

## Chapter 6

### Experimental Results and System Model Validification

#### 6.1 Experimental Results

The experiments are set in Table 5.4. The results are shown in Tables 6.1, 6.2 and 6.3 and are plotted in Fig. 6.1

The bed temperature  $T_B$  is the average temperature calculated from the temperatures measured by thermocouple TC1 and TC2 at a certain time. The gas temperature  $T_G$  is measured by thermocouple TC3 which is above the bed. When the bed is in steady state, the bed temperature and the gas temperature at this steady state are  $\bar{T}_B$  and  $\bar{T}_G$ .

The superficial velocity at room temperature  $U_{orm}$  is transformed into the superficial velocity at steady state bed temperature  $U_o$  by calculation using the perfect gas law.

Concentration of oxygen in the freeboard is measured by orsat and assumed to be the concentration in the bubble at the bed height,  $C_{Ab}$

The carbon overflow rate  $F_{1c}$  and the carbon elutriation rate  $F_{2c}$  are calculated from the coal ash flow rates in overflow and elutriation respectively and the ultimate analysis of carbon content left in the coal ash collected from the experiments.

Calculations of air-to-fuel ratios and excess air are shown in Appendix E and Appendix F respectively.

Fig. 6.1 Combustion Efficiency and Operating Variable

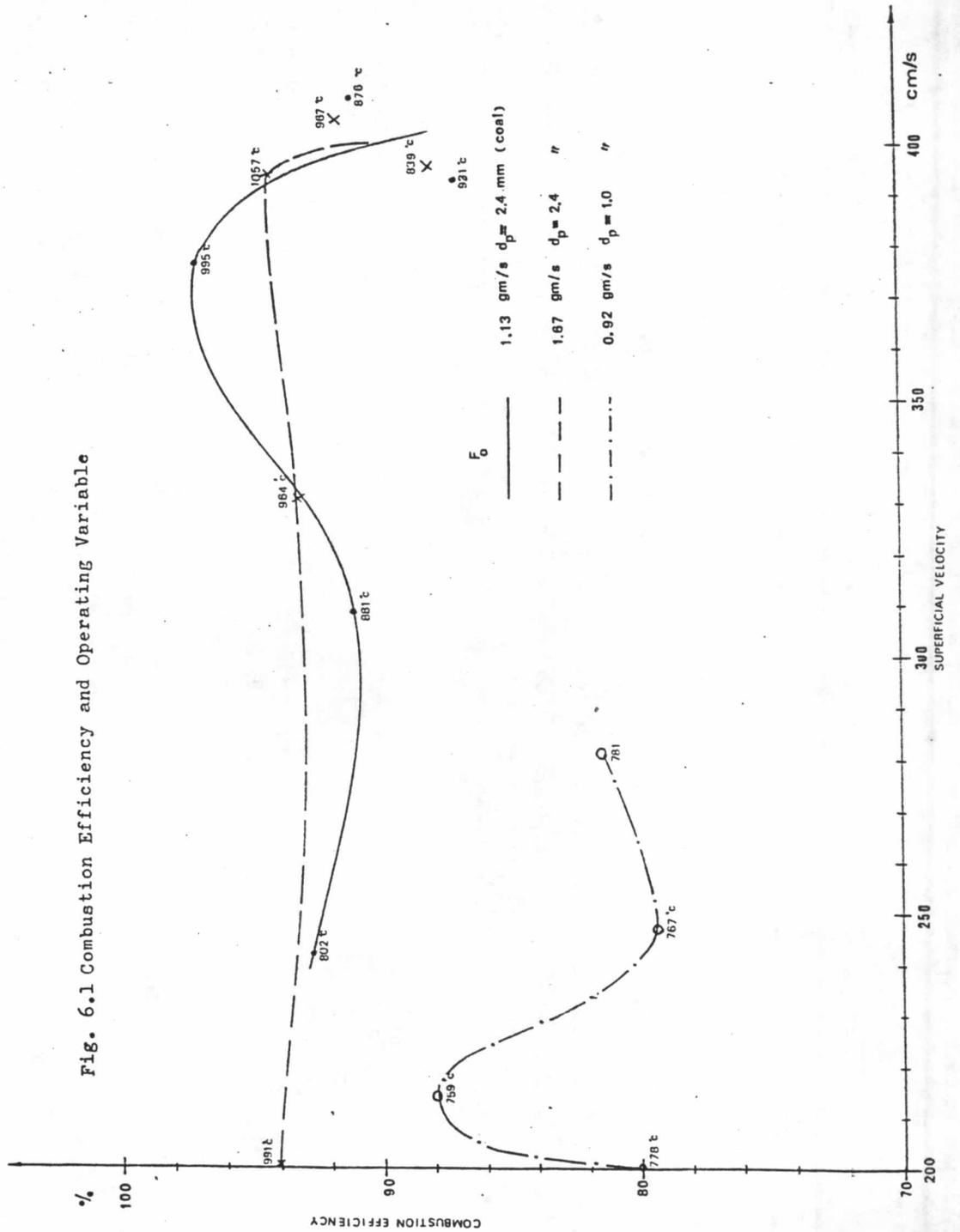


Table 6.1 Results of Series 1 Experiments

run Series 1 average lignite particle diameter = 0.24 cm, coal feed rate = 1.1314 gm/s  $L_f = 30$  cm  
 percent of carbon in coal = 41.48 % carbon feed rate = 0.4693 gm/s  $d_t = 15$  cm

Data No	$U_{orm}$ cm/s	Time hr:mn:s	$T_B$ °C	$T_G$ °C	$\bar{T}_B$ °C	$\bar{T}_G$ °C	$U_o$ cm/s	$F_{1c}$ gm/s	$F_{2c}$ gm/s	$\eta_c$ %	air/fuel ratio	excess air %	$SO_2$ PPM	$O_2$ %	CO PPM	$Re_c$
1	64.732	0:0:0	748	385												
		0:31:0	802	389	802	389	242.09	0.0228	0.0113	92.73	13.08	160.41	20	21	6026	12,589
2	72.823	0:20:0	848	424												
		0:37:0	915	421	881	422	307.83	0.0390	0.0039	90.85	14.70	208.45	65	20.5	3514	14,784
3	80.920	0:0:0	976	408												
		0:34:0	983	419												
		0:36:0	992	416												
		0:37:0	1005	418	995	418	375.85	0.0028	0.0120	96.85	16.34	242.75	78	19	1561	18,236
4	89.00	0:0:0	864	425												
		0:75:0	821	410												
		0:31:0	909	412												
		0:33:0	931	409	931	409	392.51	0.0391	0.0250	86.35	17.96	276.97	68	18	1186	19,311
5	97.10	0:0:0	834	419												
		0:28:0	867	408												
		0:30:0	885	417	876	412	408.67	0.0074	0.0349	91.00	19.60	311.28	64	19	1307	20,026

- $U_{orm}$  = superficial velocity of air at room temperature,  $F_{oc}$  = carbon feed rate of coal
- $U_o$  = superficial velocity of air at bed temperature  $T_B$ ,  $F_{1c}$  = carbon overflow rate of coal
- $T_B$  = bed temperature,  $F_{2c}$  = carbon elutriation rate of coal
- $\bar{T}_B$  = average steady state bed temperature,  $\eta_c$  = carbon combustion efficiency
- $T_G$  = flue gas temperature,  $C_{O_2}$  = oxygen concentration of flue gas in free-board
- $\bar{T}_G$  = average steady state gas temperature,  $L_f$  = expanded bed height
- $d_t$  = bed diameter,  $Re_c$  = Reynolds number of combustor column

Table 6.2 Results of : Series 2 Experiments

Run Series 2, average lignit particle diameter = 0.24 cm, coal feed rate = 1.6717 gm/s  $L_f = 30$  cm

Percent of carbon in coal = 41.48% , carbon feed rate=0.6934 "  $d_c = 15$  cm

Data No.	$U_{orm}$ cm/s	Time hr:min:s	$T_B$	$T_G$	$T_B$	$T_G$	$\bar{U}_O$ cm/s	$F_{1C}$ gm/s	$F_{2C}$ gm/s	$\eta_c$ %	air/fuel ratio	exass air, %	SO <sub>2</sub> PPM	O <sub>2</sub> %	NO PPM	CO PPM	Re <sub>c</sub>	
1	64.73	0:36:0	995	423														
		0:37:0	990	421														
		0:43:40	988	421	991	420	200.70	0.0164	0.0237	94.22	8.86	85.56	70	21	56	4183	9,694	
2	78.82	0:32:0	1064	421														
		0:35:0	1057	423														
		0:39:0	975	430														
		0:41:0	987	432	964	430	329.96	0.0217	0.0256	93.17	9.94	108.75	68	21	25	6366	15,541	
		0:54:0	930	430														
3	80.92	0:30:0	1025	449														
		0:48:0	1057	454	1057	454	394.23	0.0107	0.0292	94.25	11.06	131.98	52	20.5	14	7638	17,543	
4	89.01	0:25:0	950	437														
		0:29:0	940	446														
		0:37:0	967	445	967	445	404.29	0.0190	0.0388	91.67	12.16	155.16	55	21	22	4183	18,355	
5	97.10	0:15:0	951	430														
		0:18:0	958	428														
		0:21:0	914	420														
		0:33:0	839	404	839	404	395.51	0.0186	0.0651	87.94	13.62	178.35	52	20.5	-	2246	19,814	

Table 6.3 Results of Series 3 Experiments

Run Series 3, average lignite particle diameter = 0.095 cm<sup>3</sup> coal feed rate = 0.9232 gm/s  $L_F = 30$  cm  
 Percent of carbon in coal = 41.46% carbon feed rate = 0.3832 gm/s  $d_c = 15$  cm

Data No.	$U_{orm}$ cm/s	Time hr:min:s	$T_D$ °C	$T_G$ °C	$\bar{T}_B$ °C	$\bar{T}_G$ °C	$\bar{U}_o$ cm/s	$F_{1c}$ gm/s	$F_{2c}$ gm/s	$\eta_c$ %	air/fuel ratio	excrs air, %	SO <sub>2</sub> PPM	O <sub>2</sub> %	CO PPM	Re <sub>c</sub>
1	51.79	0:40:0	772	290												
		0:47:0	782	294												
		0:52:0	778	295												
		0:59:0	777	299	778	295	199.38	0.0665	0.0116	79.64	12.80	168.66	26	21	7818	13,259
2	56.64	0:30:0	762	295												
		0:34:0	759	294												
		0:36:0	757	293	759	294	214.11	0.0443	0.0189	88.21	14.02	193.82	23	18.5	5623	14,260
3	64.73	0:30:0	770	306												
		0:36:0	772	312												
		0:42:0	760	315												
		0:47:0	765	314	767	312	246.59	0.0625	0.0269	79.48	16.02	235.79	24	19	5534	15,659
4	72.82	0:30:0	780	323												
		0:39:0	781	319												
		0:41:0	782	317	781	319	281.14	0.0352	0.0352	81.64	18.02	277.75	24	19	3935	17,515

## 6.2 System Model Validification

The carbon combustion efficiencies calculated from the proposed system model are compared with experimental results and presented in Table 6.4

The average absolute relative deviation of computed carbon combustion efficiencies from the experimental values  $|\Delta\eta|$  are 1.7 %, 1.5 % and 3 % for run series 1,2, and 3 respectively. These small relative deviations show that the system model developed is in good agreement with the experimental results.

## 6.3 SO<sub>2</sub> and NO emission

In the experiments, the molar ratio of Ca: S in the fuel mixture is 12 : 1. And the SO<sub>2</sub> emissions from the experiments are shown in Table 6.1, 6.2 and 6.3. The average SO<sub>2</sub> emission is 50 PPM which is much lower than 500 PPM, the acceptable emission standard.

From Table 6.2 the average NO emission from the experiment is about 30 PPM under the bed temperature between 950-1050°C, which is very low when compared with the acceptable emission standard of 500 PPM.

## 6.4 Change of Bed Temperature with Air-to-fuel Ratio

Fig. 6.2 shows the bed temperature as a function of air-to-fuel ratio for several feed rates and average lignite particles diameter. The bed temperatures are between 750-1050°C. The bed temperature

TABLE 6.4

Comparison of Experimental and  
Predicted Combustion Efficiencies of Lignite for  
Atmospheric Pressure Fluidized Bed Combustion

Run No.	Data No.	$\bar{d}_p$ lignite (cm)	$\bar{d}_p$ limestone (cm)	$F_{ocl}$ gm/s	$U$ (cm/s)	XS AIR(%)	$\frac{\text{air}}{\text{fuel}}$ (by wt.)	$T_B$ °K	$\eta$ (%) exp.	$\eta$ (%) calc.	$\Delta\eta$	$ \overline{\Delta\eta} $
1	1	0.2401	0.0927	1.1314	242.09	160.41	13.08	1075	92.73	92.04	-0.69	1.746
	2	"	"	"	307.83	208.45	14.70	1154	90.85	88.77	-2.08	
	3	"	"	"	375.85	242.75	16.34	1268	96.85	95.14	-1.71	
	4	"	"	"	392.51	276.97	17.98	1204	86.35	87.77	+1.42	
	5	"	"	"	408.07	311.28	19.60	1149	91.00	93.83	+2.83	
3	1	"	"	1.6717	299.70	85.56	8.86	1264	94.22	94.39	+0.17	1.468
	2	"	"	"	329.96	108.75	9.94	1237	93.17	93.49	+0.32	
	3	"	"	"	394.23	131.98	11.06	1330	94.25	94.32	+0.07	
	4	"	"	"	404.29	155.16	12.16	1240	91.67	93.12	+1.45	
	5	"	"	"	395.51	178.35	13.62	1112	87.94	93.27	+5.33	
5	1	0.0954	0.0600	0.9236	199.38	168.66	12.80	1051	79.64	82.66	+3.02	3.005
	2	"	"	"	214.11	193.82	14.02	1032	83.50	88.21	+4.71	
	3	"	"	"	246.59	235.79	16.02	1040	76.69	79.48	+2.79	
	4	"	"	"	281.14	277.75	18.02	1054	81.64	80.14	-1.50	

Stoichiometric of air fuel ratio of lignite = 4.78

$\bar{d}_p$  = average particle diameter

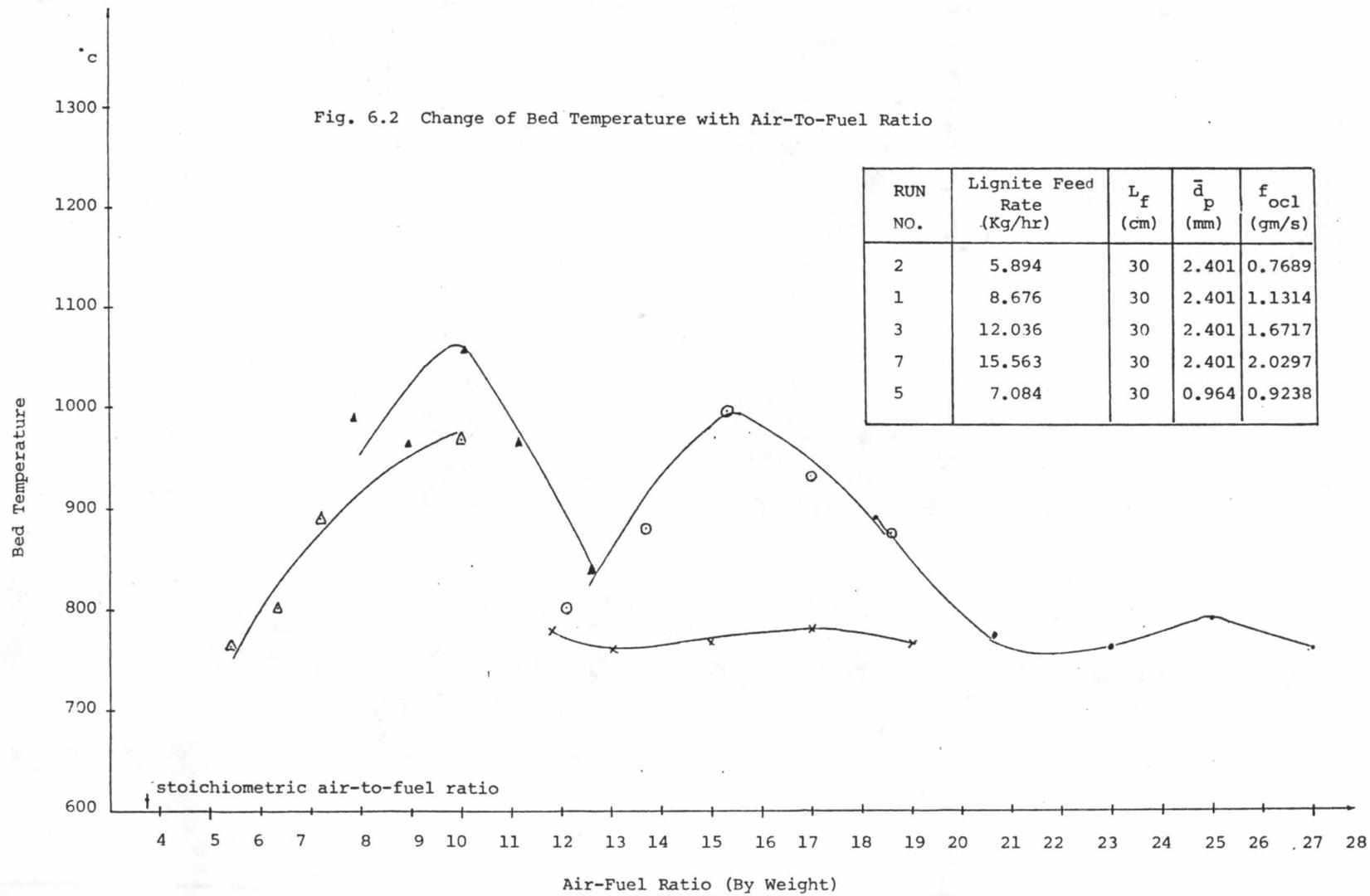
XS = excess air

$F_{ocl}$  = coal feed rate

$\bar{T}_B$  = average steady state bed temperature

$\Delta\eta$  = deviation of calculated carbon combustion efficiency from experimental value

$|\overline{\Delta\eta}|$  = absolute deviation of calculated carbon combustion efficiency from experimental value.



increases as the air-to-fuel ratio increases until the maximum temperature is reached, then decreases.

The minimum air-to-fuel ratio with which the bed can sustain self combustion in the fluidizing state throughout the bed is about 6 which is higher than the stoichiometric air-to-fuel ratio by 30 %.

#### 6.5 Carbon Particle Interaction

Since the char particles in the bed comprise about 0.1 % and 0.23 of run series 1 and series 2 respectively (see Table 6.5) the carbon particle interaction should be small and corresponding to single-particle Sherwood number correlation used in the model.

#### 6.6 Reynolds Number of Combustor Column

The combustor column Reynolds number in these experiments are between 9,000 and 20,000 and shown in Fig. 6.3. The gas density is not constant due to the combustion of coal in the bed. These can be used to predict the gas flow on the column surface ( laminar or turbulent flow)

#### 6.7 Carbon Monoxide (CO)

From Table 6.1 and 6.2 the average concentration of CO in the flue gas is 3,826 PPM or 0.38 %. If the carbon combustion efficiency is 95 %, carbon feed rate is 0.7 gm/s, and superficial velocity of air is 3.5 m/s at STP, the complete reaction in the

reactor would produce only  $\text{CO}_2$ , but in fact from the experiment CO is about 0.38 %, hence the uncomplete combustion is about 19 % of the complete one. At higher temperature than  $700^\circ\text{C}$ , CO may come from the endothermic reaction of



This reaction increases with increased bed temperature

#### 6.8 Bed Temperature and Coal Feed

From Fig 6.1, the graph corresponding to 1.0 mm particles is lower than other graphs. It is to be noticed that the bed temperature shown in this graph is lower than the other ones in those two graphs. The lower bed temperature may be affected by insufficiently feeding of coal.



Table 6.5. Calculated Data Based on Bed Particles (Limestone)

Run No.	Data No.	$\bar{d}_p$ limestone cm	$U_o$ cm/s	$T_B$ °K	$U_{mf}$ cm/s	$\frac{U_o}{U_{mf}}$	$d_b$ cm	$(K_{bp})_b$ $s^{-1}$	$X_b$	$C_{AP}$ gm-mole/cm <sup>3</sup>	$W_B$ gm	$F_{ocl}$ gm/s	$W_{cl}$ gm	$\frac{W_{cl}}{W_B} \times 100$	$\bar{t}, s$ $W_{cl}/F_{ocl}$	$\eta$
1	1	0.0927	242.09	1075	68.65	3.53	15	21.07	2.434	$2.38 \times 10^{-6}$	6797.0	1.1314	6.67	0.098	5.890	92.04
	2	"	307.83	1154	65.89	4.67	15	21.35	1.952	$2.16 \times 10^{-6}$	6685.7	"	6.08	0.091	5.372	88.77
	3	"	357.85	1268	62.24	6.04	15	20.38	1.529	$1.74 \times 10^{-6}$	6636.8	"	6.64	0.100	5.270	95.14
	4	"	392.51	1204	64.29	6.11	15	20.92	1.514	$1.73 \times 10^{-6}$	6563.1	"	6.69	0.102	5.192	87.77
	5	"	408.67	1149	65.92	6.19	15	21.36	1.494	$1.91 \times 10^{-6}$	6497.7	"	6.69	0.103	5.915	93.83
3	1	0.0927	299.70	1264	67.37	4.45	15	21.91	2.064	$2.02 \times 10^{-6}$	6794.8	1.6717	9.26	0.136	5.54	94.39
	2	"	329.96	1237	63.25	5.22	15	20.65	1.755	$2.07 \times 10^{-6}$	6699.3	"	8.93	0.133	5.34	93.49
	3	"	394.23	1330	60.46	6.52	15	19.91	1.422	$1.89 \times 10^{-6}$	6648.4	"	8.66	0.130	5.18	94.32
	4	"	404.29	1240	63.14	6.40	15	20.62	1.447	$2.06 \times 10^{-6}$	6570.5	"	8.37	0.127	5.00	93.12
	5	"	395.51	1112	67.16	5.89	15	21.68	1.569	$2.21 \times 10^{-6}$	6465.1	"	8.85	0.137	5.29	93.27
5	1	0.06	199.38	1051	26.68	7.47	15	9.47	1.097	$2.15 \times 10^{-6}$	6778.8	0.7238	1.49	0.022	1.61	82.66
	2	"	214.11	1032	27.73	7.72	15	9.76	1.074	$2.04 \times 10^{-6}$	6720.4	"	1.65	0.021	1.79	88.21
	3	"	246.54	1040	27.41	8.99	15	9.67	0.950	$2.11 \times 10^{-6}$	6642.3	"	1.42	0.023	1.54	79.48
	4	"	281.14	1039	26.62	10.56	15	9.45	0.832	$2.07 \times 10^{-6}$	6575.3	"	1.41	0.022	1.53	78.36

$W_B$  = weight of bed material

$W_{cl}$  = weight of coal in bed

$\bar{t}$  = average coal particle resident time in bed

Fig. 6.3 Combustion Efficiency and Reynolds Number of Reactor Column

