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## APPENDIX

### (Supportive Evidence for Gradient Method Criteria)

There are many theories to predict the  $T_g$  of a miscible blend. One of the most well known theories is the Flory-Fox equation [Paul and Newman, 1978] as shown belows:

$$\frac{1}{T_g} = \frac{W_1}{T_{g,1}} + \frac{W_2}{T_{g,2}}$$

where  $T_g$  = glass transition temperature of the mixture  
 $W_i$  = weight fraction of the  $i$ th component  
 $T_{g,i}$  = glass transition temperature of the  $i$ th component

The gradient method was created to construct the phase diagram in this study. In this section, the criteria used for determining the phase behaviour of the blends from gradient value of the gradient method were used to determine the  $T_g$  of the blends as predicted from Flory-Fox equation.

The  $T_g$  of the blends of poly(bisphenol A carbonate) (PC) and low molar mass liquid crystal were calculated by Flory-Fox equation. The  $T_g$  of pure PC is  $150^\circ\text{C}$ . The  $T_g$  of pure low molar mass liquid crystal is assumed to be  $25^\circ\text{C}$ . (In reality, the  $T_g$  of pure low molar mass liquid crystal can not be detected even started DSC scan at  $-150^\circ\text{C}$ .)

Let 1 = low molar mass liquid crystal (LC)

2 = PC

$T_{g,1} = 25^{\circ}\text{C}$  or 298K

$T_{g,2} = 150^{\circ}\text{C}$  or 423K

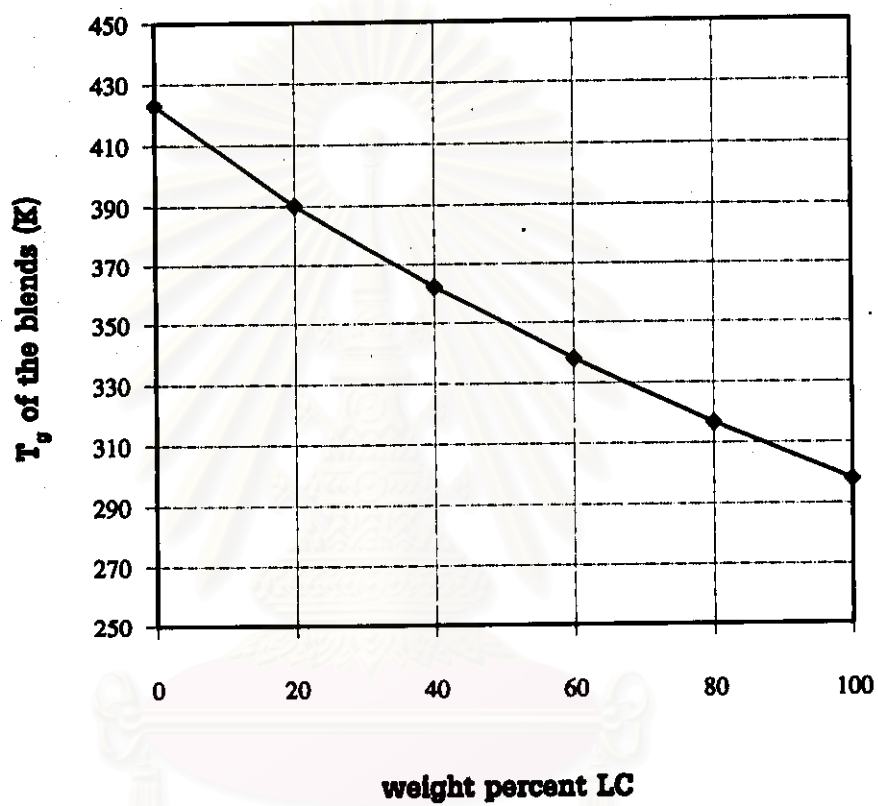
$T_g$  = glass transition temperature of the blend

Flory-Fox equation: 
$$\frac{1}{T_g} = \frac{W_1}{298} + \frac{W_2}{423}$$

The plot of  $T_g$  versus LC weight percent as calculated from Flory-Fox equation above is shown in Figure A-1.

The gradient values ( $\tan\theta$ ) were calculated in the same way as described previously in section 5.2 (Phase Diagram Construction Procedure). The determination of the phase behaviour of the blends was based on the criteria represented in the Table 5-7.

The  $T_g$  of the blends of PC and low molar mass liquid crystal are presented in Table A-1. The gradient value ( $\tan\theta$ ),  $\theta$  (degree) and symbols of the regions are presented in Table A-2.



**Figure A-1** The graph of the glass transition temperatures ( $T_g$ ) of the blends against the weight percent of low molar mass liquid crystal.



**Table A-1** The  $T_g$  of the blends of PC and low molar mass liquid crystal predicted from Flory-Fox equation.

% by weight of LC with PC	$T_g$ of the blends (Kelvin)
0	423.0
20	390.3
40	362.2
60	337.9
80	316.7
100	298.0

**Table A-2** Gradient value ( $\tan\theta$ ) and  $\theta$  (degree) calculated from the  $T_g$  of the blends of PC and low molar mass liquid crystal predicted from Flory-Fox equation in Table A-1. o represents the absolutely partially miscible. + represents the possibly partially miscible.

% by weight of LC with PC	gradient value ( $\tan\theta$ )	$\theta$ (degree)	region symbols
0-20	-1.637	-58.58	o
20-40	-1.402	-54.50	o
40-60	-1.214	-50.52	o
60-80	-1.061	-46.71	o
80-100	-0.936	-43.10	+

Flory-Fox equation is the equation that estimates the  $T_g$  of the miscible blend. The  $T_g$  of the blends (PC and low molar mass liquid crystal) presented in Table A-1 are calculated from Flory-Fox equation. It means that the blend (PC and low molar mass liquid crystal) is assumed to be the miscible blend. From above reason, if we use the  $T_g$  in Table A-1 to calculate the gradient value and determine the phase behaviour based on the criteria of the gradient method, it should show the miscible characteristics.

From Table A-2, it can be seen that the phase behaviour determined base on the criteria of the gradient method is the partially miscible blend. This is consistent with the fact described in above paragraph. So it can be concluded that the criteria of the gradient method is suitable for determining the phase behaviour of the blends in this study.

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## VITA

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