

บรรณานุกรม

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กระทรวงพาณิชย์, 1984 (อัดสำเนา)
- Annual book of ASTM standards "Standard test methods for moisture content of wood" American society for testing and materials, Philadelphia, pp.622-636., 1980.
- Ashworth, J.C. and Hill, M.C. "Use of simulation techniques to evaluate strategies for improvement of industrial multizone through-circulation trolley dryer" International drying symposium (Mujumdar, A.S.) pp.508-522, 1980
- Brown, A.H. and Van Arsdel, W.B. "Drying rate monographs. III. White potato strips-vertical air flow" USDA (1951) : AIC-31-III
- Chien, K.S., Matthes, R.K. and Verma, B.P., "Dimension analysis of seed-moisture movement in deep-bed drying" Trans Amer Soc Agr Eng, Gen Ed. 14(2), (1971) : 227-281.
- Chirife, J. and Cachero, R.A., "Through-circulation drying of tapioca root" J.Food Science. 35(1970) : 364-368.
- Garden, R.G. and Mitchell, T.J., "Through-circulation drying of seaweed" J.Sci. Food Agr. 8(1953) : 370
- Hochstetler, T. "Using waste engine heat to dry grain" Agric Eng. 62(3), (1981) : 18-19.

- Hubble and Prestion, E., "Consider microwave drying" Chem Eng (New York). 89(20), (1982) : 125-127.
- Marshall, W.R. and Hougen, O.A., "Through-circulation drying of seaweed" J.Sci.Food Agr. 3, (1942) : 113.
- McGaw, D.R., Farabi, H. and Jairam, J. "The optimisation of batch operated packed bed dryers for the drying of Tropical agricultural products" International drying symposium (Toei, R.) pp. 616-619, 1984.
- Ouhab, R. and Pourhiet, A.LE., "Optimum drying condition of grain" International drying symposium (Toei, R.) pp.579-584, 1984.
- Roberts, D.E. and Brooker, D.B., "Grain drying with a recirculation" Trans Amer Soc Agric Eng., Gen Ed. 18(1), (1975) : 181-184.
- Rusmitus, S. "Study of variable effecting drying rate of Tapioca chips" Master's Thesis, Department of Chemical Technology, Chulalongkorn University, 1978.
- Sabbah, M.A., Meyer, G.E., Keener, H.M. and Roller, W.L. "Reversed-direction-air-flow drying for soybean seed" Trans Amer Soc Agric Eng. Gen Ed. 20(3), (1977) : 562-566.
- Shanokprasith, S. and Bunrungsanor, S. "Through-circulation drying of freshly harvested paddy" Senior project, Department of Chemical Technology, Chulalongkorn University, 1976.
- Svensson, C. "Industrial applications for new steam drying process in forest and agricultural industry" International drying symposium (Toei, R.) pp.541-546, 1984.

- Tanthapanichakoon, W. and Loychirakul, T. "Through flow drying characteristics of some Thai fruits" International drying symposium (Toei, R.) pp.591-596, 1984.
- Thanh, N.C. "Technological improvement of Tapioca chips and pellets produced in Thailand" AIT research report 57, 1976.
- Thanh, N.C., Muttamara, S., Lahani, B.N. and Burintratikul "Optimisation of drying and pelleting techniques for tapioca roots" Enviromental division, AIT, Thailand, 1979.
- Toei, R., ed. Kanso Sochi, 6th ed., pp. 58, Asakura shaten, 1967.
- Thompson and James, F. "Reducing energy use in agricultural drying operation" In conference on energy use manage : pp. 22-26, 1979.
- Yoshida, F. and Mori Shoron Kagaku Kogaku II pp. 648-656, Nikkan Kogyo Shembun-sha, 1972.

ภาคผนวก

ภาคผนวก ก-1

ภาคผนวกนี้แสดงโปรแกรมคอมพิวเตอร์และลักษณะการกระจายความชื้นในชั้น
มันสำปะหลังหนา 40 ซม. ของทั้งการคำนวณและการทดลอง สำหรับทั้งกรณีการอบแห้ง
แบบปกติและการอบแห้งโดยลมวัสดุเป็นครั้งคราว (ในที่นี้จะแสดงตัวอย่างของกรณีลมวัสดุ
ทุก ๆ 50 นาที)

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5150 DBAL4444 KAMONFAT PHANAFAYA
1 DIMENSION ZI(200),REXP(200),ETA(100),FI(100),FCAL(200),AI(50),A
*TA(50),TIME(100),WEXP(20,10),A(100),YA(50),AEXP(20,10)
C CA=INITIAL MOISTURE CONTENT (KG WATER/ KG DRY SOLID) (THIN BED EXP)
C CB=FINAL MOISTURE CONTENT(KG WATER/ KG DRY SOLID) (THIN BED EXP)
C EC=EQUILIBRIUM MOISTURE CONTENT(KG WATER/KG DRY SOLID)
C DEN=DENSITY (KG/CUBIC M)
C ZI(1)=DISTANCE (CM)
C ETAL=DISTANCE (DIMENSIONLESS)
C ETAL= BED HEIGHT(DIMENSIONLESS)
C CCMASS=MASS TRANSFER COEFFICIENT (KG/CUBIC M.HR.DELTA H)
C AFSIGN=FRACTION OF VOL OCCUPIED BY DRY MATERIAL IN PACKED BED
C =1-(VOID FRACTION)
C CCNA,CCNB,CCNC=CONSTANT VALUE IN RATE OF DRYING FORMULA
C CCOH=INITIAL VALUE OF CRITICAL MOISTURE CONTENT USED IN TRIAL AND ERROR
C CALCULATION TO FIND OPTIMUM CRITICAL MOISTURE CONTENT
C CCDIFF=INTERVAL OF CRITICAL MOISTURE CONTENT TO BE VARIED
C CCOFF=FINAL VALUE OF CRITICAL MOISTURE CONTENT USED IN TRIAL AND ERROR
C CALCULATION TO FIND OPTIMUM CRITICAL MOISTURE CONTENT
C NUMBER=NUMBER OF DATA FROM THE EXPERIMENT (THIN BED EXP)
C ZT(1)=TIME(HR) (THIN BED EXP)
C AI(1)=MOISTURE CONTENT THAT CORRESPONDED WITH ZT(1) (THIN BED EXP)
C REXP=RATE OF DRYING FROM THE EXPERIMENT (THIN BED EXP)
C FI=VALUE OF MOISTURE CONTENT OF AIR AT WET BULB TEMPERATURE MINUS VALUE OF
MOISTURE CONTENT OF AIR BEFORE ENTER THE BED
C FLOW=MASS FLOW RATE (KG DRY AIR/HR.SQUARE M)
C MPOINT=NUMBER OF COLUMN OF DATA (MOISTURE CONTENT) FROM THE LONG BED EXP
(DIRECT FLOW OR MIXING) PLUS COLUMN OF TIME AND AVERAGE MOISTURE CONTENT
C LPOINT=NUMBER OF COLUMN OF DATA (MOISTURE CONTENT) FROM THE LONG BED EXP
(DIRECT FLOW OR MIXING) PLUS COLUMN OF TIME
C NATA=NUMBER OF ROW OF DATA(TIME) FROM THE LONG BED EXP(DIRECT FLOW)
C NATA=NUMBER OF ROW OF DATA(TIME) FROM THE LONG BED EXP(MIXING)
C NPOINT=NUMBER OF CALCULATION OF THE PROFILE OF MOISTURE CONTENT IN LONG BED
BEFORE EACH MIXING.
C =MIXING TIME INTERVAL DEVIDED BY TIME INTERVAL OF EACH CALCULATION
C OF PROFILE
C ZTADI=TIME INTERVAL OF EACH CALCULATION OF PROFILE OF MOISTURE CONTENT
C XMIX=FINAL VALUE OF MIXING TIME INTERVAL
C WEXP(I,J)=VALUE OF MOISTURE CONTENT OF THE DRYING MATERIAL IN THE BED AT
DIFFERENT HEIGHT IN CASE OF DIRECT FLOW EXP
C AEXP(I,J)=VALUE OF MOISTURE CONTENT OF THE DRYING MATERIAL IN THE BED AT
DIFFERENT HEIGHT IN CASE OF MIXING EXP
C TIME(I)=VALUE OF TIME(MIN) FROM THE EXPERIMENT(LONG BED EXP)
2 READ(5,66) CA,CB,EC,CCNA,CCNB,CCNC,DEN,ETAL,CCMASS,AFSIGN
3 66 FORMAT(8F10.3)
4 WRITE(6,101)
5 101 FORMAT(1H)
6 WRITE(6,67) CA,CB,EC,CCNA,CCNB,CCNC,DEN,ETAL,CCMASS,AFSIGN
7 67 FORMAT(1/2X,' CA=',F10.5,2X,' CB=',F10.5,2X,' EC=',F10.5,2X,
*' CCNA=',F10.5,2X,' CCNB=',F10.5,2X,' CCNC=',F10.5,2X,' DEN=
*',F10.5,' ETAL=',F10.5,2X,' CCMASS=',F15.5,2X,' AFSIGN=',F10.5)
8 READ(5,10) CCOH,CCDIFF,CCOFF,NUMBER
9 10 FORMAT(3F5.2,110)
10 READ(5,20) (ZT(I),I=1,NUMBER)
11 20 FORMAT(9F5.3)
12 WRITE(6,22) (ZT(I),I=1,NUMBER)
13 22 FORMAT(1/711 THETA=',F10.3)
14 READ(5,12) (AI(I),I=1,NUMBER)
15 12 FORMAT(11F5.3)
16 WRITE(5,13) (AI(I),I=1,NUMBER)

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17 17 FORMAT(17) (MPCINT,PL=1,41,31)
18 READ(5,20) (REXPER(I),I=1,NUMBER)
19 20 FORMAT(10F5,2)
20 WRITE(6,13) (REXPER(I),I=1,NUMBER)
21 21 FORMAT(17) ('REXPER=',F10,2)
22 READ(5,40) (F1,FLCH,MPCINT,NATA,LPCINT,MATA)
23 40 FORMAT(2F8,4,4I10)
24 WRITE(6,11) (F1,FLCH,MPCINT,NATA,LPCINT,MATA)
25 11 FORMAT(1/2X,'F1=',F6,4,2X,'MASSFLCHRATE=',F10,2,2X,'MPCINT=',I10,2X
*, 'NATA=',I10,2X,'LPCINT=',I10,2X,'MATA=',I10)
26 READ(5,18) (TIME(I),I=1,NATA)
27 18 FORMAT(12F5,1)
28 READ(5,16) (MATA(J),J=3,MPCINT)
29 16 FORMAT(12F5,3)
30 READ(5,7) ((WEXP(I,J),J=1,LPCINT),I=1,NATA)
31 17 FORMAT(2F8,4)
32 READ(5,60) (MPCINT,XMIX,ZTAD)
33 60 FORMAT(1I0,2F10,0)
34 READ(5,150) ((AEXP(I,J),J=1,LPCINT),I=1,NATA)
35 150 FORMAT(2F8,4)
C WRITE & SHOW DATA FROM THE EXPERIMENT
36 WRITE(6,101)
37 WRITE(6,41) (MATA(J),J=3,MPCINT)
38 41 FORMAT(10X,'TABLE OF RAW DATA BETWEEN TIME & MOISTURE'//7/2X,'TIME (
*(MIN) * * *',30X,'VALUE OF MOISTURE AT DISTANCE(CM)='//2C
*X,'MEAN'//25X,'*',2X,'F10.5'//7)
39 DC 7 I=1,NATA
40 WEXP(I,MPCINT)=(WEXP(I,2)+WEXP(I,3)+WEXP(I,4)+WEXP(I,5)+WEXP(I,6)+
*WEXP(I,7)+WEXP(I,8)+WEXP(I,9))/8.
41 7 CONTINUE
42 WRITE(6,42) ((WEXP(I,J),J=1,MPCINT),I=1,NATA)
43 42 FORMAT(2X,7F7,2,19X,9F10,5)
C WRITE DATA FOR CALCULATION CC MINIMUM
44 WRITE(6,70) (CCCN,CCDIFF,CCOFF,NUMBER)
45 70 FORMAT(1/54X,'CALCULATION VALE OF CC'//5X,'CC CN=',F10,5,5X,
* 'CC DIFFERENT='//F10,5,5X,'CC OFF=',F10,5,5X,'NUMBER OF THETA=',
*15)
C CALCULATION CC
46 CC = CC0N
47 SUMMIN = 1.0E6
48 222 EXPCC=EXP(CONA/(CC-FC))
49 SUM = 0.0
50 DC 44 I=1,NUMBER
51 EXPZTA=EXP(CONB*ZTA(I)/(CC-FC))
52 RCAL(I)=CONC*EXPZTA*(1.0-EXPCC)/(1.0-EXPZTA*(1.0-EXPCC))
53 RDIFF = REXPER(I)-RCAL(I)
54 SUM = SUM+RDIFF*RDIFF
55 44 CONTINUE
56 IF (SUM.GT.SUMMIN) GO TO 111
57 SUMMIN = SUM
58 CCMIN = CC
59 111 IF(CC.GT.CCOFF) GO TO 222
60 CC = CC+CCDIFF
61 GO TO 222
C WRITE VALUE OF CALCULATION FROM CC MINIMUM
62 222 WRITE(6,80) SUMMIN,CCMIN
63 80 FORMAT(1/10X,'SUMMATION=',F10,5,2X,'CC MINIMUM=',F10,5/)
64 WRITE(6,90)
65 90 FORMAT(1/10X,'THETA(M)',20X,'DATE OF EXPERIMENT',20X,'DATE OF CALCU
* (AT:MM)

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66 EXPCC=EXP(CCNNA/(CCMIN-EC))
67 DC 100 I=1,NUMBER
68 EXPZTA=EXP(CCNNA*ZTA(I)/(CCMIN-EC))
69 FCAL(I)=CCNC*EXPZTA*(1.0-EXPCC)/(1.0-EXPZTA*(1.0-EXPCC))
70 WRITE (6,110) ZTA(I),FEXPER(I),FCAL(I)
71 110 FORMAT (10X,F9.5,20X,F18.9,20X,F18.9)
72 100 CONTINUE
73 C WRITE 5 SHOW DATA FROM THE EXPERIMENT IN DIMENSIONLESS FORM
74 DO 4 I=1,NATA
75 DC 4 J=2,LPOINT
76 WEXP(I,J)=(WEXP(I,J))/CCMIN
77 4 CONTINUE
78 CCA=(WEXP(I,2)+WEXP(I,3)+WEXP(I,4)+WEXP(I,5)+WEXP(I,6)+WEXP(I,7)+W
*EXP(I,8)+WEXP(I,9))/8.
79 DO 23 J=3,MPCINT
80 ETA(J)=ATA(J)*CCMASS/100./FLCW
81 23 CONTINUE
82 WRITE(6,101)
83 WRITE(6,55) CCMIN
84 55 FORMAT(15X,'CCMIN=',F6.2//)
85 DO 3 I=1,NATA
86 WEXP(I,10)=(WEXP(I,2)+WEXP(I,3)+WEXP(I,4)+WEXP(I,5)+WEXP(I,6)+WEXP
*(I,7)+WEXP(I,8)+WEXP(I,9))/8.
87 3 CONTINUE
88 WRITE(6,24)(ETA(J),J=3,MPCINT)
89 24 FORMAT(150X,'TABLE OF DATA IN DIMENSIONLESS'///2X,'TIME(MIN) TAU
* ',35X,'VALUE OF FI AT ETA=',32X,' FI MEAN'//25X,'**',8F10.5/
*///)
90 WRITE(6,52)((WEXP(I,J),J=1,MPCINT),I=1,NATA)
91 52 FORMAT(2X,F7.2,17X,9F10.5)
92 C SHOW DATA FROM CALCULATION
93 WRITE(6,101)
94 FICNA=CCA
95 WRITE(6,105) FICNA
96 109 FORMAT(5X,'FICNA=',F8.4)
97 WRITE(6,25)(ETA(J),J=3,MPCINT)
98 25 FORMAT(150X,'TABLE OF DATA IN DIMENSIONLESS'///2X,'TIME(MIN) TAU
* ',35X,'VALUE OF FI AT ETA=',32X,' FI MEAN',3X,'RATE'//25X,'
**',8F10.5///)
99 TF=5.
100 TUF=CCMASS*TF/(AFSICN*DEN*CCMIN*60.)
101 TUT=0.
102 TG=0.
103 56 W=EXP(PI*TUT)
104 I=3
105 57 A(I)=FICNA*(EXP(FICNA*ETA(I)))/(W*EXP(FICNA*ETA(I))-1)
106 I=I+1
107 IF(I>GT-MPCINT) GO TO 58
108 GO TO 57
109 58 C=EXP((-FICNA)*ETAL)
110 E=EXP(FICNA*ETAL)
111 D=EXP(-PI*TUT)
112 KA=(FICNA*ETAL+LOG(D*(1.-C)+C))/ETAL
113 RATE=T(PI+FICNA*T*(1.-E))/(ETAL*(FICNA-(FICNA*C)+(FICNA*D*E)))*(CC
*MASS/(AFSICN*DEN))
114 WRITE(6,91) TG,TUT,(Z(I),I=3,MPCINT),DA,RATE
115 91 FORMAT(2X,F7.2,2X,F9.2,7X,10F10.5)
116 IF(MPCINT<1) GO TO 5
117 TUT=TUT+TF

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117      GC TO 55
118      G  WRITE(6,101)
119      5 WRITE(6,101)
120      151 FORMAT(50X,'TABLE OF F/W DATA BETWEEN TIME&MOISTURE IN CASE OF MI
      *XING'//2X,'TIME(MIN) * * * * *',20X,'VALUE OF MOISTURE AT
      *DISTANCE(CM)=',20X,'MEAN'//25X,'*',2X,'BFIC.5'//)
121      DO 152 I=1,MATA
122      AEXP(I,MATA)=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+A
      *XP(I,7)+AEXP(I,8)+AEXP(I,9))/8.
123      152 CONTINUE
124      WRITE(6,153)((AEXP(I,J),J=1,MPCINT),I=1,MATA)
125      153 FORMAT(2X,F7.2,19X,9F10.5)
126      G  WRITE(6,101)
127      DO 154 I=1,MATA
128      DO 154 J=2,LPCINT
129      AEXP(I,J)=(AEXP(I,J))/CCMIN
130      154 CCONTINUE
131      ACA=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+AEXP(I,7)+A
      *EXP(I,8)+AEXP(I,9))/8.
132      DO 155 J=3,MPCINT
133      ETA(J)=ATA(J)*CCMASS/100./FLOW
134      155 CCONTINUE
135      WRITE(6,101)
136      156 FORMAT(75X,'CCMIN=',F6.2//)
137      DO 157 I=1,MATA
138      AEXP(I,10)=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+AEXP
      *(I,7)+AEXP(I,8)+AEXP(I,9))/8.
139      157 CONTINUE
140      WRITE(6,158)(ETA(J),J=3,MPCINT)
141      158 FORMAT(50X,'TABLE OF DATA IN DIMENSIONLESS IN CASE OF MIXING'//2
      *X,'TIME(MIN) TAU * * * * *',25X,'VALUE OF FI AT ETA=',32X,'FI MEAN'
      *//25X,'*',8F10.5//)
142      WRITE(6,159)((AEXP(I,J),J=1,MPCINT),I=1,MATA)
143      159 FORMAT(2X,F7.2,17X,9F10.5)
144      FIGMA=ACA
145      I=1
146      J=3
147      113 YA(I)=ETA(J)
148      I=I+1
149      J=J+1
150      IF(J.GT.MPCINT) GC TO 51
151      GO TO 113
152      51 I=1
153      14 ETA(I)=YA(I)
154      I=I+1
155      IF(I.GT.8) GC TO 551
156      GO TO 14
157      551 MPCINT=8
158      ZTADN=0.0000
159      ZTACF=1000.
160      IPOINT = MPCINT
161      NPOINT = 0
162      222 NPOINT = NPOINT+IPOINT
163      ZTAMX = FLOW*(NPOINT)*7TAD1
164      FIGN=FIGMA
165      WRITE(6,104)
166      104 FORMAT(14I1)
167      WRITE(6,60) NPOINT,ZTACF,ZTAMX,FIG

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160      63 FORMAT(//2X,' NPOINT=',I3,' ZTADI=',F10.5,' XMIX=',F10.5,' FIX='
      *,F10.5)
161      WRITE(6,161)ZTAMIX
162      166 FORMAT(//10X,'#####' MIXING EVERY ',F10.2,' MIN #####)
      C WRITE TYPE OF CALCULATION FOR PROFILE AFTER MIXING
163      WRITE(6,160)(ETA(I),I=1,MPOINT)
164      160 FORMAT(//35X,'TABLE OF CALCULATION FOR PROFILE AFTER MIXING'//)
      *HETA(MIN) * TAU * *,4CX,'VALE OF FI AT ETA='// SUM
      * NONSUM* SUM NCNSUM* ,ICFIC,5//)
165      WRITE (6,106)
166      106 FORMAT(140)
      C CALCUTION FOR PROFILE AFTER MIXING
167      THETA =ZTACN
168      ZTASUM = ZTACN
169      DO 170 K=1,MPOINT
170      F1(K)=F1CN
171      170 CONTINUE
172      TAUSUM = 0.0
173      688 TAU = 0.0
174      N = 0
175      777 WRITE (6,180) ZTASUM,THETA,TAUSUM,TAU,(F1(K),K=1,MPOINT)
176      180 FORMAT(1X,F7.2,1X,F7.2,'*',F7.2,F8.2,'*',ICF10.5)
177      FIOFF=0.00001
178      IF (F1(MPOINT).LT.FIOFF) GO TO 666
179      IF (ZTASUM.GT.ZTACFF) GO TO 666
180      IF (N.EQ.MPOINT) GO TO 999
181      THETA = THETA+ZTADI
182      ZTASUM=ZTASUM+ZTADI
183      N =N+1
184      TAU=CMASS*THETA/(AFSICK*DEN*(CCMIN-EC)*60.0)
185      TAUSUM=ZTASUM*CMASS/(AFSICK*DEN*(CCMIN-EC)*60.0)
186      AE=EXP(PI*TAU)
187      DO 190 K=1,MPOINT
188      B= EXP(F1CN*ETA(K))
189      F1(K)=F1CN*(AE+(B-1.0))
190      190 CONTINUE
191      GO TO 777
192      999 C=EXP((-F1CN)*ETA/L)
193      D=EXP((-PI)*TAU)
194      F1CN=(F1CN*ETA/L+ALOG(D*(1.0-C)+C))/ETA/L
195      THETA = ZTACN
196      WRITE(6,105)
197      105 FORMAT(140)
198      DO 3333 IJ=1,MPOINT
199      F1(IJ) = F1CN
200      3333 CONTINUE
201      GO TO 888
202      666 IF(ZTAMIX.GT.XMIX) GO TO 1111
203      GO TO 2222
204      1111 STOP
205      END

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RETRY

CA= 0.80000 CR= 0.00000 EC= 0.00000 CONA= 3.06000 CCNP= -10.71000 CCNC= -2.30400

DEN= 224.12980 ETAL= 30.53000 CCMASS= 162626.00000 AFSIGN= 0.23000

THETA= 0.000 THETA= 0.117 THETA= 0.183 THETA= 0.283 THETA= 0.400 THETA= 0.567 THETA= 0.800
THETA= 1.133 THETA=

MOISTURE= 0.800 MOISTURE= 0.700 MOISTURE= 0.600 MOISTURE= 0.500 MOISTURE= 0.400 MOISTURE= 0.300 MOISTURE= 0.200
MOISTURE= 0.100 MOISTURE=

REXPER= 1.624 REXPER= 1.382 REXPER= 1.095 REXPER= 0.900 REXPER= 0.708 REXPER= 0.539 REXPER= 0.360
REXPER= 0.224 REXPER=

PI=0.0140 MASSFLOWRATE= 2130.00 MPCINT= 10 NATA= 20 LPCINT= 9 MATA= 10

TABLE OF FAW DATA BETWEEN TIME & MOISTURE

TIME(MIN)	*	*	*	VALUE OF MOISTURE AT DISTANCE(CM)=							MEAN
	*	2.50000	7.50000	12.50000	17.50000	22.50000	27.50000	32.50000	37.50000		
0.00		1.66100	1.67600	1.66700	1.70400	1.68500	1.67900	1.66300	1.63600	1.67762	
30.00		0.66700	1.33000	1.57600	1.68300	1.67300	1.67900	1.65800	1.67000	1.49200	
60.00		0.23100	0.71900	1.28600	1.58500	1.63100	1.63600	1.62600	1.63200	1.29325	
90.00		0.06500	0.27800	0.75000	1.35100	1.56000	1.61400	1.60500	1.61600	1.10487	
120.00		0.02700	0.08600	0.20500	0.81200	1.32700	1.53300	1.57200	1.57900	0.90500	
165.00		0.01600	0.02700	0.07000	0.22900	0.56300	1.05200	1.40600	1.51900	0.61025	
195.00		0.00900	0.01600	0.03800	0.09300	0.26500	0.62500	1.13300	1.42200	0.45012	
225.00		0.00500	0.00500	0.02100	0.04000	0.09900	0.27600	0.62100	1.10100	0.27100	
255.00		0.00000	0.00500	0.01100	0.02200	0.03800	0.10400	0.29300	0.57700	0.14375	
285.00		0.00000	0.00000	0.00500	0.01600	0.01600	0.04100	0.12000	0.31900	0.06525	
305.00		0.00000	0.00000	0.00500	0.00500	0.01100	0.01900	0.04000	0.13500	0.02750	
335.00		0.00000	0.00000	0.00500	0.00500	0.00600	0.01400	0.01300	0.05400	0.01212	
395.00		0.00000	0.00000	0.00000	0.00500	0.00000	0.00000	0.00000	0.00500	0.00125	
425.00		0.00000	0.00000	0.00000	0.00500	0.00000	0.00000	0.00000	0.00500	0.00125	
455.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
495.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
515.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
545.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
575.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
605.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	

CALCULATION VAULE OF CC

CC ON= 0.90000 CC DIFFERENT= 0.05000 CC OFF= 10.00000 NUMBER OF THETA= 3
 SUMMATION= 0.04747 CC MINIMUM= 3.84996

THETA(THK)	RATE OF EXPERIMENT	RATE OF CALCULATION
0.00000	1.623999000	1.537529000
0.11700	1.381955000	1.309927000
0.18300	1.095000000	1.182901000
0.28300	0.899999900	0.997869600
0.40000	0.708000000	0.799710500
0.56700	0.538999900	0.562116200
0.80000	0.360000000	0.325071800
1.13300	0.223999900	0.138419000

CCM11= 2.25

TABLE OF DATA IN DIMENSIONLESS

TIME(MIN)	TAU	VALUE OF FI AT ETA=								FI MEAN
	*	1.90876	5.72627	9.54378	13.36129	17.17879	20.99631	24.81381	28.53133	
0.00		0.43143	0.43533	0.43299	0.44260	0.43767	0.43611	0.43195	0.43793	0.43575
30.00		0.17325	0.24546	0.40936	0.43715	0.43455	0.43611	0.43065	0.43377	0.38754
60.00		0.06000	0.18676	0.33403	0.41165	0.42364	0.42494	0.42234	0.42390	0.33591
90.00		0.01688	0.07221	0.19481	0.25091	0.40520	0.41923	0.41689	0.41775	0.28698
120.00		0.00761	0.02234	0.07922	0.21091	0.34468	0.39819	0.40832	0.40997	0.23507
150.00		0.00416	0.00701	0.01818	0.05948	0.14624	0.27325	0.36520	0.37433	0.15851
175.00		0.00234	0.00416	0.00987	0.02416	0.06893	0.16234	0.29429	0.35935	0.11692
225.00		0.00130	0.00130	0.00545	0.01039	0.02571	0.07169	0.16130	0.23528	0.07039
255.00		0.00000	0.00130	0.00286	0.00571	0.00587	0.02701	0.07610	0.17595	0.03734
295.00		0.00000	0.00130	0.00130	0.00416	0.00416	0.01065	0.03117	0.03236	0.01695
305.00		0.00000	0.00130	0.00130	0.00130	0.00286	0.00494	0.01039	0.03507	0.00714
335.00		0.00000	0.00000	0.00130	0.00130	0.00156	0.00364	0.00338	0.01403	0.00315
375.00		0.00000	0.00000	0.00000	0.00130	0.00000	0.00000	0.00000	0.00130	0.00032
425.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00130	0.00032
455.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
495.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
515.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
545.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
575.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
605.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

FI7MA= C.4355

TABLE OF DATA IN DIMENSIONLESS

TIME(MIN)	TAU	VALUE OF FI AT ETA=									FI MEAN	RATE
		*	1.90876	5.72627	9.54378	13.36129	17.17879	20.99631	24.81381	28.63133		
0.00	0.00		0.43575	0.43575	0.43575	0.43575	0.43575	0.43575	0.43575	0.43575	0.43575	-0.35086
5.00	16.56		C.39131	C.42657	0.43398	0.43542	0.43569	0.43574	0.43575	0.43575	0.42816	-0.35086
10.00	33.12		C.34671	C.41553	0.43177	0.43499	0.43561	0.43572	0.43575	0.43575	0.42056	-0.35086
15.00	49.68		C.30315	0.40240	0.42901	0.43446	0.43551	0.43570	0.43574	0.43575	0.41297	-0.35086
20.00	66.24		C.26169	C.38698	0.42559	0.43379	0.43539	0.43568	0.43574	0.43575	0.40537	-0.35086
25.00	82.81		0.22320	0.36915	0.42135	0.43295	0.43522	0.43565	0.43573	0.43575	0.39778	-0.35086
30.00	99.37		C.18828	0.34887	0.41612	0.43185	0.43501	0.43561	0.43572	0.43575	0.39019	-0.35085
35.00	115.93		C.15726	0.32627	0.40970	0.43056	0.43476	0.43556	0.43572	0.43574	0.38259	-0.35085
40.00	132.49		0.13021	C.30164	0.40189	0.42891	0.43444	0.43550	0.43570	0.43574	0.37500	-0.35085
45.00	149.05		C.10700	0.27542	0.39246	0.42683	0.43403	0.43542	0.43569	0.43574	0.36740	-0.35085
50.00	165.61		C.08736	0.24821	0.38118	0.42424	0.43352	0.43533	0.43567	0.43574	0.35981	-0.35085
55.00	182.17		C.07095	0.22072	0.36785	0.42102	0.43288	0.43520	0.43565	0.43573	0.35221	-0.35085
60.00	198.73		C.05736	C.19267	C.35231	0.41704	0.43208	0.43505	0.43562	0.43573	0.34462	-0.35085
65.00	215.30		0.04620	C.16774	0.33449	0.41211	0.43107	0.43486	0.43558	0.43572	0.33703	-0.35084
70.00	231.86		C.03710	0.14352	C.31444	C.40607	0.42980	0.43461	0.43553	0.43571	0.32943	-0.35084
75.00	248.42		C.02972	C.12141	0.29234	C.39869	0.42821	0.43430	0.43548	0.43570	0.32184	-0.35084
80.00	264.98		C.02376	0.10167	C.26855	C.38977	C.42622	0.43391	0.43540	0.43563	0.31424	-0.35083
85.00	281.54		C.01896	0.08437	C.24355	C.37907	C.42375	0.43342	0.43531	0.43561	0.30665	-0.35083
90.00	298.10		C.01511	0.06946	0.21796	0.36639	0.42066	0.43281	0.43519	0.43564	0.29906	-0.35082
95.00	314.66		0.01204	C.05681	0.19247	0.35155	0.41684	0.43204	0.43504	0.43562	0.29146	-0.35081
100.00	331.22		C.00958	0.04619	0.16775	0.33448	0.41211	0.43107	0.43486	0.43559	0.28387	-0.35080
105.00	347.78		C.00761	0.03739	0.14424	0.31518	C.40630	0.42985	0.43462	0.43554	0.27628	-0.35078
110.00	364.35		C.00605	0.03014	0.12275	0.29381	0.39921	0.42832	0.43432	0.43548	0.26868	-0.35076
115.00	380.91		C.00481	C.02422	0.10328	C.27066	0.39061	0.42641	0.43395	0.43541	0.26109	-0.35074
120.00	397.47		C.00382	0.01941	0.08606	0.24620	0.38028	0.42403	0.43348	0.43532	0.25350	-0.35070
125.00	414.03		C.00303	0.01553	0.07111	0.22102	0.36800	0.42106	0.43289	0.43521	0.24591	-0.35066
130.00	430.59		C.00240	0.01240	C.05834	0.19577	C.35362	0.41738	0.43215	0.43506	0.23832	-0.35061
135.00	447.15		C.00191	0.00989	0.04756	0.17112	0.33700	0.41283	0.43121	0.43483	0.23073	-0.35055
140.00	463.71		0.00151	0.00787	0.03858	0.14767	0.31815	0.40723	0.43004	0.43466	0.22315	-0.35047
145.00	480.27		C.00120	0.00627	0.03116	0.12592	0.29719	0.40038	0.42858	0.43437	0.21556	-0.35037
150.00	496.83		C.00095	0.00498	0.02507	0.10619	0.27440	0.39207	0.42674	0.43402	0.20798	-0.35024
155.00	513.39		C.00076	0.00356	0.02012	0.08867	0.25020	0.38206	0.42445	0.43356	0.20040	-0.35008
160.00	529.96		C.00060	0.00315	0.01611	0.07341	0.22516	0.37015	0.42159	0.43300	0.19282	-0.34988
165.00	546.52		C.00048	0.00250	0.01287	C.06031	0.19993	0.35616	0.41805	0.43223	0.18525	-0.34963
170.00	563.08		C.00038	C.00198	0.01027	0.04924	C.17518	0.33994	0.41366	0.43137	0.17769	-0.34931
175.00	579.64		C.00030	0.00157	C.00818	C.03998	C.15153	0.32149	0.40826	0.43025	0.17013	-0.34891
180.00	596.20		C.00024	0.00125	C.00652	0.03232	0.12949	0.20090	0.40165	0.42935	0.16258	-0.34841
185.00	612.76		C.00019	0.00099	0.00518	C.02603	0.10941	0.27841	0.39360	0.42799	0.15505	-0.34777
190.00	629.32		C.00015	0.00079	0.00412	0.02090	0.09153	0.25444	0.38391	0.42438	0.14753	-0.34698
195.00	645.88		C.00012	0.00062	C.00327	C.01674	0.07588	0.22951	0.37235	0.42213	0.14003	-0.34598
200.00	662.44		C.00009	0.00050	0.00260	C.01338	0.06242	0.20428	0.35873	0.41972	0.13255	-0.34473
205.00	679.01		C.00007	0.00039	0.00206	C.01068	0.05102	0.17941	0.34292	0.41749	0.12511	-0.34316
210.00	695.57		C.00006	0.00031	0.00164	C.00851	0.04147	0.15553	0.32486	0.41523	0.11770	-0.34121
215.00	712.13		C.00005	0.00025	C.00130	C.00678	0.03355	0.13318	0.30462	0.41297	0.11034	-0.33878
220.00	728.69		C.00004	0.00020	C.00102	C.00539	0.02703	0.11275	0.28245	0.41071	0.10304	-0.33576
225.00	745.25		C.00003	0.00016	C.00082	C.00429	0.02172	C.09448	0.25878	0.40849	0.09591	-0.33253
230.00	761.81		C.00002	0.00012	C.00065	C.00341	0.01740	0.07945	C.23390	0.40621	0.08967	-0.32745
235.00	778.37		C.00002	0.00010	C.00052	C.00271	C.01392	C.06462	0.20867	0.40395	0.08354	-0.32184



240.00	704.93	C.CCCCC1	O.CCCCC8	C.CCCCC4	C.CCCCC15	C.CCCCC11	C.CCCCC23	O.CCCCC18	O.CCCCC34	O.CCCCC74	-O.CCCCC150
245.00	811.48	C.CCCCC1	O.CCCCC8	C.CCCCC22	C.CCCCC71	C.CCCCC86	O.CCCCC30	O.CCCCC156	O.CCCCC31	O.CCCCC80	-O.CCCCC68
250.00	828.05	C.CCCCC1	O.CCCCC8	C.CCCCC26	C.CCCCC35	C.CCCCC70	O.CCCCC48	O.CCCCC136	O.CCCCC33	O.CCCCC149	-O.CCCCC29
255.00	844.62	C.CCCCC1	O.CCCCC8	C.CCCCC20	C.CCCCC07	C.CCCCC56	O.CCCCC08	O.CCCCC167	O.CCCCC54	O.CCCCC55	-O.CCCCC54
260.00	861.18	C.CCCCC1	O.CCCCC8	C.CCCCC16	C.CCCCC85	C.CCCCC46	O.CCCCC25	O.CCCCC75	O.CCCCC29	O.CCCCC92	-O.CCCCC74
265.00	877.74	C.CCCCC0	O.CCCCC2	C.CCCCC3	O.CCCCC6	C.CCCCC55	O.CCCCC0	O.CCCCC10	O.CCCCC29	O.CCCCC39	-O.CCCCC54
270.00	894.30	C.CCCCC0	O.CCCCC2	C.CCCCC0	O.CCCCC5	O.CCCCC2	O.CCCCC1	O.CCCCC8	O.CCCCC9	O.CCCCC9	-O.CCCCC2
275.00	910.86	C.CCCCC0	O.CCCCC2	C.CCCCC8	C.CCCCC4	O.CCCCC2	O.CCCCC1	O.CCCCC5	O.CCCCC1	O.CCCCC1	-O.CCCCC2
280.00	927.42	O.CCCCC0	O.CCCCC1	C.CCCCC6	O.CCCCC2	C.CCCCC7	O.CCCCC9	O.CCCCC4	O.CCCCC1	O.CCCCC1	-O.CCCCC2
285.00	943.98	O.CCCCC0	O.CCCCC1	O.CCCCC5	O.CCCCC2	C.CCCCC1	O.CCCCC7	O.CCCCC3	O.CCCCC1	O.CCCCC1	-O.CCCCC2
290.00	960.54	O.CCCCC0	O.CCCCC1	C.CCCCC4	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC1	O.CCCCC1	O.CCCCC1	-O.CCCCC2
295.00	977.10	O.CCCCC0	O.CCCCC1	O.CCCCC3	O.CCCCC1	C.CCCCC7	O.CCCCC8	O.CCCCC5	O.CCCCC2	O.CCCCC1	-O.CCCCC2
300.00	993.66	O.CCCCC0	O.CCCCC0	O.CCCCC3	O.CCCCC1	O.CCCCC7	O.CCCCC3	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC2
305.00	1010.23	O.CCCCC0	O.CCCCC0	C.CCCCC2	O.CCCCC1	O.CCCCC5	O.CCCCC2	O.CCCCC1	O.CCCCC1	O.CCCCC1	-O.CCCCC2
310.00	1026.79	O.CCCCC0	O.CCCCC0	C.CCCCC2	O.CCCCC0	O.CCCCC4	O.CCCCC3	O.CCCCC1	O.CCCCC1	O.CCCCC1	-O.CCCCC2
315.00	1043.35	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC7	O.CCCCC3	O.CCCCC1	O.CCCCC5	O.CCCCC9	O.CCCCC8	-O.CCCCC9
320.00	1059.91	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC5	O.CCCCC2	O.CCCCC1	O.CCCCC7	O.CCCCC1	O.CCCCC1	-O.CCCCC9
325.00	1076.47	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC4	O.CCCCC2	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
330.00	1093.03	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC3	O.CCCCC1	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
335.00	1109.59	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC3	O.CCCCC1	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
340.00	1126.15	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC2	O.CCCCC1	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
345.00	1142.71	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC2	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
350.00	1159.28	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
355.00	1175.84	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC6	O.CCCCC2	O.CCCCC1	O.CCCCC1	O.CCCCC1	-O.CCCCC9
360.00	1192.40	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC2	O.CCCCC1	O.CCCCC1	O.CCCCC1	-O.CCCCC9
365.00	1208.96	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
370.00	1225.52	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
375.00	1242.08	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
380.00	1258.64	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
385.00	1275.20	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
390.00	1291.76	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
395.00	1308.32	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
400.00	1324.89	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
405.00	1341.45	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
410.00	1358.01	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
415.00	1374.57	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
420.00	1391.13	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
425.00	1407.69	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
430.00	1424.25	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
435.00	1440.81	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
440.00	1457.37	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
445.00	1473.93	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
450.00	1490.50	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
455.00	1507.06	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
460.00	1523.62	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
465.00	1540.18	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
470.00	1556.74	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
475.00	1573.30	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
480.00	1589.86	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
485.00	1606.42	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
490.00	1622.98	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
495.00	1639.55	O.CCCCC0	O.CCCCC0	C.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9
500.00	1656.11	O.CCCCC0	O.CCCCC0	O.CCCCC1	O.CCCCC1	O.CCCCC0	O.CCCCC1	O.CCCCC6	O.CCCCC1	O.CCCCC1	-O.CCCCC9

TABLE OF RAW DATA BETWEEN TIME & MOISTURE IN CASE OF MIXTURE

TIME (MIN)	VALUE OF MOISTURE AT DISTANCE (CM) =								MEAN
	2.50000	7.50000	12.50000	17.50000	22.50000	27.50000	32.50000	37.50000	
0.00	1.65200	1.69800	1.65200	1.65200	1.64100	1.64100	1.64400	1.52400	1.65050
75.00	0.09700	0.48000	1.16600	1.46500	1.56500	1.59200	1.60100	1.54700	1.18912
150.00	0.02700	0.03200	0.09900	0.38800	0.93500	1.33900	1.49000	1.45600	0.72075
0.00	0.71400	0.71100	0.71400	0.71400	0.70700	0.70700	0.70900	0.69600	0.70900
75.00	0.03200	0.05500	0.10700	0.19600	0.33900	0.47700	0.58400	0.61200	0.30025
150.00	0.00200	0.00800	0.02600	0.01300	0.00500	0.02500	0.04800	0.13200	0.03287
0.00	0.02500	0.02800	0.02900	0.02900	0.02500	0.02500	0.02700	0.01900	0.02637
20.00	0.00700	0.00700	0.01100	0.01100	0.01100	0.01100	0.01300	0.01300	0.01050
40.00	0.00500	0.00200	0.00300	0.00500	0.00300	0.00700	0.00700	0.00500	0.00475
60.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

CC MIN= 2.85

TABLE OF DATA IN DIMENSIONLESS IN CASE OF MIXING

TIME(TIN)	TAU	VALUE OF FI AT ETA=								FI MEAN
	*	1.90876	5.72627	9.54378	13.36129	17.17879	20.99631	24.81381	28.63133	
0.00		0.42910	0.44104	0.42910	0.42910	0.42624	0.42624	0.42702	0.42192	0.42871
75.00		0.02520	0.12468	0.20286	0.28052	0.40650	0.41351	0.41585	0.41132	0.30887
150.00		0.00701	0.00821	0.02571	0.10078	0.24286	0.34780	0.38702	0.37119	0.18721
0.00		0.18546	0.18468	0.18546	0.18546	0.18364	0.18364	0.18416	0.13078	0.18416
75.00		0.00821	0.01425	0.02779	0.05091	0.08805	0.12390	0.15169	0.13196	0.07799
150.00		0.00052	0.00208	0.00675	0.00338	0.00130	0.00753	0.01247	0.03429	0.00854
0.00		0.00753	0.00727	0.00753	0.00753	0.00649	0.00649	0.00701	0.03414	0.00685
20.00		0.00182	0.00182	0.00286	0.00286	0.00286	0.00286	0.00338	0.03338	0.00273
40.00		0.00130	0.00078	0.00078	0.00130	0.00078	0.00182	0.00182	0.03130	0.00123
60.00		0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.03000	0.00000

VPINT= 2 TACI= 25.CCCCC XMIX= 45C.CCCCO FIX=UUUUUUUUU

***** MIXING EVERY 50.00 MIN *****

TABLE OF CALCULATION FOR PROFILE AFTER MIXING

THETA(MIN) *		TAU *		VALUE OF FI AT FTA=								
S/M	NONSUM*	SUM	NONSUM*	1.90876	5.72627	9.54378	13.36129	17.17979	20.99631	24.91381	28.63133	
0.00	0.00*	0.00	0.00*	0.42871	0.42871	0.42871	0.42871	0.42871	0.42871	0.42871	0.42871	
25.00	25.00*	82.81	82.81*	0.21815	0.26091	0.41358	0.42568	0.42811	0.42359	0.42363	0.42870	
50.00	50.00*	165.61	165.61*	0.08503	0.23994	0.37178	0.41630	0.42623	0.42822	0.42361	0.42869	
50.00	0.00*	165.61	0.00*	0.35276	0.35276	0.35276	0.35276	0.35276	0.35276	0.35276	0.35276	
75.00	25.00*	243.42	82.81*	0.16673	0.27342	0.32800	0.34597	0.35097	0.35229	0.35264	0.35273	
100.00	50.00*	331.22	165.61*	0.06219	0.15924	0.26804	0.32596	0.34538	0.35081	0.35225	0.35263	
100.00	0.00*	331.22	0.00*	0.27682	0.27682	0.27682	0.27682	0.27682	0.27682	0.27682	0.27682	
125.00	25.00*	414.03	82.81*	0.12090	0.19114	0.23951	0.26260	0.27171	0.27503	0.27520	0.27661	
150.00	50.00*	496.84	165.61*	0.04325	0.09621	0.16752	0.22565	0.25660	0.26944	0.27421	0.27591	
150.00	0.00*	496.84	0.00*	0.20094	0.20094	0.20094	0.20094	0.20094	0.20094	0.20094	0.20094	
175.00	25.00*	579.64	82.81*	0.08068	0.11875	0.15206	0.17485	0.18792	0.19468	0.19793	0.19956	
200.00	50.00*	662.45	165.61*	0.02774	0.05154	0.08565	0.12365	0.15574	0.17708	0.18311	0.19527	
200.00	0.00*	662.45	0.00*	0.12564	0.12564	0.12564	0.12564	0.12564	0.12564	0.12564	0.12564	
225.00	25.00*	745.25	82.81*	0.04617	0.06083	0.07571	0.08922	0.10020	0.10865	0.11455	0.11854	
250.00	50.00*	828.06	165.61*	0.01521	0.02201	0.03340	0.04637	0.06105	0.07592	0.08943	0.10044	
250.00	0.00*	828.06	0.00*	0.05561	0.05561	0.05561	0.05561	0.05561	0.05561	0.05561	0.05561	
275.00	25.00*	910.87	82.81*	0.01874	0.02146	0.02432	0.02725	0.03020	0.03309	0.03597	0.03843	
300.00	50.00*	993.67	165.61*	0.00602	0.00726	0.00870	0.01038	0.01229	0.01444	0.01683	0.01942	
300.00	0.00*	993.67	0.00*	0.01192	0.01192	0.01192	0.01192	0.01192	0.01192	0.01192	0.01192	
325.00	25.00*	1076.43	82.81*	0.00380	0.00392	0.00404	0.00416	0.00429	0.00441	0.00454	0.00467	
350.00	50.00*	1159.23	165.61*	0.00120	0.00125	0.00130	0.00135	0.00141	0.00147	0.00153	0.00159	
350.00	0.00*	1159.23	0.00*	0.00139	0.00139	0.00139	0.00139	0.00139	0.00139	0.00139	0.00139	
375.00	25.00*	1242.03	82.81*	0.00044	0.00044	0.00044	0.00044	0.00044	0.00044	0.00044	0.00044	
400.00	50.00*	1324.83	165.61*	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	
400.00	0.00*	1324.83	0.00*	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	0.00014	
425.00	25.00*	1407.70	82.81*	0.00004	0.00004	0.00004	0.00004	0.00004	0.00004	0.00004	0.00004	
450.00	50.00*	1490.51	165.61*	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	
450.00	0.00*	1490.51	0.00*	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	
475.00	25.00*	1573.31	82.81*	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
500.00	50.00*	1656.11	165.61*	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	



ภาคผนวก ก-2

ภาคผนวกนี้แสดงโปรแกรมคอมพิวเตอร์และลักษณะการกระจายความชื้นในชั้นผนังสำเร็จ
หนา 40 ซม. ของทั้งการคำนวณและการทดลองสำหรับกรณีการอบแห้งโดยลู่สับทิศทางลมร้อนเป็น
ครั้งคราว (ในที่นี้จะแสดงตัวอย่างของกรณีลู่สับทิศทางลมร้อนทุก ๆ 30 นาที)

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      *JLB      DBAL4444 KAMPFAT PHANARAYA
1  DIMENSION ETA(100),A(100),HJ(100),ATA(100),AEXP(20,10),BTA(100),FT
      *A(100)
C  AEXP(I,J)=VALUE OF MOISTURE CONTENT OF THE DRYING MATERIAL IN THE BED AT
C  DIFFERENT HEIGHT
C  CA=FINAL MOISTURE CONTENT(KG WATER/ KG DRY SOLID)
C  EC=EQUILIBRIUM MOISTURE CONTENT(KG WATER/KG DRY SOLID)
C  DEN=DENSITY (KG/CUBIC M)
C  AFSICN=FRACTION OF VOL OCCUPIED BY DRY MATERIAL IN PACKED BED
C  -1-(VOID FRACTION)
C  CC=CRITICAL MOISTURE CONTENT(KG WATER/KG DRY SOLID)
C  CCMASS=MASS TRANSFER COEFFICIENT(KG/CUBIC M*HR*DELTA H)
C  NPCINT=NUMBER OF COLUMN OF DATA (MOISTURE CONTENT) FROM THE LONG BED EXP
C  I-----REVERSE FLOW PLUS COLUMN OF TIME AND AVERAGE MOISTURE CONTENT
C  NATA=NUMBER OF ROW OF DATA(TIME) FROM THE LONG BED EXP( REVERSE FLOW)
C  ATA(J)=DISTANCE(CM) FROM THE EXP
C  BTA(J)=DISTANCE(CM) (USED IN THE CALCULATION)
C  FLOW=MASS FLOW RATE (KG DRY AIR/HR* SQUARE M)
C  LPCINT=NUMBER OF COLUMN OF DATA (MOISTURE CONTENT) FROM THE LONG BED EXP
C  I REVERSE FLOW PLUS COLUMN OF TIME
C  JPCINT=NUMBER OF DATA OF DISTANCE AT DIFFERENT HEIGHT OF BED
C  N=NUMBER OF MOISTURE CONTENT CALCULATED FROM THE NUMERICAL INTEGRATION
C  SN=NUMBER OF DEVICED INTERVAL IN THE NUMERICAL INTEGRATION
C  TS=TIME INTERVAL BEFORE EACH REVERSE DIRECTION OF AIR FLOW
C  TV=TIME INTERVAL ADDED TO INCREASE TIME INTERVAL BEFORE EACH REVERSE
C  DIRECTION OF AIR FLOW
C  TF=TIME INTERVAL OF EACH CALCULATION OF PROFILE OF MOISTURE CONTENT
C  PI=VALUE OF MOISTURE CONTENT OF AIR AT WET BULB TEMPERATURE MINUS VALUE OF
C  MOISTURE CONTENT OF AIR BEFORE ENTER THE BED
C  READ ALL DATA USED IN THE CALCULATION
2  READ(5,66) CB,EC,DEN,ETA,L,AFSICN,CC
3  66 FORMAT(8F10.5)
4  READ(5,222) CCMASS,NPCINT,NATA
5  222 FORMAT(F15.5,2I10)
6  READ(5,181) FLOW,LPCINT,JPCINT
7  181 FORMAT(F8.4,2I10)
8  READ(5,161)(ATA(J),J=2,NPCINT)
9  161 FORMAT(10F5.3)
10 READ(5,171)(BTA(J),J=1,JPCINT)
11 171 FORMAT(16F5.3)
12 READ(5,150)((AEXP(I,J),J=1,LPCINT),I=1,NATA)
13 150 FORMAT(9F8.4)
14 WRITE(6,101)
15 101 FORMAT(1H1)
16 WRITE(6,67) CB,EC,DEN,ETA,L,AFSICN,CC
17 67 FORMAT(/2X,'CB=',F10.5,2X,'EC=',F10.5,2X,'DEN=',F10.2,2X,'ETA=',F
      *10.5//2X,'AFSICN=',F10.5,2X,'CC=',F10.5)
18 WRITE(6,223) CCMASS,NPCINT,NATA
19 223 FORMAT(/2X,'CCMASS=',F12.2,2X,'NPCINT=',110,2X,'NATA=',110)
20 WRITE(6,182) FLOW,LPCINT,JPCINT
21 182 FORMAT(/2X,'MASS FLOW RATE=',F10.2,2X,'LPCINT=',110,2X,'JPCINT=',1
      *10)
22 READ(5,40) N,SN,TS,TV,PI,TF
23 40 FORMAT(110,5F10.5)
24 WRITE(6,73) N,SN,TS,TV,PI,TF
25 73 FORMAT(/2X,'N=',110,2X,'SN=',F10.5,2X,'TS=',F10.2,2X,'TV=',F10.2//
      *2X,'PI=',F10.5,2X,'TF=',F10.5)
C  WRITE(6,SHCW) DATA FROM THE EXPERIMENT IN CASE OF REVERSE FLOW
26 5 WRITE(6,101)
27 WRITE(6,151)(ATA(J),J=2,NPCINT)

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28 151 FORMAT(50X,'TABLE OF RAW DATA BETWEEN TIME(MIN) IN CASE OF REV
*ERSE FLOW'///2X,'TIME(MIN) * * *',3X,'VALUE OF MOISTURE
*AT DISTANCE(CM)=' ,2X,'MEAN'///25X,'*',2X,8F10.5///)
29 DO 152 I=1,NATA
30 AEXP(I,NPCINT)=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+
*AEXP(I,7)+AEXP(I,8)+AEXP(I,9))/8.
31 152 CONTINUE
32 WRITE(6,153)((AEXP(I,J),J=1,NPCINT),I=1,NATA)
33 153 FORMAT(2X,F7.2,19X,9F10.5)
C WRITE$SHOW DATA IN DIMENSIONLESS FORM IN CASE OF REVERSE FLOW
34 DO 154 I=1,NATA
35 DO 154 J=2,NPCINT
36 AEXP(I,J)=(AEXP(I,J))/CC
37 154 CONTINUE
38 ACA=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+AEXP(I,7)+
*AEXP(I,8)+AEXP(I,9))/8.
39 DO 155 J=3,NPCINT
40 ETA(J)=ATA(J)*CCMASS/100./FLOW
41 155 CONTINUE
42 WRITE(6,101)
43 DO 157 I=1,NATA
44 AEXP(I,NPCINT)=(AEXP(I,2)+AEXP(I,3)+AEXP(I,4)+AEXP(I,5)+AEXP(I,6)+
*AEXP(I,7)+AEXP(I,8)+AEXP(I,9))/8.
45 157 CONTINUE
46 WRITE(6,158)(ETA(J),J=3,NPCINT)
47 158 FORMAT(/50X,'TABLE OF DATA IN DIMENSIONLESS IN CASE OF REVERSE FLOW
*W'///2X,'TIME(MIN) TAU *',25X,'VALUE OF FI AT ETA=' ,32X,'FI
* MEAN'///25X,'*',8F10.5///)
48 WRITE(6,159)((AEXP(I,J),J=1,NPCINT),I=1,NATA)
49 159 FORMAT(2X,F7.2,17X,9F10.5)
50 CA=(ACA*CC)
C PROGRAM TO CALCULATE PROFILE OF MOISTURE IN THROUGH FLOW DRYER
51 FIGNA=(CA-EC)/(CC-EC)
52 FICFF=(CB-EC)/(CC-EC)
53 WRITE(6,131) FIGNA,FICFF
54 131 FORMAT(/2X,'FIGNA=',F10.5,2X,'FICFF=',F10.5)
C WRITE TYPING OF CALATION FOR PROFILE
55 DO 401 J=1,JPCINT
56 FTA(J)=BTA(J)*CCMASS/100./FLOW
57 401 CONTINUE
58 WRITE(6,120)(FTA(J),J=1,8)
59 120 FORMAT(/50X,'TABLE OF CALCULATION FOR PROFILE'///2X,'TIME(MIN) *
* TAU *',30X,'VALUE OF FI AT ETA ='///25X,'*',2X,10F10.5///)
60 WRITE(6,627)(FTA(J),J=9,JPCINT)
61 627 FORMAT(25X,'*',2X,10F10.5///)
62 TUS=CCMASS*TS/(AFSICN*DEN*(CC-EC)*60.)
63 TUV=CCMASS*TV/(AFSICN*DEN*(CC-EC)*60.)
64 TUE=CCMASS*TF/(AFSICN*DEN*(CC-EC)*60.)
65 H=ETAL/SN
66 31 WRITE(6,185)
67 185 FORMAT(2X,'DIRECTION OF FLOW IS FORWARD')
68 TTF=0.
69 20 TUT=0.
70 TG=0.
71 42 W=EXP(PI*TUT)
72 I=1
73 SS=0.0
74 45 S=(SS*H)
75 A(I)=FIGNA*(EXP(FIGNA*S))/(W+EXP(FIGNA*S)-1)
76 SS=SS+1.

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77      I=I+1
78      IF(I.GT.N) GO TO 46
79      GO TO 45
-----
80      46 WRITE(6,96) TG,TUT,A(1),A(3),A(5),A(7),A(9),A(11),A(13),A(15)
81      96 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
-----
82      47 WRITE(6,91) TG,TUT,A(17),A(19),A(21),A(23),A(25),A(27),A(29),A(31)
83      *,A(33)
84      91 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
85      TUT=TUT+TUF
-----
86      TG=TG+TF
87      IF(TUT.GT.TUS) GO TO 308
88      GO TO 42
-----
89      308 TTG=TG+TTF-TF
90      WRITE(6,711) TTG
91      711 FORMAT(55X,'ACCUMULATE TIME (MIN) ',F10.2)
-----
92      311 WRITE(6,11)
93      11 FORMAT(//2X,'DIRECTION OF FLOW IS BACKWARD')
94      TUT=0.
95      TG=0.
96      WRITE(6,15) TG,TUT,A(1),A(3),A(5),A(7),A(9),A(11),A(13),A(15)
97      15 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
-----
98      WRITE(6,37) TG,TUT,A(17),A(19),A(21),A(23),A(25),A(27),A(29),A(31)
99      *,A(33)
100     37 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
-----
101     559 TTG=TG+TTF-TF
102     WRITE(6,901) TTG
103     901 FORMAT(55X,'ACCUMULATE TIME (MIN) = ',F10.2)
-----
104     100 FORMAT(//2X,'DIRECTION OF FLOW IS BACKWARD')
105     TUT=0.
106     TG=0.
107     WRITE(6,500) TG,TUT,A(1),A(3),A(5),A(7),A(9),A(11),A(13),A(15)
108     500 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
-----
109     WRITE(6,503) TG,TUT,A(17),A(19),A(21),A(23),A(25),A(27),A(29),A(31)
110     *,A(33)
111     503 FORMAT(2X,F10.4,4X,F10.4,2X,1CF10.5)
112     TUT=TUF
113     TG=TF
-----
114     78 W=EXP(-PI*TUT)
115     I=N
116     FL=A(N)
117     CB=FL/W
118     HJ(N)=CB
119     I=N-1
-----
120     D=0.
121     E=1.
122     Y=A(N)
123     75 AJ=(A(I)+Y)*(H/2.)
124     Y=A(I)
-----
125     D=D+AJ
126     U=EXP(D)
127     V=(U+E)*(H/2.)
-----
128     E=U
129     D=D+V
130     HJ(I)=U/((W/FL)+C)
-----
131     IF(I.EQ.1) GO TO 85
132     I=I-1
133     GO TO 75

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134      85 WRITE(6,104) TG,TUT,HJ(1),HJ(3),HJ(5),HJ(7),HJ(9),HJ(11),HJ(13),HJ
      *(15)
135      104 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
136      WRITE(6,112) TG,TUT,HJ(17),HJ(19),HJ(21),HJ(23),HJ(25),HJ(27),HJ(2
      *9),HJ(31),HJ(33)
137      112 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
138      TUT=TUT+TUF
139      TG=TG+TF
140      IF(TUT.GT.TUS) GO TO 92
141      GO TO 70
142      92 Z=0/ETAL
143      IF(Z.LT.FICFF) GO TO 95
144      GO TO 751
145      95 WRITE(6,89)
146      95 FORMAT(50X,RF-FINISHED//)
147      TUS=TUS+TUV
148      IF(TUS.GT.496.83) GO TO 107
149      GO TO 31
150      751 TTF=TG+TTG-TF
151      WRITE(6,721) TTF
152      721 FORMAT(55X,'ACCUMULATE TIME (MIN) ',F10.2)
153      102 WRITE(6,185)
154      TUT=0.
155      TG=0.
156      WRITE(6,500) TG,TUT,HJ(1),HJ(3),HJ(5),HJ(7),HJ(9),HJ(11),HJ(13),HJ
      *(15)
157      500 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
158      WRITE(6,611) TG,TUT,HJ(17),HJ(19),HJ(21),HJ(23),HJ(25),HJ(27),HJ(2
      *9),HJ(31),HJ(33)
159      611 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
160      TUT=TUF
161      TG=TF
162      111 W=EXP(PI*TUT)
163      I=1
164      FL=HJ(1)
165      CB=FL/W
166      A(1)=CB
167      I=2
168      D=C.
169      E=1.
170      D=C.
171      Y=HJ(1)
172      121 AJ=(4J(I)+Y)*(H/2.)
173      Y=HJ(I)
174      D=C+AJ
175      U=EXP(D)
176      V=(U+E)*(H/2.)
177      E=U
178      D=D+V
179      A(I)=U/((W/FL)+D)
180      IF(I.EQ.N) GO TO 190
181      I=I+1
182      GO TO 121
183      190 WRITE(6,138) TG,TUT,A(1),A(3),A(5),A(7),A(9),A(11),A(13),A(15)
184      138 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
185      WRITE(6,647) TG,TUT,A(17),A(19),A(21),A(23),A(25),A(27),A(29),A(31
      *),A(33)
186      647 FORMAT(2X,F10.4,4X,F10.4,2X,10F10.5)
187      TUT=TUT+TUF
188      TG=TG+TF

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189 IF(TUT.GT.TUS) GC TC 140
190 GO TO 111
191 14C Z=C/ETAL
192 IF(Z:LT:FICFF) GC TC 95
193 GO TO 550
194 1G7 STGP
195 END
SENTRY



C3= 0.0010 EC= 0.00000 DEN= 924.12 ETAL= 30.53000

AFSTON= 0.23000 CC= 3.85000

CJMASS= 162626.00 NPDINT= 10 NATA= 20

MASS FLOW RATE= 2130.00 LPCINT= 5 JPCINT= 17

N= 53 SN= 32.00000 TS= 30.00 TV= 30.00

PI= 0.01400 TF= 10.00000

TABLE OF RAW DATA BETWEEN TIME & MOISTURE IN CASE OF REVERSE FLOW

TIME (MIN)	VALUE OF MOISTURE AT DISTANCE (CM) =									MEAN
	*	*	*	*	*	*	*	*	*	
	2.50000	7.50000	12.50000	17.50000	22.50000	27.50000	32.50000	37.50000		
0.00	1.84100	1.81900	1.82500	1.82500	1.82100	1.82100	1.81800	1.92100	1.92375	
30.00	0.75000	1.54200	1.75600	1.79900	1.81200	1.81700	1.81000	1.79500	1.63512	
60.00	0.72400	1.48500	1.72200	1.77100	1.77500	1.74100	1.53900	0.77700	1.44175	
90.00	0.15700	0.76400	1.42900	1.58400	1.73500	1.71200	1.51000	0.74500	1.21825	
120.00	0.02300	0.71000	1.29700	1.64800	1.66400	1.51200	0.90400	0.19100	1.00625	
150.00	0.02800	0.19900	0.81400	1.42400	1.57900	1.47300	0.53400	0.23400	0.78562	
180.00	0.09500	0.22100	0.75900	1.37200	1.46700	1.10300	0.32600	0.03300	0.67325	
210.00	0.01600	0.03900	0.22800	0.84800	1.27600	1.02900	0.32600	0.11900	0.48637	
240.00	0.07700	0.10500	0.22800	0.72700	0.89800	0.43200	0.06500	0.01900	0.32000	
270.00	0.01500	0.02500	0.24700	0.32600	0.63700	0.37500	0.10800	0.01200	0.22497	
300.00	0.03700	0.02700	0.05900	0.16100	0.24400	0.09400	0.01500	0.01200	0.08237	
330.00	0.00500	0.02900	0.05200	0.02900	0.06300	0.03400	0.01500	0.01200	0.03250	
360.00	0.00500	0.00500	0.00500	0.00900	0.00000	0.00000	0.00000	0.00000	0.00300	
390.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
420.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
450.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
480.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
510.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
540.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
570.00	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	

TABLE OF DATA IN DIMENSIONLESS IN CASE OF REVERSE FLJ4

TIME (MIN)	TAU	VALUE OF FI AT ETA =										FI MEAN
	*	1.90876	5.72627	9.54278	13.36129	17.17879	20.99631	24.81381	28.63133			
0.00		C.47818	0.47221	C.47403	C.47403	0.47299	0.47299	0.47221	0.47299	0.47370		
30.00		C.19481	0.40052	C.45610	C.46727	0.47065	0.47195	0.47013	0.46523	0.42471		
50.00		C.18805	C.38571	0.44727	C.46000	0.46104	0.45221	0.39974	0.20182	0.37448		
70.00		0.04078	0.19844	C.27377	C.43740	0.45065	0.44468	0.39221	0.13351	0.31643		
120.00		0.00597	0.18442	C.26296	C.42805	C.42221	C.39299	0.23481	0.04951	0.26136		
150.00		C.C0727	C.C5169	C.21143	C.36987	0.41013	C.38260	0.13870	0.05079	0.20406		
170.00		C.C2571	0.C5740	0.19714	C.35636	0.28104	0.28649	0.08468	0.01013	0.17487		
210.00		C.C0416	0.C1013	C.C6182	C.22026	C.23143	0.26727	0.08468	C.03091	0.12633		
240.00		C.C2000	0.C2727	C.C6182	C.18882	C.23325	0.11221	0.01688	0.00469	0.09312		
270.00		C.C0390	0.C0649	C.C6416	C.C8468	0.16545	0.C9740	0.02805	0.01714	0.05841		
300.00		C.C0961	0.C0961	C.C1532	0.C4182	C.C6338	0.C2442	0.00390	0.00312	0.02140		
330.00		C.C0130	0.C1013	C.C1377	C.C1013	0.01636	0.C0883	0.00390	0.00312	0.03844		
360.00		C.C0130	0.C0130	C.C0130	C.C0234	C.C0000	0.C0000	0.00000	0.00000	0.00078		
370.00		C.C0000	0.C0000	0.00000	0.00000	C.C0000	0.C0000	0.00000	0.00000	0.00000		
420.00		C.C0000	C.C0000	C.C0000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
450.00		C.C0000	0.C0000	C.C0000	C.C0000	0.00000	0.C0000	0.00000	0.00000	0.00000		
490.00		C.C0000	0.00000	0.00000	C.C0000	C.C0000	0.C0000	0.00000	0.00000	0.00000		
510.00		C.C0000	0.C0000	C.C0000	C.C0000	C.C0000	C.C0000	0.00000	0.00000	0.00000		
540.00		C.C0000	0.00000	0.00000	0.00000	C.C0000	0.C0000	0.00000	0.00000	0.00000		
570.00		C.C0000	0.00000	C.C0000	C.C0000	C.C0000	0.C0000	0.00000	0.00000	0.00000		

FI04 = 0.47370 FI0FF = C.C0000

TABLE OF CALCULATION FOR PROFILE

TIME (MIN)	* TAU *	VALUE OF FI AT ETA =									
	*	C.C0000	1.90876	3.81751	5.72627	7.63502	9.54378	11.45253	13.36129		
	*	15.27005	17.17879	19.08755	20.99631	22.90506	24.81381	26.72253	28.63133	30.54008	
DIRECTION OF FLOW IS FORWARD											
0.0000	0.0000	C.47370	C.47370	0.47370	C.47370	C.47370	C.47370	0.47370	0.47370	0.47370	
0.0000	0.0000	0.47370	C.47370	C.47370	C.47370	C.47370	C.47370	0.47247	0.47320		
10.0000	33.1220	C.29793	C.28235	C.43191	C.45584	C.46630	C.47067	0.47370	0.47370	0.47370	
10.0000	33.1220	C.47350	0.47362	C.47367	C.47369	C.47370	C.47370	0.47370	0.47370	0.47370	
20.0000	66.2441	0.19738	C.29262	C.27877	C.43005	0.45500	0.46594	0.47053	0.47241		
20.0000	66.2441	0.47318	C.47349	C.47361	C.47367	C.47369	C.47369	0.47370	0.47370	0.47370	
30.0000	99.3661	0.11785	C.21311	C.31681	C.39456	0.43811	0.45861	0.46747	0.47116		
30.0000	99.3661	0.47267	C.47328	C.47353	C.47362	C.47367	C.47369	0.47370	0.47370	0.47370	
											ACCUMULATE TIME (MIN) = 30.00

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	C.11785	C.21311	C.31681	C.39456	0.43811	C.45861	0.46747	0.47116		
0.0000	0.0000	C.47267	C.47328	C.47353	C.47362	0.47367	C.47369	0.47370	0.47370	0.47370	
10.0000	33.1220	0.25528	C.32420	C.38583	C.42695	C.44864	C.45857	0.46280	0.45431		
10.0000	33.1220	C.46512	C.46512	0.46456	C.46292	C.45882	C.44899	0.42637	0.37926	0.29793	
20.0000	66.2441	C.25528	C.32420	C.38583	C.42695	C.44862	C.45855	0.46275	0.45439		

20.0000	66.2441	0.46481	0.46437	0.46268	0.45835	0.44788	0.42395	0.37452	0.29031	0.18738
30.0000	99.3661	0.25528	0.32420	0.38583	0.42694	0.44862	0.45852	0.46267	0.46419	
30.0000	99.3661	0.46431	0.46316	0.45972	0.45125	0.43151	0.38942	0.31383	0.21214	0.11785

ACCUMULATE TIME (MIN) = 60.00

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	0.25528	0.32420	0.38583	0.42694	0.44862	0.45852	0.46267	0.46419	
0.0000	0.0000	0.46431	0.46216	0.45972	0.45125	0.43151	0.38942	0.31383	0.21214	0.11785
10.0000	33.1220	0.16056	0.19811	0.25335	0.31754	0.37434	0.41358	0.43617	0.44771	
10.0000	33.1220	0.45206	0.45498	0.45449	0.45097	0.44169	0.42097	0.38135	0.32147	0.25389
20.0000	66.2441	0.10098	0.13962	0.19924	0.27461	0.34668	0.39880	0.42921	0.44435	
20.0000	66.2441	0.45176	0.45444	0.45427	0.45087	0.44165	0.42095	0.38135	0.32147	0.25389
30.0000	99.3661	0.06351	0.09502	0.14874	0.22603	0.31024	0.37736	0.41853	0.43933	
30.0000	99.3661	0.44571	0.45355	0.45391	0.45073	0.44159	0.42093	0.38134	0.32145	0.25389

ACCUMULATE TIME (MIN) = 90.00

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	0.06351	0.09502	0.14874	0.22603	0.31024	0.37736	0.41853	0.43933	
0.0000	0.0000	0.44571	0.45359	0.45391	0.45073	0.44159	0.42093	0.38134	0.32145	0.25389
10.0000	33.1220	0.17028	0.21050	0.26211	0.32007	0.37252	0.40954	0.43043	0.43933	
10.0000	33.1220	0.44234	0.43897	0.42841	0.40660	0.36847	0.31328	0.25073	0.19671	0.15968
20.0000	66.2441	0.17027	0.21050	0.26211	0.32005	0.37248	0.40943	0.43017	0.43933	
20.0000	66.2441	0.44097	0.43576	0.42122	0.39155	0.34066	0.27046	0.19697	0.13934	0.10043
30.0000	99.3661	0.17027	0.21049	0.26209	0.32001	0.37241	0.40927	0.42979	0.43947	
30.0000	99.3661	0.43879	0.43076	0.41027	0.36580	0.30416	0.22217	0.14685	0.09424	0.06317

ACCUMULATE TIME (MIN) = 120.00

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	0.17027	0.21049	0.26209	0.32001	0.37241	0.40927	0.42979	0.43947	
0.0000	0.0000	0.43879	0.43076	0.41027	0.36580	0.30416	0.22217	0.14685	0.09424	0.06317
10.0000	33.1220	0.10709	0.12345	0.14923	0.18834	0.24164	0.30188	0.35565	0.39353	
10.0000	33.1220	0.41493	0.42266	0.41836	0.40025	0.36518	0.31463	0.25847	0.20823	0.16885
20.0000	66.2441	0.06735	0.08378	0.10932	0.14854	0.20564	0.27356	0.33722	0.39343	
20.0000	66.2441	0.40999	0.40241	0.41737	0.39982	0.36495	0.31455	0.25845	0.20921	0.16884
30.0000	99.3661	0.04236	0.05544	0.07670	0.11177	0.16626	0.23806	0.31154	0.36841	
30.0000	99.3661	0.40238	0.41689	0.41581	0.39514	0.36470	0.31442	0.25839	0.20819	0.16882

ACCUMULATE TIME (MIN) = 150.00

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	0.04236	0.05544	0.07670	0.11177	0.16626	0.23806	0.31154	0.36841	
0.0000	0.0000	0.40238	0.41689	0.41581	0.39514	0.36470	0.31442	0.25839	0.20819	0.16882
10.0000	33.1220	0.12567	0.14866	0.17912	0.21879	0.26706	0.31791	0.36063	0.39637	
10.0000	33.1220	0.39251	0.37879	0.34504	0.29421	0.23651	0.18521	0.14735	0.12222	0.10618
20.0000	66.2441	0.12564	0.14862	0.17905	0.21867	0.26681	0.31740	0.35949	0.39316	
20.0000	66.2441	0.38730	0.36822	0.32631	0.26584	0.20074	0.14616	0.10779	0.08233	0.06678
30.0000	99.3661	0.12559	0.14655	0.17894	0.21846	0.26642	0.31659	0.35774	0.38016	
30.0000	99.3661	0.37930	0.35282	0.30038	0.23050	0.16182	0.10947	0.07554	0.05433	0.04200

ACCUMULATE TIME (MIN) = 180.00

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	0.12559	0.14855	0.17894	0.21846	0.26642	0.31659	0.35774	0.38016	
0.0000	0.0000	0.37930	0.35282	0.30038	0.23050	0.16182	0.10947	0.07554	0.05433	0.04200
10.0000	33.1220	0.07899	0.08748	0.09991	0.11842	0.14604	0.18557	0.23593	0.29323	
10.0000	33.1220	0.32818	0.34491	0.33454	0.30155	0.25680	0.21236	0.17502	0.14514	0.12379
20.0000	66.2441	0.04968	0.05819	0.07031	0.08824	0.11538	0.15548	0.20895	0.25713	
20.0000	66.2441	0.31471	0.23770	0.23071	0.20957	0.25586	0.21186	0.17473	0.14577	0.12368
30.0000	99.3661	0.03125	0.03797	0.04779	0.06280	0.08650	0.12261	0.17682	0.23717	
30.0000	99.3661	0.29544	0.32595	0.32481	0.29673	0.25427	0.21107	0.17423	0.14519	0.12349

ACCUMULATE TIME (MIN) = 210.00

DIRECTION OF FLOW IS BACKWARD										
0.0000	0.0000	C.03125	C.03797	C.04779	C.06280	C.08650	C.12361	C.17692	C.23937	
0.0000	0.0000	C.29544	C.32599	C.32481	C.29673	C.25437	C.21107	C.17423	C.14549	0.12349
10.0000	33.1220	C.09700	C.11067	C.12802	C.15019	C.17821	C.21177	C.24675	C.27315	
10.0000	33.1220	C.27848	C.25759	C.21840	C.17583	C.14053	C.11508	C.09769	C.08534	0.07767
20.0000	66.2441	C.09671	C.11026	C.12742	C.14920	C.17676	C.20928	C.24230	C.26512	
20.0000	66.2441	C.26482	C.23705	C.19205	C.14648	C.11055	C.08550	C.06961	C.05735	0.04885
30.0000	99.3661	C.05625	C.10962	C.12651	C.14790	C.17451	C.20545	C.23553	C.25327	
30.0000	99.3661	C.24566	C.21038	C.16114	C.11576	C.08256	C.06069	C.04657	C.03720	0.03072

ACCUMULATE TIME (MIN) 240.00

DIRECTION OF FLOW IS FORWARD										
0.0000	0.0000	C.09625	C.10962	C.12651	C.14790	C.17451	C.20545	C.23553	C.25327	
0.0000	0.0000	C.24566	C.21038	C.16114	C.11576	C.08256	C.06069	C.04657	C.03720	0.03072
10.0000	33.1220	C.06054	C.06532	C.07176	C.08059	C.09285	C.10993	C.13287	C.16033	
10.0000	33.1220	C.18568	C.19866	C.19419	C.17704	C.15553	C.13505	C.11755	C.10316	0.09143
20.0000	66.2441	C.03807	C.04288	C.04918	C.05768	C.06947	C.08606	C.10891	C.13749	
20.0000	66.2441	C.16592	C.18356	C.18283	C.17021	C.15118	C.13217	C.11557	C.10175	0.09039
30.0000	99.3661	C.02395	C.02773	C.03278	C.03973	C.04961	C.06297	C.08464	C.11210	
30.0000	99.3661	C.14191	C.16377	C.16945	C.16061	C.14474	C.12783	C.11255	C.09939	0.08878

ACCUMULATE TIME (MIN) = 270.00

DIRECTION OF FLOW IS BACKWARD										
0.0000	0.0000	C.02395	C.02773	C.03278	C.03973	C.04961	C.06297	C.08464	C.11210	
0.0000	0.0000	C.14191	C.16277	C.16945	C.16061	C.14474	C.12783	C.11255	C.09939	0.08978
10.0000	33.1220	C.06888	C.07522	C.08253	C.09088	C.10017	C.10989	C.11874	C.12427	
10.0000	33.1220	C.12366	C.11607	C.10407	C.09144	C.08048	C.07175	C.06501	C.05933	0.05584
20.0000	66.2441	C.06654	C.07221	C.07884	C.08612	C.09394	C.10165	C.10785	C.11024	
20.0000	66.2441	C.10648	C.09648	C.08321	C.07022	C.05935	C.05093	C.04426	C.03915	0.03512
30.0000	99.3661	C.06313	C.06811	C.07260	C.07950	C.08549	C.09083	C.09415	C.09347	
30.0000	99.3661	C.08722	C.07607	C.06310	C.05129	C.04187	C.03473	C.02935	C.02526	0.02209

ACCUMULATE TIME (MIN) 300.00

DIRECTION OF FLOW IS FORWARD										
0.0000	0.0000	C.06212	C.06811	C.07360	C.07950	C.08549	C.09083	C.09415	C.09347	
0.0000	0.0000	C.09722	C.07607	C.06310	C.05129	C.04187	C.03473	C.02935	C.02526	0.02209
10.0000	33.1220	C.03970	C.04164	C.04392	C.04663	C.04978	C.05339	C.05732	C.06126	
10.0000	33.1220	C.06458	C.06660	C.06694	C.06575	C.06350	C.06067	C.05760	C.05432	0.05155
20.0000	66.2441	C.02497	C.02693	C.02922	C.03190	C.03503	C.03864	C.04269	C.04639	
20.0000	66.2441	C.05078	C.05372	C.05528	C.05545	C.05454	C.05294	C.05093	C.04910	0.04661
30.0000	99.3661	C.01571	C.01725	C.01907	C.02124	C.02382	C.02685	C.03035	C.03415	
30.0000	99.3661	C.03790	C.04109	C.04325	C.04439	C.04455	C.04403	C.04306	C.04133	0.04046

ACCUMULATE TIME (MIN) = 330.00

DIRECTION OF FLOW IS BACKWARD										
0.0000	0.0000	C.01571	C.01725	C.01907	C.02124	C.02382	C.02685	C.03035	C.03415	
0.0000	0.0000	C.03790	C.04109	C.04325	C.04439	C.04455	C.04403	C.04306	C.04133	0.04046
10.0000	33.1220	C.02879	C.02949	C.03016	C.03076	C.03126	C.03153	C.03182	C.03130	
10.0000	33.1220	C.02152	C.03104	C.03036	C.02957	C.02871	C.02785	C.02700	C.02620	0.02544
20.0000	66.2441	C.02326	C.02357	C.02382	C.02399	C.02406	C.02401	C.02379	C.02340	
20.0000	66.2441	C.02284	C.02210	C.02125	C.02034	C.01940	C.01848	C.01761	C.01679	0.01600
30.0000	99.3661	C.01782	C.01787	C.01786	C.01778	C.01762	C.01735	C.01693	C.01647	
30.0000	99.3661	C.01587	C.01516	C.01439	C.01359	C.01280	C.01205	C.01133	C.01057	0.01007

ACCUMULATE TIME (MIN) 360.00

DIRECTION OF FLOW IS FORWARD										
0.0000	0.0000	C.01782	C.01787	C.01786	C.01778	C.01762	C.01735	C.01693	C.01649	
0.0000	0.0000	C.01597	C.01516	C.01439	C.01359	C.01280	C.01205	C.01133	C.01057	0.01007
10.0000	33.1220	C.01121	C.01135	C.01149	C.01163	C.01176	C.01189	C.01201	C.01212	
10.0000	33.1220	C.01221	C.01229	C.01234	C.01238	C.01240	C.01240	C.01233	C.01235	0.01231
20.0000	66.2441	C.00705	C.00719	C.00734	C.00749	C.00763	C.00778	C.00792	C.00805	



20.0000	66.2441	C.C0818	C.C0829	C.C0839	C.00848	C.C0856	C.C0862	0.C0857	0.00514	0.00525	0.00874
30.0000	99.3661	0.C0443	C.C0455	G.00466	0.00478	C.C0490	C.00502	0.C0514	0.00587	0.00593	0.00598
30.0000	99.3661	0.C0556	C.00547	C.C0556	0.C0565	C.00573	C.C0581	0.00587	0.00593	0.00593	0.00598
ACCUMULATE TIME (MIN) = 390.00											

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	C.C0443	C.C0455	C.C0466	0.00478	C.C0490	C.00502	0.C0514	0.00587	0.00593	0.00598
0.0000	0.0000	C.C0536	C.C0547	C.C0556	0.00565	0.00573	C.C0581	0.00587	0.00593	0.00593	0.00598
10.0000	33.1220	C.C0393	C.C0393	G.C0392	C.C0392	0.00391	C.C0390	0.00389	0.00389	0.00389	0.00376
10.0000	33.1220	0.00387	C.00386	0.00385	C.C0383	0.00382	C.C0381	0.00379	0.00379	0.00379	0.00376
20.0000	66.2441	C.C0258	C.00257	G.C0256	C.00255	0.00254	C.C0253	0.00251	0.00251	0.00251	0.00237
20.0000	66.2441	0.00249	C.C0247	C.00246	0.00244	0.00243	C.C0241	0.00240	0.00240	0.00240	0.00237
30.0000	99.3661	C.C0167	C.C0166	C.C0165	0.00164	0.00163	C.C0162	0.00161	0.00161	0.00161	0.00149
30.0000	99.3661	C.00159	C.C0157	C.C0156	C.00155	0.00154	C.C0153	0.00151	0.00151	0.00151	0.00149
ACCUMULATE TIME (MIN) = 420.00											

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	C.C0167	C.C0166	0.00165	C.C0164	0.00163	C.C0162	0.C0161	0.00151	0.00151	0.00149
0.0000	0.0000	0.C0159	C.C0157	C.C0156	C.00155	0.00154	C.C0153	0.00151	0.00151	0.00151	0.00149
10.0000	33.1220	0.C0105	0.C0105	C.C0105	C.00105	0.00105	C.C0105	0.00105	0.00105	0.00105	0.00107
10.0000	33.1220	0.C0106	C.00106	0.00106	C.00106	0.00106	C.C0106	0.00106	0.00106	0.00106	0.00107
20.0000	66.2441	0.00066	C.C0066	C.C0066	0.00066	0.00066	C.C0067	0.C0067	0.00067	0.00067	0.00068
20.0000	66.2441	0.C0067	C.00067	C.C0067	C.00067	0.00067	C.C0067	0.00067	0.00067	0.00067	0.00068
30.0000	99.3661	C.C0041	0.00042	C.C0042	C.00042	0.00042	C.C0042	0.00042	0.00042	0.00042	0.00043
30.0000	99.3661	0.C0042	C.00042	0.00042	0.C0043	0.00043	C.C0043	0.00043	0.00043	0.00043	0.00043
ACCUMULATE TIME (MIN) = 450.00											

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	C.C0041	C.C0042	0.00042	C.C0042	0.00042	C.C0042	0.00042	0.00043	0.00043	0.00043
0.0000	0.0000	C.C0042	0.C0042	C.C0042	C.00043	0.00043	C.C0043	0.00043	0.00043	0.00043	0.00043
10.0000	33.1220	C.C0027	C.C0027	C.C0027	C.00027	0.00027	C.C0027	0.00027	0.00027	0.00027	0.00027
10.0000	33.1220	C.C0027	C.C0027	C.C0027	C.00027	0.00027	C.C0027	0.00027	0.00027	0.00027	0.00027
20.0000	66.2441	C.C0017	C.C0017	C.C0017	C.00017	0.00017	C.C0017	0.00017	0.00017	0.00017	0.00017
20.0000	66.2441	C.C0017	C.C0017	C.C0017	C.00017	0.00017	C.C0017	0.00017	0.00017	0.00017	0.00017
30.0000	99.3661	0.C0011	C.C0011	0.00011	C.C0011	0.00011	C.C0011	0.00011	0.00011	0.00011	0.00011
30.0000	99.3661	C.C0011	C.C0011	0.00011	C.C0011	0.00011	C.C0011	0.00011	0.00011	0.00011	0.00011
ACCUMULATE TIME (MIN) = 480.00											

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	0.C0011	C.C0011	0.00011	C.C0011	0.00011	C.C0011	0.00011	0.00011	0.00011	0.00011
0.0000	0.0000	0.C0011	C.C0011	0.00011	C.C0011	0.00011	C.C0011	0.00011	0.00011	0.00011	0.00011
10.0000	33.1220	C.C0007	C.C0007	C.C0007	C.00007	0.00007	C.C0007	0.00007	0.00007	0.00007	0.00007
10.0000	33.1220	0.C0007	C.C0007	C.C0007	C.00007	0.00007	C.C0007	0.00007	0.00007	0.00007	0.00007
20.0000	66.2441	0.C0004	C.C0004	C.C0004	C.00004	0.00004	C.C0004	0.00004	0.00004	0.00004	0.00004
20.0000	66.2441	0.C0004	C.C0004	C.C0004	C.00004	0.00004	C.C0004	0.00004	0.00004	0.00004	0.00004
30.0000	99.3661	0.C0003	C.C0003	C.C0003	C.00003	0.00003	C.C0003	0.00003	0.00003	0.00003	0.00003
30.0000	99.3661	C.C0003	C.C0003	C.C0003	C.00003	0.00003	C.C0003	0.00003	0.00003	0.00003	0.00003
ACCUMULATE TIME (MIN) = 510.00											

DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	C.C0003	C.C0003	C.C0003	C.00003	0.00003	C.C0003	0.00003	0.00003	0.00003	0.00003
0.0000	0.0000	C.C0003	C.C0003	C.C0003	C.00003	0.00003	C.C0003	0.00003	0.00003	0.00003	0.00003
10.0000	33.1220	C.C0002	C.C0002	C.C0002	C.00002	0.00002	C.C0002	0.00002	0.00002	0.00002	0.00002
10.0000	33.1220	C.C0002	C.C0002	C.C0002	C.00002	0.00002	C.C0002	0.00002	0.00002	0.00002	0.00002
20.0000	66.2441	C.C0001	C.C0001	C.C0001	C.00001	0.00001	C.C0001	0.00001	0.00001	0.00001	0.00001
20.0000	66.2441	C.C0001	C.C0001	C.C0001	C.00001	0.00001	C.C0001	0.00001	0.00001	0.00001	0.00001
30.0000	99.3661	C.C0001	C.C0001	C.C0001	C.00001	0.00001	C.C0001	0.00001	0.00001	0.00001	0.00001
30.0000	99.3661	C.C0001	C.C0001	C.C0001	C.00001	0.00001	C.C0001	0.00001	0.00001	0.00001	0.00001
ACCUMULATE TIME (MIN) = 540.00											

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	C.00001									
0.0000	0.0000	C.00001									
10.0000	33.1220	C.00000									
10.0000	33.1220	C.00000									
20.0000	66.2441	C.00000									
20.0000	66.2441	C.00000									
30.0000	99.3661	C.00000									
30.0000	99.3661	C.00000									

FINISHED

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	C.47370									
0.0000	0.0000	C.47370									
10.0000	33.1220	C.29793	C.28235	C.43191	C.45584	C.46630	C.47067	C.47247	C.47320	C.47370	C.47370
10.0000	33.1220	C.47350	C.47362	C.47367	C.47369	C.47370	C.47370	C.47370	C.47370	C.47370	C.47370
20.0000	66.2441	C.18738	C.29262	C.37877	C.43005	C.45500	C.46594	C.47053	C.47241	C.47370	C.47370
20.0000	66.2441	C.47318	C.47349	C.47361	C.47367	C.47369	C.47369	C.47370	C.47370	C.47370	C.47370
30.0000	99.3661	C.11785	C.21311	C.31681	C.39456	C.43811	C.45861	C.46747	C.47116	C.47370	C.47370
30.0000	99.3661	C.47267	C.47229	C.47252	C.47263	C.47367	C.47369	C.47370	C.47370	C.47370	C.47370
40.0000	132.4882	C.07412	C.14881	C.25141	C.34880	C.41370	C.44742	C.46269	C.46919	C.47370	C.47370
40.0000	132.4882	C.47186	C.47295	C.47340	C.47358	C.47365	C.47368	C.47369	C.47370	C.47370	C.47370
50.0000	165.6102	C.04662	C.10057	C.18929	C.29449	C.38004	C.43071	C.45530	C.46607	C.47370	C.47370
50.0000	165.6102	C.47058	C.47243	C.47319	C.47349	C.47362	C.47367	C.47369	C.47369	C.47370	C.47370
60.0000	198.7322	C.02932	C.06036	C.13589	C.23606	C.33650	C.40657	C.44401	C.45121	C.47370	C.47370
60.0000	198.7322	C.46856	C.47161	C.47285	C.47336	C.47356	C.47364	C.47369	C.47369	C.47370	C.47370

ACCUMULATE TIME (MIN) 60.00

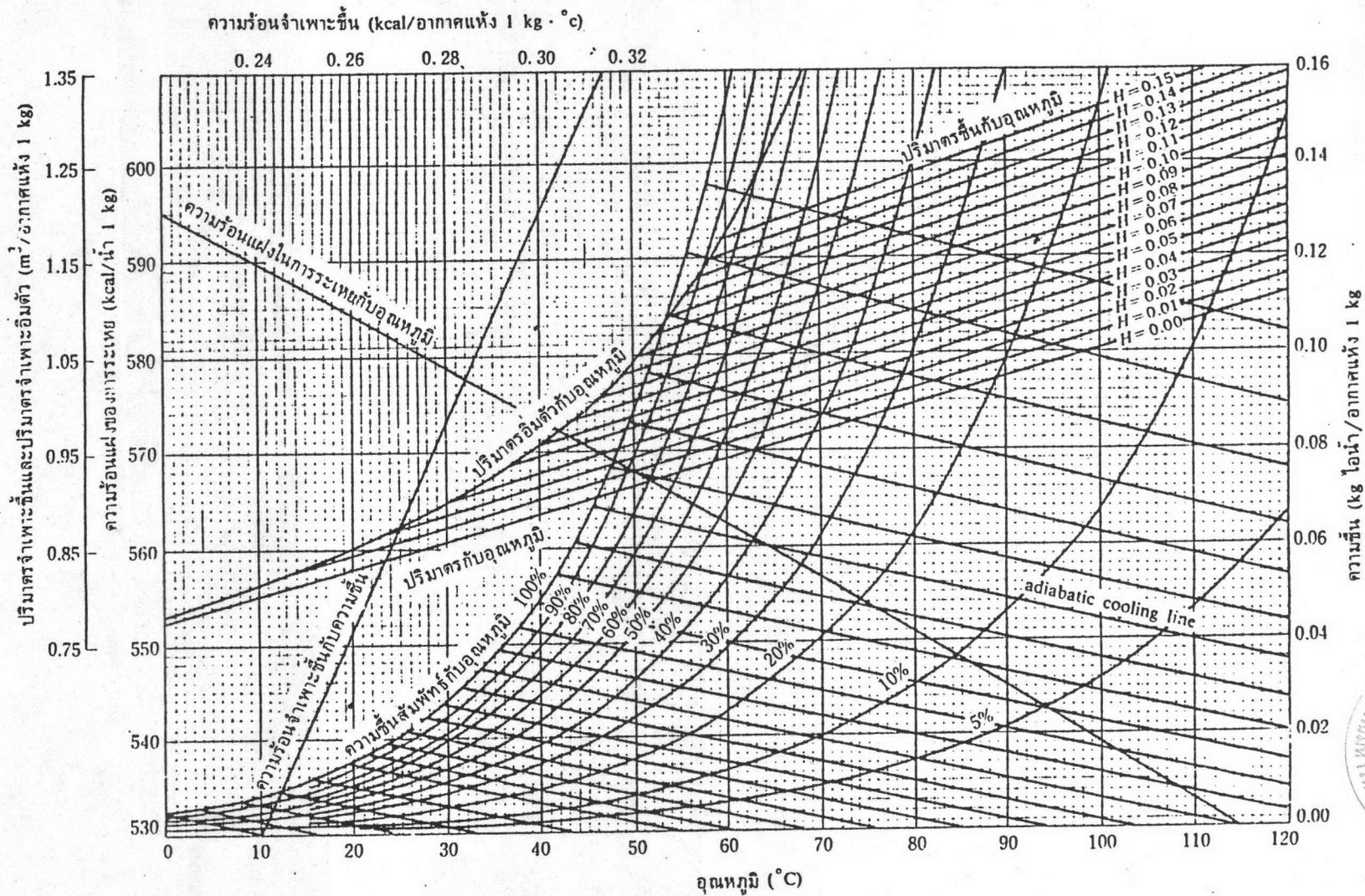
DIRECTION OF FLOW IS BACKWARD

0.0000	0.0000	C.02932	C.06636	C.13589	C.23606	C.33650	C.40657	C.44401	C.45121	C.47370	C.47370
0.0000	0.0000	C.46856	C.47161	C.47285	C.47336	C.47356	C.47364	C.47369	C.47369	C.47370	C.47370
10.0000	33.1220	C.15993	C.20727	C.26976	C.33872	C.39657	C.43300	C.45149	C.45976	C.47370	C.47370
10.0000	33.1220	C.46216	C.46423	C.46424	C.46279	C.45878	C.44897	C.42633	C.37325	C.29793	C.29793
20.0000	66.2441	C.15993	C.20727	C.26976	C.33871	C.39657	C.43298	C.45144	C.45952	C.47370	C.47370
20.0000	66.2441	C.46285	C.46257	C.46236	C.45821	C.44782	C.42393	C.37451	C.23030	C.18738	C.18738
30.0000	99.3661	C.15993	C.20727	C.26976	C.33871	C.39655	C.43295	C.45135	C.45943	C.47370	C.47370
30.0000	99.3661	C.46236	C.46236	C.45940	C.45112	C.43146	C.38940	C.31382	C.21214	C.11785	C.11785
40.0000	132.4882	C.15993	C.20727	C.26976	C.33870	C.39652	C.43290	C.45123	C.45911	C.47370	C.47370
40.0000	132.4882	C.46158	C.46044	C.45478	C.44028	C.40776	C.34475	C.24952	C.14934	C.07412	C.07412
50.0000	165.6102	C.15993	C.20727	C.26975	C.33868	C.39650	C.43281	C.45102	C.45851	C.47370	C.47370
50.0000	165.6102	C.46034	C.45743	C.44762	C.42407	C.37501	C.29160	C.18821	C.10035	C.04662	C.04662
60.0000	198.7322	C.15993	C.20726	C.26974	C.33866	C.39644	C.43268	C.45070	C.45731	C.47370	C.47370
60.0000	198.7322	C.45838	C.45272	C.43668	C.40063	C.33254	C.23419	C.13534	C.06627	C.02932	C.02932

ACCUMULATE TIME (MIN) 120.00

DIRECTION OF FLOW IS FORWARD

0.0000	0.0000	C.15993	C.20726	C.26974	C.33866	C.39644	C.43268	C.45070	C.45731	C.47370	C.47370
0.0000	0.0000	C.45828	C.45273	C.43668	C.40063	C.33254	C.23419	C.13534	C.06627	C.02932	C.02932
10.0000	33.1220	C.10055	C.11597	C.14269	C.18631	C.24810	C.21731	C.27605	C.41474	C.47370	C.47370
10.0000	33.1220	C.43530	C.44297	C.44022	C.42481	C.39069	C.33494	C.26764	C.20614	C.15931	C.15931
20.0000	66.2441	C.06326	C.07835	C.10375	C.14622	C.21014	C.28730	C.35705	C.40475	C.47370	C.47370
20.0000	66.2441	C.43066	C.44094	C.43926	C.42445	C.39054	C.33487	C.26761	C.20613	C.15930	C.15930
30.0000	99.3661	C.03979	C.05169	C.07236	C.10895	C.16902	C.24973	C.33050	C.39935	C.47370	C.47370
30.0000	99.3661	C.42347	C.42776	C.43801	C.42388	C.39030	C.33477	C.26757	C.20611	C.15929	C.15929
40.0000	132.4882	C.02503	C.03355	C.04885	C.07752	C.12891	C.20675	C.29555	C.36820	C.47370	C.47370
40.0000	132.4882	C.41252	C.43275	C.43587	C.42298	C.38992	C.33461	C.26743	C.20607	C.15927	C.15927
50.0000	165.6102	C.01574	C.02153	C.03221	C.05315	C.09360	C.16233	C.25202	C.33951	C.47370	C.47370
50.0000	165.6102	C.39625	C.42511	C.43251	C.42156	C.38932	C.33435	C.26733	C.20601	C.15924	C.15924
60.0000	198.7322	C.00990	C.01372	C.02090	C.03544	C.06520	C.12100	C.20590	C.27935	C.47370	C.47370



๒ ๒๕ พฤษภาคม



รูป ๒1 รูปกราฟความชื้นในหน่วยมวล (มาตรฐาน : ความดันรวม 760 mm Hg , อากาศแห้ง 1 kg)

ภาคผนวก ค-1

วิธีคำนวณปริมาณความชื้นของวัสดุ

การคำนวณหาปริมาณความชื้นของวัสดุทำได้ดังนี้

จากข้อมูลการทดลองที่เวลา t_1

$$\text{น้ำหนักวัสดุ} = X_1 \quad \text{กรัม}$$

$$\text{น้ำหนักวัสดุแห้ง} = X_2 \quad \text{กรัม}$$

$$\text{น้ำหนักน้ำที่มีอยู่ในวัสดุ} = X_1 - X_2 \quad \text{กรัม}$$

$$\text{ปริมาณความชื้นของ วัสดุที่เวลา } t_1 = \frac{X_1 - X_2}{X_2} \quad \text{กก.น้ำ/กก. วัสดุแห้ง}$$

ภาคผนวก ค-2

วิธีคำนวณอัตราการรอบแห้ง

$$\text{อัตราการรอบแห้ง} = \frac{\text{น้ำหนักของน้ำที่ระเหยไปในช่วงเวลานั้น}}{\text{น้ำหนักของวัสดุแห้ง} \times \text{ช่วงเวลานั้น}}$$

นอกจากการใช้ความสัมพันธ์ข้างต้นแล้ว อัตราการรอบแห้งยังหาได้จากการลากเส้นสัมพันธ์กับเส้นกราฟที่พลอตระหว่างความชื้นกับเวลาแล้วอ่านความชันของเส้นสัมพันธ์นั้น

ในงานวิจัยนี้การหาอัตราการรอบแห้งจะใช้วิธีหลัง

ภาคผนวก ง

ภาคผนวกนี้แสดงขั้นตอนการคำนวณอัตราการอบแห้งเชิงทฤษฎี (R_{theo}) เพื่อกำหนดค่า c_c ที่เหมาะสมที่สุดโดยการเปรียบเทียบกับอัตราการอบแห้งที่ได้จากการทดลอง

วัสดุ : ขึ้นมันสีปะหลังขนาด 0.5 ซม. x 0.5 ซม. x 0.3 ซม

อุณหภูมิเข้าของลมร้อน 65°ซ

ความเร็วของลมร้อน 0.6 ม/วินาที

ความชื้นของลมร้อน 0.018 กก.น้ำ/กก.อากาศแห้ง

อัตราส่วนว่างของขึ้นวัสดุ 0.768

ความหนาแน่นจริงของวัสดุแห้ง 924 กก./ลบ.ม.

เส้นผ่าศูนย์กลางสัมมูลของขึ้นวัสดุ 0.409×10^{-2} ม.

ความชื้นแรกเริ่ม 0.80 กก.น้ำ/กก.วัสดุแห้ง

ความชื้นสัมตลย 0.00 กก.น้ำ/กก.วัสดุแห้ง

ก่อนอื่นสมมุติว่าลมร้อนที่ออกจากขึ้นวัสดุมีอุณหภูมิ = 30°ซ และมีความชื้น = 0.032 กก.น้ำ/กก.อากาศแห้ง จากแผนภูมิความชื้น ลมร้อนอุณหภูมิ 65°ซ ความชื้น 0.018 กก.น้ำ/กก.อากาศแห้ง จะมีปริมาตรจำเพาะ (v_H) = 1.02 ลบ.ม./กก.อากาศแห้ง

$$\begin{aligned} \text{ความเร็วเชิงมวลของลมร้อน (G)} &= \frac{0.6(3600) \left\{ 1 + \frac{(0.018 + 0.032)}{2} \right\}}{1.02} \\ &= 2170 \text{ กก./ตร.ม.ชม.} \end{aligned}$$

$$\begin{aligned} \text{ที่อุณหภูมิ 65°ซ ความหนืด } (\mu) \text{ ของอากาศ} &= 0.023 \text{ เซนต์พอยซ์} \\ &= 7.2 \times 10^{-2} \text{ กก./ม.ชม.} \end{aligned}$$

ดังนั้น

$$\text{Rep} = \frac{GD_p}{\mu} = \frac{2170 \times 0.409 \times 10^{-2}}{7.2 \times 10^{-2}} = 123.2$$

จาก

$$\frac{k}{G} = 2.566 (\text{Re})^{0.51}$$

เราได้

$$k = 2.566 (123.2)^{-0.51} \times 2170 = 477.83 \text{ กก./ตร.ม.ชม.}$$

จาก

$$\begin{aligned} a &= 6(1-\epsilon)/D_p \\ &= 6(1-0.768)/0.409 \times 10^{-2} \\ &= 340.34 \text{ ม}^{-1} \end{aligned}$$

$$\begin{aligned} ka &= 477.83 \times 340.34 \\ &= 162,626 \text{ กก./ชม.ลบ.ม.} \end{aligned}$$

ผนังสมร่อนที่อุณหภูมิ 65°C ความชื้น 0.018 กก.น้ำ/กก.อากาศแห้ง มีอุณหภูมิ
กระเปาะเปียก = 32.8°C และความชื้นอิ่มตัวที่อุณหภูมิกระเปาะเปียก = 0.032 กก.น้ำ/
กก.อากาศแห้ง

จาก

$$\xi_L = \ln \left\{ \frac{H_w - H_i}{H_w - H_L} \right\}$$

โดยที่

$$\xi_L = \frac{kaL}{G_o} \quad ; \quad G_o = \frac{G}{1 + H_i}$$

H_i = ความชื้นของสมร่อนก่อนเข้าชั้นวัสดุ

H_L = ความชื้นของสมร่อนที่ออกจากชั้นวัสดุ

H_w = ความชื้นของสมร่อนที่อุณหภูมิกระเปาะเปียก

ดังนั้น

$$\xi_L = \frac{162,626 \times 0.05}{2170/(1+0.018)} = 3.82$$

จาก

$$H_L = \frac{H_w - \frac{(H_w - H_i)}{\xi_L}}{\xi_L}$$

$$H_L = \frac{0.032 - \frac{(0.032 - 0.018)}{3.82}}{3.82}$$

หรือ

$$H_L = 0.0316 \text{ ซึ่งใกล้เคียงกับที่เราได้สมมุติไว้ตอนแรก}$$

ดังนั้น

$$\pi_o = H_w - H_i = 0.032 - 0.018 = 0.014$$

และ

$$R_{\text{theo}} = - \frac{dw}{d\theta} = \frac{ka}{(1-\epsilon)\rho_s} \cdot \frac{\pi_o \xi_L^{-\pi_o \tau} (1-\xi_L^{\phi_o \xi_L})}{\xi_L \frac{1-\xi_L^{-\pi_o \tau}}{1-\xi_L^{-\pi_o \tau}} (1-\xi_L^{\phi_o \xi_L})}$$

$$\text{โดยที่ } \tau = \frac{ka\theta}{(1-\epsilon)\rho_s (c_c - c_e)}$$

$$\phi = \frac{(c - c_c)}{(c_c - c_e)}$$

หลังจากการแทนค่าต่าง ๆ ลงไปในสมการข้างต้นเราจะเห็นว่าเหลือเพียงตัวแปร θ และ c_c ที่ต้องรู้ในการคำนวณค่า R_{theo}

โดยการทดลองใช้ C_c ค่าหนึ่งเราจะได้ค่า R_{theo} ที่เวลา θ ต่าง ๆ ซึ่งเอาไปเปรียบเทียบกับอัตราการอบแห้งที่ได้จากการทดลองได้ สรุปลแล้วค่า C_c ที่เหมาะสมที่สุดคือค่าที่ทำให้ผลรวมของกำลังสองของผลต่างระหว่าง R_{theo} และ R_{exp} มีค่าน้อยที่สุดนั่นเอง

ประวัติการศึกษา

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ในปี พ.ศ. 2525



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