DESIGN AND USE OF IONIC LIQUIDS IN SEPARATION PROCESSES FOR AZEOTROPIC MIXTURES

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ABSTRACT

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Separation of azeotrope and close-boiling mixtures is a challenge in several industries. Ionic liquids (ILs) have been recently determined as alternative entrainers in the extractive distillation (ED) owing to the flexibility in their tailor-made molecular structures and properties for a specific work. A systematic methodology of selection and design of the best IL-based separation process was developed to investigate the viability of the azeotropic separation process using ILs through five different mixtures as case studies including the mixtures of ethanol + water, ethanol + hexane, benzene + hexane, toluene + methylcyclohexane (MCH), and ethylbenzene (EB) + p-xylene (PX). The Hildebrand solubility Group Contribution parameter along with the capacity and selectivity of ILs are the key parameters for selecting the suitable ILs as entrainers. All first four azeotropic mixtures were successfully demonstrated and four best ILs were identified, i.e. [MMIM][DMP] from ethanol + water, [EMIM][BTI] from ethanol + hexane mixture, [EMIM][EtSO4] from benzene + hexane mixture, and [HMIM][TCB] from toluene + methylcyclohexane (MCH) mixture. However, the proposed screening criteria cannot effectively demonstrate the isomer mixture, i.e. EB + PX mixture, due to the similarity of these isomers causing no differences in the calculated Hildebrand solubility parameter, selectivity and capacity. A simulation process of ILs was carried out successfully, which a minimum energy requirement and a solvent usage were determined and compared with the conventional solvent process. In order to get a supported decision-making in an investment, economic evaluation was determined and compared between the IL and conventional solvent processes.

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บทคัดย่อ

วรวิทย์ เพิ่งหนู : การออกแบบการเลือกใช้ไอออนิกลิควิคในกระบวนการแยกสำหรับ ของผสมอะซีโอโทรป (Design and Use of Ionic Liquids in Separation Processes for Azeotropic Mixtures) อ. ที่ปรึกษา: คร. อุทัยพร สุริยประภาคิลก และ ศ.คร. ราฟิก กานี่ 432 หน้า

การจัดการกับปั้ณหาที่เกี่ยวข้องกับกระบวนการแยกของผสมอะซีโอโทรป (Azeotrope) และของผสมที่มีจุดเดือดใกล้เคียงกัน (Close-boiling) เป็นปัญหาที่ท้าทายในหลากหลาย อุตสาหกรรมนั้น ทำให้ไม่นานมานี้ของเหลวไอออนิก (Ionic liquids) ได้ถูกพิจารณานำมาเลือกใช้ เป็นสารช่วยกลั่น (Entrainers) ในหอกลั่นแบบสกัด (Extractive distillation) อันเนื่องมาจากการ ยืดหยุ่นปรับแต่งได้ในตัวโครงสร้างโมเลกุลและคุณสมบัติเฉพาะของของเหลวไอออนิก ดังนั้น ระบบวิธีการสำหรับการคัคเลือกและการออกแบบกระบวนการแยกโคยใช้ของเหลวไอออนิกที่คี ที่สุดถูกพัฒนาขึ้นมาโดยผ่านการตรวจสอบการนำไปใช้งานได้จริงในทุกๆระบบจากของผสมห้า ้ชนิดซึ่งเป็นกรณีศึกษาในครั้งนี้ ได้แก่ของผสมเอทานอลกับน้ำ เอทานอลกับเฮกเซน เบนซีนกับ เฮกเซน โทลูอื่นกับเมทิลไซโคลเฮกเซน และ เอทิลเบนซึนกับพาราไซลีน พารามิเตอร์หลักที่เสนอ ใช้ในการคัดเลือกของเหลวไอออนิกที่ดีที่สุดของแต่ละระบบในงานวิจัยนี้ มีดังนี้ พารามิเตอร์ของ การละลายของฮิลเคอแบรนด์ (Hildebrand solubility Group Contribution parameter) พร้อมด้วย พารามิเตอร์ของความสามารถในการละลายใค้ (Capacity) และความสามารถในการเลือกการ ละลาย (Selectivity) ของของเหลวไอออนิก ซึ่งของเหลวไอออนิกที่ดีที่สุดที่ผ่านการคัดเลือกคือ [MMIM][DMP] จากของผสมเอทานอลกับน้ำ [EMIM][BTI] จากของผสมเอทานอลกับเฮกเซน [EMIM][EtSO4] จากของผสมเบนซึนกับเฮกเซน และ [HMIM][TCB] จากของผสมโทลูอื่นกับ เมทิลไซโคลเฮกเซน อันเนื่องด้วยหลักการคัดเลือกนี้ยังไม่สามารถตอบสนองการทำงานอย่างมี ประสิทธิภาพกับของผสมไอโซเมอร์ (Isomer)ได้ ทำให้ของผสมเอทิลเบนซีนกับพาราไซลีนไม่ถูก นำไปวิเคราะห์ต่อจนจบในท้ายที่สุด จากความคล้ายกันของสารไอโซเมอร์ทำให้ไม่มีความ แตกต่างในก่าพารามิเตอร์ Hildebrand ก่าพารามิเตอร์ Capacity และ ก่าพารามิเตอร์ Selectivity แบบจำลอง (Simulation) กระบวนการของของเหลวไอออนิกได้ถูกสร้างขึ้นใหม่และคำนวณค่า การใช้พลังงานและการใช้สารละลายที่น้อยที่สุด เพื่อนำไปเปรียบเทียบกับกระบวนการที่ใช้ตัวทำ ้ละลายอินทรีย์ (Conventional solvent) แต่เพื่อให้ได้ข้อมูลประกอบการตัดสินใจในการลงทุน การ ้ประเมินเชิงธุรกิจได้ถูกจัดทำขึ้นเพื่อเสนอเปรียบเทียบกระบวนการแยกด้วยของของเหลวไอออนิก และตัวทำละลายอินทรีย์ในขั้นตอนสุดท้าย

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| I6 | VLE graph of [EMIM][BTI] in ethanol + heptane mixture. | 415 |
| I7 | VLE graph of [BMIM][BTI] in ethanol + heptane mixture. | 415 |
| J1 | Hildebrand solubility parameters of ILs (x-axis) vs | |
| | Capacity (C_2^{∞}) of ILs (primary <i>y</i> -axis) and Selectivity (S_{12}^{∞}) | |
| | of ILs (secondary <i>y</i> -axis) of the water + ethanol mixture. | |
| | Water is the target solute. | 419 |
| J2 | VLE comparison graph for separation capability of ILs | |
| | in water + ethanol mixture. | 420 |
| J3 | Hildebrand solubility parameters of ILs (x-axis) vs | |
| | Capacity (C_2^{∞}) of ILs (primary <i>y</i> -axis) and Selectivity (S_{12}^{∞}) | |
| | of ILs (secondary <i>y</i> -axis) of the benzene + hexane mixture. | |
| | Benzene is the target solute. | 422 |
| J4 | VLE comparison graph for separation capability of ILs | |
| | in benzene + hexane mixture. | 423 |
| J5 | IL process flowsheet in benzene + hexane mixture | |
| | using [EMPY][TOS]. | 424 |
| J6 | Hildebrand solubility parameters of ILs (x-axis) vs | |
| | Capacity (C_2^{∞}) of ILs (primary <i>y</i> -axis) and Selectivity (S_{12}^{∞}) | |
| | of ILs (secondary <i>y</i> -axis) of the ethanol + hexane mixture. | |
| | Ethanol is the target solute. | 425 |
| J7 | Hildebrand solubility parameters of ILs (x-axis) vs | |
| | Capacity (C_2^{∞}) of ILs (primary <i>y</i> -axis) and Selectivity (S_{12}^{∞}) | |
| | of ILs (secondary y-axis) of the toluene + MCH mixture. | |
| | Toluene is the target solute. | 425 |
| J8 | Hildebrand solubility parameters of ILs (x-axis) vs | |
| | Capacity (C_2^{∞}) of ILs (primary <i>y</i> -axis) and Selectivity (S_{12}^{∞}) | |
| | of ILs (secondary <i>y</i> -axis) of the EB + PX mixture. | |
| | EB is the target solute. | 425 |

| FIGURE | PAGE |
|--------|------|
| | |
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| | |

| K1 | IL process flowsheet in ethanol + hexane mixture | |
|----|--|-----|
| | using [EMIM][BTI] (No.4). | 425 |
| K2 | IL process flowsheet in ethanol + hexane mixture | |
| | using [EMIM][BTI] (No.9). | 425 |

ABBREVIATIONS

Nomenclature of the Ionic Liquids

| Cations | |
|-------------------------------|--|
| $[MMIM]^+$ | 1-Methyl-3-Methylimidazolium |
| $[EMIM]^+$ | 1-Ethyl-3-Methylimidazolium |
| $[EM2IM]^+$ | 1,2-Dimethyl-3-Methylimidazolium |
| $[PMIM]^+$ | 1-Propyl-3-Methylimidazolium |
| $[BMIM]^+$ | 1-Butyl-3-Methylimidazolium |
| $[HMIM]^+$ | 1-Hexyl-3-Methylimidazolium |
| $[OMIM]^+$ | 1-Methyl-3-Octylimidazolium |
| $[DMIM]^+$ | 1-Decyl-3-Methylimidazolium |
| [PDMIM] ⁺ | 1-Propyl-2,3-Dimethylimidazolium |
| [16MIM] ⁺ | 1-Hexadecyl-3-Methylimidazolium |
| [OHDMIM] ⁺ | 1-(2-Hydroxyethyl)-3-Methylimidazolium |
| [C6H13OCH2MIM] ⁺ | 1-Hexyloxymethyl-3-Methylimidazolium |
| [(C6H13OCH2)2IM] ⁺ | 1,3-Dihexyloxymethylimidazolium |
| $[EMPY]^+$ | 1-Ethyl-3-methylpyridinium |
| $[BMPY]^+$ | 1-Butyl-3-methylpyridinium |
| $[EMPYR]^+$ | 1-Ethyl-1-methylpyrrolidinium |
| $[BMPYR]^+$ | 1-Butyl-1-methylpyrrolidinium |
| $[PMPIP]^+$ | 1-Propyl-1-Methylpiperidinium |
| $[PeMPIP]^+$ | 1-Pentyl-1-Methylpiperidinium |
| [HMPIP] ⁺ | 1-Hexyl-1-Methylpiperidinium |
| $[3C6C14P]^{+}$ | Trihexyltetradecylphosphonium |
| $[3BMP]^+$ | Tributylmethylphosphonium |
| $[P1444]^+$ | Triisobutylmethylphosphonium |
| $[E3S]^+$ | Triethylsulphonium |
| $[OMA]^+$ | Trioctylmethylammonium |
| [TMHA] ⁺ | Trimethylhexylammonium |

| Bromide |
|--|
| Chloride |
| Hexafluorophosphate |
| Tetrafluoroborate |
| Trifluoromethanesulfonate |
| Bis(trifluoromethylsulfonyl)imide |
| Tris(pentafluoroethyl)trifluorophosphate |
| Acetate |
| Trifluoroacetate |
| Nitrate |
| Tosylate |
| Thiocyanate |
| Dicyanamide |
| Tricyanomethanide |
| Tetracyanoborate |
| Bis[oxalato(2-)]-borate |
| Ethylsulfate |
| Methylsulfate |
| Octylsulfate |
| Diethylenglycol monomethyl ether sulfate |
| or 2-(2-methoxyethoxy)ethylsulfate |
| Hydrogensulfate |
| Methanesulfonate |
| P-Toluenesulfonate |
| Methylphosphonate |
| Dimethylphosphate |
| |

LIST OF SYMBOLS

- c_{ii} = cohesive energy density
- C_i = contribution of group i
- g_{ij} = energy parameter characteristic of the i-j interaction
- g_{ij} = energy parameter characteristic of the i-j interaction
- Δg_{ij} = binary interaction parameter between component i and j

 Δh_{vap} = enthalpy of vaporization

 $K_1 = K$ -factor for component 1

 $K_2 = K$ -factor for component 2

M = the molecular mass

- n_i = the number of groups of type i
- n_i = the number of times that a group appears in the molecule
- N = number of stages
- N_F = feed stage location
- P_1^s = vapor pressures of component 1
- P_2^s = vapor pressures of component 2
- R = gas constant
- T = absolute temperature
- T_b = normal boiling temperature
- T_c = critical temperature
- $v_i = molar volume of component i$
- $V_i = volume/mole$ fraction of component i
- V_C = critical volume
- x_1 = mole fraction for component 1 in the liquid phase
- x_2 = mole fraction for component 2 in the liquid phase
- y_1 = mole fraction for component 1 in the vapor phase
- y_2 = mole fraction for component 2 in the vapor phase

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Greek Symbols

 α_{12} = separation factor or relative volatility

 α_{ij} = non-randomness parameter in the NRTL equation

 γ_1 = activity coefficient of component 1

 γ_2 = activity coefficient of component 2

 γ_i^c = caombination part of the activity coefficient of component i

 γ_i^R = residual part of the activity coefficient of component i

 δ_i = solubility parameter of component i

 ω = acentric factor

 ρ_L = liquid densities of the ionic liquids