0.024 0.992
- Radius bearing at small-end (m)	0.01 0.0171	0.0104 0.0184	0.0108 0.0199	0.0112 0.214	0.0116 0.0231	0.012 0.0246
- Radius clearance at small-end (mm)	0.0162 -0.0081	0.017 -0.0077	0.0177 -0.0071	0.0185 -0.0065	0.0192 -0.006	0.02 -0.0055
- Bearing width at small-end (m)	0.02 0.0068	0.0208 0.0068	0.0216 0.0068	0.0224 0.0068	0.0232 0.0068	0.024 0.0068
ข) Crankshaft bearing						
- Radius of bearing (m)	0.021 2.297	0.022 2.521	0.023 2.755	0.024 3.001	0.025 3.255	0.026 3.521
- Bearing width (m)	0.02 1	0.0208 1	0.0216 1	0.0224 1	0.0232 1	0.024 1
- Radius clearance (mm)	0.022 -1.191	0.023 -1.089	0.024 -1.001	0.025 -0.922	0.026 -0.852	0.027 -0.791
ค) Piston ring and skirt						
- Piston clearance (mm)	0.06 -1.358	0.064 -1.193	0.068 -1.007	0.072 -0.992	0.076 -0.846	0.08 -0.763
- Skirt length (m)	0.036 1.001	0.0376 1.001	0.0392 1.001	0.0408 1.001	0.0424 1.001	0.044 1.001
- Pressure ring depth (mm)	3 0.873	3.17 0.874	3.34 0.875	3.51 0.876	3.68 0.878	3.85 0.881
- Oil ring depth (mm)	1 0.1099	1.042 0.1035	1.084 0.103	1.126 0.1031	1.168 0.1031	1.21 0.1032

ภาคผนวก ข

ข้อมูลตัวแปรการออกแบบจาก baseline engine data

สำหรับข้อมูลจาก baseline engine data ที่ใช้ในการคำนวณในโปรแกรม Indicate , Engine และ Optimum สามารถแสดงได้ดังตาราง ข.1

ตาราง ข.1 แสดงข้อมูล baseline engine data

ตัวแปรต่างๆใน baseline engine data	ค่าตัวแปร
ก) ตัวแปรในทางเทอร์โมไดนามิกส์	
- θ_s (spark advance) , degree crank angle	-26
- θ_b (combustion duration) , degree crank angle	40
- l (connecting rod length) , m	0.14
- R_c (compression ratio)	9.5
ข) ตัวแปรในส่วนของเครื่องยนต์	
- V_d (displacement volume) , m^3	0.001587
- B (piston bore) , m	0.081
- n_c (number cylinder) , cylinder	4
- a (crank arm) , m	0.0385
- r (connecting rod length to crank arm ratio , l/a)	3.636
- b'_{press} (pressure ring width) , mm	3.5
- b'_{oil} (oil ring width) , mm	1.1
- n_{press} (number pressure ring)	2
- n_{oil} (number oil ring)	1
- h'_2 (oil minimum thickness) , μm	5
- L_{skirt} (skirt length) , m	0.04
- C_p (piston clearance) , mm	0.07
- μ (absolute viscosity) , Pa.s	0.0136
- C_{big} (radius clearance at big-end side) , m	3.5×10^{-5}
- R_{big} (radius bearing at big-end side) , m	0.024
- L_{big} (bearing width at big-end side) , m	0.022
- ϵ_{big} (eccentricity ratio at big-end side)	0.9
- C_{small} (radius clearance at small-end side) , m	1.8×10^{-5}
- R_{small} (radius bearing at small-end side) , m	0.011
- L_{small} (bearing width at small-end side) , m	0.022
- ϵ_{small} (eccentricity ratio at small-end side)	0.9
- C_{crank} (radius clearance in crankshaft bearing) , m	2.4×10^{-5}
- R_{crank} (radius bearing in crankshaft bearing) , m	0.024
- L_{crank} (bearing width in crankshaft bearing) , m	0.022
- ϵ_{crank} (eccentricity ratio)	0.9
- n_b (number bearing in crankshaft)	5
- m (valve follower mass) , kg	0.1
- K (spring stiffness) , N/m	24000

ตาราง ข.1 (ต่อ) แสดงข้อมูล baseline engine data

ตัวแปรต่างๆใน baseline engine data	ค่าตัวแปร
ข) ตัวแปรในส่วนของเครื่องยนต์	
- r (tip radius) , mm	2.5
- R (base radius) , mm	15.9
- ϕ (starting angle) , degree	31
- μ_c (friction coefficient on cam surface)	0.11
- L_{vf} (valve follower lift) , mm	10
- N_{valv} (number valve follower per cylinder) , valve/cylinder	4
- N_{iv} (number inlet valve per cylinder) , valve/cylinder	2
- D_v (inlet vale diameter) , m	0.03
- P_e (exhaust pressure at full load) , In.Hg	10
- P_a (ambient pressure) , kPa	101.325
- k (isentropic of R12)	1.136
- e_c (compression efficiency)	0.7
- e_m (mechanical efficiency in compressor)	0.8
- P_2 (condenser pressure) , Pa	1.53×10^6
- P_1 (evaporator pressure) , Pa	0.255×10^6
- B_{com} (piston bore in compressor) , m	0.048
- Cooling load , W	2500
- L_{com} (stroke length in compressor) , m	0.04
- D_a (rotor diameter in alternator) , m	0.115
- L_a (rotor length in alternator) , m	0.1
- ρ_{Hg} (mercury density) , kg/m^3	13550
ค) ตัวแปรในส่วนของยานยนต์	
- G_1 (gear ratio # 1)	3.166
- G_2 (gear ratio # 2)	1.904
- G_3 (gear ratio # 3)	1.31
- G_4 (gear ratio # 4)	0.969
- G_5 (gear ratio # 5)	0.815
- G_D (differential ratio)	4.058
- C_d (drag coefficient)	0.33
- A_f (frontal area) , m^2	1.94
- f (rolling coefficient)	0.01536
- m_v (vehicle mass) , kg	1110
- R_w (wheel radius) , m	0.281
- ρ_{air} (air density) , kg/m^3	1.17

ภาคผนวก ค
เพิ่มข้อมูลป้อนค่าตัวแปรการออกแบบ

ในการคำนวณจากโปรแกรม Engine และ Optimum จะมีเพิ่มข้อมูลที่ใช้เป็นฐานข้อมูลเบื้องต้นในการคำนวณ โดยเพิ่มข้อมูลคือ base.dat ซึ่งประกอบด้วยข้อมูล 2 กลุ่ม ประกอบด้วยดังต่อไปนี้

- 1) กลุ่มที่หนึ่ง เป็นกลุ่มของข้อมูลตัวแปรการออกแบบและตัวแปรค่าคงที่
- 2) กลุ่มที่สอง เป็นกลุ่มข้อมูลของช่วงของตัวแปรการออกแบบที่พิจารณา โดยช่วงตัวแปรการออกแบบนั้น จะพิจารณาจากการเพิ่มลดค่าจาก baseline engine data ประมาณร้อยละ 10 หรือมีความเป็นไปได้ในทางปฏิบัติ เป็นช่วงตัวแปรการออกแบบที่พิจารณา

สำหรับสัญลักษณ์ตัวแปรๆของเพิ่มข้อมูลป้อนค่าตัวแปรการออกแบบ base.dat สามารถแสดงได้ดังนี้

ข้อมูลกลุ่มที่หนึ่ง ประกอบด้วยดังนี้

VISB, RCRANKB, CRANKLB, CCRANKB, BN, QB
RKB, EMB, ECB, CONDP, EVAPP, BCOMB, SCOMB
BPRESSB, BOILB, NPRESSB, NOILB
BRCONB, BCCONB, BLCONB
SRCONB, SCCONB, SLCONB
NCB, BOREB, ARMB, CONLB
NVCB, SDEGB, TRB, VLB
FMB, SCB, PLB, BRB
RDALTB, RLALTB
DVB, RCB, NVB
PCB, PISLB
G1, G2, G3, G4, G5, GD
CDB, AREAB, FRB, MGB, WR

ข้อมูลกลุ่มที่สอง ประกอบด้วยดังนี้

RCRANKL, RCRANKH
CRANKLL, CRANKLH
CCRANKL, CCRANKH
BRCONL, BRCONH
BCCONL, BCCONH
BLCONL, BLCONH
SRCONL, SRCONH
SCCONL, SCCONH
SLCONL, SLCONH
BPRESSL, BPRESSH
BOILL, BOILH
BOREL, BOREH

VISL, VISH
 ARML, ARMH
 RDALTL, RDALTH
 RLALTL, RLALTH
 CONLL, CONLH
 PISLL, PISLH
 DVL, DVH
 RCL, RCH
 PCL, PCH
 FML, FMH
 SCL, SCH
 PLL, PLH
 BRL, BRH
 TRL, TRH
 VLL, VLH
 QL, QH
 CDL, CDH
 AFL, AFH
 FRL, FRH
 MGL, MGH

สำหรับคำอธิบายสัญลักษณ์ของตัวแปรการออกแบบและช่วงตัวแปรการออกแบบ
 แสดงได้ดังต่อไปนี้

VIS	= ABSOLUTE VISCOSITY	: (Pa.s)
RCRANK	= RADIUS OF CRANK-SHAFT BEARING	: (m)
CRANKL	= CRANK-SHAFT BEARING WIDTH	: (m)
CCRANK	= RADIUS CLEARANCE IN CRANK-SHAFT BEARING	: (m)
BN	= AMOUNT OF BEARING SUPPORT	
RKB	= REFRIGERANT ISENTROPIC INDEX	
EMB	= MECHANICAL EFFICIENCY	
ECB	= COMPRESSION EFFICIENCY	
CONDP	= CONDENSER PRESSURE	: (Pa)
EVAPP	= EVAPORATOR PRESSURE	: (Pa)
BCOMB	= PISTON BORE AT COMPRESSOR	: (m)
SCOMB	COMPRESSOR STROKE LENGTH	: (m)
BPRESS	= PRESSURE RING SURFACE DEPTH	: (mm)
BOIL	= OIL RING SURFACE DEPTH	: (mm)
NPRESS	= AMOUNT OF PRESSURE RING	
NOIL	= AMOUNT OF OIL RING	
BRCON	= RADIUS OF CONNECTING ROD BEARING AT BIG-END	: (m)
BCCON	= RADIUS CLEARANCE IN CONNECTING ROD BIG-END	: (m)
BLCON	= CONNECTING ROD BEARING WIDTH AT BIG-END	: (m)
SRCON	= RADIUS OF CONNECTING ROD BEARING AT SMALL-END	: (m)
SCCON	= RADIUS CLEARANCE IN CONNECTING ROD SMALL-END	: (m)
SLCON	= CONNECTING ROD BEARING WIDTH AT SMALL-END	: (m)
NCB	= NUMBER OF CYLINDER	
BORE	= PISTON BORE	: (m)
ARM	= CRANK ARM	: (m)
CONL	= CONNECTING ROD LENGTH	: (m)
NVCB	= NUMBER VALVE PER CYLINDER	
SDEGB	= STARTING ANGLE	: (deg.)
TR	= TIP RADIUS OF CAM	: (mm)
BR	= BASE RADIUS OF CAM	: (mm)
VL	= VALVE FOLLOWER LIFT	: (mm)
FM	= VALVE FOLLOWER MASS	: (mm)
SC	= SPRING STIFFNESS	: (N/m)
PL	= VALVE PRELOAD	: (N)
RDALTB	= ROTOR DIAMETER OF ALTERNATOR	: (m)

RLALTB	= ROTOR LENGTH OF ALTERATOR	: (m)
DV	= INLET VALVE DIAMETER	: (m)
RC	= COMPRESSION RATIO	
NVB	= NUMBER OF INLET VALVE PER CYLINDER	
PC	= PISTON CLEARANCE	: (m)
PISL	= PISTON SKIRT LENGTH	: (m)
G	= GEAR RATIO IN 1-5 AND DIFFERENT	
CD	= DRAG COEFFICIENT	
AREA	= FRONTAL AREA	: (m ³)
FR	= ROLLING COEFFICIENT	
MG	= VEHICLE MASS	: (kg)
WR	= WHEEL RADIUS	: (m)

สำหรับสัญลักษณ์ตัวแปรที่มีอักษรต่อท้ายดังต่อไปนี้

อักษร B ต่อท้ายจะหมายถึง ข้อมูลตัวแปรการออกแบบจาก baseline engine data

อักษร L ต่อท้ายจะหมายถึง ข้อมูลที่เป็นช่วงตัวแปร ที่ช่วงต่ำสุด(lower limit)

อักษร H ต่อท้ายจะหมายถึง ข้อมูลที่เป็นช่วงตัวแปร ที่ช่วงสูงสุด(upper limit)

ยกตัวอย่างเช่น ตัวแปร MG เมื่อมีอักษร B, L และ H ต่อท้ายจะหมายถึง

MGB จะเป็นตัวแปรออกแบบจาก baseline engine data

MGL จะเป็นข้อมูลช่วงตัวแปร ที่ช่วงต่ำสุด(lower limit)

MGH จะเป็นข้อมูลช่วงตัวแปร ที่ช่วงสูงสุด(upper limit)

คำอธิบายกลุ่มข้อมูลตัวแปรคงที่แสดงได้ดังนี้

CONDP	= CONDENSER PRESSURE	: (Pa)
EVAPP	= EVAPORATOR PRESSURE	: (Pa)
RKB	= REFRIGERANT ISENTROPIC INDEX	
EMB	= MECHANICAL EFFICIENCY	
ECB	= COMPRESSION EFFICIENCY	
NCB	= NUMBER OF CYLINDER	
BN	= AMOUNT OF BEARING SUPPORT	
NPRESS	= AMOUNT OF PRESSURE RING	
NOIL	= AMOUNT OF OIL RING	
NVCB	= NUMBER VALVE PER CYLINDER	
SDEGB	= STARTING ANGLE	: (deg.)
NVB	= NUMBER OF INLET VALVE PER CYLINDER	
G	= GEAR RATIO IN 1-5 AND DIFFERENT	
WR	= WHEEL RADIUS	: (m)

สำหรับข้อมูลป้อนค่าตัวแปรการออกแบบจากแฟ้มข้อมูล base.dat สามารถแสดงได้ดังนี้

```

0.0136 0.024 0.022 2.4E-5 5. 2500.
1.136 0.8 0.7 1530E+3 255E+3 0.047 0.047
3.5 1.1 2 1
0.024 3.5E-5 0.022
0.011 1.8E-5 0.022
4 0.081 0.0385 0.14
4 31 2.5 10
0.1 24000 155 15.9
0.115 0.1

```

0.03 9.5 2
 0.00007 0.04
 3.166 1.904 1.31 0.969 0.815 4.058
 0.33 1.94 0.01536 1110 0.281
 0.021 0.026
 0.02 0.024
 2.2E-5 2.7E-5
 0.021 0.026
 3.15E-5 3.85E-5
 0.02 0.024
 0.01 0.012
 1.62E-5 2E-5
 0.02 0.024
 3. 3.85
 1. 1.21
 0.07 0.09
 0.012 0.015
 0.0346 0.042
 0.1 0.125
 0.09 0.11
 0.12 0.16
 0.036 0.044
 0.027 0.033
 8.5 10.5
 0.00006 0.00008
 0.09 0.15
 21600. 26400.
 140. 170.
 14. 17.5
 2.2 2.75
 9. 11.
 2300. 2700.
 0.3 0.36
 1.75 2.
 0.0145 0.0168
 1000 1200



สถาบันวิทยบริการ
 จุฬาลงกรณ์มหาวิทยาลัย

ภาคผนวก ง

รายละเอียดโปรแกรม INDICATE

โปรแกรม indicate สามารถแสดงรายละเอียดดังต่อไปนี้

```

C*****-----*****C
C          PROGRAM FOR DETERMINATION NET INDICATED POWER          C
C*****-----*****C
PROGRAM INDICATE
DATA DEG1/-180./,DEG2/180./,GRAM/1.3/,RC/9.5/,NC/4./,DENHG/13550./
$,B/0.081/,A/0.0385/,CL/0.14/,C/4/,RCL/8.5/,RCH/10.5/,CLL/0.12/,
$CLH/0.16/,DEGS1L/-30./,DEGS1H/-20./,DEGBL/36./,DEGBH/44./,NVB/2./,
$DV/0.03/
DHE = 10.
PE = 9.81*DENHG*DHE*0.0254/1000.
PI = 2.*ASIN(1.)
PA = 101.325
C*****-----*****C
C          CONSTANT VALUE FOR CALCULATION                          C
C DENHG = MERCURY DENSITY : (kg/m^3) C
C DEG1 = CRANK ANGLE AT BDC IN COMPRESSION STROKE : (degree) C
C DEG2 = CRANK ANGLE AT BDC IN EXPANSION STROKE : (degree) C
C PA = AMBIENT PRESSURE : (kPa) C
C PE = EXHAUST PRESSURE AT FULL LOAD : (kPa) C
C CL = CONNECTING ROD LENGTH : (m) C
C A = CRANK ARM : (m) C
C B = PISTON BORE : (m) C
C QIN = HEAT ADDITION : (J/cycle/cylinder) C
C C = INDEX OF FRACTION OF THE HEAT RELEASE C
C NC = NUMBER OF CYLINDER C
C RC = COMPRESSION RATIO C
C NV = AMOUNT OF INLET VALVE C
C GRAM = SPECIFIC HEAT RATIO C
C*****-----*****C
WRITE(6,*) ' PLEASE ENTER DATA TO CALCULATE INDICATED POWER '
WRITE(6,*) ' ENTER HEAT ADDITION : (J/cycle/cylinder) '
READ(*,*) QIN
WRITE(6,*) ' ENTER ENGINE SPEED TO CALCULATION : (RPM) '
READ(*,*) RPM
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF PARAMETERS : (TIMES) '
READ(*,*) M
DDEGS1 = (DEGS1H-DEGS1L)/M
DDEGB = (DEGBH-DEGBL)/M
C.....CALCULATION AT BASELINE DATA
OPEN(UNIT=1,FILE='RESULT1.OUT',STATUS='OLD')
WRITE(1,*) ' INDICATED POWER BASELINE DATA '
WRITE(6,*) ' INDICATED POWER BASELINE DATA '
WRITE(1,*) ' '
WRITE(6,*) ' '
IF (RPM.LE.1300.) THEN
DH = 9.9
ELSE
IF (RPM.LE.1700.) THEN
DH = 10.2
ELSE
IF (RPM.LE.2000.) THEN
DH = 11.
ELSE
IF (RPM.LE.2400.) THEN
DH = 12.
ELSE
IF (RPM.LE.2700.) THEN

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      DH = 13.
    ELSE
      IF (RPM.LE.3000.) THEN
        DH = 13.7
      ELSE
        IF (RPM.LE.3400.) THEN
          DH = 14.9
        ELSE
          IF (RPM.LE.3700.) THEN
            DH = 15.9
          ELSE
            IF (RPM.LE.4000.) THEN
              DH = 16.5
            ELSE
              WRITE(*,*) ' OVER ENGINE SPEED '
            ENDIF
          ENDIF
        ENDIF
      ENDIF
    ENDIF
  ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
DEGS1 = -26.
DEGB = 40.
DEGS1B = -26.
DEGBB = 40.
DEGS2 = DEGS1+DEGB
R = CL/A
VD = 2.*A*PI*(B**2.)/4.
VC = VD/(RC-1.)
V1 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG1/180.)
$ -SQRT(R**2.-SIN(PI*DEG1/180.)**2.) )/4.
V2 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS1/180.)
$ -SQRT(R**2.-SIN(PI*DEGS1/180.)**2.) )/4.
V3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS2/180.)
$ -SQRT(R**2.-SIN(PI*DEGS2/180.)**2.) )/4.
V4 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG2/180.)
$ -SQRT(R**2.-SIN(PI*DEG2/180.)**2.) )/4.
P1 = 9.81*DENHG*DH*0.0254
C.....THIS PART CALCULATE P-V DIAGRAM IN COMPRESSION STROKE
N = 200
SUM1 = 0.
DDEG1 = (DEG1-DEGS1)/N
DO 90 I = 0,N
  DEG1 = DEG1-I*DDEG1
  VX1 = VC + A*PI*((B**2.)/4.)*( R + 1. - COS(DEG1*PI/180.)
$ -SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )
  PX1 = P1*(V1/VX1)**GRAM
  DV1 = A*PI*((B**2.)/4.)*( SIN(PI*DEG1/180.) +
$ 0.5*SIN(2.*DEG1*PI/180.) /
$ SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )*(PI/180.)
  WX1 = PX1*DV1
  SUM1 = SUM1 + WX1
90 CONTINUE
  WX01 = P1*A*PI*(B**2.)*( SIN(DEG1*PI/180.) +
$ 0.5*SIN(2.*DEG1*PI/180.) /
$ SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )/4.
  WXN1 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEGS1/180.) +
$ 0.5*SIN(2.*DEGS1*PI/180.) /
$ SQRT(R**2.-SIN(DEGS1*PI/180.)**2.) )/4.
  POWER1 = (-WX01-WXN1 + 2.*SUM1)*(-DDEG1)/2.
C.....THIS PART CALCULATE P-V DIAGRAM DURING COMBUSTION PERIOD
N = 200
SUM2 = 0.
DDEG2 = DEGB/N
PREO = PX1

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DEG0 = DEGS1
DO 190 I = 0,N
DEGX2 = DEGS1+I*DDEG2
VX2 = VC + A*PI*(B**2.)*( R + 1. - COS(DEGX2*PI/180.)
      -SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )/4.
$
DV2 = A*PI*((B**2.)/4.)*( SIN(DEGX2*PI/180.) +
      0.5*SIN(2.*DEGX2*PI/180.) /
      SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )*(PI/180.)
$
WX2 = PRE0*DV2
SUM2 = SUM2 + WX2
SLOPE = (GRAM-1)/VX2*QIN*C/DEGB*((DEGX2-DEGS1)/DEGB)**(C-1))*
      EXP( -((DEGX2-DEGS1)/DEGB)**C ) - GRAM*PRE0/VX2*A*(PI*
      (B**2)/4.)*(PI/180.)*( SIN(DEGX2*PI/180.) +
      0.5*SIN(2.*DEGX2*PI/180.) /
      SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )
$
PRE1 = PRE0 + SLOPE*DDEG2
PRE0 = PRE1
190 CONTINUE
WX20 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(DEGS1*PI/180.) +
      0.5*SIN(2.*DEGS1*PI/180.) /
      SQRT(R**2.-SIN(DEGS1*PI/180.)**2.) )/4.
$
WX2N = WX2
POWER2 = (-WX20-WX2N+2.*SUM2)*(DDEG2)/2.
C.....THIS PART CALCULATE P-V DIAGRAM IN EXPANSION STROKE
P3 = PRE0
N = 200
SUM3 = 0.
DDEG3 = (DEG2-DEGS2)/N
DO 290 I = 0,N
DEGX3 = DEGS2+I*DDEG3
VX3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGX3/180.)
      -SQRT(R**2.-SIN(PI*DEGX3/180.)**2.) )/4.
$
PX3 = P3*(V3/VX3)**GRAM
DV3 = A*PI*((B**2.)/4.)*( SIN(PI*DEGX3/180.) +
      0.5*SIN(2.*DEGX3*PI/180.) /
      SQRT(R**2.-SIN(DEGX3*PI/180.)**2.) )*(PI/180.)
$
WX3 = P3*DV3
SUM3 = SUM3 + WX3
290 CONTINUE
WX03 = P3*A*PI*(B**2.)*( SIN(DEGS2*PI/180.) +
      0.5*SIN(2.*DEGS2*PI/180.) /
      SQRT(R**2.-SIN(DEGS2*PI/180.)**2.) )/4.
$
WXN3 = (P3*(V3/V1)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEG2/180.) +
      0.5*SIN(2.*DEG2*PI/180.) /
      SQRT(R**2.-SIN(DEG2*PI/180.)**2.) )/4.
$
POWER3 = (-WX03-WXN3+2.*SUM3)*(DDEG3)/2.
C.....SHOW RESULTS FROM CALCULATION
POWER = POWER1+POWER2+POWER3
CALL PUMPING(RPM, DH, NC, B, A, DV, RC, NVB, DENHG, PE, PA, PPUMP, PI)
WNTB = (POWER/1000.)*NC*RPM/(2.*60.)-PPUMP/1000
C*****-----*****C
PMA1 = 0.
DO 1000 J1 = 0,M
OPEN(UNIT=1, FILE='RESULT1.OUT', STATUS='OLD')
DRC = (RCH-RCL)/M
RC = RCL+J1*DRC
WRITE(1,*) RC
WRITE(6,*) RC
WRITE(1,*) ' '
DO 2000 J2 = 0,M
DCL = (CLH-CLL)/M
CL = CLL+J2*DCL
R = CL/A
WRITE(1,*) CL
WRITE(6,*) CL
WRITE(1,*) ' '
DO 3000 J3 = 0,M
DEGB = DEGBL+J3*DDEGB

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OPEN(UNIT=1,FILE='RESULT1.OUT',STATUS='OLD')
WRITE(1,1001) DEGB
WRITE(6,1001) DEGB
WRITE(1,*) ' '
1001 FORMAT(2X,'COMBUSTION DURATION(degree) : ',F8.2)
DO 4000 J4 = 0,M
    DEGS1 = DEGS1+J4*DDEGS1
OPEN(UNIT=1,FILE='RESULT1.OUT',STATUS='OLD')
DEGS2 = DEGS1+DEGB
R = CL/A
VD = 2.*A*PI*(B**2.)/4.
VC = VD/(RC-1)
V1 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG1/180.)
$ -SQRT(R**2.-SIN(PI*DEG1/180.)**2.) )/4.
V2 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS1/180.)
$ -SQRT(R**2.-SIN(PI*DEGS1/180.)**2.) )/4.
V3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS2/180.)
$ -SQRT(R**2.-SIN(PI*DEGS2/180.)**2.) )/4.
V4 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG2/180.)
$ -SQRT(R**2.-SIN(PI*DEG2/180.)**2.) )/4.
P1 = 9.81*DENHG*DH*0.0254
C.....THIS PART CALCULATE P-V DIAGRAM IN COMPRESSION STROKE
N = 200
SUM1 = 0.
DDEG1 = (DEG1-DEGS1)/N
DO 100 I = 0,N
    DEG1 = DEG1-I*DDEG1
    VX1 = VC + A*PI*((B**2.)/4.)*( R + 1. - COS(DEG1*PI/180.)
$ -SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )
    PX1 = P1*(V1/VX1)**GRAM
    DV1 = A*PI*((B**2.)/4.)*( SIN(PI*DEG1/180.) +
$ 0.5*SIN(2.*DEG1*PI/180.) /
$ SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )*(PI/180.)
    WX1 = PX1*DV1
    SUM1 = SUM1 + WX1
100 CONTINUE
    WX01 = P1*A*PI*(B**2.)*( SIN(DEG1*PI/180.) +
$ 0.5*SIN(2.*DEG1*PI/180.) /
$ SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )/4.
    WXN1 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEGS1/180.) +
$ 0.5*SIN(2.*DEGS1*PI/180.) /
$ SQRT(R**2.-SIN(DEGS1*PI/180.)**2.) )/4.
    POWER1 = (-WX01-WXN1 + 2.*SUM1)*(-DDEG1)/2.
C.....THIS PART CALCULATE P-V DIAGRAM DURING COMBUSTION PERIOD
N = 200
SUM2 = 0.
DDEG2 = DEGB/N
PRE0 = PX1
DEG0 = DEGS1
DO 200 I = 0,N
    DEG2 = DEG0+I*DDEG2
    VX2 = VC + A*PI*(B**2.)*( R + 1. - COS(DEG2*PI/180.)
$ -SQRT(R**2.-SIN(DEG2*PI/180.)**2.) )/4.
    DV2 = A*PI*((B**2.)/4.)*( SIN(DEG2*PI/180.) +
$ 0.5*SIN(2.*DEG2*PI/180.) /
$ SQRT(R**2.-SIN(DEG2*PI/180.)**2.) )*(PI/180.)
    WX2 = PRE0*DV2
    SUM2 = SUM2 + WX2
    SLOPE = (GRAM-1)/VX2*QIN*C/DEGB*((DEG2-DEGS1)/DEGB)**(C-1))*
$ EXP(-((DEG2-DEGS1)/DEGB)**C) - GRAM*PRE0/VX2*A*(PI*
$ (B**2.)/4.)*(PI/180.)*( SIN(DEG2*PI/180.) +
$ 0.5*SIN(2.*DEG2*PI/180.) /
$ SQRT(R**2.-SIN(DEG2*PI/180.)**2.) )
    PRE1 = PRE0 + SLOPE*DDEG2
    PRE0 = PRE1
200 CONTINUE
    WX20 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEGS1/180.) +
$ 0.5*SIN(2.*DEGS1*PI/180.) /

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$          SQRT(R**2.-SIN(DEGS1*PI/180.))**2.) )/4.
    WX2N = WX2
    POWER2 = (-WX20-WX2N+2.*SUM2)*(DDEG2)/2.
C.....THIS PART CALCULATE P-V DIAGRAM IN EXPANSION STROKE
    P3 = PRE0
    N = 200
    SUM3 = 0.
    DDEG3 = (DEG2-DEGS2)/N
    DO 300 I = 0,N
    DEG3 = DEGS2+I*DDEG3
    VX3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG3/180.)
$          -SQRT(R**2.-SIN(PI*DEG3/180.))**2.) )/4.
    PX3 = P3*(V3/VX3)**GRAM
    DV3 = A*PI*((B**2.)/4.)*( SIN(PI*DEG3/180.) +
$          0.5*SIN(2.*DEG3*PI/180) /
$          SQRT(R**2.-SIN(DEG3*PI/180.))**2.) )*(PI/180.)
    WX3 = P3*DV3
    SUM3 = SUM3 + WX3
300 CONTINUE
    WX03 = P3*A*PI*(B**2.)*( SIN(DEGS2*PI/180.) +
$          0.5*SIN(2.*DEGS2*PI/180.) /
$          SQRT(R**2.-SIN(DEGS2*PI/180.))**2.) )/4.
    WXN3 = (P3*(V3/V1)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEG2/180.) +
$          0.5*SIN(2.*DEG2*PI/180.) /
$          SQRT(R**2.-SIN(DEG2*PI/180.))**2.) )/4.
    POWER3 = (-WX03-WXN3+2.*SUM3)*(DDEG3)/2.
C.....SHOW RESULTS FROM CALCULATION
    POWER = POWER1+POWER2+POWER3
    CALL PUMPING(RPM,DH,NC,B,A,DV,RC,NVB,DENHG,PE,PA,PPUMP,PI)
    WNT = (POWER/1000.)*NC*RPM/(2.*60.)-PPUMP/1000
    WRITE(1,400) DEGS1,WNT
    WRITE(6,400) DEGS1,WNT
C.....      DETERMINATION INDICATED POWER MAXIMUM
C.....      FROM SPARK ADVANCE & COMBUSTION DURATION
    IF(PMAX1.LT.WNT) THEN
        PMAX1 = WNT
        XMAX11 = DEGS1
        XMAX12 = DEGB
        XMAX2 = CL
        XMAX3 = RC
    ENDIF
400 FORMAT(2X,F8.2,T20,F8.2)
4000 CONTINUE
3000 CONTINUE
2000 CONTINUE
1000 CONTINUE
    WRITE(1,*) ' '
    WRITE(1,*) ' OPTIMUM PARAMETERS OF INDICATED POWER '
    WRITE(6,*) ' '
    WRITE(6,*) ' OPTIMUM PARAMETERS OF INDICATED POWER '
    WRITE(1,500) RPM,DH
    WRITE(1,501) XMAX11
    WRITE(1,502) XMAX12
    WRITE(1,*) ' '
    WRITE(1,503) DEGS1B,DEG1B
    WRITE(1,504) XMAX2
    WRITE(1,505) XMAX3
    WRITE(6,500) RPM,DH
    WRITE(6,501) XMAX11
    WRITE(6,502) XMAX12
    WRITE(6,*) ' '
    WRITE(6,503) DEGS1B,DEG1B
    WRITE(6,504) XMAX2
    WRITE(6,505) XMAX3
500 FORMAT(2X,' AT ',2X,F7.2,' (RPM) : ',2X,F5.2,' (INCH)')
501 FORMAT(2X,' SPARK ADVANCE AT ',T30,F7.2,' : (degree) ')
502 FORMAT(2X,' COMBUSTION DURATION ',T30,F7.2,' : (degree) ')
503 FORMAT(2X,' SPARK ADV. AT ',F7.2,2X,' DURATION AT ',F7.2)

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504 FORMAT(2X,'CONNECTING ROD LENGTH ',T30,F7.2,' : (m) ')
505 FORMAT(2X,'COMPRESSION RATIO ',T30,F7.2)
C*****-----*****C
WRITE(1,*) ' INDICATED POWER OPTIMUM DATA '
WRITE(6,*) ' INDICATED POWER OPTIMUM DATA '
WRITE(1,*) ' '
WRITE(6,*) ' '
OPEN(UNIT=1,FILE='RESULT1.OUT',STATUS='OLD')
RC = XMAX3
DEGB = XMAX12
DEGS1 = XMAX11
DEGS2 = DEGS1+DEGB
CL = XMAX2
R = CL/A
VD = 2.*A*PI*(B**2.)/4.
VC = VD/(RC-1)
V1 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG1/180.)
$ -SQRT(R**2.-SIN(PI*DEG1/180.)**2.) )/4.
V2 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS1/180.)
$ -SQRT(R**2.-SIN(PI*DEGS1/180.)**2.) )/4.
V3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEGS2/180.)
$ -SQRT(R**2.-SIN(PI*DEGS2/180.)**2.) )/4.
V4 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG2/180.)
$ -SQRT(R**2.-SIN(PI*DEG2/180.)**2.) )/4.
P1 = 9.81*DENHG*DH*0.0254
C.....THIS PART CALCULATE P-V DIAGRAM IN COMPRESSION STROKE
N = 200
SUM1 = 0.
DDEG1 = (DEG1-DEGS1)/N
DO 130 I = 0,N
DEGX1 = DEG1-I*DDEG1
VX1 = VC + A*PI*((B**2.)/4.)*( R + 1. - COS(DEGX1*PI/180.)
$ -SQRT(R**2.-SIN(DEGX1*PI/180.)**2.) )
PX1 = P1*(V1/VX1)**GRAM
DV1 = A*PI*((B**2.)/4.)*( SIN(PI*DEGX1/180.) +
$ 0.5*SIN(2.*DEGX1*PI/180.) /
$ SQRT(R**2.-SIN(DEGX1*PI/180.)**2.) )*(PI/180.)
WX1 = PX1*DV1
SUM1 = SUM1 + WX1
130 CONTINUE
WX01 = P1*A*PI*(B**2.)*( SIN(DEG1*PI/180.) +
$ 0.5*SIN(2.*DEG1*PI/180.) /
$ SQRT(R**2.-SIN(DEG1*PI/180.)**2.) )/4.
WXN1 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEGS1/180.) +
$ 0.5*SIN(2.*DEGS1*PI/180.) /
$ SQRT(R**2.-SIN(DEGS1*PI/180.)**2.) )/4.
POWER1 = (-WX01-WXN1 + 2.*SUM1)*(-DDEG1)/2.
C.....THIS PART CALCULATE P-V DIAGRAM DURING COMBUSTION PERIOD
N = 200
SUM2 = 0.
DDEG2 = DEGB/N
PRE0 = PX1
DEG0 = DEGS1
DO 230 I = 0,N
DEGX2 = DEGS1+I*DDEG2
VX2 = VC + A*PI*(B**2.)*( R + 1. - COS(DEGX2*PI/180.)
$ -SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )/4.
DV2 = A*PI*((B**2.)/4.)*( SIN(DEGX2*PI/180.) +
$ 0.5*SIN(2.*DEGX2*PI/180.) /
$ SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )*(PI/180.)
WX2 = PRE0*DV2
SUM2 = SUM2 + WX2
SLOPE = (GRAM-1)/VX2*QIN*C/DEGB*((DEGX2-DEGS1)/DEGB)**(C-1))*
$ EXP(-((DEGX2-DEGS1)/DEGB)**C) - GRAM*PRE0/VX2*A*(PI*
$ (B**2.)/4.)*(PI/180.)*( SIN(DEGX2*PI/180.) +
$ 0.5*SIN(2.*DEGX2*PI/180.) /
$ SQRT(R**2.-SIN(DEGX2*PI/180.)**2.) )
PRE1 = PRE0 + SLOPE*DDEG2

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      PRE0 = PRE1
230 CONTINUE
      WX20 = (P1*(V1/V2)**GRAM)*A*PI*(B**2.)*( SIN(DEGS1*PI/180.) +
$         0.5*SIN(2.*DEGS1*PI/180) /
$         SQRT(R**2.-SIN(DEGS1*PI/180.))**2.)) /4.
      WX2N = WX2
      POWER2 = (-WX20-WX2N+2.*SUM2)*(DDEG2)/2.
C.....THIS PART CALCULATE P-V DIAGRAM IN EXPANSION STROKE
      P3 = PRE0
      N = 200
      SUM3 = 0.
      DDEG3 = (DEG2-DEGS2)/N
DO 330 I = 0,N
      DEG3 = DEGS2+I*DDEG3
      VX3 = VC + A*PI*(B**2.)*( R + 1. - COS(PI*DEG3/180.)
$         -SQRT(R**2.-SIN(PI*DEG3/180.))**2.)) /4.
      PX3 = P3*(V3/VX3)**GRAM
      DV3 = A*PI*((B**2.)/4.)*( SIN(PI*DEG3/180.) +
$         0.5*SIN(2.*DEG3*PI/180) /
$         SQRT(R**2.-SIN(DEG3*PI/180.))**2.)) *(PI/180.)
      WX3 = P3*DV3
      SUM3 = SUM3 + WX3
330 CONTINUE
      WX03 = P3*A*PI*(B**2.)*( SIN(DEGS2*PI/180.) +
$         0.5*SIN(2.*DEGS2*PI/180.) /
$         SQRT(R**2.-SIN(DEGS2*PI/180.))**2.)) /4.
      WXN3 = (P3*(V3/V1)**GRAM)*A*PI*(B**2.)*( SIN(PI*DEG2/180.) +
$         0.5*SIN(2.*DEG2*PI/180.) /
$         SQRT(R**2.-SIN(DEG2*PI/180.))**2.)) /4.
      POWER3 = (-WX03-WXN3+2.*SUM3)*(DDEG3)/2.
C.....SHOW RESULTS FROM CALCULATION
      POWER = POWER1+POWER2+POWER3
      CALL PUMPING(RPM,DH,NC,B,A,DV,RC,NVB,DENHG,PE,PA,PPUMP,PI)
      WNT0 = (POWER/1000.)*NC*RPM/(2.*60.)-PPUMP/1000
      DWNT = (WNT0-WNTB)/WNTB*100
      WRITE(1,*) ' COMPARATIVE BASELINE WITH OPTIMUM DATA '
      WRITE(1,*) ' BASELINE DATA : OPTIMUM DATA : IMPROVEMENT '
      WRITE(6,*) ' COMPARATIVE BASELINE WITH OPTIMUM DATA '
      WRITE(6,*) ' BASELINE DATA : OPTIMUM DATA : IMPROVEMENT '
      WRITE(1,333) WNTB,WNT0,DWNT
      WRITE(6,333) WNTB,WNT0,DWNT
333 FORMAT(2X,F7.2,2X,F7.2,2X,F7.2)
      STOP
      END

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```

C*****-----*****C
C          SUBROUTINE FOR PUMPING LOSSES
C*****-----*****C
      SUBROUTINE PUMPING(RPM,DH,NC,B,A,DV,RC,NVB,DENHG,PE,PA,PPUMP,PI)
      PIA = 9.81*DENHG*DH*0.0254/1000
      CIMEP = 12.87*PA*((PIA/PA)-0.1)
      PIG = PA-(CIMEP/12.8)-10.14
      F = (NVB*NC*(DV**2))/(2*A*PI*NC*(B**2)/4)
      PPUMP = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*RPM)/(3904000))**2) +
$         8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)
$         *((2.984/F)**1.28) + (SQRT((PA-PIG)/97.94))
$         *(11.86*(RC**0.4)-(3.38+0.103*RC)*((RPM/1000)**1.185)))
$         *1000*(2*A*PI*NC*(B**2)/4)*(RPM/120)
      RETURN
      END

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ภาคผนวก จ

รายละเอียดโปรแกรม ENGINE

โปรแกรม engine สามารถแสดงรายละเอียดดังต่อไปนี้

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C*****-----*****C
C          PROGRAM FOR CALCULATION ENGINE POWER REQUIRED          C
C          WRITTEN BY                                          C
C          MR. PAIRAT LERTARAYAPONG                          C
C*****-----*****C
PROGRAM ENGINE
C-----READ DATA FROM BASELINE AND LIMIT DATA FILE-----C
AIRDEN = 1.17
DENHG  = 13550.
FCOE   = 0.11
CORRK  = 0.06
RALT   = 2.
PCLE   = 4.5
RCOM   = 1.18
NCOM   = 1.
DHE    = 10.
RP     = 0.5
RO     = 1.
PI     = 2.*ASIN(1.)
PA     = 101.325
ESM    = 0.9
EC     = 0.9
E      = 0.9
H      = 0.005
PE     = 9.81*DENHG*DHE*0.0254/1000.
H1     = 185.*1000.
H2     = 95.7*1000.
V1     = 0.0666252
FRAC   = 25.

C*****-----*****C
C          CONSTANT VALUE FOR CALCULATION                      C
C AIRDEN  = AIR DENSITY                                       : (kg/m^3) C
C DENHG  = MERCURY DENSITY                                     : (kg/m^3) C
C FCOE   = FRICTION COEFFICIENT IN CAM SURFACE                C
C RCOM   = PULLEY RATIO AT COMPRESSOR                         C
C NCOM   = NUMBER OF CYLINDER AT COMPRESSOR                  C
C PCLE   = PERCENT CLEARANCE AT COMPRESSOR                   : (%)    C
C FRAC   = PERCENT BETWEEN MECH. LOSS WITH TOTAL LOSS       : (%)    C
C CORRK  = CORRECTION FACTOR OF ALTERNATOR                   C
C RALT   = PULLEY RATIO AT ALTERNATOR                         C
C RP     = PRESSURE RING CONSTANT                             C
C RO     = OIL RING CONSTANT                                  C
C PA     = AMBIENT PRESSURE                                    : (kPa)  C
C DHE    = EXHAUST MANIFOLD PRESSURE AT FULL LOAD            : (INCH) C
C H      = OIL MINIMUM THICKNESS                              : (mm)   C
C PE     = EXHAUST MANIFOLD PRESSURE AT FULL LOAD            : (kPa)  C
C EC     = ECCENTRICITY RATIO IN CRANK-SHAFT BEARING         C
C E      = ECCENTRICITY RATIO IN CONNECTION ROD BIG-END     C
C ESM    = ECCENTRICITY RATIO IN CONNECTION ROD SMALL-END   C
C H1     = ENTHALPY AT SATURATED VAPOUR                      : (kJ/kg) C
C H2     = ENTHALPY AT SATURATED LIQUID                      : (kJ/kg) C
C V1     = SPECIFIC VOLUME OF REFRIGERANT                    : (m^3/kg) C
C*****-----*****C
OPEN(UNIT=7, FILE='BASE.DAT', STATUS='OLD')
READ(7, *) VISB, RCRANKB, CRANKLB, CCRANKB, BN, QB
READ(7, *) RKB, EMB, ECB, CONDP, EVAPP, BCOMB, SCOMB
READ(7, *) BPRESSB, BOILB, NPRESSB, NOILB
    
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READ (7,*) BRCONB, BCCONB, BLCONB
 READ (7,*) SRCONB, SCCONB, SLCONB
 READ (7,*) NCB, BOREB, ARMB, CONLB
 READ (7,*) NVCB, SDEGB, TRB, VLB
 READ (7,*) FMB, SCB, PLB, BRB
 READ (7,*) RDALTB, RLALTB
 READ (7,*) DVB, RCB, NVB
 READ (7,*) PCB, PISLB
 READ (7,*) G1, G2, G3, G4, G5, GD
 READ (7,*) CDB, AREAB, FRB, MGB, WR

-----DATA LIMIT FOR CALCULATION-----C

READ (7,*) RCRANKL, RCRANKH
 READ (7,*) CRANKLL, CRANKLH
 READ (7,*) CCRANKL, CCRANKH
 READ (7,*) BRCONL, BRCONH
 READ (7,*) BCCONL, BCCONH
 READ (7,*) BLCONL, BLCONH
 READ (7,*) SRCONL, SRCONH
 READ (7,*) SCCONL, SCCONH
 READ (7,*) SLCONL, SLCONH
 READ (7,*) BPRESSL, BPRESSH
 READ (7,*) BOILL, BOILH
 READ (7,*) BOREL, BOREH
 READ (7,*) VISL, VISH
 READ (7,*) ARML, ARMH
 READ (7,*) RDALTL, RDALTH
 READ (7,*) RLALTL, RLALTH
 READ (7,*) CONLL, CONLH
 READ (7,*) PISLL, PISLH
 READ (7,*) DVL, DVH
 READ (7,*) RCL, RCH
 READ (7,*) PCL, PCH
 READ (7,*) FML, FMH
 READ (7,*) SCL, SCH
 READ (7,*) PLL, PLH
 READ (7,*) BRL, BRH
 READ (7,*) TRL, TRH
 READ (7,*) VLL, VLH
 READ (7,*) QL, QH
 READ (7,*) CDL, CDH
 READ (7,*) AFL, AFH
 READ (7,*) FRL, FRH
 READ (7,*) MGL, MGH

C*****-----*****C

ENGINE PARAMETERS		
C	VIS	= ABSOLUTE VISCOSITY : (Pa.s) C
C	RCRANK	= RADIUS OF CRANK-SHAFT BEARING : (m) C
C	CRANKL	= CRANK-SHAFT BEARING WIDTH : (m) C
C	CCRANK	= RADIUS CLEARANCE IN CRANK-SHAFT BEARING : (m) C
C	BN	= AMOUNT OF BEARING SUPPORT C
C	RKB	= REFRIGERANT ISENTROPIC INDEX C
C	EMB	= MECHANICAL EFFICIENCY C
C	ECB	= COMPRESSION EFFICIENCY C
C	CONDP	= CONDENSOR PRESSURE : (Pa) C
C	EVAPP	= EVAPOURATOR PRESSURE : (Pa) C
C	BCOMB	= PISTON BORE AT COMPRESSOR : (m) C
C	SCOMB	COMPRESSOR STROKE LENGTH : (m) C
C	BPRESS	= PRESSURE RING SURFACE DEPTH : (mm) C
C	BOIL	= OIL RING SURFACE DEPTH : (mm) C
C	NPRESS	= AMOUNT OF PRESSURE RING C
C	NOIL	= AMOUNT OF OIL RING C
C	BRCON	= RADIUS OF CONNECTING ROD BEARING AT BIG-END : (m) C
C	BCCON	= RADIUS CLEARANCE IN CONNECTING ROD BIG-END : (m) C
C	BLCON	= CONNECTING ROD BEARING WIDTH AT BIG-END : (m) C
C	SRCON	= RADIUS OF CONNECTING ROD BEARING AT SMALL-END : (m) C
C	SCCON	= RADIUS CLEARANCE IN CONNECTING ROD SMALL-END : (m) C
C	SLCON	= CONNECTING ROD BEARING WIDTH AT SMALL-END : (m) C
C	NCB	= NUMBER OF CYLINDER C
C	BORE	= PISTON BORE : (m) C

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C  ARM    = CRANK ARM                      : (m)      C
C  CONL   = CONNECTING ROD LENGTH          : (m)      C
C  NVCB   = NUMBER VALVE PER CYLINDER     :          C
C  SDEGB  = STARTING ANGLE                 : (deg.)   C
C  TR     = TIP RADIUS OF CAM              : (mm)     C
C  BR     = BASE RADIUS OF CAM            : (mm)     C
C  VL     = VALVE FOLLOWER LIFT            : (mm)     C
C  FM     = VALVE FOLLOWER MASS            : (mm)     C
C  SC     = SPRING STIFFNESS              : (N/m)    C
C  PL     = VALVE PRELOAD                  : (N)      C
C  RDALTB = ROTOR DIAMETER OF ALTERNATOR  : (m)      C
C  RLALTB = ROTOR LENGTH OF ALTERNATOR    : (m)      C
C  DV     = INLET VALVE DIAMETER          : (m)      C
C  RC     = COMPRESSION RATIO              :          C
C  NVB    = NUMBER OF INLET VALVE PER CYLINDER :          C
C  PC     = PISTON CLEARANCE              : (m)      C
C  PISL   = PISTON SKIRT LENGTH           : (m)      C
C  G      = GEAR RATIO IN 1-5 AND DIFFERENT :          C
C  CD     = DRAG COEFFICIENT              :          C
C  AREA   = FRONTAL AREA                  : (m^3)    C
C  FR     = ROLLING COEFFICIENT            :          C
C  MG     = VEHICLE MASS                   : (kg)     C
C  WR     = WHEEL RADIUS                   : (m)      C
C*****-----*****
C*****-----*****
C                                MAIN PROGRAM FOR CALCULATION POWER LOSS
C*****-----*****
C
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF PARAMETERS : (TIMES) '
READ(*,*) N
WRITE(6,*) ' ENTER ENGINE UPPER LIMIT SPEED : (RPM) '
READ(*,*) RPMH
WRITE(6,*) ' ENTER ENGINE LOWER LIMIT SPEED : (RPM) '
READ(*,*) RPML
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF ENGINE SPEED : (TIMES) '
READ(*,*) RPMN
WRITE(6,*) ' ENTER AMBIENT PRESSURE : (APPROX 30 INCH) '
READ(*,*) DHH
WRITE(6,*) ' ENTER LOWER MANIFOLD PRESSURE LIMIT : (INCH) '
READ(*,*) DHL
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF MANI-PRESSURE : (TIMES) '
READ(*,*) M
RPMMAX = RPMH
POINT = 1
CALL P1(N, RPMH, RPML, RPMN, VISL, VISH, ARML, ARMH, CONLL, CONLH,
$ BRCONL, BRCONH, BCCONL, BCCONH, BLCONL, BLCONH, SRCONL, SRCONH,
$ SCCONL, SCCONH, SLCONL, SLCONH, VISB, NCB, CONLB, ARMB, BRCONB,
$ BCCONB, BLCONB, SRCONB, SCCONB, SLCONB, PVIS, PCONL, PARM, PBRCON,
$ PBCCON, PBLCON, PSRCON, PSCCON, PRCON, PSLCON, E, ESM, PI, POINT,
$ RPMMAX)
POINT = 2
CALL P2(N, RPMH, RPML, RPMN, VISB, RCRANKB, CRANKLB, CCRANKB, BN,
$ VISL, VISH, RCRANKL, RCRANKH, CRANKLL, CRANKLH, CCRANKL, CCRANKH,
$ PVIS, PRCRANK, PLCRANK, PCCRANK, EC, PI, POINT, RPMMAX)
POINT = 3
CALL P3(N, RPMH, RPML, RPMN, VISL, VISH, PCL, PCH, PISLL, PISLH, NCB,
$ ARMH, ARML, BOREH, BOREL, BOREB, ARMB, VISB, PCB, PISLB, VVPIS, PCPPIS,
$ PPLPIS, PAPIB, PBPIS, PI, POINT, RPMMAX)
POINT = 4
CALL P4(N, RPMH, RPML, RPMN, VISL, VISH, BPRESSL, BPRESSH,
$ BOILL, BOILH, BOREL, BOREH, ARML, ARMH, NCB, BOREB, ARMB, VISB, BPRESSB,
$ BOILB, NPRESSB, NOILB, H, PVRING, PBPRING, PBORING, PBRING, PARING,
$ PI, RP, RO, POINT, RPMMAX)
POINT = 5
CALL P5(N, RPMH, RPML, RPMN, FML, FMH, SCL, SCH, PLL, PLH, BRL, BRH,
$ TRL, TRH, VLL, VLH, NVCB, NCB, FMB, SCB, PLB, BRB, TRB, VLB, SDEGB,
$ PFCAM, PSCAM, PPCAM, PBCAM, PTCAM, PFCAM, PI, FCOE, POINT, RPMMAX)
POINT = 6
CALL P6(N, RPMH, RPML, RPMN, BCOMB, SCOMB, NCB, BOREB, ARMB, RKB, EMB, ECB,
$ RDALTB, RLALTB, QH, QL, H1, H2, V1, RDALTL, RDALTH, RLALTL, RLALTH, RCOM,

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$NCOM, PCLE, EVAPP, CONDP, CORRK, RALT, PWP, PAIRQ, PALTD, PALT, PI, POINT,
$FRAC, RPMMAX)
POINT = 7
CALL P7 (N, RPMH, RPML, RPMN, DHH, DHL, M, DVL, DVH, RCL, RCH, NCB,
$ BOREB, ARMB, DVB, RCB, NVB, DENHG, PE, PA, PDFUMP, PRPUMP, PI, POINT,
$ RPMMAX)
POINT = 8
CALL P8 (N, CDB, AREAB, FRB, MGB, WR, RPMH, RPML, RPMN, CDL, CDH, AFL, AFH,
$ FRL, FRH, MGL, MGH, G1, G2, G3, G4, G5, GD, PI, AIRDEN, PAIRC,
$ PAIRA, PROLLF, PROLLM, POINT, RPMMAX)
STOP
END

```

```

C*****-----*****C
C                                     END OF THE MAIN PROGRAM                                     C
C*****-----*****C
C                                     (P1) SUBROUTINE FOR CONNECTING ROD                                     C
C*****-----*****C
SUBROUTINE P1 (N, RPMH, RPML, RPMN, VISL, VISH, ARML, ARMH, CONLL, CONLH,
$ BRCONL, BRCONH, BCCONL, BCCONH, BLCONL, BLCONH, SRCONL, SRCONH,
$ SCCONL, SCCONH, SLCONL, SLCONH, VISB, NCB, CONLB, ARMB, BRCONB,
$ BCCONB, BLCONB, SRCONB, SCCONB, SLCONB, FVIS, PCONL, PARM, PBRCON,
$ PBCCON, PBLCON, PSRCON, PSCCON, PSLCON, PRCON, E, ESM, PI, POINT,
$ RPMMAX)
IF (POINT.EQ.1) THEN
    RPMH = RPMMAX
    RPMMAX = RPMMAX
ENDIF
DRPM = (RPMH-RPML)/RPMN
OPEN(UNIT=9, FILE='RESULT2.OUT', STATUS='OLD')
WRITE(9,*) 'POWER LOSS FROM CONNECTING ROD'
WRITE(9,*) ' * POWER LOSS VARY WITH ABSOLUTE VISCOSITY '
WRITE(9,*) ' ABSOLUTE VISCOSITY (Pa.s) & POWER LOSS (W) '
DO 11 I = 0, RPMN, 1
DO 12 J = 0, N, 1
    DVIS = (VISH-VISL)/N
    RPM = RPML + I*DRPM
    VIS = VISL + J*DVIS
C.....SUBPROGRAM MAEN 1 FOR CALCULATION MEAN ANGULAR VELOCITY
CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
FVIS = VIS*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +
$      VIS*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE(9,100) RPM, VIS, FVIS
WRITE(6,100) RPM, VIS, FVIS
12 CONTINUE
WRITE(9,*) ' '
11 CONTINUE
100 FORMAT(1X, F7.2, 3X, F10.6, 3X, F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH CRANK ARM '
WRITE(9,*) ' CRANK ARM (m) & POWER LOSS (W) '
DO 21 I = 0, RPMN, 1
DO 22 J = 0, N, 1
    DARM = (ARMH-ARML)/N
    RPM = RPML + I*DRPM
    ARM = ARML + J*DARM
C.....SUBPROGRAM MAEN 2 FOR CALCULATION MEAN ANGULAR VELOCITY
CALL MEAN2 (CONLB, ARM, VBMEAN2, VSMEAN2)
PARM = VIS*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN2 +
$      VIS*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN2
WRITE(9,200) RPM, ARM, PARM
WRITE(6,200) RPM, ARM, PARM
22 CONTINUE
WRITE(9,*) ' '
21 CONTINUE

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```

200 FORMAT (1X, F7.2, 3X, F7.5, 3X, F7.2)
C*****-----*****C
WRITE (9,*) ' * POWER LOSS VARY WITH CONNECTING ROD '
WRITE (9,*) ' CONNECTING ROD LENGTH (m) & POWER LOSS (W) '
DO 31 I = 0, RPMN, 1
DO 32 J = 0, N, 1
    DCONL = (CONLH-CONLL)/N
    RPM = RPML + I*DRPM
    CONL = CONLL + J*DCONL
C.....SUBPROGRAM MAEN 3 FOR CALCULATION MEAN ANGULAR VELOCITY
CALL MEAN3 (CONL, ARMB, VBMEAN3, VSMEAN3)
PCONL = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN3 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN3
WRITE (9,300) RPM, CONL, PCONL
WRITE (6,300) RPM, CONL, PCONL
32 CONTINUE
WRITE (9,*) ' '
31 CONTINUE
300 FORMAT (1X, F7.2, 3X, F9.6, 3X, F7.2)
C*****-----*****C
WRITE (9,*) ' * POWER LOSS VARY WITH REDIUS BEARING BIG-END '
WRITE (9,*) ' REDIUS BEARING BIG-END (m) & POWER LOSS (W) '
DO 41 I = 0, RPMN, 1
DO 42 J = 0, N, 1
    DBRCON = (BRCONH-BRCONL)/N
    RPM = RPML + I*DRPM
    BRCON = BRCONL + J*DBRCON
    PBRCON = VISB*(BRCON**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE (9,400) RPM, BRCON, PBRCON
WRITE (6,400) RPM, BRCON, PBRCON
42 CONTINUE
WRITE (9,*) ' '
41 CONTINUE
400 FORMAT (1X, F7.2, 3X, F9.5, 3X, F7.2)
C*****-----*****C
WRITE (9,*) ' * POWER LOSS VARY WITH REDIUS CLEARANCE BIG-END '
WRITE (9,*) ' REDIUS CLEARANCE BIG-END (m) & POWER LOSS (W) '
DO 51 I = 0, RPMN, 1
DO 52 J = 0, N, 1
    DBCCON = (BCCONH-BCCONL)/N
    RPM = RPML + I*DRPM
    BCCON = BCCONL + J*DBCCON
    PBCCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCON*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE (9,500) RPM, BCCON, PBCCON
WRITE (6,500) RPM, BCCON, PBCCON
52 CONTINUE
WRITE (9,*) ' '
51 CONTINUE
500 FORMAT (1X, F7.2, 3X, F9.7, 3X, F7.2)
C*****-----*****C
WRITE (9,*) ' * POWER LOSS VARY WITH BEARING WIDTH BIG-END '
WRITE (9,*) ' BEARING WIDTH BIG-END (m) & POWER LOSS (W) '
DO 61 I = 0, RPMN, 1
DO 62 J = 0, N, 1
    DBLCON = (BLCONH-BLCONL)/N
    RPM = RPML + I*DRPM
    BLCON = BLCONL + J*DBLCON
C.....SUBPROGRAM MAEN 1 FOR CALCULATION MEAN ANGULAR VELOCITY
CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
PBLCON = VISB*(BRCONB**3)*BLCON*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +

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$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE(9,600) RPM,BLCON,PBLCON
WRITE(6,600) RPM,BLCON,PBLCON
62 CONTINUE
WRITE(9,*) ' '
61 CONTINUE
600 FORMAT(1X,F7.2,3X,F9.5,3X,F7.2)
C*****
WRITE(9,*) ' * POWER LOSS VARY WITH REDIUS BEARING SMALL-END '
WRITE(9,*) ' REDIUD BEARING SMALL-END (m) & POWER LOSS (W) '
DO 71 I = 0,RPMN,1
DO 72 J = 0,N,1
DSRCON = (SRCONH-SRCONL)/N
RPM = RPML + I*DRPM
SRCON = SRCONL + J*DSRCON
C.....SUBPROGRAM MAEN 1 FOR CALCULATION MEAN ANGULAR VELOCITY
CALL MEAN1(CONLB,ARMB,VEMEAN1,VSMEAN1)
PSRCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE(9,700) RPM,SRCON,PSRCON
WRITE(6,700) RPM,SRCON,PSRCON
72 CONTINUE
WRITE(9,*) ' '
71 CONTINUE
700 FORMAT(1X,F7.2,3X,F9.6,3X,F7.2)
C*****
WRITE(9,*) ' * POWER LOSS VARY WITH REDIUS CLEARANCE SMALL-END '
WRITE(9,*) ' REDIUS CLEARANCE SAMLL-END (m) & POWER LOSS (W) '
DO 81 I = 0,RPMN,1
DO 82 J = 0,N,1
DSCCON = (SCCONH-SCCONL)/N
RPM = RPML + I*DRPM
SCCON = SCCONL + J*DSCCON
PSCCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCON*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE(9,800) RPM,SCCON,PSCCON
WRITE(6,800) RPM,SCCON,PSCCON
82 CONTINUE
WRITE(9,*) ' '
81 CONTINUE
800 FORMAT(1X,F7.2,3X,F9.7,3X,F7.2)
C*****
WRITE(9,*) ' * POWER LOSS VARY WITH BEARING WIDTH SMALL-END '
WRITE(9,*) ' BEARING WIDTH SMALL-END (m) & POWER LOSS (W) '
DO 91 I = 0,RPMN,1
DO 92 J = 0,N,1
DSLCON = (SLCONH-SLCONL)/N
RPM = RPML + I*DRPM
SLCON = SLCONL + J*DSLCON
PSLCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$      VISB*(SRCONB**3)*SLCON*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
WRITE(9,900) RPM,SLCON,PSLCON
WRITE(6,900) RPM,SLCON,PSLCON
92 CONTINUE
WRITE(9,*) ' '
91 CONTINUE
900 FORMAT(1X,F7.2,3X,F9.5,3X,F7.2)
C*****
WRITE(9,*) ' * POWER LOSS VARY WITH CON-ROD TO CRANK RATIO '
WRITE(9,*) ' CON-ROD TO CRANK RATIO & POWER LOSS (W) '
RH = CONLH/ARML
RL = CONLL/ARMH

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DO 93 I = 0, RPMN, 1
DO 94 J = 0, N, 1
  DR = (RH-RL)/N
  RPM = RPML + I*DRPM
  R = RL + J*DR
CALL MEAN4 (R, VMEAN4, VSMEAN4)
  PRCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
  $      *((2*PI*(RPM/60))**2)*NCB*VMEAN4 +
  $      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
  $      *((2*PI*(RPM/60))**2)*NCB*VSMEAN4
  WRITE(9,901) RPM,R,PRCON
  WRITE(6,901) RPM,R,PRCON
94 CONTINUE
  WRITE(9,*) ' '
93 CONTINUE
901 FORMAT(1X,F7.2,3X,F9.5,3X,F7.2)
RETURN
END

```

```

C*****-----*****C
C          (P2) SUBROUTINE FOR CRANK-SHAFT BEARING          C
C*****-----*****C

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```

SUBROUTINE P2 (N, RPMH, RPML, RPMN, VISB, RCRAKKB, CRANKLB, CCRANKB, BN,
$ VISL, VISH, RCRANKL, RCRANKH, CRANKLL, CRANKLH, CCRANKL, CCRANKH,
$ PVIS, PRCRANK, PLCRANK, PCCRANK, EC, PI, POINT, RPMMAX)
IF (POINT.EQ.2) THEN
  RPMH = RPMMAX
  RPMMAX = RPMMAX
ENDIF
DRPM = (RPMH-RPML)/RPMN
OPEN(UNIT=9, FILE='RESULT2.OUT', STATUS='OLD')
WRITE(9,*) 'POWER LOSS FROM CRANK-SHAFT BEARING '
WRITE(9,*) ' * POWER LOSS VARY WITH ABSOLUTE VISCOSITY '
WRITE(9,*) ' ABSOLUTE VISCOSITY (Pa.s) $ POWER LOSS (W) '
DO 11 I = 0, RPMN, 1
  DO 12 J = 0, N, 1
    DRPM = (RPMH-RPML)/RPMN
    DVIS = (VISH-VISL)/N
    RPM = RPML + I*DRPM
    VIS = VISL + J*DVIS
    PVIS = VIS*(RCRAKKB**3)*CRANKLB*((2*PI)/
  $      (CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
    WRITE(9,100) RPM,VIS,PVIS
    WRITE(6,100) RPM,VIS,PVIS
12 CONTINUE
  WRITE(9,*) ' '
11 CONTINUE
100 FORMAT(1X,F7.2,3X,F9.6,3X,F7.2)

```

```

C*****-----*****C

```

```

WRITE(9,*) ' * POWER LOSS VARY WITH REDIUS BEARING '
WRITE(9,*) ' REDIUS BEARING (m) & POWER LOSS (W) '
DO 21 I = 0, RPMN, 1
  DO 22 J = 0, N, 1
    DRCRANK = (RCRANKH-RCRANKL)/N
    RPM = RPML + I*DRPM
    RCRANK = RCRANKL + J*DRCRANK
    PRCRANK = VISB*(RCRANK**3)*CRANKLB*((2*PI)
  $      / (CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
    WRITE(9,200) RPM,RCRANK,PRCRANK
    WRITE(6,200) RPM,RCRANK,PRCRANK
22 CONTINUE
  WRITE(9,*) ' '
21 CONTINUE
200 FORMAT(1X,F7.2,3X,F9.6,3X,F8.2)

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C*****-----*****C

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```

WRITE(9,*) ' * POWER LOSS VARY WITH BEARING WIDTH '
WRITE(9,*) ' BEARING WIDTH (m) & POWER LOSS (W) '
DO 31 I = 0, RPMN, 1
  DO 32 J = 0, N, 1
    DLCRANK = (CRANKLH-CRANKLL)/N

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```

RPM = RPML + I*DRPM
CRANKL = CRANKLL + J*DLCRANK
PLCRANK = VISB*(RCRANKB**3)*CRANKL*((2*PI)
$ /((CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
WRITE(9,300) RPM,CRANKL,PLCRANK
WRITE(6,300) RPM,CRANKL,PLCRANK
32 CONTINUE
WRITE(9,*) ' '
31 CONTINUE
300 FORMAT(1X,F7.2,3X,F9.6,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH REDIUS CLEARANCE '
WRITE(9,*) ' REDIUS CLEARANCE (m) & POWER LOSS (W) '
DO 41 I = 0,RPMN,1
DO 42 J = 0,N,1
DCCRANK = (CCRANKH-CCRANKL)/N
RPM = RPML + I*DRPM
CCRANK = CCRANKL + J*DCCRANK
PCCRANK = VISB*(RCRANKB**3)*CRANKLB*((2*PI)
$ /((CCRANK*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
WRITE(9,400) RPM,CCRANK,PCCRANK
WRITE(6,400) RPM,CCRANK,PCCRANK
42 CONTINUE
WRITE(9,*) ' '
41 CONTINUE
400 FORMAT(1X,F7.2,3X,F9.7,3X,F7.2)
RETURN
END
C*****-----*****C
C (P3) SUBROUTINE FOR PISTON SKIRT C
C*****-----*****C
SUBROUTINE P3(N,RPMH,RPML,RPMN,VISL,VISH,PCL,PCH,PISLL,PISLH,NCB,
$ARMH,ARML,BOREH,BOREL,BOREB,ARMB,VISB,PCB,PISLB,PVPIS,PCPPIS,
$PLPIS,PAPIS,PBPIS,PI,POINT,RPMMAX)
IF (POINT.EQ.3) THEN
RPMH = RPMMAX
RPMMAX = RPMMAX
ENDIF
DRPM = (RPMH-RPML)/RPMN
OPEN(UNIT=9,FILE='RESULT2.OUT',STATUS='OLD')
WRITE(9,*) 'POWER LOSS FROM PISTON SKIRT '
WRITE(9,*) ' * POWER LOSS VARY WITH ABSOLUTE VISCOSITY '
WRITE(9,*) ' ABSOLUTE VISCOSITY (Pa.s) & POWER LOSS (W) '
DO 11 I = 0,RPMN,1
DO 12 J = 0,N,1
DVIS = (VISH-VISL)/N
RPM = RPML + I*DRPM
VIS = VISL + J*DVIS
PVPIS = (VIS*PI*BOREB*PISLB/PCB)*((ARMB*(RPM/15))**2)*NCB
WRITE(9,100) RPM,VIS,PVPIS
WRITE(6,100) RPM,VIS,PVPIS
12 CONTINUE
WRITE(9,*) ' '
11 CONTINUE
100 FORMAT(1X,F7.2,3X,F9.7,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH PISTON CLEARANCE '
WRITE(9,*) ' PISTON CLEARANCE (mm) & POWER LOSS (W) '
DO 21 I = 0,RPMN,1
DO 22 J = 0,N,1
DPC = (PCH-PCL)/N
RPM = RPML + I*DRPM
PC = PCL + J*DPC
PCPPIS = (VISB*PI*BOREB*PISLB/PC)*((ARMB*(RPM/15))**2)*NCB
WRITE(9,200) RPM,PC,PCPPIS
WRITE(6,200) RPM,PC,PCPPIS
22 CONTINUE
WRITE(9,*) ' '
21 CONTINUE

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200 FORMAT (1X,F7.2,3X,F9.7,3X,F7.2)
C*****-----*****C
  WRITE (9,*) ' * POWER LOSS VARY WITH SKIRT LENGTH '
  WRITE (9,*) ' SKIRT LENGTH (m) & POWER LOSS (W) '
  DO 31 I = 0,RPMN,1
  DO 32 J = 0,N,1
    DPISL = (PISLH-PISLL)/N
    RPM = RPML + I*DRPM
    PISL = PISLL + J*DPISL
    PLPIS = (VISB*PI*BOREB*PISL/PCB)*((ARMB*(RPM/15))**2)*NCB
    WRITE (9,300) RPM,PISL,PLPIS
    WRITE (6,300) RPM,PISL,PLPIS
  32 CONTINUE
  WRITE (9,*) ' '
  31 CONTINUE
300 FORMAT (1X,F7.2,3X,F8.5,3X,F7.2)
C*****-----*****C
  WRITE (9,*) ' * POWER LOSS VARY WITH CRANK ARM '
  WRITE (9,*) ' CRANK ARM (m) & POWER LOSS (W) '
  DO 41 I = 0,RPMN,1
  DO 42 J = 0,N,1
    DARM = (ARMH-ARML)/N
    RPM = RPML + I*DRPM
    ARM = ARML + J*DARM
    PAPIS = (VISB*PI*BOREB*PISLB/PCB)*((ARM*(RPM/15))**2)*NCB
    WRITE (9,400) RPM,ARM,PAPIS
    WRITE (6,400) RPM,ARM,PAPIS
  42 CONTINUE
  WRITE (9,*) ' '
  41 CONTINUE
400 FORMAT (1X,F7.2,3X,F7.4,3X,F7.2)
C*****-----*****C
  WRITE (9,*) ' * POWER LOSS VARY WITH PISTON BORE '
  WRITE (9,*) ' PISTON BORE (m) & POWER LOSS (W) '
  DO 51 I = 0,RPMN,1
  DO 52 J = 0,N,1
    DBORE = (BOREH-BOREL)/N
    RPM = RPML + I*DRPM
    BORE = BOREL + J*DBORE
    PBPIS = (VISB*PI*BORE*PISLB/PCB)*((ARMB*(RPM/15))**2)*NCB
    WRITE (9,500) RPM,BORE,PBPIS
    WRITE (6,500) RPM,BORE,PBPIS
  52 CONTINUE
  WRITE (9,*) ' '
  51 CONTINUE
500 FORMAT (1X,F7.2,3X,F7.4,3X,F7.2)
  RETURN
  END
C*****-----*****C
C (P4) SUBROUTINE FOR PISTON RING C
C*****-----*****C
  SUBROUTINE P4 (N,RPMH,RPML,RPMN,VISL,VISH,BPRESSL,BPRESSH,
  $ BOILL,BOILH,BOREL,BOREH,ARML,ARMH,NCB,BOREB,ARMB,VISB,BPRESSB,
  $ BOILB,NPRESSB,NOILB,H,PVRING,PBPRING,PBORING,PBRING,PARING,
  $ PI,RP,RO,POINT,RPMMAX)
  IF (POINT.EQ.4) THEN
    RPMH = RPMMAX
    RPMMAX = RPMMAX
  ENDIF
  DRPM = (RPMH-RPML)/RPMN
  OPEN (UNIT=9,FILE='RESULT2.OUT',STATUS='OLD')
C*****-----*****C
  WRITE (9,*) 'POWER LOSS PISTON RING '
  WRITE (9,*) ' * POWER LOSS VARY WITH ABSOLUTE VISCOSITY '
  WRITE (9,*) ' ABSOLUTE VISCOSITY (Pa.s) & POWER LOSS (W) '
  DO 11 I = 0,RPMN,1
  DO 12 J = 0,N,1
    DVIS = (VISH-VISL)/N
    RPM = RPML + I*DRPM

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      VIS = VISL + J*DVIS
C.....SUBPROGRAM FOR INTERATION NUM 1
CALL NUM1 (BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
PVRING = VIS*ARMB*2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB
$      *(1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$      VIS*ARMB*2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB
$      *(1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
      WRITE (9,100) RPM,VIS,PVRING
      WRITE (6,100) RPM,VIS,PVRING
12 CONTINUE
      WRITE (9,*) ' '
11 CONTINUE
100 FORMAT (1X,F7.2,3X,F8.6,3X,F7.2)
C*****-----*****C
      WRITE (9,*) ' * POWER LOSS VARY WITH PRESSURE RING WIDTH '
      WRITE (9,*) ' PRESSURE RING WIDTH (mm) & POWER LOSS (W) '
      DO 21 I = 0,RPMN,1
      DO 22 J = 0,N,1
      DBPRESS = (BPRESSH-BPRESSL)/N
      RPM = RPML + I*DRPM
      BPRESS = BPRESSL + J*DBPRESS
C.....SUBPROGRAM FOR INTERATION NUM 2
CALL NUM2 (BPRESS,BOILB,RP,RO,H,HP4,HO4,HP5,HO5,HP6,HO6)
PBPRING = VISB*ARMB*2*PI*(RPM/60)*(4*HO4-3*(HO5**2)/HO6+BOILB
$      *(1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$      VISB*ARMB*2*PI*(RPM/60)*(4*HP4-3*(HP5**2)/HP6+(BPRESS
$      *(1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
      WRITE (9,200) RPM,BPRESS,PBPRING
      WRITE (6,200) RPM,BPRESS,PBPRING
22 CONTINUE
      WRITE (9,*) ' '
21 CONTINUE
200 FORMAT (1X,F7.2,3X,F6.3,3X,F7.2)
C*****-----*****C
      WRITE (9,*) ' * POWER LOSS VARY WITH OIL RING WIDTH '
      WRITE (9,*) ' OIL RING WIDTH (mm) & POWER LOSS (W) '
      DO 31 I = 0,RPMN,1
      DO 32 J = 0,N,1
      DBOIL = (BOILH-BOIL)/N
      RPM = RPML + I*DRPM
      BOIL = BOILL + J*DBOIL
C.....SUBPROGRAM FOR INTERATION NUM 3
CALL NUM3 (BPRESSB,BOIL,RP,RO,H,HP7,HO7,HP8,HO8,HP9,HO9)
PBORING = VISB*ARMB*2*PI*(RPM/60)*(4*HO7-3*(HO8**2)/HO9+BOIL
$      *(1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$      VISB*ARMB*2*PI*(RPM/60)*(4*HP7-3*(HP8**2)/HP9+(BPRESSB
$      *(1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
      WRITE (9,300) RPM,BOIL,PBORING
      WRITE (6,300) RPM,BOIL,PBORING
32 CONTINUE
      WRITE (9,*) ' '
31 CONTINUE
300 FORMAT (1X,F7.2,3X,F6.3,3X,F7.2)
C*****-----*****C
      WRITE (9,*) ' * POWER LOSS VARY WITH PISTON BORE '
      WRITE (9,*) ' PISTON BORE (m) & POWER LOSS (W) '
      DO 41 I = 0,RPMN,1
      DO 42 J = 0,N,1
      DBORE = (BOREH-BOREL)/N
      RPM = RPML + I*DRPM
      BORE = BOREL + J*DBORE
      ARMV = ARMB*((BOREB/BORE)**2)
      CALL NUM1 (BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
      PBRING = VISB*ARMV*2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB
$      *(1-RO)/(1+RO))*4*ARMV*PI*BORE*(RPM/60)*NOILB*NCB +
$      VIS*ARMV*2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB
$      *(1-RP)/(1+RP))/H)*4*ARMV*PI*BORE*(RPM/60)*NPRESSB*NCB
      WRITE (9,400) RPM,BORE,PBRING
      WRITE (6,400) RPM,BORE,PBRING

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42 CONTINUE
WRITE(9,*) ' '
41 CONTINUE
400 FORMAT(1X,F7.2,3X,F7.5,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH CRANK ARM '
WRITE(9,*) ' CRANK ARM (m) & POWER LOSS (W) '
DO 51 I = 0,RPMN,1
DO 52 J = 0,N,1
DARM = (ARMH-ARML)/N
RPM = RPML + I*DRPM
ARM = ARML + J*DARM
CALL NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
BOREV = BOREB*SQRT(ARMB/ARM)
PARING = VISB*ARM*2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB
$ *(1-RO)/(1+RO))*4*ARM*PI*BOREV*(RPM/60)*NOILB*NCB +
$ VIS*ARM*2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB
$ *(1-RP)/(1+RP))/H)*4*ARM*PI*BOREV*(RPM/60)*NPRESSB*NCB
WRITE(9,500) RPM,ARM,PARING
WRITE(6,500) RPM,ARM,PARING
52 CONTINUE
WRITE(9,*) ' '
51 CONTINUE
500 FORMAT(1X,F7.2,3X,F7.5,3X,F7.2)
RETURN
END
C*****-----*****C
C (P5) SUBROUTINE FOR CAM LOAD C
C*****-----*****C
SUBROUTINE P5(N,RPMH,RPML,RPMN,FML,FMH,SCL,SCH,PLL,PLH,BRL,BRH
$ ,TRL,TRH,VLL,VLH,NVCB,NCB,FMB,SCB,PLB,BRB,TRB,VLB,SDEGB
$ ,PFCAM,PSCAM,PPCAM,PBCAM,PTCAM,PVCAM,PI,FCOE,POINT,RPMMAX)
FB = (BRB**2-TRB**2+(BRB+VLB-TRB)**2-2*BRB*(BRB+VLB-TRB)
$ *SIN(SDEGB*PI/180))/(2*(BRB-TRB-(BRB+VLB-TRB)
$ *SIN(SDEGB*PI/180)))
IF (POINT.EQ.5) THEN
RPMH = 3000.
RPMMAX = RPMMAX
ENDIF
CDEGB = ACOS( (FB-BRB)*COS(SDEGB*PI/180)/(FB-TRB) )*180/PI
OPEN(UNIT=9,FILE='RESULT2.OUT',STATUS='OLD')
WRITE(9,*) 'POWER LOSS CAM LOAD '
WRITE(9,*) ' * POWER LOSS VARY WITH FOLLOWER MASS '
WRITE(9,*) ' FOLLOWER MASS(kg) & POWER LOSS (W) '
DRPM = (RPMH-RPML)/RPMN
DO 11 I = 0,RPMN,1
DO 12 J = 0,N,1
DFM = (FMH-FML)/N
RPM = RPML + I*DRPM
RPMC = RPM/2
RADC = (RPMC*2*PI/60)
FM = FML + J*DFM
C.....SUBPROGRAM TMEAN1 FOR CALCULATE MEAN TORQUE
CALL TMEAN1(FCOE,SDEGB,FB,CDEGB,FM,SCB,PLB,BRB,TRB,VLB,RADC,TOR1
$ ,PI)
PFCAM = -TOR1*RADC*NCB*NVCB
WRITE(9,100) RPM,FM,PFCAM
WRITE(6,100) RPM,FM,PFCAM
12 CONTINUE
WRITE(9,*) ' '
11 CONTINUE
100 FORMAT(1X,F7.2,3X,F6.3,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH SPRING CONSTANT '
WRITE(9,*) ' SPRING CONSTANT (N/m) & POWER LOSS (W) '
DO 21 I = 0,RPMN,1
DO 22 J = 0,N,1
DSC = (SCH-SCL)/N
RPM = RPML + I*DRPM

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RPMC = RPM/2
RADC = (RPMC*2*PI/60)
SC = SCL + J*DSC
C.....SUBPROGRAM TMEAN2 FOR CALCULATE MEAN TORQUE
CALL TMEAN2 (FCOE, SDEGB, FB, CDEGB, FMB, SC, PLB, BRB, TRB, VLB, RADC, TOR2
$, PI)
PSCAM = -TOR2*RADC*NCB*NVCB
WRITE(9,200) RPM, SC, PSCAM
WRITE(6,200) RPM, SC, PSCAM
22 CONTINUE
WRITE(9,*) ' '
21 CONTINUE
200 FORMAT(1X,F7.2,3X,F8.2,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH SPRING PRELOAD '
WRITE(9,*) ' SPRING PRELOAD (N) & POWER LOSS (W) '
DO 31 I = 0, RPMN, 1
DO 32 J = 0, N, 1
DPL = (PLH-PLL)/N
RPM = RPML + I*DRPM
RPMC = RPM/2
RADC = (RPMC*2*PI/60)
PL = PLL + J*DPL
C.....SUBPROGRAM TMEAN3 FOR CALCULATE MEAN TORQUE
CALL TMEAN3 (FCOE, SDEGB, FB, CDEGB, FMB, SCB, PL, BRB, TRB, VLB, RADC, TOR3
$, PI)
PPCAM = -TOR3*RADC*NCB*NVCB
WRITE(9,300) RPM, PL, PPCAM
WRITE(6,300) RPM, PL, PPCAM
32 CONTINUE
WRITE(9,*) ' '
31 CONTINUE
300 FORMAT(1X,F7.2,3X,F6.2,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH BASE RADIUS '
WRITE(9,*) ' BASE RADIUS (mm.) & POWER LOSS (W) '
DO 41 I = 0, RPMN, 1
DO 42 J = 0, N, 1
DBR = (BRH-BRL)/N
RPM = RPML + I*DRPM
RPMC = RPM/2
RADC = (RPMC*2*PI/60)
BR = BRL + J*DBR
FBR = (BR**2-TRB**2+(BR+VLB-TRB)**2-2*BR*(BR+VLB-TRB)
$ *SIN(SDEGB*PI/180))
$ / (2*(BR-TRB-(BR+VLB-TRB)*SIN(SDEGB*PI/180)))
CDEGBR = ACOS( (FBR-BR)*COS(SDEGB*PI/180)/(FBR-TRB) ) *180/PI
C.....SUBPROGRAM TMEAN4 FOR CALCULATE MEAN TORQUE
CALL TMEAN4 (FCOE, SDEGB, FBR, CDEGBR, FMB, SCB, PLB, BR, TRB, VLB, RADC
$, TOR4, PI)
PBCAM = -TOR4*RADC*NCB*NVCB
WRITE(9,400) RPM, BR, PBCAM
WRITE(6,400) RPM, BR, PBCAM
42 CONTINUE
WRITE(9,*) ' '
41 CONTINUE
400 FORMAT(1X,F7.2,3X,F6.3,3X,F7.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH TIP RADIUS '
WRITE(9,*) ' TIP RADIUS (mm.) & POWER LOSS (W) '
DO 51 I = 0, RPMN, 1
DO 52 J = 0, N, 1
DTR = (TRH-TRL)/N
RPM = RPML + I*DRPM
RPMC = RPM/2
RADC = (RPMC*2*PI/60)
TR = TRL + J*DTR
FTR = (BRB**2-TR**2+(BRB+VLB-TR)**2-2*BRB*(BRB+VLB-TR)
$ *SIN(SDEGB*PI/180))

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$          / (2* (BRB-TR- (BRB+VLB-TR) *SIN (SDEGB*PI/180)))
CDEGTR = ACOS ( (FTR-BRB)*COS (SDEGB*PI/180) / (FTR-TR) ) *180/PI
C.....SUBPROGRAM TMEANS FOR CALCULATE MEAN TORQUE
CALL TMEANS (FCOE, SDEGB, FTR, CDEGTR, FMB, SCB, PLB, BRB, TR, VLB, RADC
$, TOR5, PI)
    PTCAM = -TOR5*RADC*NCB*NVCB
    WRITE (9, 500) RPM, TR, PTCAM
    WRITE (6, 500) RPM, TR, PTCAM
52 CONTINUE
    WRITE (9, *) ' '
51 CONTINUE
500 FORMAT (1X, F7.2, 3X, F6.3, 3X, F7.2)
C*****-----*****C
    WRITE (9, *) ' * POWER LOSS VARY WITH TIP RADIUS '
    WRITE (9, *) ' BASE , TIP RADIUS (mm.) & POWER LOSS. (W) '
    DO 511 I = 0, RPMN, 1
    DO 521 J = 0, N, 1
    DO 531 K = 0, N, 1
        DRPM = (RPMH-RPML) / RPMN
        DBR = (BRH-BRL) / N
        DTR = (TRH-TRL) / N
        RPM = RPML + I*DRPM
        BR = BRL + J*DBR
        TR = TRL + K*DTR
        RPMC = RPM/2
        RADC = (RPMC*2*PI/60)
        FBTR = (BR**2-TR**2+ (BR+VLB-TR) **2
$           -2*BR* (BR+VLB-TR) *SIN (SDEGB*PI/180))
$           / (2* (BR-TR- (BR+VLB-TR)
$           *SIN (SDEGB*PI/180)))
        CDEGBTR = (ACOS ( (FBTR-BR) *COS (SDEGB*PI/180)
$           / (FBTR-TR))) *180/PI
C.....SUBPROGRAM TMEAS1 FOR CALCULATE MEAN TORQUE
CALL TMEAS1 (FCOE, SDEGB, FBTR, CDEGBTR, FMB, SCB, PLB, BR, TR
$, VLB, RADC, TOR51, PI)
    PBTCAM = -TOR51*RADC*NCB*NVCB
    WRITE (9, 501) RPM, BR, TR, PBTCAM
    WRITE (6, 501) RPM, BR, TR, PBTCAM
531 CONTINUE
521 CONTINUE
    WRITE (9, *) ' '
511 CONTINUE
501 FORMAT (1X, F7.2, 3X, F6.3, 3X, F6.3, 3X, F7.2)
C*****-----*****C
    WRITE (9, *) ' * POWER LOSS VARY WITH VALVE LIFT '
    WRITE (9, *) ' VALVE LIFT (mm.) & POWER LOSS (W) '
    DO 61 I = 0, RPMN, 1
    DO 62 J = 0, N, 1
        DVL = (VLH-VLL) / N
        RPM = RPML + I*DRPM
        RPMC = RPM/2
        RADC = (RPMC*2*PI/60)
        VL = VLL + J*DVL
        FVL = (BRB**2-TRB**2+ (BRB+VL-TRB) **2-2*BRB* (BRB+VL-TRB)
$           *SIN (SDEGB*PI/180))
$           / (2* (BRB-TRB- (BRB+VL-TRB) *SIN (SDEGB*PI/180)))
        CDEGVL = (ACOS ( (FVL-BRB) *COS (SDEGB*PI/180)
$           / (FVL-TRB))) *180/PI
C.....SUBPROGRAM TMEAN6 FOR CALCULATE MEAN TORQUE
CALL TMEAN6 (FCOE, SDEGB, FVL, CDEGVL, FMB, SCB, PLB, BRB, TRB, VL, RADC
$, TOR6, PI)
    PVCAM = -TOR6*RADC*NCB*NVCB
    WRITE (9, 600) RPM, VL, PVCAM
    WRITE (6, 600) RPM, VL, PVCAM
62 CONTINUE
    WRITE (6, *) ' '
61 CONTINUE
600 FORMAT (1X, F7.2, 3X, F7.2, 3X, F7.2)
RETURN

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END
C*****-----*****C
C          (P6) SUBROUTINE FOR ACCESSORIES LOAD          C
C*****-----*****C
SUBROUTINE P6(N,RPMH,RPML,RPMN,BCOMB,SCOMB,NCB,BOREB,ARMS,RKB,EMB,
$ECB,RDALTB,RLALTB,QH,QL,H1,H2,V1,RDALTL,RDALTH,RLALTL,RLALTH,RCOM,
$NCOM,PCLE,EVAPP,CONDP,CORRK,RALT,PWP,PAIRQ,PALTD,PALTL,PI,POINT,
$FRAC,RPMMAX)
  AMPB = 50.
  VOLTB = 12.
  VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)
  IF (POINT.EQ.6) THEN
    RPMH = 2600.
    RPMMAX = RPMMAX
  ENDIF
  DRPM = (RPMH-RPML)/RPMN
  OPEN(UNIT=9,FILE='RESULT2.OUT',STATUS='OLD')
  WRITE(9,*) 'POWER LOSS FROM ACCESSORIES LOAD'
  WRITE(9,*) ' * POWER LOSS VARY WITH COOLING LOAD'
  WRITE(9,*) ' COOLING LOAD (W) & POWER LOSS (W)'
  DO 11 I = 1,2,1
    DO 12 J = 0,N,1
      DQ = (QH-QL)/N
      Q = QL + J*DQ
    DO 13 K = 0,RPMN,1
      IF (I.EQ.1) THEN
        RPMCOOL = Q/(H1-H2)*4.*60.*V1/
        $ (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2)
        DRPMC = (RPMCOOL-RPML)/RPMN
        RPMV = RPML + K*DRPMC
        PAIRQ = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(RPMV/60.)*VOLEEF
        $ *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
        $ *EVAPP*(1./(EMB*ECB))*(-1.)
      ELSE
        DRPMC = (RPMH-RPMCOOL)/RPMN
        RPMV = RPMCOOL + K*DRPMC
        PAIRQ = Q/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
        $ *(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
        $ *(1./(EMB*ECB))*(-1.)
      ENDIF
      WRITE(9,101) RPMV,Q,PAIRQ
      WRITE(6,101) RPMV,Q,PAIRQ
    13 CONTINUE
    WRITE(9,*) ' '
    12 CONTINUE
    WRITE(9,*) ' '
    11 CONTINUE
  101 FORMAT(1X,F7.2,3X,F7.2,3X,F8.2)
C*****-----*****C
  WRITE(9,*) ' * POWER LOSS VARY WITH ROTOR DIAMETER'
  WRITE(9,*) ' ROTOR DIAMETER (m) & POWER LOSS (W)'
  DO 21 I = 0,RPMN,1
    DO 22 J = 0,N,1
      DRDALT = (RDALTH - RDALTL)/N
      RPM = RPML + I*DRPM
      RDALT = RDALTL + J*DRDALT
      PALTD = AMPB*VOLTB + (100./FRAC)*(1./3.)*CORRK*
      $ ((RALT*PI*RDALT*RPM/3048.)**2.5)*1000
      $ *(RDALT/0.0254)*((RLALTB/0.0254)**0.5)
      WRITE(9,201) RPM,RDALT,PALTD
      WRITE(6,201) RPM,RDALT,PALTD
    22 CONTINUE
    WRITE(9,*) ' '
    21 CONTINUE
  201 FORMAT(1X,F7.2,3X,F7.4,3X,F7.2)
C*****-----*****C
  WRITE(9,*) ' * POWER LOSS VARY WITH ROTOR LENGTH'
  WRITE(9,*) ' ROTOR LENGTH (m) & POWER LOSS (W)'
  DO 23 I = 0,RPMN,1

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DO 24 J = 0,N,1
  DRLALT = (RLALTH - RLALTL)/N
  RPM = RPML + I*DRPM
  RLALT = RLALTL + J*DRLALT
  PALTL = AMPB*VOLTB + (100./FRAC)*(1/3.)*CORRK*
$      ((RALT*PI*RDALTB*RPM/3048.))**2.5)*1000
$      *(RDALTB/0.0254)*((RLALT/0.0254)**0.5)
  WRITE(9,202) RPM,RLALT,PALTL
  WRITE(6,202) RPM,RLALT,PALTL
24 CONTINUE
  WRITE(9,*) ' '
23 CONTINUE
202 FORMAT(1X,F7.2,3X,F7.4,3X,F7.2)
C*****-----*****C
  WRITE(9,*) ' * POWER LOSS VARY WITH WATER&OIL PUMP '
  WRITE(9,*) ' ENGINE SPEED (rpm) & POWER LOSS (W) '
  RPMH = RPMMAX
  DRPM = (RPMH-RPML)/RPMN
DO 25 I = 0,RPMN,1
  RPM = RPML + I*DRPM
  PWP = (269./12.)*((RPM/1000.))**1.5)*RPM
$      *(2.*ARMB*NCB*PI*(BOREB**2.)/4.)
  WRITE(9,203) RPM,PWP
  WRITE(6,203) RPM,PWP
25 CONTINUE
  WRITE(9,*) ' '
203 FORMAT(1X,F7.2,3X,F7.2)
  RETURN
  END
C*****-----*****C
C      (P7) SUBROUTINE FOR PUMPING LOSSES C
C*****-----*****C
  SUBROUTINE P7(N,RPMH,RPML,RPMN,DHH,DHL,M,DVL,DVH,RCL,RCH,NCB,
$BOREB,ARMB,DVB,RCB,NVB,DENHG,PE,PA,PDPUMP,PRPUMP,PI,POINT,RPMMAX)
  IF (POINT.EQ.7) THEN
    RPMH = 4000.
    RPMMAX = RPMMAX
  ENDIF
  DRPM = (RPMH-RPML)/RPMN
  DDH = (DHH-DHL)/M
  OPEN(UNIT=9,FILE='RESULT2.OUT',STATUS='OLD')
  WRITE(9,*) 'POWER LOSS FROM PUMPING LOSSES '
  WRITE(9,*) ' * POWER LOSS VARY WITH VALVE DIAMETER '
  WRITE(9,*) ' VALVE DAIMETER (m) & PUMPING LOSS (W) '
DO 11 I = 0,RPMN,1
DO 12 J = 0,M,1
  DO 13 K = 0,N,1
    DDV = (DVH-DVL)/N
    RPM = RPML + I*DRPM
    DH = DHL + J*DDH
    DV = DVL + K*DDV
    PIA = 9.81*DENHG*DH*0.0254/1000
    CIMEP = 12.87*PA*((PIA/PA)-0.1)
    PIG = PA-(CIMEP/12.8)-10.14
    F = (NVB*NCB*(DV**2))/(2*ARMB*PI*NCB*(BOREB**2)/4)
    PDPUMP = (PA-(CIMEP/12.8)-10.14+PE*((CIMEP*RPM)/(3904000))**2) +
$      8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)
$      *((2.984/F)**1.28) + (SQRT((PA-PIG)/97.94))
$      *(11.86*(RCB**0.4)-(3.38+0.103*RCB))*((RPM/1000)**1.185))
$      *1000*(2*ARMB*PI*NCB*(BOREB**2)/4)*(RPM/120)
  WRITE(9,100) RPM,DH,DV,PDPUMP
  WRITE(6,100) RPM,DH,DV,PDPUMP
13 CONTINUE
  WRITE(9,*) ' '
12 CONTINUE
  WRITE(9,*) ' '
11 CONTINUE
100 FORMAT(1X,F7.2,3X,F5.2,3X,F9.6,2X,F9.2)
C*****-----*****C

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WRITE(9,*) ' * POWER LOSS VARY WITH COMPRESSION RATIO '
WRITE(9,*) ' COMPRESSION RATIO & PUMPING LOSS (W) '
DO 21 I = 0, RPMN, 1
DO 22 J = 0, M, 1
DO 23 K = 0, N, 1
    DRC = (RCH-RCL)/N
    RPM = RPML + I*DRPM
    DH = DHL + J*DDH
    RC = RCL + K*DRC
    PIA = 9.81*DENHG*DH*0.0254/1000
    CIMEP = 12.87*PA*((PIA/PA)-0.1)
    PIG = PA-(CIMEP/12.8)-10.14
    F = (NVB*NCB*(DVB**2))/(2*ARMB*PI*NCB*(BOREB**2)/4)
    PRPUMP = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*RPM)/(3904000))**2) +
$      8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)
$      *((2.984/F)**1.28) + (SQRT((PA-PIG)/97.94))
$      *(11.86*(RC**0.4)-(3.38+0.103*RC))*((RPM/1000)**1.185)))
$      *1000*(2*ARMB*PI*NCB*(BOREB**2)/4)*(RPM/120)
    WRITE(9,200) RPM, DH, RC, PRPUMP
    WRITE(6,200) RPM, DH, RC, PRPUMP
23 CONTINUE
    WRITE(9,*) ' '
22 CONTINUE
    WRITE(9,*) ' '
21 CONTINUE
200 FORMAT(1X, F7.2, 3X, F6.2, 3X, F6.2, 3X, F9.2)
RETURN
END

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C*****-----*****C
C      (P8) SUBROUTINE FOR CALCULATION ENGINE POWER REQUIRED      C
C*****-----*****C

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SUBROUTINE P8(N, CDB, AREAB, FRB, MGB, WR, RPMH, RPML, RPMN, CDL, CDH, AFL,
$ AFH, FRL, FRH, MGL, MGH, G1, G2, G3, G4, G5, GD, PI, AIRDEN, PAIRC, PAIRA,
$ PROLLF, PROLLM, POINT, RPMMAX)
IF (POINT.EQ.8) THEN
    RPMH = RPMMAX
    RPMMAX = RPMMAX
ENDIF
DRPM = (RPMH-RPML)/RPMN
OPEN(UNIT=9, FILE='RESULT2.OUT', STATUS='OLD')

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C*****-----*****C

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WRITE(9,*) ' * POWER LOSS VARY WITH CD '
WRITE(9,*) ' CD & POWER LOSS (W) '
DO 11 I = 0, RPMN, 1
DO 12 J = 0, N, 1
    RPM = RPML + I*DRPM
    DCD = (CDH-CDL)/N
    CD = CDL + J*DCD
    CALL SEL1(RPM, GN, G1, G2, G3, G4, G5, GD, TEFF, GT)
    PAIRC = 0.5*CD*AIRDEN*AREAB*(((RPM/60)*2*PI*WR/GT)**3)
    V1 = (RPM/60)*2*PI*WR/GT*3.6
    WRITE(9,100) V1, CD, PAIRC
    WRITE(6,100) V1, CD, PAIRC

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12 CONTINUE

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    WRITE(9,*) ' '

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11 CONTINUE

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100 FORMAT(1X, F7.2, 3X, F7.4, 3X, F10.2)

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C*****-----*****C

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WRITE(9,*) ' * POWER LOSS VARY WITH FRONTAL AREA '
WRITE(9,*) ' A (m^2) & POWER LOSS (W) '
DO 21 I = 0, RPMN, 1
DO 22 J = 0, N, 1
    RPM = RPML + I*DRPM
    DAF = (AFH-AFL)/N
    AF = AFL + J*DAF
    CALL SEL1(RPM, GN, G1, G2, G3, G4, G5, GD, TEFF, GT)
    PAIRA = 0.5*CDB*AIRDEN*AF*(((RPM/60)*2*PI*WR/GT)**3)
    V2 = (RPM/60)*2*PI*WR/GT*3.6
    WRITE(9,200) V2, AF, PAIRA

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WRITE(6,200) V2,AF,PAIRA
22 CONTINUE
WRITE(9,*) ' '
21 CONTINUE
200 FORMAT(1X,F7.2,3X,F7.3,3X,F10.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH ROLLING COEFFICIENT '
WRITE(9,*) ' f & POWER LOSS (W) '
DO 31 I = 0,RPMN,1
DO 32 J = 0,N,1
RPM = RPML + I*DRPM
DFR = (FRH-FRL)/N
FR = FRL + J*DFR
CALL SEL1(RPM,GN,G1,G2,G3,G4,G5,GD,TEFF,GT)
PROLLF = FR*MGB*9.81*( (RPM/60)*2*PI*WR/GT )
V3 = (RPM/60)*2*PI*WR/GT*3.6
WRITE(9,300) V3,FR,PROLLF
WRITE(6,300) V3,FR,PROLLF
32 CONTINUE
WRITE(9,*) ' '
31 CONTINUE
300 FORMAT(1X,F7.2,3X,F9.7,3X,F9.2)
C*****-----*****C
WRITE(9,*) ' * POWER LOSS VARY WITH VEHICLE MASS '
WRITE(9,*) ' M & POWER LOSS (W) '
DO 41 I = 0,RPMN,1
DO 42 J = 0,N,1
RPM = RPML + I*DRPM
DMG = (MGH-MGL)/N
VMG = MGL + J*DMG
CALL SEL1(RPM,GN,G1,G2,G3,G4,G5,GD,TEFF,GT)
PROLLM = FRB*VMG*9.81*( (RPM/60)*2*PI*WR/GT )
V4 = (RPM/60)*2*PI*WR/GT*3.6
WRITE(9,400) V4,VMG,PROLLM
WRITE(6,400) V4,VMG,PROLLM
42 CONTINUE
WRITE(9,*) ' '
41 CONTINUE
400 FORMAT(1X,F7.2,3X,F9.3,3X,F9.2)
RETURN
END
C*****-----*****C
C THIS PARTS ARE SUBPROGRAM FOR NUMERICAL CALCULATION C
C*****-----*****C
C SUBROUTINE NUM 1 C
C*****-----*****C
SUBROUTINE NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
N = 100
A = 0.
A1P = 0.0015
A1O = 0.0025
BP = RP*(BPRESSB/(1+RP))
BO = RO*(BOILB/(1+RO))
DHP = (BP-A)/N
DHO = (BO-A)/N
SUMP1 = 0.
SUMO1 = 0.
SUMP2 = 0.
SUMO2 = 0.
SUMP3 = 0.
SUMO3 = 0.
DO 10 I = 1,N-1
XP = I*DHP
XO = I*DHO
FXP1 = 1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
(1+RP))*XP+H+BPRESSB/1000)
$ FXO1 = 1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
$ (1+RP))*XO+H+BOILB/1000)
FXP2 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/

```

```

$      (1+RP))*XP+H+BPRESSB/1000))**2
FXO2 = (1/(A10*XO**2-((1+RO)/(1000*RO)+(A10*RO*BOILB)/
$      (1+RP))*XO+H+BOILB/1000))**2
FXP3 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
$      (1+RP))*XP+H+BPRESSB/1000))**3
FXO3 = (1/(A10*XO**2-((1+RO)/(1000*RO)+(A10*RO*BOILB)/
$      (1+RP))*XO+H+BOILB/1000))**3
SUMP1 = SUMP1 + FXP1
SUMO1 = SUMO1 + FXO1
SUMP2 = SUMP2 + FXP2
SUMO2 = SUMO2 + FXO2
SUMP3 = SUMP3 + FXP3
SUMO3 = SUMO3 + FXO3
10 CONTINUE
FXP01 = 1/(H+BPRESSB/1000)
FXO01 = 1/(H+BOILB/1000)
FXP02 = (1/(H+BPRESSB/1000))**2
FXO02 = (1/(H+BOILB/1000))**2
FXP03 = (1/(H+BPRESSB/1000))**3
FXO03 = (1/(H+BOILB/1000))**3
FXPN1 = 1/H
FXON1 = 1/H
FXPN2 = (1/H)**2
FXON2 = (1/H)**2
FXPN3 = (1/H)**3
FXON3 = (1/H)**3
HP1 = (+FXP01+FXPN1+2*SUMP1)*DHP/2
HO1 = (+FXO01+FXON1+2*SUMP1)*DHO/2
HP2 = (+FXP02+FXPN2+2*SUMP2)*DHP/2
HO2 = (+FXO02+FXON2+2*SUMP2)*DHO/2
HP3 = (+FXP03+FXPN3+2*SUMP3)*DHP/2
HO3 = (+FXO03+FXON3+2*SUMP3)*DHO/2
RETURN
END

```

```

C*****-----*****C
C                      SUBROUTINE NUM 2                      C
C*****-----*****C

```

```

SUBROUTINE NUM2 (BPRESS, BOILB, RP, RO, H, HP4, HO4, HP5, HO5, HP6, HO6)
N      = 100
A      = 0.
A1P    = 0.0015
A10    = 0.0025
BP     = RP*(BPRESS/(1+RP))
BO     = RO*(BOILB/(1+RO))
DHP    = (BP-A)/N
DHO    = (BO-A)/N
SUMP4  = 0.
SUMO4  = 0.
SUMP5  = 0.
SUMO5  = 0.
SUMP6  = 0.
SUMO6  = 0.
DO 10 I = 1,N-1
  XP = I*DHP
  XO = I*DHO
  FXP4 = 1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
$      (1+RP))*XP+H+BPRESS/1000)
FXO4 = 1/(A10*XO**2-((1+RO)/(1000*RO)+(A10*RO*BOILB)/
$      (1+RP))*XO+H+BOILB/1000)
FXP5 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
$      (1+RP))*XP+H+BPRESS/1000))**2
FXO5 = (1/(A10*XO**2-((1+RO)/(1000*RO)+(A10*RO*BOILB)/
$      (1+RP))*XO+H+BOILB/1000))**2
FXP6 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
$      (1+RP))*XP+H+BPRESS/1000))**3
FXO6 = (1/(A10*XO**2-((1+RO)/(1000*RO)+(A10*RO*BOILB)/
$      (1+RP))*XO+H+BOILB/1000))**3
SUMP4 = SUMP4 + FXP4
SUMO4 = SUMO4 + FXO4

```

```

SUMP5 = SUMP5 + FXP5
SUMO5 = SUMO5 + FXO5
SUMP6 = SUMP6 + FXP6
SUMO6 = SUMO6 + FXO6
10 CONTINUE
FXP04 = 1/(H+BPRESS/1000)
FXO04 = 1/(H+BOIL/1000)
FXP05 = (1/(H+BPRESS/1000))**2
FXO05 = (1/(H+BOIL/1000))**2
FXP06 = (1/(H+BPRESS/1000))**3
FXO06 = (1/(H+BOIL/1000))**3
FXPN4 = 1/H
FXON4 = 1/H
FXPN5 = (1/H)**2
FXON5 = (1/H)**2
FXPN6 = (1/H)**3
FXON6 = (1/H)**3
HP4 = (+FXP04+FXPN4+2*SUMP4)*DHP/2
HO4 = (+FXO04+FXON4+2*SUMO4)*DHO/2
HP5 = (+FXP05+FXPN5+2*SUMP5)*DHP/2
HO5 = (+FXO05+FXON5+2*SUMO5)*DHO/2
HP6 = (+FXP06+FXPN6+2*SUMP6)*DHP/2
HO6 = (+FXO06+FXON6+2*SUMO6)*DHO/2
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE NUM 3                               C
C*****-----*****C

```

```

SUBROUTINE NUM3 (BPRESSB, BOIL, RP, RO, H, HP7, HO7, HP8, HO8, HP9, HO9)

```

```

N = 100
A = 0.
A1P = 0.0015
A1O = 0.0025
BP = RP*(BPRESSB/(1+RP))
BO = RO*(BOIL/(1+RO))
DHP = (BP-A)/N
DHO = (BO-A)/N
SUMP7 = 0.
SUMO7 = 0.
SUMP8 = 0.
SUMO8 = 0.
SUMP9 = 0.
SUMO9 = 0.
DO 10 I = 1, N-1
  XP = I*DHP
  XO = I*DHO
  FXP7 = 1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
$ (1+RP))*XP+H+BPRESSB/1000)
  FXO7 = 1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOIL)/
$ (1+RP))*XO+H+BOIL/1000)
  FXP8 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
$ (1+RP))*XP+H+BPRESSB/1000))**2
  FXO8 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOIL)/
$ (1+RP))*XO+H+BOIL/1000))**2
  FXP9 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
$ (1+RP))*XP+H+BPRESSB/1000))**3
  FXO9 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOIL)/
$ (1+RP))*XO+H+BOIL/1000))**3
  SUMP7 = SUMP7 + FXP7
  SUMO7 = SUMO7 + FXO7
  SUMP8 = SUMP8 + FXP8
  SUMO8 = SUMO8 + FXO8
  SUMP9 = SUMP9 + FXP9
  SUMO9 = SUMO9 + FXO9

```

```

10 CONTINUE
FXP07 = 1/(H+BPRESSB/1000)
FXO07 = 1/(H+BOIL/1000)
FXP08 = (1/(H+BPRESSB/1000))**2
FXO08 = (1/(H+BOIL/1000))**2

```

```

FXP09 = (1/(H+BPRESSB/1000))**3
FXO09 = (1/(H+BOIL/1000))**3
FXPN7 = 1/H
FXON7 = 1/H
FXPN8 = (1/H)**2
FXON8 = (1/H)**2
FXPN9 = (1/H)**3
FXON9 = (1/H)**3
HP7 = (+FXP07+FXPN7+2*SUMP7)*DHP/2
HO7 = (+FXO07+FXON7+2*SUMP7)*DHO/2
HP8 = (+FXP08+FXPN8+2*SUMP8)*DHP/2
HO8 = (+FXO08+FXON8+2*SUMP8)*DHO/2
HP9 = (+FXP09+FXPN9+2*SUMP9)*DHP/2
HO9 = (+FXO09+FXON9+2*SUMP9)*DHO/2
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE MEAN 1                               C
C*****-----*****C

```

```

SUBROUTINE MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
PI = 2.*ASIN(1.)
R = CONLB/ARMB
N = 360
DEG1 = 0.
DEG2 = 2*PI
DDEG = (DEG2-DEG1)/N
BSUMP = 0.
SSUMP = 0.
DO 11 I = 1, N-1
X = I*DDEG
FXB = (1+COS(X)/SQRT(R**2-(SIN(X))**2))**2
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2)))
BSUMP = BSUMP + FXB
SSUMP = SSUMP + FXS
11 CONTINUE
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0 = ((COS(DEG1)/R)**2)*((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2)))
$      *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2)))
FXSN = ((COS(DEG2)/R)**2)*((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2)))
$      *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2)))
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN1 = BIG/(2*PI)
VSMEAN1 = SML/(2*PI)
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE MEAN 2                               C
C*****-----*****C

```

```

SUBROUTINE MEAN2 (CONLB, ARM, VBMEAN2, VSMEAN2)
PI = 2.*ASIN(1.)
R = CONLB/ARM
N = 360
DEG1 = 0.
DEG2 = 2*PI
DDEG = (DEG2-DEG1)/N
BSUMP = 0.
SSUMP = 0.
DO 12 I = 1, N-1
X = I*DDEG
FXB = (1+COS(X)/SQRT(R**2-(SIN(X))**2))**2
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2)))
BSUMP = BSUMP + FXB
SSUMP = SSUMP + FXS
12 CONTINUE
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0 = ((COS(DEG1)/R)**2)

```



```

$          * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2)))
$ FXSN = ((COS(DEG2)/R)**2)
$          * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2)))
$ BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
$ SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN2 = BIG/(2*PI)
VSMEAN2 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 3                               C
C*****-----*****C
SUBROUTINE MEAN3 (CONL, ARMB, VBMEAN3, VSMEAN3)
PI      = 2.*ASIN(1.)
R       = CONL/ARMB
N       = 100
DEG1   = 0.
DEG2   = 2*PI
DDEG   = (DEG2-DEG1)/N
BSUMP  = 0.
SSUMP  = 0.
DO 13 I = 1, N-1
X      = I*DDEG
FXB    = (1+COS(X)/SQRT(R**2-(SIN(X)**2)))**2
FXS    = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2)))
BSUMP  = BSUMP + FXB
SSUMP  = SSUMP + FXS
13 CONTINUE
FXB0   = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1)**2)))**2
FXBN   = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2)**2)))**2
FXS0   = ((COS(DEG1)/R)**2)
$      * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2)))
$ FXSN = ((COS(DEG2)/R)**2)
$      * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2)))
$ BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
$ SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN3 = BIG/(2*PI)
VSMEAN3 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 4                               C
C*****-----*****C
SUBROUTINE MEAN4 (R, VBMEAN4, VSMEAN4)
PI      = 2.*ASIN(1.)
N       = 100
DEG1   = 0.
DEG2   = 2*PI
DDEG   = (DEG2-DEG1)/N
BSUMP  = 0.
SSUMP  = 0.
DO 13 I = 1, N-1
X      = I*DDEG
FXB    = (1+COS(X)/SQRT(R**2-(SIN(X)**2)))**2
FXS    = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2)))
BSUMP  = BSUMP + FXB
SSUMP  = SSUMP + FXS
13 CONTINUE
FXB0   = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1)**2)))**2
FXBN   = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2)**2)))**2
FXS0   = ((COS(DEG1)/R)**2)
$      * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2)))
$ FXSN = ((COS(DEG2)/R)**2)
$      * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2)))
$ BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
$ SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN4 = BIG/(2*PI)
VSMEAN4 = SML/(2*PI)
RETURN

```

```

END
C*****-----C
C          SUBROUTINE TOR 1          C
C*****-----C
SUBROUTINE TMEAN1 (FCOE, SDEGB, FB, CDEGB, FM, SCB, PLB, BRB, TRB, VLB, RADC
$          , TOR1, PI)
N      = 360
D1     = SDEGB
D2     = CDEGB
D3     = 180-CDEGB
D4     = 180-SDEGB
DEGO   = 0.
DEGN   = 360.
DDEG   = (DEGN-DEGO)/N
SUMP   = 0.
DO 10 I = 0, N, 1
X      = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S      = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
V      = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
A      = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
FX     = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S      = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
V      = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000
A      = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
FX     = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S      = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
V      = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
A      = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
FX     = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
FX     = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR1 = SUMP/N
RETURN
END

```

```

C*****-----C
C          SUBROUTINE TOR 2          C
C*****-----C
SUBROUTINE TMEAN2 (FCOE, SDEGB, FB, CDEGB, FMB, SC, PLB, BRB, TRB, VLB, RADC
$          , TOR2, PI)
N      = 360
D1     = SDEGB
D2     = CDEGB
D3     = 180-CDEGB
D4     = 180-SDEGB
DEGO   = 0.
DEGN   = 360.
DDEG   = (DEGN-DEGO)/N
SUMP   = 0.
DO 10 I = 0, N, 1
X      = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S      = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
V      = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
A      = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
FX     = -1*(SC*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S      = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
V      = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000

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      A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
      FX = -1*(SC*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      IF ((X.GT.D3).AND.(X.LE.D4)) THEN
        S = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
        V = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
        A = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
        FX = -1*(SC*S+PLB+FMB*A)
          *(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        FX = 0
      ENDIF
    ENDIF
  ENDIF
  SUMP = SUMP + FX
10 CONTINUE
  TOR2 = SUMP/N
  RETURN
END
C*****-----*****C
C                                     SUBROUTINE TOR 3                                     C
C*****-----*****C
SUBROUTINE TMEAN3 (FCOE, SDEGB, FB, CDEGB, FMB, SCB, PL, BRB, TRB, VLB, RADC
$ , TOR3, PI)
  N = 360
  D1 = SDEGB
  D2 = CDEGB
  D3 = 180-CDEGB
  D4 = 180-SDEGB
  DEGO = 0.
  DEGN = 360.
  DDEG = (DEGN-DEGO)/N
  SUMP = 0.
  DO 10 I = 0, N, 1
    X = I*DDEG
    IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
      V = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
      A = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
      FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      IF ((X.GE.D2).AND.(X.LE.D3)) THEN
        S = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
        V = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000
        A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
        FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        IF ((X.GT.D3).AND.(X.LE.D4)) THEN
          S = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
          V = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
          A = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
          FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
        ELSE
          FX = 0
        ENDIF
      ENDIF
    ENDIF
    SUMP = SUMP + FX
  10 CONTINUE
  TOR3 = SUMP/N
  RETURN
END
C*****-----*****C
C                                     SUBROUTINE TOR 4                                     C
C*****-----*****C
SUBROUTINE TMEAN4 (FCOE, SDEGB, FBR, CDEGBR, FMB, SCB, PLB, BR, TRB, VLB
$ , RADC, TOR4, PI)
  N = 360
  D1 = SDEGB

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```

D2 = CDEGBR
D3 = 180-CDEGBR
D4 = 180-SDEGB
DEGO = 0.
DEGN = 360.
DDEG = (DEGN-DEGO)/N
SUMP = 0.
DO 10 I = 0,N,1
X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S = (FBR-BR)*(1-COS((X-D1)*PI/180))/1000
V = (FBR-BR)*RADC*SIN((X-D1)*PI/180)/1000
A = (FBR-BR)*(RADC**2)*COS((X-D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S = ((BR+VLB-TRB)*SIN(X*PI/180)+TRB-BR)/1000
V = (BR+VLB-TRB)*RADC*COS(X*PI/180)/1000
A = -1*(BR+VLB-TRB)*(RADC**2)*SIN(X*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S = (FBR-BR)*(1+COS((X+D1)*PI/180))/1000
V = -1*(FBR-BR)*RADC*SIN((X+D1)*PI/180)/1000
A = -1*(FBR-BR)*(RADC**2)*COS((X+D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR4 = SUMP/N
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 51                               C
C*****-----*****C
SUBROUTINE TMEAN51(FCOE,SDEGB,FBTR,CDEGBTR,FMB,SCB,PLB,BR,TR,VLB,
$ RADC,TOR51,PI)
N = 360
D1 = SDEGB
D2 = CDEGBTR
D3 = 180-CDEGBTR
D4 = 180-SDEGB
DEGO = 0.
DEGN = 360.
DDEG = (DEGN-DEGO)/N
SUMP = 0.
DO 10 I = 0,N,1
X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S = (FBTR-BR)*(1-COS((X-D1)*PI/180))/1000
V = (FBTR-BR)*RADC*SIN((X-D1)*PI/180)/1000
A = (FBTR-BR)*(RADC**2)*COS((X-D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S = ((BR+VLB-TR)*SIN(X*PI/180)+TR-BR)/1000
V = (BR+VLB-TR)*RADC*COS(X*PI/180)/1000
A = -1*(BR+VLB-TR)*(RADC**2)*SIN(X*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S = (FBTR-BR)*(1+COS((X+D1)*PI/180))/1000
V = -1*(FBTR-BR)*RADC*SIN((X+D1)*PI/180)/1000
A = -1*(FBTR-BR)*(RADC**2)*COS((X+D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)

```

```

ELSE
  FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR51 = SUMP/N
RETURN
END

C*****-----*****C
C                               SUBROUTINE TOR 5                               C
C*****-----*****C
SUBROUTINE TMEAN5 (FCOE, SDEGB, FTR, CDEGTR, FMB, SCB, PLB, BRB, TR, VLB
$                , RADC, TOR5, PI)
N      = 360
D1     = SDEGB
D2     = CDEGTR
D3     = 180-CDEGTR
D4     = 180-SDEGB
DEGO   = 0.
DEGN   = 360.
DDEG   = (DEGN-DEGO)/N
SUMP   = 0.
DO 10 I = 0, N, 1
  X = I*DDEG
  IF ((X.GE.D1).AND.(X.LT.D2)) THEN
    S = (FTR-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
    V = (FTR-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
    A = (FTR-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
    FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
  ELSE
    IF ((X.GE.D2).AND.(X.LE.D3)) THEN
      S = ((BRB+VLB-TR)*SIN( X*PI/180 )+TR-BRB)/1000
      V = (BRB+VLB-TR)*RADC*COS( X*PI/180 )/1000
      A = -1*(BRB+VLB-TR)*(RADC**2)*SIN( X*PI/180 )/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      IF ((X.GT.D3).AND.(X.LE.D4)) THEN
        S = (FTR-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
        V = -1*(FTR-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
        A = -1*(FTR-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
        FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        FX = 0
      ENDIF
    ENDIF
  ENDIF
  SUMP = SUMP + FX
10 CONTINUE
TOR5 = SUMP/N
RETURN
END

C*****-----*****C
C                               SUBROUTINE TOR 6                               C
C*****-----*****C
SUBROUTINE TMEAN6 (FCOE, SDEGB, FVL, CDEGVL, FMB, SCB, PLB, BRB, TRB, VL
$                , RADC, TOR6, PI)
N      = 360
D1     = SDEGB
D2     = CDEGVL
D3     = 180-CDEGVL
D4     = 180-SDEGB
DEGO   = 0.
DEGN   = 360.
DDEG   = (DEGN-DEGO)/N
SUMP   = 0.
DO 10 I = 0, N, 1
  X = I*DDEG

```

```

IF ((X.GE.D1).AND.(X.LT.D2)) THEN
  S = (FVL-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
  V = (FVL-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
  A = (FVL-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
  FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
  IF ((X.GE.D2).AND.(X.LE.D3)) THEN
    S = ((BRB+VL-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
    V = (BRB+VL-TRB)*RADC*COS( X*PI/180 )/1000
    A = -1*(BRB+VL-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
    FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
  ELSE
    IF ((X.GT.D3).AND.(X.LE.D4)) THEN
      S = (FVL-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
      V = -1*(FVL-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
      A = -1*(FVL-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      FX = 0
    ENDIF
  ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR6 = SUMP/N
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 7                               C
C*****-----*****C

```

```

SUBROUTINE TMEAN7(FCOE,SDEGB,FB,CDEGB,FMB,SCB,PLB,BRB,TRB,VLB,RADC
$,TOR7,PI)
  N = 360
  D1 = SDEGB
  D2 = CDEGB
  D3 = 180-CDEGB
  D4 = 180-SDEGB
  DEGO = 0.
  DEGN = 360.
  DDEG = (DEGN-DEGO)/N
  SUMP = 0.
  DO 10 I=0,N,1
    X = I*DDEG
    IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
      V = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
      A = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      IF ((X.GE.D2).AND.(X.LE.D3)) THEN
        S = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
        V = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000
        A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
        FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        IF ((X.GT.D3).AND.(X.LE.D4)) THEN
          S = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
          V = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
          A = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
          FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
        ELSE
          FX = 0
        ENDIF
      ENDIF
    ENDIF
    SUMP = SUMP + FX
  10 CONTINUE
  TOR7 = SUMP/N
  RETURN

```

```

END
C*****-----*****C
C                               SUBROUTINE TOR 71                               C
C*****-----*****C
SUBROUTINE TMEAN71 (FCOE, SDEGB, FB, CDEGB, FM, SC, PL, BR, TR, VL, RADC,
$ TOR7, PI)
  N      = 360
  D1     = SDEGB
  D2     = CDEGB
  D3     = 180-CDEGB
  D4     = 180-SDEGB
  DEGO   = 0.
  DEGN   = 360.
  DDEG   = (DEGN-DEGO)/N
  SUMP   = 0.
  DO 10 I=0,N,1
    X = I*DDEG
    IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FB-BR)*(1-COS( (X-D1)*PI/180 ))/1000
      V = (FB-BR)*RADC*SIN( (X-D1)*PI/180 )/1000
      A = (FB-BR)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
      FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
    ELSE
      IF ((X.GE.D2).AND.(X.LE.D3)) THEN
        S = ((BR+VL-TR)*SIN( X*PI/180 )+TR-BR)/1000
        V = (BR+VL-TR)*RADC*COS( X*PI/180 )/1000
        A = -1*(BR+VL-TR)*(RADC**2)*SIN( X*PI/180 )/1000
        FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
      ELSE
        IF ((X.GT.D3).AND.(X.LE.D4)) THEN
          S = (FB-BR)*(1+COS( (X+D1)*PI/180 ))/1000
          V = -1*(FB-BR)*RADC*SIN( (X+D1)*PI/180 )/1000
          A = -1*(FB-BR)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
          FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
        ELSE
          FX = 0
        ENDIF
      ENDIF
    ENDIF
    SUMP = SUMP + FX
  10 CONTINUE
  TOR7 = SUMP/N
  RETURN
END
C*****-----*****C
C                               (SEL1) SUBROUTINE FOR CALCULATION                               C
C*****-----*****C
SUBROUTINE SEL1 (RPM, GN, G1, G2, G3, G4, G5, GD, TEFF, GT)
  IF (RPM.LE.1200.) THEN
    GN = 1.
  ELSE
    IF (RPM.LE.1800.) THEN
      GN = 2.
    ELSE
      IF (RPM.LE.2000.) THEN
        GN = 3.
      ELSE
        IF (RPM.LE.2200.) THEN
          GN = 4.
        ELSE
          GN = 5.
        ENDIF
      ENDIF
    ENDIF
  ENDIF
  IF ( GN.EQ.1 ) THEN
    GT = G1*GD
    TEFF = 0.8
  ELSE

```

```
IF ( GN.EQ.2 ) THEN
  GT = G2*GD
  TEFF = 0.8
ELSE
  IF ( GN.EQ.3 ) THEN
    GT = G3*GD
    TEFF = 0.85
  ELSE
    IF ( GN.EQ.4 ) THEN
      GT = G4*GD
      TEFF = 0.9
    ELSE
      IF ( GN.EQ.5 ) THEN
        GT = G5*GD
        TEFF = 0.9
      ELSE
        WRITE(6,*) ' ENTER NEW GEAR NUMBER '
      ENDIF
    ENDIF
  ENDIF
ENDIF
RETURN
END
```



สถาบันวิทยบริการ
จุฬาลงกรณ์มหาวิทยาลัย

ภาคผนวก ฉ

รายละเอียดโปรแกรม OPTIMUM

โปรแกรม optimum สามารถแสดงรายละเอียดดังต่อไปนี้

```

C*****-----*****C
C          PROGRAM FOR DETERMINATION OPTIMUM PARAMETERS          C
C          WRITTEN BY                                             C
C          MR. PAIRAT LERTARAYAPONG                             C
C*****-----*****C
PROGRAM OPTIMUM
WRITE(6,*) ' ENTER ENGINE DISPLACEMENT VOLUME           : (CC) '
READ(*,*)  VDB
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF PARAMETERS      : (TIMES) '
READ(*,*)  N
WRITE(6,*) ' ENTER ENGINE UPPER LIMIT SPEED              : (RPM) '
READ(*,*)  RPMH
WRITE(6,*) ' ENTER ENGINE LOWER LIMIT SPEED              : (RPM) '
READ(*,*)  RPML
WRITE(6,*) ' ENTER AMOUNT OF INTERVAL OF ENGINE SPEED    : (TIMES) '
READ(*,*)  RPMN
WRITE(6,*) ' ENTER OPERATION ENGINE SPEED                : (RPM) '
READ(*,*)  ORPM
C*****-----*****C
AIRDEN = 1.17
DENHG  = 13550.
FCOE   = 0.11
CORRK  = 0.06
RALT   = 2.
PCLE   = 4.5
RCOM   = 1.18
NCOM   = 1.
DHE    = 10.
RP     = 0.5
RO     = 1.
PI     = 2.*ASIN(1.)
PA     = 101.325
ESM    = 0.9
EC     = 0.9
E      = 0.9
H      = 0.005
PE     = 9.81*DENHG*DHE*0.0254/1000.
H1     = 185.*1000.
H2     = 95.7*1000.
V1     = 0.0666252
FRAC   = 25.
AMPB   = 50.
VOLTB  = 12.
C*****-----*****C
C          CONSTANT VALUE FOR CALCULATION                       C
C AIRDEN  = AIR DENSITY                                         : (kg/m^3) C
C DENHG   = MERCURY DENSITY                                     : (kg/m^3) C
C FCOE    = FRICTION COEFFICIENT IN CAM SURFACE                C
C RCOM    = PULLEY RATIO AT COMPRESSOR                         C
C NCOM    = NUMBER OF CYLINDER AT COMPRESSOR                   C
C PCLE    = PERCENT CLEARANCE AT COMPRESSOR                    : (%)      C
C FRAC    = PERCENT BETWEEN MECH. LOSS WITH TOTAL LOSS        : (%)      C
C CORRK   = CORRECTION FACTOR OF ALTERNATOR                   C
C RALT    = PULLEY RATIO AT ALTERNATOR                         C
C RP      = PRESSURE RING CONSTANT                             C
C RO      = OIL RING CONSTANT                                  C
C PA      = AMBIENT PRESSURE                                    : (kPa)    C

```

```

C   DHE = EXHAUST MANIFOLD PRESSURE AT FULL LOAD      : (INCH)   C
C   H   = OIL MINIMUM THICKNESS                       : (mm)     C
C   PE  = EXHAUST MANIFOLD PRESSURE AT FULL LOAD      : (kPa)    C
C   EC  = ECCENTRICITY RATIO IN CRANK-SHAFT BEARING   :           C
C   E   = ECCENTRICITY RATIO IN CONNECTION ROD BIG-END :           C
C   ESM = ECCENTRICITY RATIO IN CONNECTION ROD SMALL-END :           C
C   H1  = ENTHALPY AT SATURATED VAPOUR                : (kJ/kg)  C
C   H2  = ENTHALPY AT SATURATED LIQUID               : (kJ/kg)  C
C   V1  = SPECIFIC VOLUME OF REFRIGERANT              : (m^3/kg) C
C*****-----*****C

```

```

OPEN(UNIT=7, FILE='BASE.DAT', STATUS='OLD')
READ(7,*) VISB,RCRANKB,CRANKLB,CCRANKB,BN,QB
READ(7,*) RKB,EMB,ECB,CONDP,EVAPP,BCOMB,SCOMB
READ(7,*) BPRESSB,BOILB,NPRESSB,NOILB
READ(7,*) BRCONB,BCCONB,BLCONB
READ(7,*) SRCONB,SCCONB,SLCONB
READ(7,*) NCB,BOREB,ARMB,CONLB
READ(7,*) NVCB,SDEGB,TRB,VLB
READ(7,*) FMB,SCB,PLB,BRB
READ(7,*) RDALTB,RLALTB
READ(7,*) DVB,RCB,NVB
READ(7,*) PCB,PISLB
READ(7,*) G1,G2,G3,G4,G5,GD
READ(7,*) CDB,AREAB,FRB,MGB,WR

```

```

C-----DATA LIMIT FOR CALCULATION-----C

```

```

READ(7,*) RCRANKL,RCRANKH
READ(7,*) CRANKLL,CRANKLH
READ(7,*) CCRANKL,CCRANKH
READ(7,*) BRCONL,BRCONH
READ(7,*) BCCONL,BCCONH
READ(7,*) BLCONL,BLCONH
READ(7,*) SRCONL,SRCONH
READ(7,*) SCCONL,SCCONH
READ(7,*) SLCONL,SLCONH
READ(7,*) BPRESSL,BPRESSH
READ(7,*) BOILL,BOILH
READ(7,*) BOREL,BOREH
READ(7,*) VISL,VISH
READ(7,*) ARML,ARMH
READ(7,*) RDALTL,RDALTH
READ(7,*) RLALTL,RLALTH
READ(7,*) CONLL,CONLH
READ(7,*) PISLL,PISLH
READ(7,*) DVL,DVH
READ(7,*) RCL,RCH
READ(7,*) PCL,PCH
READ(7,*) FML,FMH
READ(7,*) SCL,SCH
READ(7,*) PLL,PLH
READ(7,*) BRL,BRH
READ(7,*) TRL,TRH
READ(7,*) VLL,VLH
READ(7,*) QL,QH
READ(7,*) CDL,CDH
READ(7,*) AFL,AFH
READ(7,*) FRL,FRH
READ(7,*) MGL,MGH

```

```

C*****-----*****C

```

```

C                                     ENGINE PARAMETERS
C   VIS = ABSOLUTE VISCOSITY           : (Pa.s)   C
C   RCRANK = RADIUS OF CRANK-SHAFT BEARING : (m)      C
C   CRANKL = CRANK-SHAFT BEARING WIDTH   : (m)      C
C   CCRANK = RADIUS CLEARANCE IN CRANK-SHAFT BEARING : (m)      C
C   BN    = AMOUNT OF BEARING SUPPORT    :           C
C   RKB   = REFRIGERANT ISENTROPIC INDEX :           C
C   EMB   = MECHANICAL EFFICIENCY        :           C
C   ECB   = COMPRESSION EFFICIENCY       :           C
C   CONDP = CONDENSOR PRESSURE           : (Pa)     C
C   EVAPP = EVAPOURATOR PRESSURE        : (Pa)     C

```

```

C BCOMB = PISTON BORE AT COMPRESSOR : (m) C
C SCOMB COMPRESSOR STROKE LENGTH : (m) C
C BPRESS = PRESSURE RING SURFACE DEPTH : (mm) C
C BOIL = OIL RING SURFACE DEPTH : (mm) C
C NPRESS = AMOUNT OF PRESSURE RING : (m) C
C NOIL = AMOUNT OF OIL RING : (m) C
C BRCON = RADIUS OF CONNECTING ROD BEARING AT BIG-END : (m) C
C BCCON = RADIUS CLEARANCE IN CONNECTING ROD BIG-END : (m) C
C BLCON = CONNECTING ROD BEARING WIDTH AT BIG-END : (m) C
C SRCON = RADIUS OF CONNECTING ROD BEARING AT SMALL-END : (m) C
C SCCON = RADIUS CLEARANCE IN CONNECTING ROD SMALL-END : (m) C
C SLCON = CONNECTING ROD BEARING WIDTH AT SMALL-END : (m) C
C NCB = NUMBER OF CYLINDER : (m) C
C BORE = PISTON BORE : (m) C
C ARM = CRANK ARM : (m) C
C CONL = CONNECTING ROD LENGTH : (m) C
C NVCB = NUMBER VALVE PER CYLINDER : (deg.) C
C SDEGB = STARTING ANGLE : (mm) C
C TR = TIP RADIUS OF CAM : (mm) C
C BR = BASE RADIUS OF CAM : (mm) C
C VL = VALVE FOLLOWER LIFT : (mm) C
C FM = VALVE FOLLOWER MASS : (mm) C
C SC = SPRING STIFFNESS : (N/m) C
C PL = VALVE PRELOAD : (N) C
C RDALTB = ROTOR DIAMETER OF ALTERNATOR : (m) C
C RLALTB = ROTOR LENGTH OF ALTERNATOR : (m) C
C DV = INLET VALVE DIAMETER : (m) C
C RC = COMPRESSION RATIO : (m) C
C NVB = NUMBER OF INLET VALVE PER CYLINDER : (m) C
C PC = PISTON CLEARANCE : (m) C
C PISL = PISTON SKIRT LENGTH : (m) C
C G = GEAR RATIO IN 1-5 AND DIFFERENT : (m^3) C
C CD = DRAG COEFFICIENT : (kg) C
C AREA = FRONTAL AREA : (m) C
C FR = ROLLING COEFFICIENT : (kg) C
C MG = VEHICLE MASS : (m) C
C WR = WHEEL RADIUS : (m) C

```

```

C*****-----*****C
C MAIN PROGRAM FOR CALCULATION
C*****-----*****C

```

```

DO 100 I1 = 0, RPMN, 1
  DRPM = (RPMH-RPML)/RPMN
  RPM = RPML + I1*DRPM
  RPMC = RPM/2
  RADC = (RPMC*2*PI/60)

```

```

C*****-----*****C
  PMIN1 = 99999.
  DO 1 J1 = 0, N, 1
    DRCRANK = (RCRANKH-RCRANKL)/N
    RCRANK = RCRANKL + J1*DRCRANK
    PRCRANK = VISB*(RCRANK**3)*CRANKLB*((2*PI)
    $ /((CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
    WRITE(6,101) RPM, RCRANK, PRCRANK
    IF ( PMIN1.GT.PRCRANK ) THEN
      PMIN1 = PRCRANK
      XMIN1 = RCRANK
    ENDIF
  1 CONTINUE
101 FORMAT(1X, F7.2, 3X, F7.5, 3X, F7.2)

```

```

C*****-----*****C
  PMIN2 = 99999.
  DO 2 J2 = 0, N, 1
    DLCRANK = (CRANKLH-CRANKLL)/N
    CRANKL = CRANKLL + J2*DLCRANK
    PLCRANK = VISB*(RCRANKB**3)*CRANKL*((2*PI)
    $ /((CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
    WRITE(6,102) RPM, CRANKL, PLCRANK
    IF ( PMIN2.GT.PLCRANK ) THEN
      PMIN2 = PLCRANK

```

```

      XMIN2 = CRANKL
    ENDIF
  2 CONTINUE
  102 FORMAT (1X,F7.2,3X,F7.5,3X,F7.2)
C-----*****C
      PMIN3 = 99999.
      DO 3 J3 = 0,N,1
      DCCRANK = (CCRANKH-CCRANKL)/N
      CCRANK = CCRANKL + J3*DCCRANK
      PCCRANK = VISB*(RCRANKB**3)*CRANKLB*((2*PI)
$          /((CCRANK*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
      WRITE(6,103) RPM,CCRANK,PCCRANK
      IF ( PMIN3.GT.PCCRANK ) THEN
        PMIN3 = PCCRANK
        XMIN3 = CCRANK
      ENDIF
  3 CONTINUE
  103 FORMAT (1X,F7.2,3X,E8.2,3X,F7.2)
C-----*****C
      IF (RPM.LE.1300.) THEN
        DH = 9.9
      ELSE
        IF (RPM.LE.1700.) THEN
          DH = 10.2
        ELSE
          IF (RPM.LE.2000.) THEN
            DH = 11.
          ELSE
            IF (RPM.LE.2400.) THEN
              DH = 12.
            ELSE
              IF (RPM.LE.2700.) THEN
                DH = 13.
              ELSE
                IF (RPM.LE.3000.) THEN
                  DH = 13.7
                ELSE
                  IF (RPM.LE.3400.) THEN
                    DH = 14.9
                  ELSE
                    IF (RPM.LE.3700.) THEN
                      DH = 15.9
                    ELSE
                      IF (RPM.LE.4000.) THEN
                        DH = 16.5
                      ELSE
                        WRITE(*,*) ' OVER ENGINE SPEED '
                      ENDIF
                    ENDIF
                  ENDIF
                ENDIF
              ENDIF
            ENDIF
          ENDIF
        ENDIF
      ENDIF
      PMIN6 = 99999.
      DO 6 J6 = 0,N,1
      DDV = (DVH-DVL)/N
      DV = DVL + J6*DDV
      PIA = 9.81*DENHG*DH*0.0254/1000
      CIMEP = 12.87*PA*((PIA/PA)-0.1)
      PIG = PA-(CIMEP/12.8)-10.14
      F = (NVB*NCB*(DV**2))/(2*ARMB*PI*NCB*(BOREB**2)/4)
      PDPUMP = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*RPM)/(3904000))**2) +
$          8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)
$          *((2.984/F)**1.28) + (SQRT((PA-PIG)/97.94))
$          *(11.86*(RCB**0.4)-(3.38+0.103*RCB)*((RPM/1000)**1.185)))
$          *1000*(2*ARMB*PI*NCB*(BOREB**2)/4)*(RPM/120)

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WRITE(6,106) RPM,DV,PDPUMP
IF ( PMIN6.GT.PDPUMP ) THEN
  PMIN6 = PDPUMP
  XMIN6 = DV
ENDIF
6 CONTINUE
106 FORMAT(1X,F7.2,3X,F5.3,3X,F7.2)
C*****
  XMIN7 = RCH
C*****
  PMIN8 = 99999.
  DO 8 J8 = 0,N,1
    DPC = (PCH-PCL)/N
    PC = PCL + J8*DPC
    PCPPIS = (VISB*PI*BOREB*PISLB/PC)*((ARMB*(RPM/15))**2)*NCB
    WRITE(6,108) RPM,PC,PCPPIS
    IF ( PMIN8.GT.PCPPIS ) THEN
      PMIN8 = PCPPIS
      XMIN8 = PC
    ENDIF
8 CONTINUE
108 FORMAT(1X,F7.2,3X,F9.6,3X,F7.2)
C*****
  PMIN9 = 99999.
  DO 9 J9 = 0,N,1
    DPISL = (PISLH-PISLL)/N
    PISL = PISLL + J9*DPISL
    PLPIS = (VISB*PI*BOREB*PISL/PCB)*((ARMB*(RPM/15))**2)*NCB
    WRITE(6,109) RPM,PISL,PLPIS
    IF ( PMIN9.GT.PLPIS ) THEN
      PMIN9 = PLPIS
      XMIN9 = PISL
    ENDIF
9 CONTINUE
109 FORMAT(1X,F7.2,3X,F6.4,3X,F7.2)
C*****
  PMIN10 = 99999.
  DO 10 J10 = 0,N,1
    DBPRESS = (BPRESSH-BPRESSL)/N
    BPRESS = BPRESSL + J10*DBPRESS
    CALL NUM2(BPRESS,BOILB,RP,RO,H,HP4,HO4,HP5,HO5,HP6,HO6)
    PBPRING = VISB*ARMB*2*PI*(RPM/60)*(4*HO4-3*(HO5**2)/HO6+BOILB
$      *(1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$      VISB*ARMB*2*PI*(RPM/60)*(4*HP4-3*(HP5**2)/HP6+(BPRESS
$      *(1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
    WRITE(6,110) RPM,BPRESS,PBPRING
    IF ( PMIN10.GT.PBPRING ) THEN
      PMIN10 = PBPRING
      XMIN10 = BPRESS
    ENDIF
10 CONTINUE
110 FORMAT(1X,F7.2,3X,F3.1,3X,F7.2)
C*****
  PMIN11 = 99999.
  DO 11 J11 = 0,N,1
    DBOIL = (BOILH-BOILL)/N
    BOIL = BOILL + J11*DBOIL
    CALL NUM3(BPRESSE,BOIL,RP,RO,H,HP7,HO7,HP8,HO8,HP9,HO9)
    PBORING = VISB*ARMB*2*PI*(RPM/60)*(4*HO7-3*(HO8**2)/HO9+BOIL
$      *(1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$      VISB*ARMB*2*PI*(RPM/60)*(4*HP7-3*(HP8**2)/HP9+(BPRESSB
$      *(1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
    WRITE(6,111) RPM,BOIL,PBORING
    IF ( PMIN11.GT.PBORING ) THEN
      PMIN11 = PBORING
      XMIN11 = BOIL
    ENDIF
11 CONTINUE
111 FORMAT(1X,F7.2,3X,F3.1,3X,F7.2)

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C*****-----*****C
      PMIN12 = 99999.
      DO 12 J12 = 0,N,1
        DBRCON = (BRCONH-BRCONL)/N
        BRCON = BRCONL + J12*DBRCON
        CALL MEAN1 (CONLB, ARMB, VMEAN1, VSMEAN1)
        PBRCON = VISB*(BRCON**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
          *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$         VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$         *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
        WRITE (6,112) RPM, BRCON, PBRCON
        IF ( PMIN12.GT.PBRCON ) THEN
          PMIN12 = PBRCON
          XMIN12 = BRCON
        ENDIF
      12 CONTINUE
      112 FORMAT (1X, F7.2, 3X, F6.4, 3X, F7.2)
C*****-----*****C
      PMIN13 = 99999.
      DO 13 J13 = 0,N,1
        DBCCON = (BCCONH-BCCONL)/N
        BCCON = BCCONL + J13*DBCCON
        CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
        PBCCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCON*SQRT(1-E**2)))
          *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$         VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$         *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
        WRITE (6,113) RPM, BCCON, PBCCON
        IF ( PMIN13.GT.PBCCON ) THEN
          PMIN13 = PBCCON
          XMIN13 = BCCON
        ENDIF
      13 CONTINUE
      113 FORMAT (1X, F7.2, 3X, F8.2, 3X, F7.2)
C*****-----*****C
      PMIN14 = 99999.
      DO 14 J14 = 0,N,1
        DBLCON = (BLCONH-BLCONL)/N
        BLCON = BLCONL + J14*DBLCON
        CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
        PBLCON = VISB*(BRCONB**3)*BLCON*((2*PI)/(BCCONB*SQRT(1-E**2)))
          *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$         VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$         *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
        WRITE (6,114) RPM, BLCON, PBLCON
        IF ( PMIN14.GT.PBLCON ) THEN
          PMIN14 = PBLCON
          XMIN14 = BLCON
        ENDIF
      14 CONTINUE
      114 FORMAT (1X, F7.2, 3X, F5.3, 3X, F7.2)
C*****-----*****C
      PMIN15 = 99999.
      DO 15 J15 = 0,N,1
        DSRCON = (SRCONH-SRCONL)/N
        SRCON = SRCONL + J15*DSRCON
        CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
        PSRCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
          *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$         VISB*(SRCON**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$         *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
        WRITE (6,115) RPM, SRCON, PSRCON
        IF ( PMIN15.GT.PSRCON ) THEN
          PMIN15 = PSRCON
          XMIN15 = SRCON
        ENDIF
      15 CONTINUE
      115 FORMAT (1X, F7.2, 3X, F6.4, 3X, F7.2)
C*****-----*****C

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    PMIN16 = 99999.
DO 16 J16 = 0,N,1
  DSCCON = (SCCONH-SCCONL)/N
  SCCON = SCCONL + J16*DSCCON
  CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
  PSCCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +
$      VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
  WRITE(6,116) RPM,SCCON,PSCCON
  IF ( PMIN16.GT.PSCCON ) THEN
    PMIN16 = PSCCON
    XMIN16 = SCCON
  ENDIF
16 CONTINUE
116 FORMAT(1X,F7.2,3X,E8.2,3X,F7.2)
C*****-----*****C

    PMIN17 = 99999.
DO 17 J17 = 0,N,1
  DSLCON = (SLCONH-SLCONL)/N
  SLCON = SLCONL + J17*DSLCON
  CALL MEAN1 (CONLB, ARMB, VBMEAN1, VSMEAN1)
  PSLCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN1 +
$      VISB*(SRCONB**3)*SLCON*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
  WRITE(6,117) RPM,SLCON,PSLCON
  IF ( PMIN17.GT.PSLCON ) THEN
    PMIN17 = PSLCON
    XMIN17 = SLCON
  ENDIF
17 CONTINUE
117 FORMAT(1X,F7.2,3X,F5.3,3X,F7.2)
C*****-----*****C

    XMIN18 = CONLH
C*****-----*****C

    PMIN19 = 99999.
DO 19 J19 = 0,N,1
  DFM = (FMH-FML)/N
  FM = FML + J19*DFM
  CALL TMEAN1 (FCOE, SDEGB, FB, CDEGB, FM, SCB, PLB, BRB, TRB, VLB, RADC, TOR1
$,PI)
  PFCAM = -TOR1*RADC*NCB*NVCB
  WRITE(6,119) RPM,FM,PFCAM
  IF ( PMIN19.GT.PFCAM ) THEN
    PMIN19 = PFCAM
    XMIN19 = FM
  ENDIF
19 CONTINUE
119 FORMAT(1X,F7.2,3X,F4.2,3X,F7.2)
C*****-----*****C

    PMIN20 = 99999.
DO 20 J20 = 0,N,1
  DSC = (SCH-SCL)/N
  SC = SCL + J20*DSC
  CALL TMEAN2 (FCOE, SDEGB, FB, CDEGB, FMB, SC, PLB, BRB, TRB, VLB, RADC, TOR2
$,PI)
  PSCAM = -TOR2*RADC*NCB*NVCB
  WRITE(6,120) RPM,SC,PSCAM
  IF ( PMIN20.GT.PSCAM ) THEN
    PMIN20 = PSCAM
    XMIN20 = SC
  ENDIF
20 CONTINUE
120 FORMAT(1X,F7.2,3X,F7.1,3X,F7.2)
C*****-----*****C

    PMIN21 = 99999.
DO 21 J21 = 0,N,1
  DPL = (PLH-PLL)/N

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      PL = PLL + J21*DPL
      CALL TMEAN3 (FCOE, SDEGB, FB, CDEGB, FMB, SCB, PL, BRB, TRB, VLB, RADC, TOR3
$, PI)
      PPCAM = -TOR3*RADC*NCB*NVCB
      WRITE (6, 121) RPM, PL, PPCAM
      IF ( PMIN21.GT.PPCAM ) THEN
        PMIN21 = PPCAM
        XMIN21 = PL
      ENDIF
21 CONTINUE
121 FORMAT (1X, F7.2, 3X, F5.1, 3X, F7.2)
C*****-----*****C
      PMIN22 = 99999.
      DO 22 J22 = 0, N, 1
        DBR = (BRH-BRL)/N
        BR = BRL + J22*DBR
      DO 23 J23 = 0, N, 1
        DTR = (TRH-TRL)/N
        TR = TRL + J23*DTR
        FBTR = (BR**2-TR**2+(BR+VLB-TR)**2
$           -2*BR*(BR+VLB-TR)*SIN(SDEGB*PI/180))
$           / (2*(BR-TR-(BR+VLB-TR)
$           *SIN(SDEGB*PI/180)))
        CDEGBTR = (ACOS((FBTR-BR)*COS(SDEGB*PI/180)
$           / (FBTR-TR)))*180/PI
      CALL TMEAN51 (FCOE, SDEGB, FBTR, CDEGBTR, FMB, SCB, PLB, BR, TR
$           , VLB, RADC, TOR51, PI)
      PBTCAM = -TOR51*RADC*NCB*NVCB
      WRITE (6, 122) RPM, BR, TR, PBTCAM
      IF ( PMIN22.GT.PBTCAM ) THEN
        PMIN22 = PBTCAM
        XMIN22 = BR
        XMIN23 = TR
      ENDIF
23 CONTINUE
22 CONTINUE
122 FORMAT (1X, F7.2, 3X, F5.2, 3X, F4.2, 3X, F7.2)
C*****-----*****C
      PMIN24 = 99999.
      DO 24 J24 = 0, N, 1
        DDVL = (VLH-VLL)/N
        VL = VLL + J24*DDVL
        FVL = (BRB**2-TRB**2+(BRB+VL-TRB)**2-2*BRB*(BRB+VL-TRB)
$           *SIN(SDEGB*PI/180))
$           / (2*(BRB-TRB-(BRB+VL-TRB)*SIN(SDEGB*PI/180)))
        CDEGVL = (ACOS((FVL-BRB)*COS(SDEGB*PI/180)
$           / (FVL-TRB)))*180/PI
      CALL TMEAN6 (FCOE, SDEGB, FVL, CDEGVL, FMB, SCB, PLB, BRB, TRB, VL, RADC
$, TOR6, PI)
      PVCAM = -TOR6*RADC*NCB*NVCB
      WRITE (6, 124) RPM, VL, PVCAM
      IF ( PMIN24.GT.PVCAM ) THEN
        PMIN24 = PVCAM
        XMIN24 = VL
      ENDIF
24 CONTINUE
124 FORMAT (1X, F7.2, 3X, F4.1, 3X, F7.2)
C*****-----*****C
      CALL P311 (RPM, BOREL, BOREH, VISL, VISH, CONLB, BN, NPRESSB, NOILB,
$           NCB, RP, RO, PI, H, EC, E, ESM, RCRANKB, CRANKLB, CCRANKB, BPRESSB,
$           BOILB, BRCONB, BCCONB, BLCONB, SRCONB, SCCONB, SILCONB, PCB, PISLB,
$           VDB, XMIN25, XMIN26, XMIN27)
C*****-----*****C
      RPM = RPML + I1*DRPM
      CALL SEL1 (RPM, GN, G1, G2, G3, G4, G5, GD, TEFF, GT)
      PMIN28 = 99999.
      DO 28 K28 = 0, N, 1
        DCD = (CDH-CDL)/N
        CD = CDL + K28*DCD

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    PAIRC = 0.5*CD*AIRDEN*AREAB*( (RPM/60)*2*PI*WR/GT )**3
  IF (PMIN28.GT.PAIRC) THEN
    PMIN28 = PAIRC
    XMIN28 = CD
  ENDIF
28 CONTINUE
C*****
    PMIN29 = 99999.
  DO 29 K29 = 0,N,1
    DAF = (AFH-AFL)/N
    AF = AFL + K29*DAF
    PAIRA = 0.5*CDB*AIRDEN*AF*( (RPM/60)*2*PI*WR/GT )**3
  IF (PMIN29.GT.PAIRA) THEN
    PMIN29 = PAIRA
    XMIN29 = AF
  ENDIF
29 CONTINUE
C*****
    PMIN30 = 99999.
  DO 30 K30 = 0,N,1
    DFR = (FRH-FRL)/N
    FR = FRL + K30*DFR
    PROLLF = FR*MGB*9.81*( (RPM/60)*2*PI*WR/GT )
  IF (PMIN30.GT.PROLLF) THEN
    PMIN30 = PROLLF
    XMIN30 = FR
  ENDIF
30 CONTINUE
C*****
    PMIN31 = 99999.
  DO 31 K31 = 0,N,1
    DMG = (MGH-MGL)/N
    VMG = MGL + K31*DMG
    PROLLM = FRB*VMG*9.81*( (RPM/60)*2*PI*WR/GT )
  IF (PMIN31.GT.PROLLM) THEN
    PMIN31 = PROLLM
    XMIN31 = VMG
  ENDIF
31 CONTINUE
C*****
  CALL ACCESS(N,RPM,BCOMB,SCOMB,RKB,EMB,ECB,RDALTB,RLALTB,QL,QH,
$RDALTL,RDALTH,RLALTL,RLALTH,RCOM,NCOM,PCLE,H1,H2,V1,FRAC,EVAPP,
$CONDP,CORRK,RALT,PAIRQ,PALTD,PALTL,PI,Q,AMPB,VOLTB,RDALT,RLALT,
$XACC1,XACC3,XACC4)
C*****
  OPEN(UNIT=1,FILE='RESULT3.OUT',STATUS='OLD')
  WRITE(1,140) RPM,VDB
  WRITE(1,141) XMIN1
  WRITE(1,142) XMIN2
  WRITE(1,143) XMIN3
  WRITE(1,146) XMIN6
  WRITE(1,148) XMIN8
  WRITE(1,149) XMIN9
  WRITE(1,150) XMIN10
  WRITE(1,151) XMIN11
  WRITE(1,152) XMIN12
  WRITE(1,153) XMIN13
  WRITE(1,154) XMIN14
  WRITE(1,155) XMIN15
  WRITE(1,156) XMIN16
  WRITE(1,157) XMIN17
  WRITE(1,159) XMIN19
  WRITE(1,160) XMIN20
  WRITE(1,161) XMIN21
  WRITE(1,162) XMIN22
  WRITE(1,163) XMIN23
  WRITE(1,164) XMIN24
  WRITE(1,165) XMIN25
  WRITE(1,166) XMIN26

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WRITE(1,167) XMIN27
WRITE(1,168) XMIN28
WRITE(1,169) XMIN29
WRITE(1,170) XMIN30
WRITE(1,171) XMIN31
WRITE(1,172) XACC1
WRITE(1,174) XACC3
WRITE(1,175) XACC4
WRITE(1,*) ' '
100 CONTINUE
C*****
140 FORMAT(' ENGINE SPEED : ',F7.2,' (RPM) : ',F6.1,' (CC) ')
141 FORMAT(' RADIUS OF BEARING IN CRANKSHAFT : ',T48,F8.5,' (m) ')
142 FORMAT(' BEARING WIDTH IN CRANKSHAFT : ',T48,F8.5,' (m) ')
143 FORMAT(' RADIUS CLEARANCE IN CRANKSHAFT : ',T48,E8.2,' (m) ')
146 FORMAT(' INLET VALVE DIAMETER : ',T48,F8.4,' (m) ')
148 FORMAT(' PISTON CLEARANCE : ',T48,F8.6,' (m) ')
149 FORMAT(' SKIRT LENGTH : ',T48,F8.4,' (m) ')
150 FORMAT(' PRESSURE RING DEPTH : ',T48,F8.1,' (mm) ')
151 FORMAT(' OIL RING DEPTH : ',T48,F8.1,' (mm) ')
152 FORMAT(' RADIUS BEARING AT BIG-END SIDE : ',T48,F8.4,' (m) ')
153 FORMAT(' RADIUS CLEARANCE AT BIG-END SIDE : ',T48,E8.2,' (m) ')
154 FORMAT(' BEARING WIDTH AT BIG-END SIDE : ',T48,F8.3,' (m) ')
155 FORMAT(' RADIUS BEARING AT SMALL-END SIDE : ',T48,F8.4,' (m) ')
156 FORMAT(' RADIUS CLEARANCE AT SMALL-END SIDE: ',T48,E8.2,' (m) ')
157 FORMAT(' BEARING WIDTH AT SMALL-END SIDE : ',T48,F8.3,' (m) ')
159 FORMAT(' VALVE FOLLOWER MASS : ',T48,F8.4,' (kg) ')
160 FORMAT(' SPRING STIFFNESS : ',T48,F8.1,' (N/m) ')
161 FORMAT(' VALVE PRELOAD : ',T48,F8.1,' (N) ')
162 FORMAT(' BASE RADIUS : ',T48,F8.2,' (mm) ')
163 FORMAT(' TIP RADIUS : ',T48,F8.2,' (mm) ')
164 FORMAT(' VALVE LIFT : ',T48,F8.1,' (mm) ')
165 FORMAT(' ABSOLUTE VISCOSITY : ',T48,F8.4,' (Pa.s) ')
166 FORMAT(' BORE : ',T48,F8.4,' (m) ')
167 FORMAT(' CRANK ARM : ',T48,F8.5,' (m) ')
168 FORMAT(' DRAG COEFFICIENT : ',T48,F8.2,' ')
169 FORMAT(' FRONTAL AREA : ',T48,F8.2,' (m^2) ')
170 FORMAT(' ROLLING COEFFICIENT : ',T48,F8.5,' ')
171 FORMAT(' VEHICLE MASS : ',T48,F8.1,' (kg) ')
172 FORMAT(' COOLING LOAD : ',T48,F7.2,' (W) ')
174 FORMAT(' ROTOR DIAMETER IN ALTERNATOR : ',T48,F7.4,' (m) ')
175 FORMAT(' ROTOR LENGTH IN ALTERNATOR : ',T48,F7.4,' (m) ')
C*****
C POWER REQUIRED IN BASE LINE DATA C
C*****
OPEN(UNIT=1,FILE='RESULT3.OUT',STATUS='OLD')
WRITE(1,*) 'RPM:PCRANK:PAIR:PWP:PALTER:PPUMP:PPIS:PRING:PCON:PC
$AM:PTOTAL'
WRITE(1,*) 'POWER REQUIRED AT BASE LINE DATA '
DO 210 I2 = 0,RPMN,1
DRPM = (RPMH-RPML)/RPMN
RPM = RPML + I2*DRPM
RPMC = RPM/2
RADC = (RPMC*2*PI/60)
IF (RPM.LE.1300.) THEN
DHM = 9.9
ELSE
IF (RPM.LE.1700.) THEN
DHM = 10.2
ELSE
IF (RPM.LE.2000.) THEN
DHM = 11.
ELSE
IF (RPM.LE.2400.) THEN
DHM = 12.
ELSE
IF (RPM.LE.2700.) THEN
DHM = 13.
ELSE

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IF (RPM.LE.3000.) THEN
  DHM = 13.7
ELSE
  IF (RPM.LE.3400.) THEN
    DHM = 14.9
  ELSE
    IF (RPM.LE.3700.) THEN
      DHM = 15.9
    ELSE
      IF (RPM.LE.4000.) THEN
        DHM = 16.5
      ELSE
        WRITE(*,*) ' OVER ENGINE SPEED '
      ENDIF
    ENDIF
  ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
PIA = 9.81*DENHG*DHM*0.0254/1000
CIMEP = 12.87*PA*((PIA/PA)-0.1)
PIG = PA-(CIMEP/12.8)-10.14
FBB = (NVB*NCB*(DVB**2))/(2*ARMB*PI*NCB*(BOREB**2)/4)
FB = (BRB**2-TRB**2+(BRB+VLB-TRB)**2-2*BRB*(BRB+VLB-TRB)
$      *SIN(SDEGB*PI/180))/(2*(BRB-TRB-(BRB+VLB-TRB)
$      *SIN(SDEGB*PI/180)))
CDEGB = ACOS((FB-BRB)*COS(SDEGB*PI/180)/(FB-TRB))*180/PI
CALL NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
CALL MEAN1(CONLB,ARMB,VMEAN1,VSMEAN1)
CALL TMEAN7(FCOE,SDEGB,FB,CDEGB,FMB,SCB,PLB,BRB,TRB,VLB,RADC,
$      TOR7,PI)
C.....POWER LOSS FROM CRANK SHAFT BEARING
PCRANK = VISB*(RCRANKB**3)*CRANKLB*((2*PI)
$      /((CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
C.....POWER LOSS FROM AIR CONDITIONING
VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)
RPMCOOL = QB/(H1-H2)*4.*60.*V1/
$      (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2)
IF (RPM.LE.RPMCOOL) THEN
  PAIR = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(RPM/60.)*VOLEEF
$      *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *EVAPP*(1./(EMB*ECB))*(-1.)
ELSE
  PAIR = QB/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
$      *(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *(1./(EMB*ECB))*(-1.)
ENDIF
C.....POWER LOSS FROM WATER PUMP AND OIL PUMP
PWP = 269.*((RPM/1000.))**1.5/12.*(RPM*VDB/1000000.)
C.....POWER LOSS FROM ALTERNATOR LOAD
PALTER = AMPB*VOLTB + (100./FRAC)*(1/3.)*CORRK
$      *((RALT*PI*RDALTB*RPM/3048.))**2.5)*1000.
$      *(RDALTB/0.0254)*(RLALTB/0.0254)**0.5
C.....POWER LOSS FROM ACCESSORIES LOAD
PACC = PAIR+PWP+PALTER
C.....POWER LOSS FROM PUMPING LOSSES
PPUMP = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*RPM)/(3904000))**2) +
$      8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)*
$      ((2.984/FBB)**1.28) +
$      (SQRT((PA-PIG)/97.94))*(11.86*(RCB**0.4)-(3.38+0.103*RCB)
$      *((RPM/1000.))**1.185))*1000.*(2.*ARMB*PI*NCB*(BOREB**2.)
$      /4.)*(RPM/120.)
C.....POWER LOSS FROM PISTON SKIRT
PPIS = (VISB*PI*BOREB*PISLB/PCB)*((ARMB*(RPM/15))**2)*NCB
C.....POWER LOSS FROM PISTON RING
PRING = VISB*ARMB*2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB*

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$          (1-RO)/(1+RO))*4*ARMB*PI*BOREB*(RPM/60)*NOILB*NCB +
$          VISB*ARMB*2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB*
$          (1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(RPM/60)*NPRESSB*NCB
C.....POWER LOSS FROM CONNECTING ROD
PCON = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$          *((2*PI*(RPM/60))**2)*NCB*VMEAN1 +
$          VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$          *((2*PI*(RPM/60))**2)*NCB*VSMEAN1
C.....POWER LOSS FROM CAM LOAD
PCAM = -TOR7*RADC*NCB*NVCB
PTOTAL = PCRANK+PAIR+PWP+PALTER+PPUMP+PPIS+PRING+PCON+PCAM
OPEN(UNIT=1,FILE='RESULT3.OUT',STATUS='OLD')
WRITE(1,202) RPM,PCRANK,PAIR,PWP,PALTER,PPUMP,PPIS,PRING,
$          PCON,PCAM,PTOTAL
WRITE(6,202) RPM,PCRANK,PAIR,PWP,PALTER,PPUMP,PPIS,PRING,
$          PCON,PCAM,PTOTAL
202 FORMAT(F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,
$1X,F6.1,1X,F6.1,1X,F6.1,1X,F7.1)
210 CONTINUE
WRITE(1,*) ' '
WRITE(6,*) ' '
WRITE(1,*) ' POWER REQUIRED AT OPTIMUM DATA '
C*****-----*****C
C          POWER REQUIRED IN OPTIMUM DATA          C
C*****-----*****C
DO 211 I3 = 0,RPMN,1
  DRPM = (RPMH-RPML)/RPMN
  RPM = RPML + I3*DRPM
  RPMC = RPM/2.
  RADC = (RPMC*2*PI/60.)
  XMIN7 = RCH
  XMIN18 = CONLH
  IF (RPM.LE.1300.) THEN
    DHM = 9.9
  ELSE
    IF (RPM.LE.1700.) THEN
      DHM = 10.2
    ELSE
      IF (RPM.LE.2000.) THEN
        DHM = 11.
      ELSE
        IF (RPM.LE.2400.) THEN
          DHM = 12.
        ELSE
          IF (RPM.LE.2700.) THEN
            DHM = 13.
          ELSE
            IF (RPM.LE.3000.) THEN
              DHM = 13.7
            ELSE
              IF (RPM.LE.3400.) THEN
                DHM = 14.9
              ELSE
                IF (RPM.LE.3700.) THEN
                  DHM = 15.9
                ELSE
                  IF (RPM.LE.4000.) THEN
                    DHM = 16.5
                  ELSE
                    WRITE(*,*) ' OVER ENGINE SPEED '
                  ENDIF
                ENDIF
              ENDIF
            ENDIF
          ENDIF
        ENDIF
      ENDIF
    ENDIF
  ENDIF
  ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
ENDIF

```

```

PIA = 9.81*DENHG*DHM*0.0254/1000.
CIMEP = 12.87*PA*((PIA/PA)-0.1)
PIG = PA-(CIMEP/12.8)-10.14
FMM = (NVB*NCB*(XMIN6**2))*1000000./VDB
FBM = (XMIN22**2.-XMIN23**2.+(XMIN22+XMIN24-XMIN23)**2.-
$      2.*XMIN22*(XMIN22+XMIN24-XMIN23)*SIN(SDEGB*PI/180.))
$      /(2.*(XMIN22-XMIN23-(XMIN22+XMIN24-XMIN23)
$      *SIN(SDEGB*PI/180.)))
CDEGM = ACOS((FBM-XMIN22)*COS(SDEGB*PI/180.)/(FBM-XMIN23))
$      *180./PI
CALL NUM4(XMIN10,XMIN11,RP,RO,H,HP11,HO11,HP21,HO21,HP31,HO31)
CALL MEAN14(XMIN18,XMIN27,VBMEAN14,VSMEAN14,PI)
CALL TMEAN71(PCOE,SDEGB,FBM,CDEGM,XMIN19,XMIN20,XMIN21,XMIN22
$      ,XMIN23,XMIN24,RADC,TOR71,PI)
C.....POWER LOSS FROM CRANK SHAFT BEARING
PCRANKM = XMIN25*(XMIN1**3.)*XMIN2*((2.*PI)
$      /(XMIN3*SQRT(1.-EC**2.)))*((2.*PI*(RPM/60.))**2.)*BN
C.....POWER LOSS FROM AIR CONDITIONING
VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)
RPMCOOL = XACC1/(H1-H2)*4.*60.*V1/
$      (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2.)
IF (RPM.LE.RPMCOOL) THEN
  PAIRM = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(RPM/60.)*VOLEEF
$      *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *EVAPP*(1./(EMB*ECB))*(-1.)
ELSE
  PAIRM = XACC1/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
$      *(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *(1./(EMB*ECB))*(-1.)
ENDIF
C.....POWER LOSS FROM WATER PUMP AND OIL PUMP
PWPM = 269.*((RPM/1000.))**1.5)/12.*RPM*VDB/1000000.
C.....POWER LOSS FROM ALTERNATOR LOAD
PALTERM = AMPB*VOLTB + (100./FRAC)*(1/3.)*CORRK
$      *((RALT*PI*XACC3*RPM/3048.))**2.5)*1000.
$      *(XACC3/0.0254)*(XACC4/0.0254)**0.5
C.....POWER LOSS FROM PUMPING LOSSES
PPUMP = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*RPM)/(3904000))**2) +
$      8.9667*(SQRT(CIMEP/1124.3))*((RPM/1000)**1.7)*
$      ((2.984/FMM)**1.28) +
$      (SQRT((PA-PIG)/97.94))*(11.86*(XMIN7**0.4)
$      -(3.38+0.103*XMIN7))*((RPM/1000)**1.185))*VDB/1000
$      *(RPM/120)
C.....POWER LOSS FROM PISTON SKIRT
PPISM = (XMIN25*PI*XMIN26*XMIN9/XMIN8)*((XMIN27*(RPM/15))**2)
$      *NCB
C.....POWER LOSS FROM PISTON RING
PRINGM = XMIN25*XMIN27*2*PI*(RPM/60)*(4*HO11-3*(HO21**2)/HO31+
$      XMIN11*(1-RO)/(1+RO))*4*XMIN27*PI*XMIN26*(RPM/60)
$      *NOILB*NCB +
$      XMIN25*XMIN27*2*PI*(RPM/60)*(4*HP11-3*(HP21**2)/HP31+
$      (XMIN10*(1-RP)/(1+RP))/H)*4*XMIN27*PI*XMIN26*(RPM/60)
$      *NPRESSB*NCB
C.....POWER LOSS FROM CONNECTING ROD
PCONM = XMIN25*(XMIN12**3)*XMIN14*((2*PI)/(XMIN13*SQRT(1-E**2)))
$      *((2*PI*(RPM/60))**2)*NCB*VBMEAN14 +
$      XMIN25*(XMIN15**3)*XMIN17*((2*PI)/
$      (XMIN16*SQRT(1-ESM**2)))*((2*PI*(RPM/60))**2)*NCB
$      *VSMEAN14
C.....POWER LOSS FROM CAM LOAD
PCAMM = -TOR71*RADC*NCB*NVCB
PTOTALM = PCRANKM+PAIRM+PWPM+PALTERM+PPUMP+PPISM+PRINGM+PCONM
$      +PCAMM
OPEN(UNIT=1,FILE='RESULT3.OUT',STATUS='OLD')
WRITE(1,203) RPM,PCRANKM,PAIRM,PWPM,PALTERM,PPUMP,PPISM,
$      PRINGM,PCONM,PCAMM,PTOTALM
WRITE(6,203) RPM,PCRANKM,PAIRM,PWPM,PALTERM,PPUMP,PPISM,
$      PRINGM,PCONM,PCAMM,PTOTALM
203 FORMAT(F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X,F6.1,

```

\$1X,F6.1,1X,F6.1,1X,F6.1,1X,F7.1)

211 CONTINUE

```
C*****-----*****C
C                               ROAD LOAD POWER AND TRANSMISSION LOSS
C*****-----*****C
```

```
WRITE(6,*) ' '
WRITE(1,*) ' '
WRITE(1,*) ' (RPM) : (km/hr) : AIR-LOAD (W) : ROLLING-LOAD (W) :
$ TRANSMISSION (W) '
WRITE(6,*) ' (RPM) : (km/hr) : AIR-LOAD (W) : ROLLING-LOAD (W) :
$ TRANSMISSION (W) '
DO 212 I4 = 0,RPMN,1
  DRPM = (RPMH-RPML)/RPMN
  RPM = RPML + I4*DRPM
  CALL SEL1(RPM,GN,G1,G2,G3,G4,G5,GD,TEFF,GT)
  SPEED = (RPM/60)*2*PI*WR*3.6/GT
  PAIRR = 0.5*CDB*AIRDEN*AREAB*( (RPM/60)*2*PI*WR/GT )**3
  PROLL = FRB*MGB*( (RPM/60)*2*PI*WR/GT )*9.81
  PTRAN = (1/TEFF-1)*(PAIRR+PROLL)
  WRITE(1,205) RPM,SPEED,PAIRR,PROLL,PTRAN
  WRITE(6,205) RPM,SPEED,PAIRR,PROLL,PTRAN
```

212 CONTINUE

```
WRITE(6,*) ' '
WRITE(1,*) ' '
WRITE(1,*) ' ROAD LOAD AND TRANSMISSION AT OPTIMUM DATA'
WRITE(1,204) GN
WRITE(1,*) ' (RPM) : (km/hr) : AIR-LOAD (W) : ROLLING-LOAD (W) :
$ TRANSMISSION (W) '
WRITE(6,*) ' (RPM) : (km/hr) : AIR-LOAD (W) : ROLLING-LOAD (W) :
$ TRANSMISSION (W) '
DO 213 I5 = 0,RPMN,1
  DRPM = (RPMH-RPML)/RPMN
  RPM = RPML + I5*DRPM
  CALL SEL1(RPM,GN,G1,G2,G3,G4,G5,GD,TEFF,GT)
  SPEED = (RPM/60)*2*PI*WR*3.6/GT
  PAIRRM = 0.5*XMIN28*AIRDEN*XMIN29*( (RPM/60)*2*PI*WR/GT )**3
  PROLLM = XMIN30*XMIN31*( (RPM/60)*2*PI*WR/GT )*9.81
  PTRANM = (1/TEFF-1)*(PAIRRM+PROLLM)
  WRITE(1,205) RPM,SPEED,PAIRRM,PROLLM,PTRANM
  WRITE(6,205) RPM,SPEED,PAIRRM,PROLLM,PTRANM
```

213 CONTINUE

204 FORMAT(1X, ' DRIVE GEAR NUMBER ',F4.0)

205 FORMAT(1X,F6.1,T12,F5.1,T24,F9.2,T36,F7.2,T48,F7.2)

```
C*****-----*****C
C-----C
C XMIN1 = RADIUS OF BEARING IN CRANKSHAFT C
C XMIN2 = BEARING WIDTH IN CRANKSHAFT C
C XMIN3 = RADIUS CLEARANCE IN CRANKSHAFT C
C XMIN6 = INLET VALVE DIAMETER C
C XMIN7 = COMPRESSION RATIO C
C XMIN8 = PISTON CLEARANCE C
C XMIN9 = SKIRT LENGTH C
C XMIN10 = PRESSURE RING DEPTH C
C XMIN11 = OIL RING DEPTH C
C XMIN12 = RADIUS OF BEARING AT BIG-END SIDE C
C XMIN13 = RADIUS CLEARANCE AT BIG-END SIDE C
C XMIN14 = BEARING WIDTH AT BIG-END SIDE C
C XMIN15 = RADIUS OF BEARING AT SMALL-END SIDE C
C XMIN16 = RADIUS CLEARANCE AT SMALL-END SIDE C
C XMIN17 = BEARING WIDTH AT SMALL-END SIDE C
C XMIN18 = CONNECTING ROD LENGTH C
C XMIN19 = VALVE FOLLOWER MASS C
C XMIN20 = SPRING STIFFNESS C
C XMIN21 = VALVE PRELOAD C
C XMIN22 = BASE RADIUS C
C XMIN23 = TIP RADIUS C
C XMIN24 = VALVE LIFT C
C XMIN25 = ABSOLUTE VISCOSITY C
C XMIN26 = BORE C
```

```

C          XMIN27 = CRANK ARM
C          XMIN28 = DRAG COEFFICIENT
C          XMIN29 = FRONTAL AREA
C          XMIN30 = ROLLING COEFFICIENT
C          XMIN31 = VEHICLE MASS
C          XACC1 = COOLING LOAD
C          XACC3 = ROTOR DIAMETER IN ALTERNATOR
C          XACC4 = ROTOR LENGTH IN ALTERNATOR
C-----C
C*****-----*****C
C          POWER REQUIRED AT OPERATION CONDITON
C*****-----*****C
C
OPEN(UNIT=1,FILE='RESULT3.OUT',STATUS='OLD')
  RPMC = ORPM/2
  RADC = (RPMC*2*PI/60)
  IF (ORPM.LE.1300.) THEN
    DHM = 9.9
  ELSE
    IF (ORPM.LE.1700.) THEN
      DHM = 10.2
    ELSE
      IF (ORPM.LE.2000.) THEN
        DHM = 11.
      ELSE
        IF (ORPM.LE.2400.) THEN
          DHM = 12.
        ELSE
          IF (ORPM.LE.2700.) THEN
            DHM = 13.
          ELSE
            IF (ORPM.LE.3000.) THEN
              DHM = 13.7
            ELSE
              IF (ORPM.LE.3400.) THEN
                DHM = 14.9
              ELSE
                IF (ORPM.LE.3700.) THEN
                  DHM = 15.9
                ELSE
                  IF (ORPM.LE.4000.) THEN
                    DHM = 16.5
                  ELSE
                    WRITE(*,*) ' OVER ENGINE SPEED '
                  ENDIF
                ENDIF
              ENDIF
            ENDIF
          ENDIF
        ENDIF
      ENDIF
    ENDIF
  ENDIF
  PIA = 9.81*DENHG*DHM*0.0254/1000
  CIMEP = 12.87*PA*((PIA/PA)-0.1)
  PIG = PA-(CIMEP/12.8)-10.14
  FBO = (NVB*NCB*(DVB**2))/(2*ARMB*PI*NCB*(BOREB**2)/4)
  FB = (BRB**2-TRB**2+(BRB+VLB-TRB)**2-2*BRB*(BRB+VLB-TRB)
$      *SIN(SDEGB*PI/180))/(2*(BRB-TRB-(BRB+VLB-TRB)
$      *SIN(SDEGB*PI/180)))
  CDEGB = ACOS((FB-BRB)*COS(SDEGB*PI/180)/(FB-TRB))*180/PI
  CALL NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
  CALL MEAN1(CONLB,ARMB,VBMEAN1,VSMEAN1)
  CALL TMEAN7(FCOE,SDEGB,FB,CDEGB,FMB,SCB,PLB,BRB,TRB,VLB,RADC
$      ,TOR7,PI)
C.....POWER LOSS FROM CRANK SHAFT BEARING
  PCRAN1 = VISB*(RCRANKB**3)*CRANKLB*((2*PI)
$      /((CCRANKB*SQRT(1-EC**2)))*((2*PI*(ORPM/60))**2)*BN
C.....POWER LOSS FROM AIR CONDITIONING
  VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)

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```

RPMCOOL = QB/(H1-H2)*4.*60.*V1/
$ (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2)
IF (ORPM.LE.RPMCOOL) THEN
  PAIR1 = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(ORPM/60.)*VOLEEF
$ *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$ *EVAPP*(1./(EMB*ECB))*(-1.)
ELSE
  PAIR1 = QB/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
$ *(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$ *(1./(EMB*ECB))*(-1.)
ENDIF
C.....POWER LOSS FROM WATER PUMP AND OIL PUMP
PWP1 = 269.*(ORPM/1000)**1.5)/12.*ORPM*VDB/1000000
C.....POWER LOSS FROM ALTERNATOR LOAD
PALT1 = AMPB*VOLTB + (100./FRAC)*(1./3.)*CORRK
$ *((RALT*PI*RDALTB*ORPM/3048.))**2.5)*1000.
$ *(RDALTB/0.0254)*(RLALTB/0.0254)**0.5
C.....POWER LOSS FROM PUMPING LOSSES
PPUMP1 = (PA-(CIMEP/12.8)-10.14+PE*((CIMEP*ORPM)/(3904000))**2) +
$ 8.9667*(SQRT(CIMEP/1124.3))*((ORPM/1000)**1.7)*
$ ((2.984/FBO)**1.28) +
$ (SQRT((PA-PIG)/97.94))*(11.86*(RCB**0.4)-(3.38+0.103*RCB)
$ *((ORPM/1000)**1.185))*1000*(2*ARMB*PI*NCB*(BOREB**2)/4)
$ *(ORPM/120)
C.....POWER LOSS FROM PISTON SKIRT
PPIS1 = (VISB*PI*BOREB*PISLB/PCB)*((ARMB*(ORPM/15))**2)*NCB
C.....POWER LOSS FROM PISTON RING
PRING1 = VISB*ARMB*2*PI*(ORPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB*
$ (1-RO)/(1+RO))*4*ARMB*PI*BOREB*(ORPM/60)*NOILB*NCB +
$ VISB*ARMB*2*PI*(ORPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB*
$ (1-RP)/(1+RP))/H)*4*ARMB*PI*BOREB*(ORPM/60)*NPRESSB*NCB
C.....POWER LOSS FROM CONNECTING ROD
PCON1 = VISB*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$ *((2*PI*(ORPM/60))**2)*NCB*VBMEAN1 +
$ VISB*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$ *((2*PI*(ORPM/60))**2)*NCB*VSMEAN1
C.....POWER LOSS FROM CAM LOAD
PCAM1 = -TOR7*RADC*NCB*NVCB
C.....TOTAL ENGINE POWER LOSS AT BASE LINE DATA
PTOT1 = PCRAN1+PAIR1+PWP1+PALT1+PPUMP1+PPIS1+PRING1+PCON1+PCAM1
C.....POWER LOSS FROM ROAD LOAD
PAIRR1 = 0.5*CDB*AIRDEN*AREAB*((ORPM/60)*2*PI*WR/GT)**3
PROLL1 = FRB*MGB*((ORPM/60)*2*PI*WR/GT)*9.81
PTRAN1 = (1/TEFF-1)*(PAIRR1+PROLL1)
BREAK1 = PAIRR1 + PROLL1 + PTRAN1
C.....POWER FRACTION EACH ENGINE POWER LOSS
PP1 = PCRAN1/PTOT1*100
PP2 = PAIR1/PTOT1*100
PP3 = PWP1/PTOT1*100
PP4 = PALT1/PTOT1*100
PP5 = PPUMP1/PTOT1*100
PP6 = PPIS1/PTOT1*100
PP7 = PRING1/PTOT1*100
PP8 = PCON1/PTOT1*100
PP9 = PCAM1/PTOT1*100
WRITE(1,*) ' '
WRITE(1,*) 'ENGINE POWER SHARING AT BASE LINE DATA '
WRITE(1,*) 'CRANK% : AIR% : PUMP% : ALT% : PUMPING% : PIS% : RING%
$ : CON% : CAM% '
WRITE(1,214) PP1,PP2,PP3,PP4,PP5,PP6,PP7,PP8,PP9
WRITE(1,*) ' '
214 FORMAT(2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,
$F5.2,2X,F5.2)
C*****-----*****C
FMO = (NVB*NCB*(XMIN6**2))*1000000/VDB
FBM = (XMIN22**2-XMIN23**2+(XMIN22+XMIN24-XMIN23)**2 -
$ /2*XMIN22*(XMIN22+XMIN24-XMIN23)*SIN(SDEGB*PI/180))
$ /(2*(XMIN22-XMIN23)-(XMIN22+XMIN24-XMIN23)
$ *SIN(SDEGB*PI/180))

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CDEGM = ACOS( (FBM-XMIN22)*COS(SDEGB*PI/180)/(FBM-XMIN23) )
$      *180/PI
CALL NUM4(XMIN10,XMIN11,RP,RO,H,HP11,HO11,HP21,HO21,HP31,HO31)
CALL MEAN14(XMIN18,XMIN27,VBMEAN14,VSMEAN14,PI)
CALL TMEAN71(PCOE,SDEGB,FBM,CDEGM,XMIN19,XMIN20,XMIN21,XMIN22
$      ,XMIN23,XMIN24,RADC,TOR71,PI)
C.....POWER LOSS FROM CRANK SHAFT BEARING
PCRAN2 = XMIN25*(XMIN1**3)*XMIN2*((2*PI)
$      /(XMIN3*SQRT(1-EC**2)))*((2*PI*(ORPM/60))**2)*BN
C.....POWER LOSS FROM AIR CONDITIONING
VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)
RPMCOOL = XACC1/(H1-H2)*4.*60.*V1/
$      (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2.)
IF (ORPM.LE.RPMCOOL) THEN
  PAIR2 = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(ORPM/60.)*VOLEEF
$      *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *EVAPP*(1./(EMB*ECB))*(-1.)
ELSE
  PAIR2 = XACC1/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
$      *(1.-(CONDP/EVAPP)**((RKB-1.)/RKB))
$      *(1./(EMB*ECB))*(-1.)
ENDIF
C.....POWER LOSS FROM WATER PUMP AND OIL PUMP
PWP2 = 269.*((ORPM/1000)**1.5)/12.*ORPM*VDB/1000000
C.....POWER LOSS FROM ALTERNATOR LOAD
PALT2 = AMPB*VOLTB + (100./FRAC)*(1/3.)*CORRK
$      *((RALT*PI*XACC3*ORPM/3048.))**2.5)*1000.
$      *(XACC3/0.0254)*(XACC4/0.0254)**0.5
C.....POWER LOSS FROM PUMPING LOSSES
PPUMP2 = (PA-(CIMEP/12.8)-10.14+PE*(((CIMEP*ORPM)/(3904000))**2)+
$      8.9667*(SQRT(CIMEP/1124.3))*((ORPM/1000)**1.7)*
$      ((2.984/FMO)**1.28) +
$      (SQRT((PA-PIG)/97.94))*(11.86*(XMIN7**0.4)
$      -(3.38+0.103*XMIN7))*((ORPM/1000)**1.185))*VDB/1000
$      *(ORPM/120)
C.....POWER LOSS FROM PISTON SKIRT
PPIS2 = (XMIN25*PI*XMIN26*XMIN9/XMIN8)*((XMIN27*(ORPM/15))**2)
$      *NCB
C.....POWER LOSS FROM PISTON RING
PRING2 = XMIN25*XMIN27*2*PI*(ORPM/60)*(4*HO11-3*(HO21**2)/HO31 +
$      BOILB*(1-RO)/(1+RO))*4*XMIN27*PI*XMIN26*(ORPM/60)*
$      NOILB*NCB + XMIN25*XMIN27*2*PI*(ORPM/60)*
$      (4*HP11-3*(HP21**2)/HP31 + (BPRESSB*(1-RP)/(1+RP))/H)*
$      4*XMIN27*PI*XMIN26*(ORPM/60)*NPRESSB*NCB
C.....POWER LOSS FROM CONNECTING ROD
PCON2 = XMIN25*(XMIN12**3)*XMIN14*((2*PI)/(XMIN13*SQRT(1-E**2)))
$      *((2*PI*(ORPM/60))**2)*NCB*VBMEAN14 +
$      XMIN25*(XMIN15**3)*XMIN17*((2*PI)/
$      (XMIN16*SQRT(1-ESM**2)))*((2*PI*(ORPM/60))**2)*NCB
$      *VSMEAN14
C.....POWER LOSS FROM CAM LOAD
PCAM2 = -TOR71*RADC*NCB*NVCB
C.....TOTAL ENGINE POWER LOSS AT OPTIMUM DATA
PTOT2 = PCRAN2+PAIR2+PWP2+PALT2+PPUMP2+PPIS2+PRING2+PCON2
$      +PCAM2
C.....POWER LOSS FROM ROAD LOAD
VELO = (ORPM/60)*2*PI*WR*3.6/GT
PAIRR2 = 0.5*XMIN28*AIRDEN*XMIN29*((ORPM/60)*2*PI*WR/GT)**3
PROLL2 = XMIN30*XMIN31*((ORPM/60)*2*PI*WR/GT)**9.81
PTRAN2 = (1/TEFF-1)*(PAIRR1+PROLL1)
BREAK2 = PAIRR2 + PROLL2 + PTRAN2
C.....POWER FRACTION EACH ENGINE POWER LOSS
DP1 = (PCRAN1-PCRAN2)*100/PCRAN1
DP2 = (PAIR1-PAIR2)*100/PAIR1
DP3 = (PALT1-PALT2)*100/PALT1
DP4 = (PPUMP1-PPUMP2)*100/PPUMP1
DP5 = (PPIS1-PPIS2)*100/PPIS1
DP6 = (PRING1-PRING2)*100/PRING1
DP7 = (PCON1-PCON2)*100/PCON1

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DP8 = (PCAM1-PCAM2)*100/PCAM1
DP9 = (PTOT1-PTOT2)*100/PTOT1
DP10 = (PAIRR1-PAIRR2)*100/PAIRR1
DP11 = (PROLL1-PROLL2)*100/PROLL1
DP12 = (BREAK1-BREAK2)*100/BREAK1
TDP = PCRAN1-PCRAN2+PAIR1-PAIR2+PALT1-PALT2+PPUMP1-PPUMP2+
      PPIS1-PPIS2+PRING1-PRING2+PCON1-PCON2+PCAM1-PCAM2
$
FD1 = (PCRAN1-PCRAN2)/TDP*100
FD2 = (PAIR1-PAIR2)/TDP*100
FD3 = (PALT1-PALT2)/TDP*100
FD4 = (PPUMP1-PPUMP2)/TDP*100
FD5 = (PPIS1-PPIS2)/TDP*100
FD6 = (PRING1-PRING2)/TDP*100
FD7 = (PCON1-PCON2)/TDP*100
FD8 = (PCAM1-PCAM2)/TDP*100
TDPV = PAIRR1-PAIRR2+PROLL1-PROLL2
FD10 = DP10/TDPV
FD11 = DP11/TDPV
FD12 = DP12/TDPV
WRITE(1,215) ORPM,DHM
WRITE(1,*) 'POWER AT BASE LINE DATA : OPTIMUM DATA : DECREASING %'
WRITE(1,*) ' '
WRITE(1,216) PCRAN1,PCRAN2,DP1
WRITE(1,217) PAIR1,PAIR2,DP2
WRITE(1,218) PALT1,PALT2,DP3
WRITE(1,219) PPUMP1,PPUMP2,DP4
WRITE(1,220) PPIS1,PPIS2,DP5
WRITE(1,221) PRING1,PRING2,DP6
WRITE(1,222) PCON1,PCON2,DP7
WRITE(1,223) PCAM1,PCAM2,DP8
WRITE(1,*) ' '
WRITE(1,*) ' TOTAL ENGINE POWER LOSS AT BASE LINE : OPTIMUM : DECR
SEASING % '
WRITE(1,224) PTOT1,PTOT2,DP9
WRITE(1,225) VELO,GN
WRITE(1,*) 'POWER AT BASE LINE DATA : OPTIMUM DATA : DECREASING %'
WRITE(1,226) PAIRR1,PAIRR2,DP10
WRITE(1,227) PROLL1,PROLL2,DP11
WRITE(1,228) BREAK1,BREAK2,DP12
WRITE(1,*) ' FRACTION OF DECREASING OF ENGINE POWER LOSS '
WRITE(1,*) ' CRANK:AIR:ALTERNATOT:PUMPING:SKIRT:RING:CON-ROD:CAM '
WRITE(1,229) FD1,FD2,FD3,FD4,FD5,FD6,FD7,FD8
WRITE(6,*) ' '
WRITE(6,215) ORPM,DHM
WRITE(6,*) ' POWER AT BASE LINE DATA : OPTIMUM DATA : DECREASING%'
WRITE(6,216) PCRAN1,PCRAN2,DP1
WRITE(6,217) PAIR1,PAIR2,DP2
WRITE(6,218) PALT1,PALT2,DP3
WRITE(6,219) PPUMP1,PPUMP2,DP4
WRITE(6,220) PPIS1,PPIS2,DP5
WRITE(6,221) PRING1,PRING2,DP6
WRITE(6,222) PCON1,PCON2,DP7
WRITE(6,223) PCAM1,PCAM2,DP8
WRITE(6,*) ' '
WRITE(6,*) ' TOTAL POWER AT BASE LINE : OPTIMUM : DECREASING. %'
WRITE(6,224) PTOT1,PTOT2,DP9
WRITE(6,225) VELO,GN
WRITE(6,*) ' POWER AT BASE LINE DATA : OPTIMUM DATA : DECREASING %'
WRITE(6,226) PAIRR1,PAIRR2,DP10
WRITE(6,227) PROLL1,PROLL2,DP11
WRITE(6,*) ' BREAK POWER AT BASE LINE : OPTIMUM : DECREASING % '
WRITE(6,228) BREAK1,BREAK2,DP12
WRITE(6,*) ' FRACTION OF DECREASING OF ENGINE POWER LOSS '
WRITE(6,*) ' CRANK:AIR:ALTERNATOR:PUMPING:SKIRT:RING:CON-ROD:CAM '
WRITE(6,229) FD1,FD2,FD3,FD4,FD5,FD6,FD7,FD8
215 FORMAT(' ENGINE SPEED ',F6.1,' (RPM) : MANIFOLD ',F4.1,
$ '(INCH)')
216 FORMAT(' CRANK-SHAFT. :',T30,F7.2,2X,F7.2,2X,F5.2)
217 FORMAT(' AIR CONDITIONING :',T30,F7.2,2X,F7.2,2X,F5.2)

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218 FORMAT(' ALTERNATOR           :',T30,F7.2,2X,F7.2,2X,F5.2)
219 FORMAT(' PUMPING               :',T30,F7.2,2X,F7.2,2X,F5.2)
220 FORMAT(' PISTON SKIRT          :',T30,F7.2,2X,F7.2,2X,F5.2)
221 FORMAT(' PISTON RING           :',T30,F7.2,2X,F7.2,2X,F5.2)
222 FORMAT(' CONNECTING ROD        :',T30,F7.2,2X,F7.2,2X,F5.2)
223 FORMAT(' CAM LOAD              :',T30,F7.2,2X,F7.2,2X,F5.2)
224 FORMAT(' TOTAL                 :',T30,F8.2,2X,F8.2,2X,F5.2)
225 FORMAT(' VEHICLE SPEED ',F6.2,' (km/hr) : GEAR NUMBER ',F3.1)
226 FORMAT(' AIR LOAD              :',T30,F8.2,2X,F8.2,2X,F5.2)
227 FORMAT(' ROLLING LOAD          :',T30,F8.2,2X,F8.2,2X,F5.2)
228 FORMAT(' BREAK POWER           :',T30,F8.2,2X,F8.2,2X,F5.2)
229 FORMAT(2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,F5.2,2X,
$F5.2)
STOP
END

```

```

C*****-----C
C                               END MAIN PROGRAM                               C
C*****-----C
C                               MULTIVARIABLE OPTIMIZATION SEARCH METHOD       C
C*****-----C
SUBROUTINE P311(RPM,BOREL,BOREH,VISL,VISH,CONLB,BN,NPRESSB,NOILB,
$ NCB,RP,RO,PI,H,EC,E,ESM,RCRANKB,CRANKLB,CCRANKB,BPRESSB,
$ BOILB,BRCONB,BCCONB,BLCONB,SRCONB,SCCONB,SLCONB,PCB,PISLB,
$ VDB,XMIN25,XMIN26,XMIN27)
YMIN25 = 999999.
YMIN26 = 999999.
TOL1 = 0.005
TOL2 = 0.005
N1 = 20
XI1 = VISL
XI2 = BOREL
DX1 = (VISH-VISL)/N1
DX2 = (BOREH-BOREL)/N1
DO 200 I = 1,50
DO 25 J25 = 0,N1
BORE = XI2 + J25*DX2
ARM = VDB*2/(PI*(BORE**2)*NCB*1000000)
C Y25 = f25(XI1,BORE)
CALL NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
CALL MEAN11(CONLB,ARM,VBMEAN11,VSMEAN11)
Y25 = XI1*(RCRANKB**3)*CRANKLB*((2*PI)/
$ (CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
C.....PISTON SKIRT
$ + (XI1*PI*BORE*PISLB/PCB)*((ARM*(RPM/15))**2)*NCB
C.....PISTON RING
$ + XI1*ARM*2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB
$ *(1-RO)/(1+RO))*4*ARM*PI*BORE*(RPM/60)*NOILB*NCB +
$ XI1*ARM*2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB
$ *(1-RP)/(1+RP))/H)*4*ARM*PI*BORE*(RPM/60)*NPRESSB*NCB
C.....CONNECTING ROD
$ + XI1*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$ *((2*PI*(RPM/60))**2)*NCB*VBMEAN11 +
$ XI1*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$ *((2*PI*(RPM/60))**2)*NCB*VSMEAN11
IF (YMIN25.GT.Y25) THEN
YMIN25 = Y25
XMIN25 = XI1
XMIN26 = BORE
XMIN27 = ARM
ENDIF
25 CONTINUE
IF ( ( ABS(XMIN25-XI1).LE.TOL1 ) .AND. ( ABS(XMIN26-XI2).LE.TOL2 ) )
$ THEN
GOTO 1000
ENDIF
DX1 = (VISH-XMIN25)/N1
DX2 = (BOREH-XMIN26)/N1
DO 26 K26 = 0,N1

```

```

      VIS = XI1 + K26*DX1
C   Y26 = F26(VIS,XMIN26)
      CALL NUM1(BPRESSB,BOILB,RP,RO,H,HP1,HO1,HP2,HO2,HP3,HO3)
      CALL MEAN12(CONLB,XMIN27,VBMEAN12,VSMEAN12)
      Y26 = VIS*(RCRANKB**3)*CRANKLB*((2*PI)/
$      (CCRANKB*SQRT(1-EC**2)))*((2*PI*(RPM/60))**2)*BN
C   PISTON SKIRT
$   + (VIS*PI*XMIN27*PISLB/PCB)*((XMIN27*(RPM/15))**2)*NCB
C   PISTON RING
$   + VIS*XMIN27**2*PI*(RPM/60)*(4*HO1-3*(HO2**2)/HO3+BOILB
$   *(1-RO)/(1+RO))*4*XMIN27*PI*XMIN26*(RPM/60)*NOILB*NCB +
$   VIS*XMIN27**2*PI*(RPM/60)*(4*HP1-3*(HP2**2)/HP3+(BPRESSB
$   *(1-RP)/(1+RP))/H)*4*XMIN27*PI*XMIN26*(RPM/60)*NPRESSB*NCB
C   CONNECTING ROD
$   + VIS*(BRCONB**3)*BLCONB*((2*PI)/(BCCONB*SQRT(1-E**2)))
$   *((2*PI*(RPM/60))**2)*NCB*VBMEAN12 +
$   VIS*(SRCONB**3)*SLCONB*((2*PI)/(SCCONB*SQRT(1-ESM**2)))
$   *((2*PI*(RPM/60))**2)*NCB*VSMEAN12
      IF (YMIN26.GT.Y26) THEN
          YMIN26 = Y26
          XMIN25 = VIS
          XMIN26 = XMIN26
      ENDIF
26 CONTINUE
      IF ( ( ABS(XMIN25-XI1).LE.TOL1 ).AND. ( ABS(XMIN26-XI2).LE.TOL2 ) )
$      THEN
          GOTO 1000
      ENDIF
          XI1 = XMIN25
          XI2 = XMIN26
          DX1 = (VISH-XMIN25)/N1
          DX2 = (BOREH-XMIN26)/N1
200 CONTINUE
1000 RETURN
      END

```

```

C*****-----*****C
C               SUBROUTINE FOR ACCESSORIES LOAD                               C
C*****-----*****C

```

```

      SUBROUTINE ACCESS(N,RPM,BCOMB,SCOMB,RKB,EMB,ECB,RDALTB,RLALTB,
$QL,QH,RDALTL,RDALH,RLALTL,RLALH,RCOM,NCOM,PCLE,H1,H2,V1,FRAC,
$EVAPP,CONDP,CORRK,RALT,PAIRQ,PALTD,PALTL,PI,Q,AMPB,VOLTB,
$RDALT,RLALT,XACC1,XACC3,XACC4)

```

```

      PACC1 = 99999.
      PACC3 = 99999.
      PACC4 = 99999.
      VOLEEF = 1.+(PCLE/100.)*(1.-CONDP/EVAPP)
      RPMCOOL = Q/(H1-H2)*4.*60.*V1/
$      (PI*SCOMB*NCOM*VOLEEF*RCOM*(BCOMB)**2)
      DO 1 J = 0,N,1
          DQ = (QH-QL)/N
          Q = QL + J*DQ
      IF (RPM.LE.RPMCOOL) THEN
          PAIRQ = (PI/4.)*(BCOMB**2.)*SCOMB*NCOM*RCOM*(RPM/60.)*VOLEEF
$          *(RKB/(RKB-1.))*(1.-(CONDP/EVAPP))*((RKB-1.)/RKB))
$          *EVAPP*(1./(EMB*ECB))*(-1.)
      ELSE
          PAIRQ = Q/(H1-H2)*EVAPP*V1*(RKB/(RKB-1.))
$          *(1.-(CONDP/EVAPP))*((RKB-1.)/RKB))
$          *(1./(EMB*ECB))*(-1.)
      ENDIF
      IF (PACC1.GT.PAIRQ) THEN
          PACC1 = PAIRQ
          XACC1 = Q
      ENDIF

```

```

C*****-----*****C
      DRDALT = (RDALH - RDALTL)/N
      RDALT = RDALTL + J*DRDALT
      PALTD = AMPB*VOLTB + (100./FRAC)*(1./3.)*CORRK
$      *((RALT*PI*RDALT*RPM/3048.))**2.5)*1000

```

```

$          *(RDALT/0.0254)*((RLALTB/0.0254)**0.5)
IF (PACC3.GT.PALTD) THEN
  PACC3 = PALTD
  XACC3 = RDALT
ENDIF
C*****-----*****C
  DRLALT = (RLALTH - RLALTL)/N
  RLALT = RLALTL + J*DRLALT
  PALTL = AMPB*VOLTB + (100./FRAC)*(1/3.)*CORRK
$          *((RALT*PI*RDALTB*RPM/3048.）**2.5)*1000
$          *(RDALTB/0.0254)*(RLALT/0.0254)**0.5
IF (PACC4.GT.PALTL) THEN
  PACC4 = PALTL
  XACC4 = RLALT
ENDIF
1 CONTINUE
RETURN
END
C*****-----*****C
C          THIS PARTS FOR NUMERICAL SUBPROGRAM CALCULATION          C
C*****-----*****C
C          SUBROUTINE NUM 1          C
C*****-----*****C
SUBROUTINE NUM1 (BPRESSB, BOILB, RP, RO, H, HP1, HO1, HP2, HO2, HP3, HO3)
  N = 100
  A = 0.
  A1P = 0.0015
  A1O = 0.0025
  BP = RP*(BPRESSB/(1+RP))
  BO = RO*(BOILB/(1+RO))
  DHP = (BP-A)/N
  DHO = (BO-A)/N
  SUMP1 = 0.
  SUMO1 = 0.
  SUMP2 = 0.
  SUMO2 = 0.
  SUMP3 = 0.
  SUMO3 = 0.
  DO 10 I = 1, N-1
    XP = I*DHP
    XO = I*DHO
    FXP1 = 1/(A1P*XP**2 - ((1+RP)/(1000*RP) + (A1P*RP*BPRESSB)/
$      (1+RP))*XP + H + BPRESSB/1000)
    FXO1 = 1/(A1O*XO**2 - ((1+RO)/(1000*RO) + (A1O*RO*BOILB)/
$      (1+RO))*XO + H + BOILB/1000)
    FXP2 = (1/(A1P*XP**2 - ((1+RP)/(1000*RP) + (A1P*RP*BPRESSB)/
$      (1+RP))*XP + H + BPRESSB/1000))**2
    FXO2 = (1/(A1O*XO**2 - ((1+RO)/(1000*RO) + (A1O*RO*BOILB)/
$      (1+RO))*XO + H + BOILB/1000))**2
    FXP3 = (1/(A1P*XP**2 - ((1+RP)/(1000*RP) + (A1P*RP*BPRESSB)/
$      (1+RP))*XP + H + BPRESSB/1000))**3
    FXO3 = (1/(A1O*XO**2 - ((1+RO)/(1000*RO) + (A1O*RO*BOILB)/
$      (1+RO))*XO + H + BOILB/1000))**3
    SUMP1 = SUMP1 + FXP1
    SUMO1 = SUMO1 + FXO1
    SUMP2 = SUMP2 + FXP2
    SUMO2 = SUMO2 + FXO2
    SUMP3 = SUMP3 + FXP3
    SUMO3 = SUMO3 + FXO3
  10 CONTINUE
  FXP01 = 1/(H + BPRESSB/1000)
  FXO01 = 1/(H + BOILB/1000)
  FXP02 = (1/(H + BPRESSB/1000))**2
  FXO02 = (1/(H + BOILB/1000))**2
  FXP03 = (1/(H + BPRESSB/1000))**3
  FXO03 = (1/(H + BOILB/1000))**3
  FXPN1 = 1/H
  FXON1 = 1/H
  FXPN2 = (1/H)**2

```

```

FXON2 = (1/H)**2
FXPN3 = (1/H)**3
FXON3 = (1/H)**3
HP1 = (+FXP01+FXPN1+2*SUMP1)*DHP/2
HO1 = (+FXO01+FXON1+2*SUMO1)*DHO/2
HP2 = (+FXP02+FXPN2+2*SUMP2)*DHP/2
HO2 = (+FXO02+FXON2+2*SUMO2)*DHO/2
HP3 = (+FXP03+FXPN3+2*SUMP3)*DHP/2
HO3 = (+FXO03+FXON3+2*SUMO3)*DHO/2
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE NUM 2                               C
C*****-----*****C

```

```

SUBROUTINE NUM2 (BPRESS, BOILB, RP, RO, H, HP4, HO4, HP5, HO5, HP6, HO6)
N = 100
A = 0.
A1P = 0.0015
A1O = 0.0025
BP = RP*(BPRESS/(1+RP))
BO = RO*(BOILB/(1+RO))
DHP = (BP-A)/N
DHO = (BO-A)/N
SUMP4 = 0.
SUMO4 = 0.
SUMP5 = 0.
SUMO5 = 0.
SUMP6 = 0.
SUMO6 = 0.
DO 10 I = 1, N-1
  XP = I*DHP
  XO = I*DHO
  FXP4 = 1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
  $ (1+RP))*XP+H+BPRESS/1000)
  FXO4 = 1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RO))*XO+H+BOILB/1000)
  FXP5 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
  $ (1+RP))*XP+H+BPRESS/1000))**2
  FXO5 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RO))*XO+H+BOILB/1000))**2
  FXP6 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESS)/
  $ (1+RP))*XP+H+BPRESS/1000))**3
  FXO6 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RO))*XO+H+BOILB/1000))**3
  SUMP4 = SUMP4 + FXP4
  SUMO4 = SUMO4 + FXO4
  SUMP5 = SUMP5 + FXP5
  SUMO5 = SUMO5 + FXO5
  SUMP6 = SUMP6 + FXP6
  SUMO6 = SUMO6 + FXO6
10 CONTINUE
  FXP04 = 1/(H+BPRESS/1000)
  FXO04 = 1/(H+BOILB/1000)
  FXP05 = (1/(H+BPRESS/1000))**2
  FXO05 = (1/(H+BOILB/1000))**2
  FXP06 = (1/(H+BPRESS/1000))**3
  FXO06 = (1/(H+BOILB/1000))**3
  FXPN4 = 1/H
  FXON4 = 1/H
  FXPN5 = (1/H)**2
  FXON5 = (1/H)**2
  FXPN6 = (1/H)**3
  FXON6 = (1/H)**3
  HP4 = (+FXP04+FXPN4+2*SUMP4)*DHP/2
  HO4 = (+FXO04+FXON4+2*SUMO4)*DHO/2
  HP5 = (+FXP05+FXPN5+2*SUMP5)*DHP/2
  HO5 = (+FXO05+FXON5+2*SUMO5)*DHO/2
  HP6 = (+FXP06+FXPN6+2*SUMP6)*DHP/2
  HO6 = (+FXO06+FXON6+2*SUMO6)*DHO/2

```

```

RETURN
END
C*****-----*****C
C                               SUBROUTINE NUM 3                               C
C*****-----*****C
SUBROUTINE NUM3 (BPRESSB, BOIL, RP, RO, H, HP7, HO7, HP8, HO8, HP9, HO9)
N      = 100
A      = 0.
ALP   = 0.0015
ALO   = 0.0025
BP    = RP*(BPRESSB/(1+RP))
BO    = RO*(BOIL/(1+RO))
DHP   = (BP-A)/N
DHO   = (BO-A)/N
SUMP7 = 0.
SUMO7 = 0.
SUMP8 = 0.
SUMO8 = 0.
SUMP9 = 0.
SUMO9 = 0.
DO 10 I = 1, N-1
  XP = I*DHP
  XO = I*DHO
  FXP7 = 1/(ALP*XP**2-((1+RP)/(1000*RP)+(ALP*RP*BPRESSB)/
$      (1+RP))*XP+H+BPRESSB/1000)
  FXO7 = 1/(ALO*XO**2-((1+RO)/(1000*RO)+(ALO*RO*BOIL)/
$      (1+RP))*XO+H+BOIL/1000)
  FXP8 = (1/(ALP*XP**2-((1+RP)/(1000*RP)+(ALP*RP*BPRESSB)/
$      (1+RP))*XP+H+BPRESSB/1000))**2
  FXO8 = (1/(ALO*XO**2-((1+RO)/(1000*RO)+(ALO*RO*BOIL)/
$      (1+RP))*XO+H+BOIL/1000))**2
  FXP9 = (1/(ALP*XP**2-((1+RP)/(1000*RP)+(ALP*RP*BPRESSB)/
$      (1+RP))*XP+H+BPRESSB/1000))**3
  FXO9 = (1/(ALO*XO**2-((1+RO)/(1000*RO)+(ALO*RO*BOIL)/
$      (1+RP))*XO+H+BOIL/1000))**3
  SUMP7 = SUMP7 + FXP7
  SUMO7 = SUMO7 + FXO7
  SUMP8 = SUMP8 + FXP8
  SUMO8 = SUMO8 + FXO8
  SUMP9 = SUMP9 + FXP9
  SUMO9 = SUMO9 + FXO9
10 CONTINUE
  FXP07 = 1/(H+BPRESSB/1000)
  FXO07 = 1/(H+BOIL/1000)
  FXP08 = (1/(H+BPRESSB/1000))**2
  FXO08 = (1/(H+BOIL/1000))**2
  FXP09 = (1/(H+BPRESSB/1000))**3
  FXO09 = (1/(H+BOIL/1000))**3
  FXPN7 = 1/H
  FXON7 = 1/H
  FXPN8 = (1/H)**2
  FXON8 = (1/H)**2
  FXPN9 = (1/H)**3
  FXON9 = (1/H)**3
  HP7  = (+FXP07+FXPN7+2*SUMP7)*DHP/2
  HO7  = (+FXO07+FXON7+2*SUMP7)*DHO/2
  HP8  = (+FXP08+FXPN8+2*SUMP8)*DHP/2
  HO8  = (+FXO08+FXON8+2*SUMP8)*DHO/2
  HP9  = (+FXP09+FXPN9+2*SUMP9)*DHP/2
  HO9  = (+FXO09+FXON9+2*SUMP9)*DHO/2
RETURN
END
C*****-----*****C
C                               SUBROUTINE NUM 4                               C
C*****-----*****C
SUBROUTINE NUM4 (XMIN10, XMIN11, RP, RO, H, HP11, HO11, HP21, HO21, HP31,
$              HO31)
N      = 100
A      = 0.

```

```

A1P = 0.0015
A1O = 0.0025
BPRESSB = XMIN10
BOILB = XMIN11
BP = RP*(BPRESSB/(1+RP))
BO = RO*(BOILB/(1+RO))
DHP = (BP-A)/N
DHO = (BO-A)/N
SUMP1 = 0.
SUMO1 = 0.
SUMP2 = 0.
SUMO2 = 0.
SUMP3 = 0.
SUMO3 = 0.
DO 10 I = 1,N-1
  XP = I*DHP
  XO = I*DHO
  FXP1 = 1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
  $ (1+RP))*XP+H+BPRESSB/1000)
  FXO1 = 1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RP))*XO+H+BOILB/1000)
  FXP2 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
  $ (1+RP))*XP+H+BPRESSB/1000))**2
  FXO2 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RP))*XO+H+BOILB/1000))**2
  FXP3 = (1/(A1P*XP**2-((1+RP)/(1000*RP)+(A1P*RP*BPRESSB)/
  $ (1+RP))*XP+H+BPRESSB/1000))**3
  FXO3 = (1/(A1O*XO**2-((1+RO)/(1000*RO)+(A1O*RO*BOILB)/
  $ (1+RP))*XO+H+BOILB/1000))**3
  SUMP1 = SUMP1 + FXP1
  SUMO1 = SUMO1 + FXO1
  SUMP2 = SUMP2 + FXP2
  SUMO2 = SUMO2 + FXO2
  SUMP3 = SUMP3 + FXP3
  SUMO3 = SUMO3 + FXO3
10 CONTINUE
  FXP01 = 1/(H+BPRESSB/1000)
  FXO01 = 1/(H+BOILB/1000)
  FXP02 = (1/(H+BPRESSB/1000))**2
  FXO02 = (1/(H+BOILB/1000))**2
  FXP03 = (1/(H+BPRESSB/1000))**3
  FXO03 = (1/(H+BOILB/1000))**3
  FXPN1 = 1/H
  FXON1 = 1/H
  FXPN2 = (1/H)**2
  FXON2 = (1/H)**2
  FXPN3 = (1/H)**3
  FXON3 = (1/H)**3
  HP11 = (+FXP01+FXPN1+2*SUMP1)*DHP/2
  HO11 = (+FXO01+FXON1+2*SUMP1)*DHO/2
  HP21 = (+FXP02+FXPN2+2*SUMP2)*DHP/2
  HO21 = (+FXO02+FXON2+2*SUMP2)*DHO/2
  HP31 = (+FXP03+FXPN3+2*SUMP3)*DHP/2
  HO31 = (+FXO03+FXON3+2*SUMP3)*DHO/2
RETURN
END
C*****-----*****C
C                               SUBROUTINE  MEAN  1                               C
C*****-----*****C
SUBROUTINE MEAN1(CONLB,ARMB,VBMEAN1,VSMEAN1)
PI = 2.*ASIN(1.)
R = CONLB/ARMB
N = 360
DEG1 = 0.
DEG2 = 2*PI
DDEG = (DEG2-DEG1)/N
BSUMP = 0.
SSUMP = 0.
DO 11 I = 1,N-1

```



```

X      = I*DDEG
FXB    = ( 1+COS(X)/SQRT(R**2-(SIN(X))**2) )**2
FXS    = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP  = BSUMP + FXB
SSUMP  = SSUMP + FXS
11 CONTINUE
FXB0   = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN   = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0   = ((COS(DEG1)/R)**2)
$      *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN   = ((COS(DEG2)/R)**2)
$      *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG    = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML    = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN1 = BIG/(2*PI)
VSMEAN1 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 10                               C
C*****-----*****C
SUBROUTINE MEAN10(CONL,ARMB,VBMEAN10,VSMEAN10)
PI      = 2.*ASIN(1.)
R       = CONL/ARMB
N       = 360
DEG1   = 0.
DEG2   = 2*PI
DDEG   = (DEG2-DEG1)/N
BSUMP  = 0.
SSUMP  = 0.
DO 11 I = 1,N-1
X      = I*DDEG
FXB    = ( 1+COS(X)/SQRT(R**2-(SIN(X))**2) )**2
FXS    = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP  = BSUMP + FXB
SSUMP  = SSUMP + FXS
11 CONTINUE
FXB0   = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN   = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0   = ((COS(DEG1)/R)**2)
$      *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN   = ((COS(DEG2)/R)**2)
$      *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG    = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML    = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN10 = BIG/(2*PI)
VSMEAN10 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 11                               C
C*****-----*****C
SUBROUTINE MEAN11(CONLB,ARM,VBMEAN11,VSMEAN11)
PI      = 2.*ASIN(1.)
R       = CONLB/ARM
N       = 100
DEG1   = 0.
DEG2   = 2*PI
DDEG   = (DEG2-DEG1)/N
BSUMP  = 0.
SSUMP  = 0.
DO 11 I = 1,N-1
X      = I*DDEG
FXB    = ( 1+COS(X)/SQRT(R**2-(SIN(X))**2) )**2
FXS    = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP  = BSUMP + FXB
SSUMP  = SSUMP + FXS
11 CONTINUE
FXB0   = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2

```

```

FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0 = ((COS(DEG1)/R)**2)
$      * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN = ((COS(DEG2)/R)**2)
$      * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN11 = BIG/(2*PI)
VSMEAN11 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 12                               C
C*****-----*****C
SUBROUTINE MEAN12 (CONLB,XMIN27,VBMEAN12,VSMEAN12)
PI = 2.*ASIN(1.)
R = CONLB/XMIN27
N = 100
DEG1 = 0.
DEG2 = 2*PI
DDEG = (DEG2-DEG1)/N
BSUMP = 0.
SSUMP = 0.
DO 11 I = 1,N-1
X = I*DDEG
FXB = ( 1+COS(X)/SQRT(R**2-(SIN(X))**2) )**2
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP = BSUMP + FXB
SSUMP = SSUMP + FXS
11 CONTINUE
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0 = ((COS(DEG1)/R)**2)
$      * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN = ((COS(DEG2)/R)**2)
$      * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN12 = BIG/(2*PI)
VSMEAN12 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE MEAN 13                               C
C*****-----*****C
SUBROUTINE MEAN13 (XMIN26,ARM,VBMEAN13,VSMEAN13)
PI = 2.*ASIN(1.)
R = XMIN26/ARM
N = 100
DEG1 = 0.
DEG2 = 2*PI
DDEG = (DEG2-DEG1)/N
BSUMP = 0.
SSUMP = 0.
DO 11 I = 1,N-1
X = I*DDEG
FXB = ( 1+COS(X)/SQRT(R**2-(SIN(X))**2) )**2
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP = BSUMP + FXB
SSUMP = SSUMP + FXS
11 CONTINUE
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0 = ((COS(DEG1)/R)**2)
$      * ((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN = ((COS(DEG2)/R)**2)
$      * ((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2

```

```
VBMEAN13 = BIG/(2*PI)
```

```
VSMEAN13 = SML/(2*PI)
```

```
RETURN
```

```
END
```

```
C*****-----*****C
C                               SUBROUTINE MEAN 14                               C
C*****-----*****C
```

```
SUBROUTINE MEAN14 (XMIN18, XMIN27, VBMEAN14, VSMEAN14, PI)
```

```
R = XMIN18/XMIN27
```

```
N = 360
```

```
DEG1 = 0.
```

```
DEG2 = 2*PI
```

```
DDEG = (DEG2-DEG1)/N
```

```
BSUMP = 0.
```

```
SSUMP = 0.
```

```
DO 11 I = 1, N-1
```

```
X = I*DDEG
```

```
FXB = (1+COS(X)/SQRT(R**2-(SIN(X))**2))**2
```

```
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
```

```
BSUMP = BSUMP + FXB
```

```
SSUMP = SSUMP + FXS
```

```
11 CONTINUE
```

```
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
```

```
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
```

```
FXS0 = ((COS(DEG1)/R)**2)
```

```
$ *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
```

```
FXSN = ((COS(DEG2)/R)**2)
```

```
$ *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
```

```
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
```

```
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
```

```
VBMEAN14 = BIG/(2*PI)
```

```
VSMEAN14 = SML/(2*PI)
```

```
RETURN
```

```
END
```

```
C*****-----*****C
C                               SUBROUTINE MEAN 2                               C
C*****-----*****C
```

```
SUBROUTINE MEAN2 (CONLB, ARM, VBMEAN2, VSMEAN2)
```

```
PI = 2.*ASIN(1.)
```

```
R = CONLB/ARM
```

```
N = 360
```

```
DEG1 = 0.
```

```
DEG2 = 2*PI
```

```
DDEG = (DEG2-DEG1)/N
```

```
BSUMP = 0.
```

```
SSUMP = 0.
```

```
DO 12 I = 1, N-1
```

```
X = I*DDEG
```

```
FXB = (1+COS(X)/SQRT(R**2-(SIN(X))**2))**2
```

```
FXS = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
```

```
BSUMP = BSUMP + FXB
```

```
SSUMP = SSUMP + FXS
```

```
12 CONTINUE
```

```
FXB0 = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
```

```
FXBN = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
```

```
FXS0 = ((COS(DEG1)/R)**2)
```

```
$ *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
```

```
FXSN = ((COS(DEG2)/R)**2)
```

```
$ *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
```

```
BIG = (+FXB0+FXBN+2*BSUMP)*DDEG/2
```

```
SML = (+FXS0+FXSN+2*SSUMP)*DDEG/2
```

```
VBMEAN2 = BIG/(2*PI)
```

```
VSMEAN2 = SML/(2*PI)
```

```
RETURN
```

```
END
```

```
C*****-----*****C
C                               SUBROUTINE MEAN 3                               C
C*****-----*****C
```

```
SUBROUTINE MEAN3 (CONL, ARMB, VBMEAN3, VSMEAN3)
```

```

PI      = 2.*ASIN(1.)
R       = CONL/ARMB
N       = 100
DEG1    = 0.
DEG2    = 2*PI
DDEG    = (DEG2-DEG1)/N
BSUMP   = 0.
SSUMP   = 0.
DO 13 I = 1,N-1
X       = I*DDEG
FXB     = (1+COS(X)/SQRT(R**2-(SIN(X))**2))**2
FXS     = ((COS(X)/R)**2)*((1+(SIN(X)**2)/(R**2-SIN(X)**2))**2)
BSUMP   = BSUMP + FXB
SSUMP   = SSUMP + FXS
13 CONTINUE
FXB0    = (1+COS(DEG1)/SQRT(R**2-(SIN(DEG1))**2))**2
FXBN    = (1+COS(DEG2)/SQRT(R**2-(SIN(DEG2))**2))**2
FXS0    = ((COS(DEG1)/R)**2)
$       *((1+(SIN(DEG1)**2)/(R**2-SIN(DEG1)**2))**2)
FXSN    = ((COS(DEG2)/R)**2)
$       *((1+(SIN(DEG2)**2)/(R**2-SIN(DEG2)**2))**2)
BIG     = (+FXB0+FXBN+2*BSUMP)*DDEG/2
SML     = (+FXS0+FXSN+2*SSUMP)*DDEG/2
VBMEAN3 = BIG/(2*PI)
VSMEAN3 = SML/(2*PI)
RETURN
END
C*****-----*****C
C                               SUBROUTINE TOR 1                               C
C*****-----*****C
SUBROUTINE TMEAN1 (FCOE, SDEGB, FB, CDEGB, FM, SCB, PLB, BRB, TRB, VLB, RADC
$                , TOR1, PI)
N = 360
D1 = SDEGB
D2 = CDEGB
D3 = 180-CDEGB
D4 = 180-SDEGB
DEG0 = 0.
DEGN = 360.
DDEG = (DEGN-DEG0)/N
SUMP = 0.
DO 10 I = 0,N,1
X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S = (FB-BRB)*(1-COS((X-D1)*PI/180))/1000
V = (FB-BRB)*RADC*SIN((X-D1)*PI/180)/1000
A = (FB-BRB)*(RADC**2)*COS((X-D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S = ((BRB+VLB-TRB)*SIN(X*PI/180)+TRB-BRB)/1000
V = (BRB+VLB-TRB)*RADC*COS(X*PI/180)/1000
A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN(X*PI/180)/1000
FX = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S = (FB-BRB)*(1+COS((X+D1)*PI/180))/1000
V = -1*(FB-BRB)*RADC*SIN((X+D1)*PI/180)/1000
A = -1*(FB-BRB)*(RADC**2)*COS((X+D1)*PI/180)/1000
FX = -1*(SCB*S+PLB+FM*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR1 = SUMP/N
RETURN

```

```

END
C*****-----*****C
C                               SUBROUTINE TOR 2                               C
C*****-----*****C
SUBROUTINE TMEAN2 (FCOE, SDEGB, FB, CDEGB, FMB, SC, PLB, BRB, TRB, VLB, RADC
$      TOR2, PI)
      N = 360
      D1 = SDEGB
      D2 = CDEGB
      D3 = 180-CDEGB
      D4 = 180-SDEGB
      DEG0 = 0.
      DEGN = 360.
      DDEG = (DEGN-DEG0)/N
      SUMP = 0.
DO 10 I = 0, N, 1
      X = I*DDEG
      IF ((X.GE.D1).AND.(X.LT.D2)) THEN
        S = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
        V = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
        A = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
        FX = -1*(SC*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        IF ((X.GE.D2).AND.(X.LE.D3)) THEN
          S = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
          V = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000
          A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
          FX = -1*(SC*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
        ELSE
          IF ((X.GT.D3).AND.(X.LE.D4)) THEN
            S = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
            V = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
            A = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
            FX = -1*(SC*S+PLB+FMB*A)
              *(FCOE*(BRB/1000+S)+V/RADC)
          ELSE
            FX = 0
          ENDIF
        ENDIF
      ENDIF
      SUMP = SUMP + FX
10 CONTINUE
      TOR2 = SUMP/N
      RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 3                               C
C*****-----*****C
SUBROUTINE TMEAN3 (FCOE, SDEGB, FB, CDEGB, FMB, SCB, PL, BRB, TRB, VLB, RADC
$      TOR3, PI)
      N = 360
      D1 = SDEGB
      D2 = CDEGB
      D3 = 180-CDEGB
      D4 = 180-SDEGB
      DEG0 = 0.
      DEGN = 360.
      DDEG = (DEGN-DEG0)/N
      SUMP = 0.
DO 10 I = 0, N, 1
      X = I*DDEG
      IF ((X.GE.D1).AND.(X.LT.D2)) THEN
        S = (FB-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
        V = (FB-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
        A = (FB-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
        FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        IF ((X.GE.D2).AND.(X.LE.D3)) THEN
          S = ((BRB+VLB-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000

```

```

V = (BRB+VLB-TRB)*RADC*COS( X*PI/180 )/1000
A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S = (FB-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
V = -1*(FB-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
A = -1*(FB-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
FX = -1*(SCB*S+PL+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR3 = SUMP/N
RETURN
END
C*****-----*****C
C                               SUBROUTINE TOR 4                               C
C*****-----*****C
SUBROUTINE TMEAN4 (FCOE, SDEGB, FBR, CDEGBR, FMB, SCB, PLB, BR, TRB, VLB
$           , RADC, TOR4, PI)
N = 360
D1 = SDEGB
D2 = CDEGBR
D3 = 180-CDEGBR
D4 = 180-SDEGB
DEG0 = 0.
DEGN = 360.
DDEG = (DEGN-DEG0)/N
SUMP = 0.
DO 10 I = 0, N, 1
X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
S = (FBR-BR)*(1-COS( (X-D1)*PI/180 ))/1000
V = (FBR-BR)*RADC*SIN( (X-D1)*PI/180 )/1000
A = (FBR-BR)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
S = ((BR+VLB-TRB)*SIN( X*PI/180 )+TRB-BR)/1000
V = (BR+VLB-TRB)*RADC*COS( X*PI/180 )/1000
A = -1*(BR+VLB-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
S = (FBR-BR)*(1+COS( (X+D1)*PI/180 ))/1000
V = -1*(FBR-BR)*RADC*SIN( (X+D1)*PI/180 )/1000
A = -1*(FBR-BR)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR4 = SUMP/N
RETURN
END
C*****-----*****C
C                               SUBROUTINE TOR 5                               C
C*****-----*****C
SUBROUTINE TMEAN5 (FCOE, SDEGB, FTR, CDEGTR, FMB, SCB, PLB, BRB, TR, VLB
$           , RADC, TOR5, PI)
N = 360
D1 = SDEGB

```

```

      D2 = CDEGTR
      D3 = 180-CDEGTR
      D4 = 180-SDEGB
      DEGO = 0.
      DEGN = 360.
      DDEG = (DEGN-DEGO)/N
      SUMP = 0.
DO 10 I = 0,N,1
      X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FTR-BRB)*(1-COS((X-D1)*PI/180))/1000
      V = (FTR-BRB)*RADC*SIN((X-D1)*PI/180)/1000
      A = (FTR-BRB)*(RADC**2)*COS((X-D1)*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
      S = ((BRB+VLB-TR)*SIN(X*PI/180)+TR-BRB)/1000
      V = (BRB+VLB-TR)*RADC*COS(X*PI/180)/1000
      A = -1*(BRB+VLB-TR)*(RADC**2)*SIN(X*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
      S = (FTR-BRB)*(1+COS((X+D1)*PI/180))/1000
      V = -1*(FTR-BRB)*RADC*SIN((X+D1)*PI/180)/1000
      A = -1*(FTR-BRB)*(RADC**2)*COS((X+D1)*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
      FX = 0
ENDIF
ENDIF
ENDIF
      SUMP = SUMP + FX
10 CONTINUE
      TOR5 = SUMP/N
      RETURN
      END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 51                               C
C*****-----*****C

```

```

SUBROUTINE TMEAN51(FCOE, SDEGB, FBTR, CDEGBTR, FMB, SCB, PLB, BR, TR, VLB,
$                 RADC, TOR51, PI)

```

```

      N = 360
      D1 = SDEGB
      D2 = CDEGBTR
      D3 = 180-CDEGBTR
      D4 = 180-SDEGB
      DEGO = 0.
      DEGN = 360.
      DDEG = (DEGN-DEGO)/N
      SUMP = 0.
DO 10 I = 0,N,1
      X = I*DDEG
IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FBTR-BR)*(1-COS((X-D1)*PI/180))/1000
      V = (FBTR-BR)*RADC*SIN((X-D1)*PI/180)/1000
      A = (FBTR-BR)*(RADC**2)*COS((X-D1)*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GE.D2).AND.(X.LE.D3)) THEN
      S = ((BR+VLB-TR)*SIN(X*PI/180)+TR-BR)/1000
      V = (BR+VLB-TR)*RADC*COS(X*PI/180)/1000
      A = -1*(BR+VLB-TR)*(RADC**2)*SIN(X*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)
ELSE
IF ((X.GT.D3).AND.(X.LE.D4)) THEN
      S = (FBTR-BR)*(1+COS((X+D1)*PI/180))/1000
      V = -1*(FBTR-BR)*RADC*SIN((X+D1)*PI/180)/1000
      A = -1*(FBTR-BR)*(RADC**2)*COS((X+D1)*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BR/1000+S)+V/RADC)

```

```

ELSE
  FX = 0
ENDIF
ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR51 = SUMP/N
RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 6                               C
C*****-----*****C

```

```

SUBROUTINE TMEAN6 (FCOE, SDEGB, FVL, CDEGVL, FMB, SCB, PLB, BRB, TRB, VL
$, RADC, TOR6, PI)

```

```

  N = 360
  D1 = SDEGB
  D2 = CDEGVL
  D3 = 180-CDEGVL
  D4 = 180-SDEGB
  DEGO = 0.
  DEGN = 360.
  DDEG = (DEGN-DEGO)/N
  SUMP = 0.
  DO 10 I = 0, N, 1
    X = I*DDEG
    IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FVL-BRB)*(1-COS( (X-D1)*PI/180 ))/1000
      V = (FVL-BRB)*RADC*SIN( (X-D1)*PI/180 )/1000
      A = (FVL-BRB)*(RADC**2)*COS( (X-D1)*PI/180 )/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      IF ((X.GE.D2).AND.(X.LE.D3)) THEN
        S = ((BRB+VL-TRB)*SIN( X*PI/180 )+TRB-BRB)/1000
        V = (BRB+VL-TRB)*RADC*COS( X*PI/180 )/1000
        A = -1*(BRB+VL-TRB)*(RADC**2)*SIN( X*PI/180 )/1000
        FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
      ELSE
        IF ((X.GT.D3).AND.(X.LE.D4)) THEN
          S = (FVL-BRB)*(1+COS( (X+D1)*PI/180 ))/1000
          V = -1*(FVL-BRB)*RADC*SIN( (X+D1)*PI/180 )/1000
          A = -1*(FVL-BRB)*(RADC**2)*COS( (X+D1)*PI/180 )/1000
          FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
        ELSE
          FX = 0
        ENDIF
      ENDIF
    ENDIF
    SUMP = SUMP + FX
  10 CONTINUE
  TOR6 = SUMP/N
  RETURN
END

```

```

C*****-----*****C
C                               SUBROUTINE TOR 7                               C
C*****-----*****C

```

```

SUBROUTINE TMEAN7 (FCOE, SDEGB, FB, CDEGB, FMB, SCB, PLB, BRB, TRB, VLB, RADC
$, TOR7, PI)

```

```

  N = 360
  D1 = SDEGB
  D2 = CDEGB
  D3 = 180-CDEGB
  D4 = 180-SDEGB
  DEGO = 0.
  DEGN = 360.
  DDEG = (DEGN-DEGO)/N
  SUMP = 0.
  DO 10 I = 0, N, 1
    X = I*DDEG

```



```

IF ((X.GE.D1).AND.(X.LT.D2)) THEN
  S = (FB-BRB)*(1-COS((X-D1)*PI/180))/1000
  V = (FB-BRB)*RADC*SIN((X-D1)*PI/180)/1000
  A = (FB-BRB)*(RADC**2)*COS((X-D1)*PI/180)/1000
  FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
ELSE
  IF ((X.GE.D2).AND.(X.LE.D3)) THEN
    S = ((BRB+VLB-TRB)*SIN(X*PI/180)+TRB-BRB)/1000
    V = (BRB+VLB-TRB)*RADC*COS(X*PI/180)/1000
    A = -1*(BRB+VLB-TRB)*(RADC**2)*SIN(X*PI/180)/1000
    FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
  ELSE
    IF ((X.GT.D3).AND.(X.LE.D4)) THEN
      S = (FB-BRB)*(1+COS((X+D1)*PI/180))/1000
      V = -1*(FB-BRB)*RADC*SIN((X+D1)*PI/180)/1000
      A = -1*(FB-BRB)*(RADC**2)*COS((X+D1)*PI/180)/1000
      FX = -1*(SCB*S+PLB+FMB*A)*(FCOE*(BRB/1000+S)+V/RADC)
    ELSE
      FX = 0
    ENDIF
  ENDIF
ENDIF
SUMP = SUMP + FX
10 CONTINUE
TOR7 = SUMP/N
RETURN
END
C*****-----*****C
C                               SUBROUTINE TOR 71                               C
C*****-----*****C
SUBROUTINE TMEAN71(FCOE,SDEGB,FBM,CDEGM,XMIN19,XMIN20,XMIN21,
$                XMIN22,XMIN23,XMIN24,RADC,TOR71,PI)
  FB = FBM
  FM = XMIN19
  SC = XMIN20
  PL = XMIN21
  BR = XMIN22
  TR = XMIN23
  VL = XMIN24
  N = 360
  D1 = SDEGB
  D2 = CDEGM
  D3 = 180-CDEGM
  D4 = 180-SDEGB
  DEGO = 0.
  DEGN = 360.
  DDEG = (DEGN-DEGO)/N
  SUMP = 0.
  DO 10 I = 0,N,1
    X = I*DDEG
    IF ((X.GE.D1).AND.(X.LT.D2)) THEN
      S = (FB-BR)*(1-COS((X-D1)*PI/180))/1000
      V = (FB-BR)*RADC*SIN((X-D1)*PI/180)/1000
      A = (FB-BR)*(RADC**2)*COS((X-D1)*PI/180)/1000
      FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
    ELSE
      IF ((X.GE.D2).AND.(X.LE.D3)) THEN
        S = ((BR+VL-TR)*SIN(X*PI/180)+TR-BR)/1000
        V = (BR+VL-TR)*RADC*COS(X*PI/180)/1000
        A = -1*(BR+VL-TR)*(RADC**2)*SIN(X*PI/180)/1000
        FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
      ELSE
        IF ((X.GT.D3).AND.(X.LE.D4)) THEN
          S = (FB-BR)*(1+COS((X+D1)*PI/180))/1000
          V = -1*(FB-BR)*RADC*SIN((X+D1)*PI/180)/1000
          A = -1*(FB-BR)*(RADC**2)*COS((X+D1)*PI/180)/1000
          FX = -1*(SC*S+PL+FM*A)*(FCOE*(BR/1000+S)+V/RADC)
        ELSE
          FX = 0
        ENDIF
      ENDIF
    ENDIF
  END DO

```

```

    ENDIF
  .ENDIF
  .ENDIF
  SUMP = SUMP + FX
10 CONTINUE
  TOR71 = SUMP/N
  RETURN
  END

```

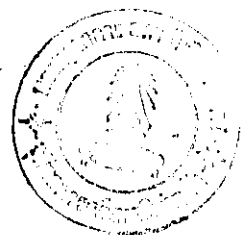
```

C*****-----*****C
C                               (SEL1) SUBROUTINE FOR CALCULATION                               C
C*****-----*****C
SUBROUTINE SEL1(RPM,GN,G1,G2,G3,G4,G5,GD,TEFF,GT)
IF (RPM.LE.1200.) THEN
  GN = 1.
ELSE
  IF (RPM.LE.1800.) THEN
    GN = 2.
  ELSE
    IF (RPM.LE.2000.) THEN
      GN = 3.
    ELSE
      IF (RPM.LE.2200.) THEN
        GN = 4.
      ELSE
        GN = 5.
      ENDIF
    ENDIF
  ENDIF
ENDIF
ENDIF
ENDIF

IF ( GN.EQ.1 ) THEN
  GT = G1*GD
  TEFF = 0.8
ELSE
  IF ( GN.EQ.2 ) THEN
    GT = G2*GD
    TEFF = 0.8
  ELSE
    IF ( GN.EQ.3 ) THEN
      GT = G3*GD
      TEFF = 0.85
    ELSE
      IF ( GN.EQ.4 ) THEN
        GT = G4*GD
        TEFF = 0.9
      ELSE
        IF ( GN.EQ.5 ) THEN
          GT = G5*GD
          TEFF = 0.9
        ELSE
          WRITE(6,*) ' ENTER NEW GEAR NUMBER '
        ENDIF
      ENDIF
    ENDIF
  ENDIF
  RETURN
END

```

ประวัติผู้วิจัย



นาย ไทรัช เลิศอารยะพงษ์ เกิดเมื่อวันที่ 13 เดือน กันยายน พุทธศักราช 2514 ที่ เขต
ชานนาва จังหวัดกรุงเทพมหานคร สำเร็จการศึกษาปริญญาวิศวกรรมศาสตรบัณฑิต ภาควิชา
วิศวกรรมเครื่องกล คณะวิศวกรรมศาสตร์ จากสถาบันเทคโนโลยีพระจอมเกล้าธนบุรี เมื่อปี
การศึกษา 2536 เข้าศึกษาต่อในหลักสูตรวิศวกรรมมหาบัณฑิต ภาควิชาวิศวกรรมเครื่องกล
คณะวิศวกรรมศาสตร์ จุฬาลงกรณ์มหาวิทยาลัยเมื่อปีการศึกษา 2539



สถาบันวิทยบริการ
จุฬาลงกรณ์มหาวิทยาลัย