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**APPENDICES**

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## APPENDIX A

### Experimental designs

Effect on tensile modulus

$$\begin{aligned}
 T \text{ Effect} &= \frac{-y_1 + y_2 - y_3 + y_4 - y_5 + y_6 - y_7 + y_8}{4} \\
 &= \frac{-2.47 + 3.46 - 2.93 + 4.17 - 2.38 + 3.78 - 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 C \text{ Effect} &= \frac{-y_1 - y_2 + y_3 + y_4 - y_5 - y_6 + y_7 + y_8}{4} \\
 &= \frac{-2.47 - 3.46 + 2.93 + 4.17 - 2.38 - 3.78 + 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 N \text{ Effect} &= \frac{-y_1 - y_2 - y_3 - y_4 + y_5 + y_6 + y_7 + y_8}{4} \\
 &= \frac{-2.47 - 3.46 - 2.93 - 4.17 + 2.38 + 3.78 + 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 TC \text{ Effect} &= \frac{+y_1 - y_2 - y_3 + y_4 + y_5 - y_6 - y_7 + y_8}{4} \\
 &= \frac{+2.47 - 3.46 - 2.93 + 4.17 + 2.38 - 3.78 - 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 TN \text{ Effect} &= \frac{+y_1 - y_2 + y_3 - y_4 - y_5 + y_6 - y_7 + y_8}{4} \\
 &= \frac{+2.47 - 3.46 + 2.93 - 4.17 - 2.38 + 3.78 - 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 CN \text{ Effect} &= \frac{+y_1 + y_2 - y_3 - y_4 - y_5 - y_6 + y_7 + y_8}{4} \\
 &= \frac{+2.47 + 3.46 - 2.93 - 4.17 - 2.38 - 3.78 + 2.78 + 4.43}{4}
 \end{aligned}$$

$$\begin{aligned}
 \text{TCN Effect} &= \frac{-y_1 + y_2 + y_3 - y_4 + y_5 - y_6 - y_7 + y_8}{4} \\
 &= \frac{-2.47 + 3.46 + 2.93 - 4.17 + 2.38 - 3.78 - 2.78 + 4.43}{4}
 \end{aligned}$$

All main and interaction effects are listed in Table A-1.

**Table A-1** Estimated effect for  $2^3$  factorial design on tensile modulus at 300 %elongation

Entry.	T	C	N	TC	TN	CN	TCN	Tensile modulus 300 %elongation (MPa)
1	-	-	-	+	+	+	-	2.47
2	+	-	-	-	-	+	+	3.46
3	-	+	-	-	+	-	+	2.93
4	+	+	-	+	-	-	-	4.17
5	-	-	+	+	-	-	+	2.38
6	+	-	+	-	+	-	-	3.78
7	-	+	+	-	-	+	-	2.77
8	+	+	+	+	+	+	+	4.43
Estimated effect	1.322	0.553	0.083	0.125	0.208	-0.030	-0.002	

**Table A-2** Calculation of standard error of estimated effect

Entry.	Result from individual runs			Average response value	Estimated variance at each set of conditions
	1	2	3		
1	2.52	2.24	2.66	2.47	0.05
2	3.51	2.82	4.04	3.46	0.37
3	3.27	2.73	2.79	2.93	0.09
4	4.02	4.40	4.09	4.17	0.04
5	2.35	2.14	2.64	2.38	0.06
6	4.18	3.79	3.37	3.78	0.16
7	2.81	2.62	2.90	2.77	0.02
8	5.01	4.28	3.99	4.43	0.28
$\Sigma$ (variance) =					1.07

$$\text{Standard error of estimated effect } (E) = \left( \frac{\sum V}{2N} \right)^{1/2} = \left( \frac{1.07}{2 * 24} \right)^{1/2} = 0.149$$

**Table A-3** Estimated effect for  $2^3$  factorial design on tear strength

Entry.	T	C	N	TC	TN	CN	TCN	Tear strength (N/mm)
1	-	-	-	+	+	+	-	34.04
2	+	-	-	-	-	+	+	44.80
3	-	+	-	-	+	-	+	33.67
4	+	+	-	+	-	-	-	47.22
5	-	-	+	+	-	-	+	35.50
6	+	-	+	-	+	-	-	42.23
7	-	+	+	-	-	+	-	35.89
8	+	+	+	+	+	+	+	38.66
Estimated effect	8.453	-0.283	-1.858	-0.295	-3.705	-1.305	-1.686	



**Table A-4** Calculation of standard error of estimated effect

Entry.	Result from individual runs			Average response value	Estimated variance at each set of conditions
	1	2	3		
1	36.50	35.01	30.60	34.04	9.41
2	45.31	43.16	45.93	44.80	2.12
3	40.11	25.43	35.46	33.67	56.26
4	48.79	44.31	48.55	47.22	6.35
5	38.60	35.17	32.73	35.50	8.68
6	43.33	43.00	40.36	42.23	2.65
7	39.35	37.38	30.96	35.89	19.23
8	40.53	39.63	35.83	38.66	6.20
$\Sigma$ (variance) =					110.89

$$\text{Standard error of estimated effect } (E) = \left( \frac{\sum V}{2N} \right)^{1/2} = \left( \frac{110.89}{2 * 24} \right)^{1/2} = 1.520$$

**Table A-5** Estimated effect for  $2^3$  factorial design on hardness

Entry.	T	C	N	TC	TN	CN	TCN	Hardness
1	-	-	-	+	+	+	-	40.6
2	+	-	-	-	-	+	+	43.8
3	-	+	-	-	+	-	+	41.5
4	+	+	-	+	-	-	-	46.2
5	-	-	+	+	-	-	+	41.2
6	+	-	+	-	+	-	-	44.1
7	-	+	+	-	-	+	-	43.0
8	+	+	+	+	+	+	+	44.4
Estimated effect	3.083	1.333	0.117	0.000	-0.917	-0.300	-0.767	

**Table A-6** Calculation of standard error of estimated effect

Entry.	Result from individual runs			Average response value	Estimated variance at each set of conditions
	1	2	3		
1	41.6	38.3	41.9	40.6	3.99
2	43.7	42.4	45.4	43.8	2.26
3	42.3	41.0	41.1	41.5	0.52
4	46.9	46.7	45.1	46.2	0.97
5	41.9	39.4	42.2	41.2	2.36
6	46.0	42.9	43.4	44.1	2.77
7	44.6	41.3	43.0	43.0	2.72
8	46.5	44.0	42.6	44.4	3.90
$\Sigma$ (variance) =					19.51

$$\text{Standard error of estimated effect } (E) = \left( \frac{\sum V}{2N} \right)^{1/2} = \left( \frac{19.51}{2 * 24} \right)^{1/2} = 0.638$$

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## APPENDIX B

**Table B-1** The tensile modulus at 300 %elongation of NR-silica vulcanizates

Sample	1	2	3	Average
NR/10 phr TEOS	2.29 ± 0.24	2.59 ± 0.19	-	2.44 ± 0.21
NR/10 phr TEOS/ 1 phr TESPT	2.52 ± 0.47	2.24 ± 0.04	2.66 ± 0.24	2.47 ± 0.22
NR/10 phr TEOS/ 5 phr TESPT	3.26 ± 0.52	2.73 ± 0.30	2.79 ± 0.22	2.93 ± 0.29
NR/10 phr TEOS/ 10 phr TESPT	4.02 ± 0.88	3.11 ± 0.37	-	3.57 ± 0.65
NR/50 phr TEOS	2.70 ± 0.34	3.97 ± 0.85	-	3.33 ± 0.90
NR/50 phr TEOS/ 1 phr TESPT	3.51 ± 0.81	2.82 ± 0.31	4.04 ± 0.18	3.46 ± 0.61
NR/50 phr TEOS/ 5 phr TESPT	4.02 ± 0.56	4.40 ± 0.10	4.09 ± 0.22	4.17 ± 0.20
NR/50 phr TEOS/ 10 phr TESPT	5.60 ± 0.31	5.06 ± 0.87	-	5.33 ± 0.38

**Table B-2** The tear strength of NR-silica vulcanizates

Sample	1	2	3	Average
NR/10 phr TEOS	32.77 ± 1.45	36.34 ± 1.21	-	34.56 ± 2.53
NR/10 phr TEOS/ 1 phr TESPT	36.50 ± 2.36	35.01 ± 1.42	30.60 ± 9.51	34.04 ± 3.07
NR/10 phr TEOS/ 5 phr TESPT	40.11 ± 6.71	25.43 ± 6.39	35.46 ± 5.97	33.67 ± 7.50
NR/10 phr TEOS/ 10 phr TESPT	42.98 ± 1.59	43.08 ± 11.65	-	43.03 ± 0.07
NR/50 phr TEOS	35.88 ± 1.31	41.22 ± 1.95	-	38.55 ± 3.78
NR/50 phr TEOS/ 1 phr TESPT	45.31 ± 2.12	43.16 ± 4.13	45.93 ± 1.85	44.80 ± 1.45
NR/50 phr TEOS/ 5 phr TESPT	48.79 ± 7.63	44.31 ± 4.83	48.55 ± 6.11	47.22 ± 2.52
NR/50 phr TEOS/ 10 phr TESPT	40.96 ± 3.92	45.78 ± 3.94	-	43.37 ± 3.40

**Table B-3** The hardness of NR-silica vulcanizates

Sample	1	2	3	Average
NR/10 phr TEOS	40.9 ± 0.59	42.5 ± 0.53	-	41.7 ± 1.13
NR/10 phr TEOS/ 1 phr TESPT	41.6 ± 0.64	38.3 ± 0.70	41.9 ± 0.76	40.6 ± 2.00
NR/10 phr TEOS/ 5 phr TESPT	42.3 ± 0.23	41.0 ± 0.67	41.1 ± 0.69	41.5 ± 0.72
NR/10 phr TEOS/ 10 phr TESPT	43.2 ± 0.44	45.1 ± 0.19	-	44.2 ± 1.34
NR/50 phr TEOS	42.0 ± 0.62	43.3 ± 0.99	-	42.7 ± 0.92
NR/50 phr TEOS/ 1 phr TESPT	43.7 ± 0.46	42.4 ± 0.58	45.4 ± 1.20	43.8 ± 1.50
NR/50 phr TEOS/ 5 phr TESPT	46.9 ± 0.99	46.7 ± 0.36	45.1 ± 0.87	46.2 ± 0.99
NR/50 phr TEOS/ 10 phr TESPT	46.6 ± 0.85	48.4 ± 0.41	-	47.5 ± 1.27

**Table B-4** The swelling ratio of NR-silica vulcanizates

Sample	1	2	3	Average
NR/10 phr TEOS	317.93	320.82	319.04	319.26 ± 1.46
NR/10 phr TEOS/ 1 phr TESPT	282.62	278.54	276.12	279.09 ± 3.29
NR/10 phr TEOS/ 5 phr TESPT	257.71	253.84	255.93	255.83 ± 1.94
NR/10 phr TEOS/ 10 phr TESPT	246.37	245.69	245.57	245.88 ± 0.43
NR/50 phr TEOS	272.69	274.07	273.96	273.57 ± 0.77
NR/50 phr TEOS/ 1 phr TESPT	268.14	260.48	269.72	266.11 ± 4.94
NR/50 phr TEOS/ 5 phr TESPT	228.30	232.15	235.77	232.07 ± 3.73
NR/50 phr TEOS/ 10 phr TESPT	214.94	218.22	204.14	212.43 ± 7.37

## VITAE

Miss Nantida Niyompanich was born in Chachoengsao, Thailand, on November 3<sup>rd</sup>, 1980. She received Bachelor Degree of Science in 2002 from Department of Chemistry, Faculty of Science, Burapha University. In the same year she was admitted as a Master Degree student in Petrochemistry and Polymer Science Program, Faculty of Science, Chulalongkorn University, and completed the program in 2005.



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