

## REFERENCES

1. Greskovich, C., and Rosolodki, J.H. Sintering of covalent. J.Am.Ceram.Soc. 59 (Jul.-Aug. 1976) : 336-343.
2. Kleebe, H. Structure and chemistry of interfaces in  $\text{Si}_3\text{N}_4$  ceramics studied by transmission electron microscopy. J.Am.Ceram.Soc.Jap. 105 (1997) : 490-510.
3. Wills, R.R. Silicon Yttrium Oxyynitrides. J.Am.Ceram.Soc. 57 (October 1974) : 459.
4. Diane M., Mieskowski, and William A. Sanders. Oxidation of silicon nitride sintered with rare-earth oxide additions. J.Am.Ceram.Soc. 68 (July 1985) : C-160-C-163.
5. Jian-Feng Yang, Tatsuki Ohji, and Koichi Niihara. Influence of Ytria-Alumina content on sintering behavior and microstructure of silicon nitride ceramics. J.Am.Ceram.Soc. 83 (August 2000) : 2094-2096.
6. Gauckler, L.J., Hohnke, H., and Tien, T.Y. The system  $\text{Si}_3\text{N}_4\text{-SiO}_2\text{-Y}_2\text{O}_3$ . J.Am.Ceram.Soc. 63 (Jan.-Feb. 1980) : 35-37.
7. Frederick, F. Lange. Fabrication and properties of dense polyphase silicon nitride. J.Am.Ceram.Bull. 62 (1983) : 1369-1374.
8. Akihiko Tsuge., Nishida, K., and Komatsu, M. Effect of crystallizing the grain boundary glass phase on the high-temperature strength of Hot-Pressed  $\text{Si}_3\text{N}_4$  containing  $\text{Y}_2\text{O}_3$ . J.Am.Ceram.Soc. 58 (Jul.-Aug. 1975) : 323-326.
9. Wills, R.R. Reaction of  $\text{Si}_3\text{N}_4$  with  $\text{Al}_2\text{O}_3$  and  $\text{Y}_2\text{O}_3$ . J.Am.Ceram.Soc. 58 (Jul.-Aug. 1975) : 335.
10. Lange, F.F. Relation between strength, Fracture Energy and microstructure of Hot-Pressed  $\text{Si}_3\text{N}_4$ . J.Am.Ceram.Soc. 56 (October 1973) : 518-522.
11. Tsuge, A., Kudo, H., and Komeya, K. Reaction of  $\text{Si}_3\text{N}_4$  and  $\text{Y}_2\text{O}_3$  in Hot-Pressing. J.Am.Ceram.Soc. 59 (June 1977) : 269-270.
12. John, A. Mangels, and Gerald J. Tennenhouse. Densification of Reaction-Bonded silicon nitride. J.Am.Ceram.Bull. 59 (1980) : 1216-1218.
13. John A., Mangels, and Gerald, J. Tennenhouse. Sintering behavior and microstructure development of Yttrium-Doped reaction-bonded silicon nitride. J.Am.Ceram.Bull. 60 (1981) : 1306-1310.
14. Priest, H.F., Priest, G.L., and Gazza, G.E. Sintering of  $\text{Si}_3\text{N}_4$  under high nitrogen

- pressure. J.Am.Ceram.Soc. 60 (Jun.-Feb. 1977) : 81.
15. Greskovich, C. Preparation of high density  $\text{Si}_3\text{N}_4$  by gas pressure sintering process. J.Am.Ceram.Soc. 64 (December 1981) : 725-730.
  16. Sunil Dutta. Fabrication, microstructure, and strength of sintered  $\beta'$   $\text{Si}_3\text{N}_4$  solid solution. J.Am.Ceram.Bull. 59 (December 1980) : 623-25,634.
  17. Lee, H.R., Lee, C.J., and Deug J. Kim. Effect of  $\alpha$ - $\text{Si}_3\text{N}_4$  powder bedding on the microstructure of gas pressure sintered  $\text{Si}_3\text{N}_4$  ceramics. Materials Letters. 52 (2002) : 355-359.
  18. Kazushige Yokoyama, et al. Solid-gas reaction during sintering of  $\text{Si}_3\text{N}_4$  ceramics (Part 1). J.Am.Ceram.Soc.Jap. 108 (2002) : 6-9.
  19. Kazushige Yokoyama, et al. Solid-gas reaction during sintering of  $\text{Si}_3\text{N}_4$  ceramics (Part 3). J.Am.Ceram.Soc.Jap. 108 (2002) : 230-235.
  20. Kazushige Yokoyama, et al. Solid-gas reaction during sintering of  $\text{Si}_3\text{N}_4$  ceramics (Part 4). J.Am.Ceram.Soc.Jap. 108 (2002) : 357-364.
  21. Shigetaka Wada. Control of instability of  $\text{Si}_3\text{N}_4$  during pressureless sintering. J.Am.Ceram.Soc.Jap. 109 (2001) : 803-808.
  22. Shigetaka Wada, et al. Sintering of  $\text{Si}_3\text{N}_4$  ceramics in air atmosphere furnace. J.Am.Ceram.Soc.Jap. 109 (2001) : 281-283.
  23. Naoto Hirosaki, et al. New ceramics based on silicon nitride[Online]. (n.d.). Available form: [http:// sakimori.nims.go.jp/oneday2000/ceramis.html](http://sakimori.nims.go.jp/oneday2000/ceramis.html) [2002, June 8]
  24. Shinroku Saito, ed. Fine ceramics. New York : Elsevier Science Publishing, 1985.
  25. Frank L. Riley. Silicon nitride and related materials. J.Am.Ceram.Soc. 83 (February 2000) : 245-265.
  26. Yet-Ming Chiang, Dunbo birnic III, w. David Kingery. Physical ceramics. New York : John Wile & Sons, 1997.
  27. Pezzotti, G. et al. Growth isotherms of liquid-phase sintered silicon nitride. J.Am.Ceram.Soc.Jap. 105 (1997) : 691.
  28. Xin Xu, Liping Huang, Xuejian Liu, Xiren Fu. Effects of  $\alpha/\beta$  ratio in starting powder on microstructure and mechanical properties of silicon nitride ceramics.

- Ceramics International. 28 (2002) : 279-281.
29. Wotting, G., Ziegler, G. Powder characteristics and sintering behavior of  $\text{Si}_3\text{N}_4$ -powders. Interceram. 35 (1986)
  30. Hiroturu, H. et al. Influence of phase transformation on densification behavior and grain growth of fine silicon nitride powder. J.Am.Ceram.Soc.Jap. 104 (1995) : 24-28.
  31. Greskovich, C., and Prochazka, S. Stability of  $\text{Si}_3\text{N}_4$  and liquid phase(s) during sintering. J.Am.Ceram.Soc.Jap. (July 1981) : C-96-C-97.
  32. Standard test methods for apparent porosity, liquid absorption, apparent specific gravity, and bulk density of refractory shapes by vacuum pressure. Annual book of ASTM standards. 15.01, 14.02 (February 1993) : 137-140.
  33. Charles, P., Gazzara, and Donald R. Messier. Determination of phase content of  $\text{Si}_3\text{N}_4$  by X-Ray diffraction analysis. J.Am.Ceram.Bull. 56 (1977) : 777-780.
  34. Shigetaka Wada. Increase of oxygen content in  $\text{Si}_3\text{N}_4$  powder during ball milling using alcohol as solvent. J.Am.Ceram.Soc.Jap. 104 (1996) : 1092-1094.
  35. Hyati, M.J., and Day, D.E. Glass properties in the Yttria-Alumina-Silica system. J.Am.Ceram.Soc. 70 (1987) : C-283-C-287.
  36. Hirosaki, N., and Matsubara, H. Effect of heat treatment of  $\text{Si}_3\text{N}_4$  on grain growth behavior and grain boundary structure. J.Am.Ceram.Soc.Jap. 105 (1996) : 234-238.
  37. Kazusige Yokoyama, and Shigetaka Wada. Solid-gas reaction during sintering of  $\text{Si}_3\text{N}_4$  ceramic (Part 5). J.Am.Ceram.Soc.Jap. 108 (2000) : 627-632.
- Testing method for toughness of high performance ceramic (JIR r 1607). 1995.
- Testing method for Vickers hardness of high performance ceramic (JIS R 1610). 1991.
40. Standard test method for biaxial flexure strength (Modus of rupture) of ceramic substrates. American national standard (ANSI / ASTM F394-398). : 780-787.
  41. Bongkoch Piempempon. Improvement of thermal conductivity of alumina for peltier element. Master's Thesis, Department of Material Science. Chulalongkorn University, 2002.
  42. Hiroshi Yamashita and Akira Yamaguchi. Oxidation of Aluminum Oxynitride-Boron

- nitride (ALON-BN) composite prepared by reaction sintering.  
J.Am.Ceram.Soc.Jap. 109 (2001) : 94-99.
43. Kazusige Yokoyama, and Shigetaka Wada. Solid-gas reaction during sintering of  $\text{Si}_3\text{N}_4$  ceramic (Part 5). J.Am.Ceram.Soc.Jap. 108 (2000) : 627-632.
44. Michel W. Barsoum. Fundamentals of ceramics. International Editions. New York : McGraw-Hill Companies, 1977.
45. Hill, R., Osgood R.M., Sakaki. Jr. H., Zunger, A. Ceramics mechanical preperities failure behabior, materials selection. New York : Springer-Verlag Berlin Heidelberg, 1998 : 34-37.
46. JANAF Thermochemical Table,2d ed. U.S. Government printing office, Washington DC., 1971



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Appendices

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## APPENDIX A

Table A-1 Properties of Si<sub>3</sub>N<sub>4</sub> (1)

Type	SN-7	SN-E10
Alpha -phase (%)	74	95
Chemical composition (%)	Si = 59 N = 38 Fe = 0.3 Al = 0.2 Ca = 0.2 Mg = <0.1 O = 1.6	- - Fe = < 100 ppm Al = trace Ca = trace - O = < 2.0 Cl = < 100 ppm
Specific surface area (m <sup>2</sup> /g)	4	9-13

Table A-2 Properties of Si<sub>3</sub>N<sub>4</sub> (2)

Type	SN-KO5	SN-F2
Alpha -phase (%)	≥ 80	< 1
Chemical composition	N = 38.8 Fe ≤ 300 (ppm) Al ≤ 500 (ppm) Ca ≤ 100 (ppm) Cl ≤ 100 (ppm) O = 0.62	Free Si < 0.5 (%) - Fe = 0.2 (%) Al = 0.1 (%) Ca = 0.1 (%) - O = < 2.0* Cl = < 100 ppm
Specific surface area (m <sup>2</sup> /g)	4.0 ~ 6.0	1
Size of crystal (μm)	-	29

\* Analyzed oxygen content was 1.29 mass %

**Table A-3** Properties of Al<sub>2</sub>O<sub>3</sub> used as packing powders

Qualitative data / Grade		AKP-30	A-11	AM-21
Chemical composition	L.O.I (%)		0.01	0.05
	Fe <sub>2</sub> O <sub>3</sub> (%)		0.01	0.01
	SiO <sub>2</sub> (%)		0.01	0.02
	Na <sub>2</sub> O (%)		0.30	0.26
	Al <sub>2</sub> O <sub>3</sub> (%)	99.99	99.7	99.7
	H <sub>2</sub> O (%)		0.06	0.10
Physical composition	True specific gravity		3.93	3.95
	Apparent specific gravity			
	Packed bulk density (g/cm <sup>3</sup> )		-	1.30
	Loose bulk density (g/cm <sup>3</sup> )		-	0.70
	Mean particle size (μm)		63	4.0
	Specific surface area (m <sup>2</sup> /g)		150	-
	Pore volume (cm <sup>3</sup> /g)		0.30	-

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**Table A-4** Properties of  $Y_2O_3$  used as an additive

Properties	Details
Chemical composition (%)	$Y_2O_3 = 99.9$ $CaO = 0.0007$ $Al_2O_3 = 0.001$ $Fe_2O_3 = 0.001$ $SiO_2 = 0.0087$
Specific surface area ( $m^2/g$ )	29.9
Size of crystal ( $\mu m$ )	4.6

**Table A-5** Properties of  $Al_2O_3$  used as an additive

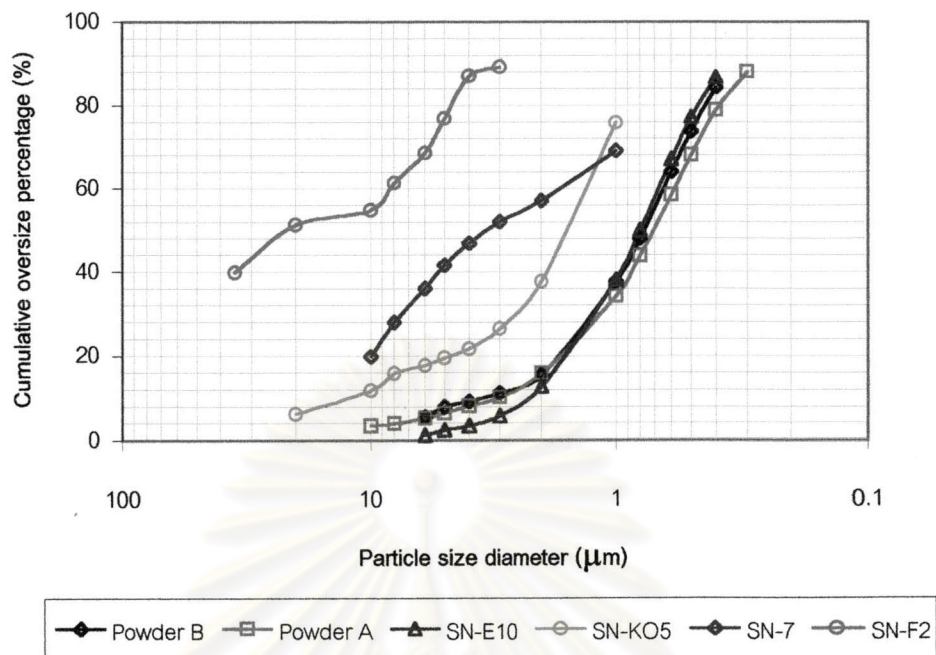
Qualitative data / Grade		AKP-30
Purity	$Al_2O_3$ (%)	99.99
Impurity Level	Fe (ppm)	$\leq 20$
	Si (ppm)	$\leq 40$
	Na (ppm)	$\leq 10$
	Mg (ppm)	$\leq 10$
	Cu (ppm)	$\leq 10$
Packed bulk density ( $g/cm^3$ )		1.1~1.5
Loose bulk density ( $g/cm^3$ )		0.7~1.1
Particle size ( $\mu m$ )		0.4~0.6
Specific surface area ( $m^2/g$ )		4-6



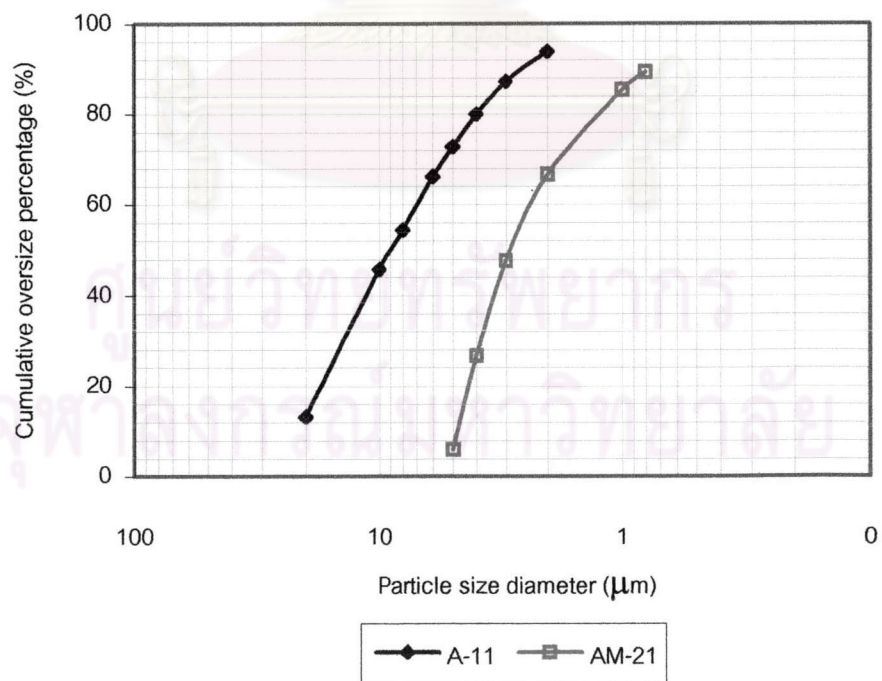
## APPENDIX B

**Table B-1** The temperature inside and outside of the crucible

T (°C)	T <sub>1</sub> (Back) (mV)	T <sub>2</sub> (Top) (mV)	T (°C)	T <sub>1</sub> (Back) (mV)	T <sub>2</sub> (Top) (mV)	T (°C)	T <sub>1</sub> (Back) (mV)	T <sub>2</sub> (Top) (mV)
29	0.00	0.00	1154	6.02	3.80	1600	10.93	10.90
106	0.10	0.00	1205	6.52	4.20	1600	10.93	10.90
156	0.10	0.00	1255	7.04	4.70	1600	10.93	10.90
204	0.10	0.00	1305	7.58	5.10	1600	10.93	10.90
251	0.26	0.00	1353	8.11	5.70	1600	10.93	10.90
307	0.37	0.08	1411	8.75	6.30	1600	10.93	10.90
353	0.52	0.10	1452	9.18	6.70	1600	10.93	10.90
408	0.70	0.20	1525	10.04	7.60	1600	10.93	10.90
453	0.88	0.20	1561	10.45	8.00	1600	10.93	10.90
483	1.10	0.30	1602	10.94	8.60	1600	10.93	10.90
556	1.35	0.50	1601	10.94	9.20	1600	10.93	10.90
601	1.62	0.60	1600	10.94	9.60	1600	10.93	10.90
656	1.95	0.80	1600	10.94	10.00	1548	10.34	10.90
703	2.23	0.90	1600	10.94	10.30	1419	8.84	10.80
754	2.56	1.10	1600	10.94	10.50	1324	7.91	10.40
805	2.98	1.40	1600	10.94	10.60	1268	7.17	9.90
853	3.31	1.60	1600	10.94	10.70	1212	6.61	9.30
906	3.76	1.90	1600	10.94	10.80	1154	6.03	8.60
949	4.11	2.20	1600	10.94	10.80	1109	5.58	8.00
1003	4.60	2.60	1600	10.94	10.80	1067	5.16	7.50
1056	5.06	3.00	1600	10.93	10.80	1023	4.79	6.90
1108	5.54	3.40	1600	10.93	10.90	986	4.43	6.40



**Fig B-1** Particle size distribution of  $\text{Si}_3\text{N}_4$  powders



**Fig B-2** Particle size distribution of  $\text{Al}_2\text{O}_3$  packing powders

**Table B-2** Particle size of SN-F2 packing powder measured by sieve analysis

NO. of sieve (mesh)	Particle size ( $\mu\text{m}$ )	Weight ratio (%)	Accumulate weight (%)
#50	300	0.00	0.00
#100	150	0.15	0.32
#140	106	4.52	9.59
#200	75	16.11	34.20
#325	45	32.11	68.16
Pan	-45	47.11	100.00

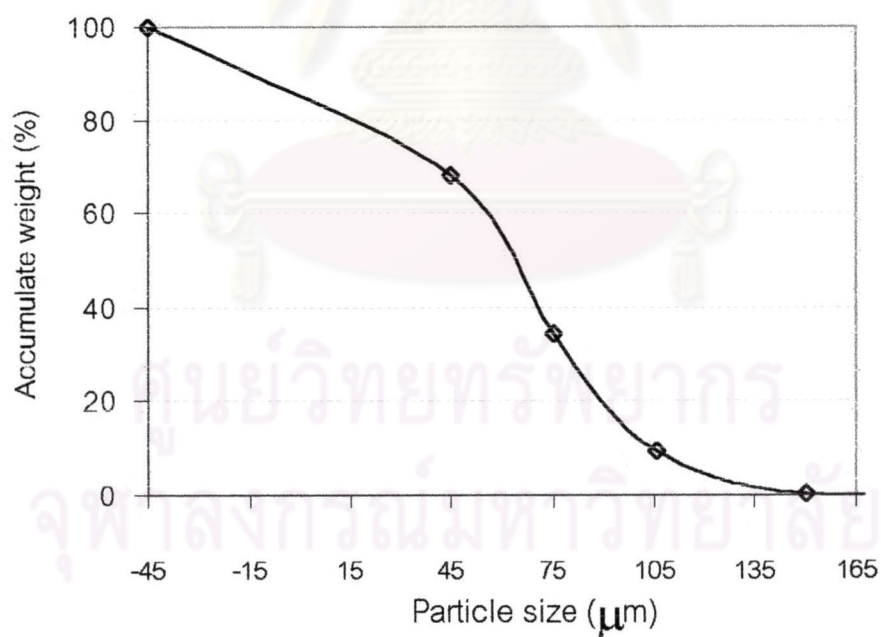
**Fig B-3** Relationship between weight ratio and particle size of SN-F2 powder by sieve analysis

Table B-3 Features of packing powder after sintering for mixed powder A

Condition No.	Temperature (°C)	Packing powder	Conglomerate		Oxide layer		surface occur			Color			Shrinkage		Lid stick		stick to crucible	
			Strong	Loose	Thick	Thin	Glass	Bubble	Crack	Gray	Creamy	White	large	Little	Strong	Little		
C1	1550, 5 °C/min	SN-7	o								o				o	o		
C2		SN-E10		o								o				o		
		AM-21	o									o	o					o
C3	1550, 5 °C/min	SN-7 (10% BN)		o					o	o					o	o		
C4		SN-E10		o					o	o					o	o		
		A-11		o							o			o				
C5	1600, 5 °C/min	SN-7 (10% BN)	o		o		o	o		o			o		o			
C6		SN-E10		o					o	o			o			o		
		A-11		o							o			o				
C7	1600, 10 °C/min	SN-7 (10% BN)	o			o	o	o		o			o		o			
C8		SN-E10		o						o			o			o		
		A-11		o							o			o				
C9	1650, 10 °C/min	SN-7 (10% BN)	o			o	o	o		o			o		o			
C10		SN-E10		o		o				o			o			o		
		A-11	o									o			o			
C11	1700, 10 °C/min	SN-7 (10% BN)	o			o				o			o			o		
C12		SN-E10		o		o				o			o			o		
		A-11	o									o			o			
	1700, 10 °C/min	SN-7 (10% BN)	No data.															
C13		SN-E10		o		o						o		o			o	
		A-11	o										o		o			o

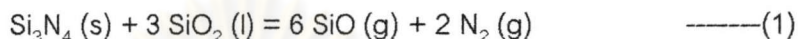
**Table B-4** Features of packing powder after sintering for mixed powder B

Condition No.	Temperature ( °c)	Packing powder	Conglomerate		Oxide layer		surface occur			Color			Shrinkage		Lid stick		stick to crucible
			Strong	Loose	Thick	Thin	Glass	Bubble	Crack	Gray	Creamy	White	large	Little	Strong	Little	
E1	1650, 10 °C/min	SN-KO5		o	o				o	o							
E2		SN-F2	o			o		o		o				o			o
		A-11		o								o					
E3,5	1700, 10 °C/min/ 1 h.	SN-KO5		o	o		o	o	o	o				o			
E4,6		SN-F2	o			o	o	o						o			
		A-11	o									o	o				
E7,8	1700, 10 OC/min/ 2 h.	SN-KO5		o			o	o	o	o				o			
E9,10		SN-F2	o				o			o			o				
		A-11	o									o	o				

## APPENDIX C

### Calculation of equilibrium $P_{\text{SiO}}(\text{g})$ as a function of temperature

In the previous work, it has been reported that the mass loss of  $\text{Si}_3\text{N}_4$  during sintering comes from the reaction between  $\text{Si}_3\text{N}_4(\text{s})$  and  $\text{SiO}_2(\text{l})$  according to reaction (1).<sup>21)</sup>



The equilibrium constant of the reaction,  $K_p$ , is calculated from the equation (2).<sup>44)</sup>

$$K_p = \frac{P_{\text{SiO}}^6 \cdot P_{\text{N}_2}^2}{a_{\text{Si}_3\text{N}_4(\text{s})} \cdot a_{\text{SiO}_2(\text{l})}} \quad \text{-----}(2)$$

As the activity of a solid and liquid is 1.<sup>44)</sup> Thus, the activity of  $\text{Si}_3\text{N}_4$ , ( $a_{\text{Si}_3\text{N}_4(\text{s})}$ ) and  $\text{SiO}_2$ , ( $a_{\text{SiO}_2(\text{l})}$ ) is 1. Then:

$$K_p = P_{\text{SiO}(\text{g})}^6 \cdot P_{\text{N}_2(\text{g})}^2 \quad \text{-----}(3)$$

From equation (3), the partial pressure of the SiO that is in equilibrium of equation (1) is determined by equation (4):

$$\Delta G = \Delta G^\circ + RT \ln K_p \quad \text{-----}(4)$$

The other extreme occurs when the driving force for the reaction is zero, that is

$\Delta G = 0$  then :

$$0 = \Delta G^\circ + RT \ln K_p$$

$$\ln K_p = -(\Delta G^\circ / RT)$$

$$\log K_p = \frac{-\Delta G^0}{2.302RT}$$

$$\log K_p = \frac{-\Delta G^0}{4.576T} \quad \text{-----}(5)$$

As equation (6),  $\Delta G^0$  is the free energy changes that calculate from the free energy of each compound  $i$  ( $\Delta G_i^0$ ). All  $\Delta G_i^0$  of each compound, which is  $\text{Si}_3\text{N}_4$  (s), Si (l),  $\text{N}_2$  (g) and Si (g)), are seen in the JANAF thermodynamic Table.<sup>46)</sup>

$$\Delta G = \Delta G_i^0(\text{products}) - \Delta G_i^0(\text{reactants}) \quad \text{-----}(6)$$

In this case, assuming Partial pressure of  $\text{N}_2$  gas,  $P_{\text{N}_2(\text{g})}$  is approximate 0.8 atm, because air includes 80 % of nitrogen.<sup>24)</sup> And  $R = 1.9872 \text{ Kcal.mol}^{-1}.\text{K}^{-1}$  is used.<sup>44)</sup>

Partial pressure of SiO gas,  $P_{\text{SiO}(\text{g})}$  calculate from take equation (3) into equation (5) Thus:

$$\log P_{\text{SiO}(\text{g})}^6 \cdot P_{\text{N}_2(\text{g})}^2 = \frac{-\Delta G^0}{4.576T}$$

$$\log P_{\text{SiO}(\text{g})}^6 + \log P_{\text{N}_2(\text{g})}^2 = \frac{-\Delta G^0}{4.576T}$$

$$6 \log P_{\text{SiO}(\text{g})} = \frac{-\Delta G^0}{4.576T} - 2 \log (0.8)$$

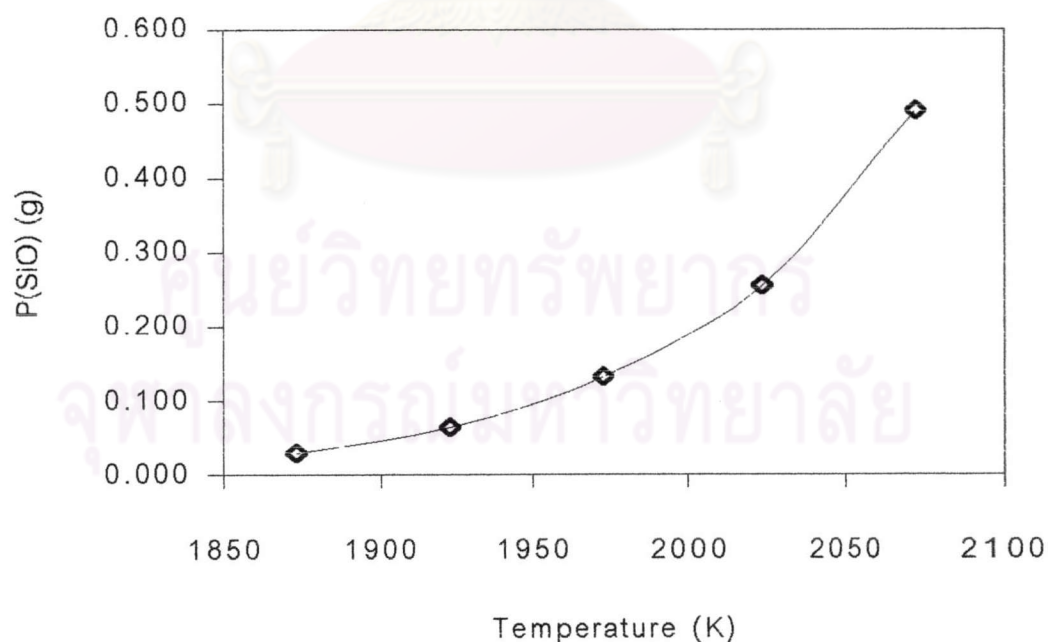
$$\log P_{\text{SiO}(\text{g})} = \left( \frac{\frac{1}{4.576T} \times (-\Delta G^0 + 0.887)}{6} \right)$$

$$P_{\text{SiO}(\text{g})} = 10^{\left( \frac{1}{27.457T} \times (-\Delta G^0 + 0.887) \right)}$$

The dependence of  $P_{\text{SiO}}(\text{g})$  upon the temperature describes by plot graph of the  $P_{\text{SiO}}(\text{g})$  calculation result versus temperature as show in Table 1. (This experimental was investigated on temperature range  $1873^{\circ}\text{C}$  to  $2023^{\circ}\text{C}$ .) In addition, The relationship between temperature ( $^{\circ}\text{C}$ ) and  $P_{\text{SiO}}(\text{g})$  is shown in Fig 1.

**Table 1** Calculation results of siliconoxide vapor pressures,  $P_{\text{SiO}}(\text{g})$  in equilibrium over  $\text{Si}_3\text{N}_4$  at on temperature range  $1600^{\circ}\text{C}$  to  $1800^{\circ}\text{C}$  ( $1873\text{ K}$  to  $2073\text{ K}$ )

T ( $^{\circ}\text{C}$ )	T (K)	$\Delta G_i^{\circ}$ (Kcal / mole)				$\Delta G^{\circ}$ (Kcal/mole)	$P_{\text{SiO}}(\text{g})$ (MPa)
		$\text{Si}_3\text{N}_4(\text{s})$	$\text{SiO}_2(\text{l})$	$\text{SiO}(\text{g})$	$\text{N}_2(\text{g})$		
1600	1873	-26.922	-137.571	-59.935	0.000	80.025	0.003
1650	1923	-22.054	-135.262	-60.491	0.000	64.894	0.006
1700	1973	-16.803	-132.961	-61.043	0.000	49.432	0.013
1750	2023	-12.347	-130.666	-61.593	0.000	34.787	0.025
1800	2073	-7.124	-128.376	-62.139	0.000	19.418	0.049



**Fig 1** Relationship between partial pressure of SiO (g) and temperature (K)



## APPENDIX D

Table D-1 Mass change, Bulk density and relative density of powder A specimens.

Code	Conditions					Sample No.	Mass change (%)	Bulk density (%)	Relative density (%)
	T (°C)	Rate (°C/min)	Soaking (h)	Packing powders					
				Si <sub>3</sub> N <sub>4</sub>	Al <sub>2</sub> O <sub>3</sub>				
C1	1550	5	2	SN-7	AM-21	1	0.71	2.49	75.91
				BN		2	0.75	2.52	76.73
C2	1550	5	2	SN-E10	AM-21	1	-0.43	2.41	73.47
						2	0.27	2.39	72.73
C3	1550	5	2	SN-7	A-11	1	-0.46	2.60	79.28
				BN		2	0.31	2.61	79.68
C4	1550	5	2	SN-E10	A-11	1	0.10	2.42	73.89
						2	2.40	2.47	75.19
C5	1600	5	2	SN-7	A-11	1	0.61	2.76	84.28
				BN		2	0.75	2.77	84.44
C6	1600	5	2	SN-E10	A-11	1	-0.99	2.81	85.56
						2	-0.38	2.76	84.15
C7	1600	10	2	SN-7	A-11	1	0.20	2.71	82.62
				BN		2	1.23	2.71	82.53
C8	1600	10	2	SN-E10	A-11	1	-0.92	2.83	86.18
						2	-0.41	2.84	86.50
C9	1650	10	2	SN-7	A-11	1	0.24	2.86	86.59
				BN		2	0.48	2.74	83.54
C10	1650	10	2	SN-E10	A-11	1	-0.74	2.94	89.63
						2	-1.91	2.97	90.55
C11	1700	10	1	SN-7	A-11	1	0.31	2.84	86.59
				BN		2	0.53	2.84	86.59
C12	1700	10	1	SN-E10	A-11	1	-0.32	2.94	89.63
						2	-1.09	2.96	90.24
C13	1700	10	2	SN-E10	A-11	1	-0.12	2.96	90.24
						2	-0.68	3.02	92.07

**Table D-2** Mass change, Bulk density and relative density of powder B specimens.

Code	Conditions					Lot No.	Mass change (%)	Bulk density (%)	Relative density (%)
	T (°C)	Rate (°C/min)	Soaking (h)	Packing powders					
				Si <sub>3</sub> N <sub>4</sub>	Al <sub>2</sub> O <sub>3</sub>				
E1	1650	10	2	SN-KO5	A-11	1	-0.20	3.10	95.09
						2	-0.72	3.08	94.48
E2	1650	10	2	SN-F2	A-11	1	-1.56	3.15	96.63
						2	-1.49	3.15	96.63
E3	1700	10	2	SN-KO5	A-11	1	-0.59	3.11	95.40
E4	1700	10	2	SN-F2	A-11	1	-0.52	3.12	95.71
E5	1700	10	2	SN-KO5	A-11	2	-0.28	3.12	95.71
E6	1700	10	2	SN-F2	A-11	2	-0.96	3.16	96.93
E7	1700	10	2	SN-KO5	A-11	1	-1.97	3.14	93.32
E8	1700	10	2	SN-F2	A-11	1	-1.44	3.16	93.93
E9	1700	10	2	SN-KO5	A-11	2	-0.95	3.15	96.93
E10	1700	10	2	SN-F2	A-11	2	-0.49	3.18	97.55

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## APPENDIX E

**Table E-1** Alpha content (%) in packing powder of powder A experiment

Temperature (°C)	Alpha content (%) SN-7+ 10 mass % BN				Alpha content (%) SN-E10			
	Top Bubble	Top	Bottom	No Layer	Top bubble	Top	Bottom	No Layer
1600 (5°C/min)	-	78.9	72.1	-	-	-	-	-
1600 (10°C/min)	-	71.7	82.6	-	-	-	-	100
1650 (10°C/min)	87.7	70.9	61.1	-	-	100	100	-
1700, 1 h (10°C/min)	-	80.0	75.9	-	-	94.9	96.4	-
1700, 2 h (10°C/min)	-	-	-	-	-	-	-	95.4

**Table E-2** Alpha content (%) in packing powder of powder B experiment

Temperature (°C)	Alpha Content (%) SN-KO5		Alpha Content (%) SN-F2	
	Top	Bottom	Top	Bottom
1650 (10°C/min)	69.7	79.8	4.9	2.5
1700, 1 h (10°C/min)	73.3	78.1	5.7	2.8
1700, 2 h (10°C/min)	73.3	75.8	3.5	2.3

**Table E-3** Crystal phase in SN-E10 and SN-7 packing powders after sintering

Type		Raw mat.	5°C/min 1600°C	10°C/min 1600°C	10°C/min 1650°C	10°C/min 1700°C	10°C/min 1700°C		
SN-E10	Top	$\alpha$	$\alpha+X_1$	-	$\alpha+X_1$	$\alpha+\beta+X_1$	$\alpha+\beta$		
	Bottom				$\alpha$	$\alpha+\beta$			
SN-7		$\alpha+\beta$	-	-	-	-	-		
SN-7+BN	Glassy phase	$\alpha+\beta$ +BN			$\alpha+\beta+BN$				
	Top				$\alpha+\beta+BN$ + $X_1$	$\alpha+\beta+BN$	$\alpha+\beta+BN$	$\alpha+\beta+BN$	-
	Bottom				$\alpha+\beta+BN$	$\alpha+\beta+BN$	$\alpha+\beta+BN$	$\alpha+\beta+BN$	-

**Table E-4** Crystal phase in SN-F2 and SN-KO5 packing powders after sintering

Type		10°C/min, 1650°C, 2 h	10°C/min, 1700°C, 1h	10°C/min, 1700°C, 2 h
SN-F2	Top surface	$\beta+X_1+X_2$	$\beta+X_1+X_2$	$\beta+X_2$
	Bottom surface	$\beta$	$\beta$	$\beta+X_2$
SN-KO5	Top surface	$\alpha+\beta+X_1$	$\alpha+\beta+X_1$	$\alpha+\beta+X_1$
	Bottom surface	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$

**Note:**  $X_1$ = Cristobalite

$X_2$ = Sinoite,  $Si_2N_2O$

**Table E-5** Alpha content (%) in specimens of powder A experiment

Temperature (°C)	Alpha content (%) SN-7+ 10 mass % BN		Alpha content (%) SN-E10	
	5 °C/min	10 °C/min	5 °C/min	10 °C/min
1550, 2 h	20.9	-	94.9	-
1550, 2 h	-	92.4	-	78.3
1600, 2 h	48.9	-	82.2	-
1600, 2 h	-	60.6	-	71.8
1650, 2 h	-	21.6	-	48.3
1700, 1 h	-	30.1	-	34.9
1700, 2 h	-	-	-	20.9

**Table E-6** Alpha content (%) in specimens of powder B experiment

Temperature (°C)	Alpha Content (%) SN-KO5		Alpha Content (%) SN-F2	
	Lot 1	Lot 2	Lot 1	Lot 2
1650, 2 h (10 °C/min)	48.5	-	34.3	30.5
1700, 1 h (10 °C/min)	48.2	52.4	40.9	39.3
1700, 2 h (10 °C/min)	25.8	25.2	14.5	18.5

**Table E-7** Crystal phase in Mixed powder A specimens

Powder packing		5°C/min, 1550°C, 2 h.	5°C/min, 1600°C, 2 h.	10°C/min, 1600°C, 2 h.	10°C/min, 1650°C, 2 h.	10°C/min, 1700°C	
						1 h.	2 h.
Sintering with SN-7	SN-E10 Crucible	$\alpha+\beta$	-	-	-	-	-
	SN-7 Crucible	$\alpha+\beta$	-	-	-	-	-
Sintering with SN-7 + BN	SN-E10 Crucible	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta+x_2$
	SN-7 Crucible	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	$\alpha+\beta$	-

**Table E-8** Crystal phase in Mixed powder B specimens

Temperature (°C)	Sintering with SN-KO5 packing powder		Sintering with SN-F2 packing powder	
	Lot 1	Lot 2	Lot 1	Lot 2
10°C/min, 1650°C	$\alpha+\beta+x_2+x_3$	-	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$
10°C/min, 1700°C, 1 h.	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$
10°C/min, 1700°C, 2 h.	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$	$\alpha+\beta+x_2+x_3$

Note:  $X_2 = \text{Si}_2\text{N}_2\text{O}$

$X_3 = \text{Unknown}$

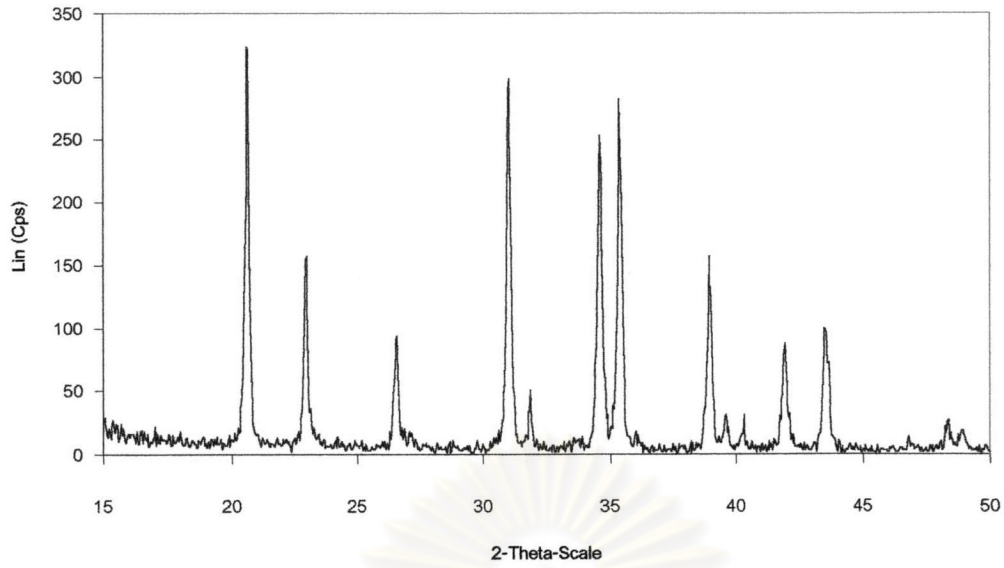


Fig E-1 X-ray diffraction pattern of the SN-E10 packing powder raw material

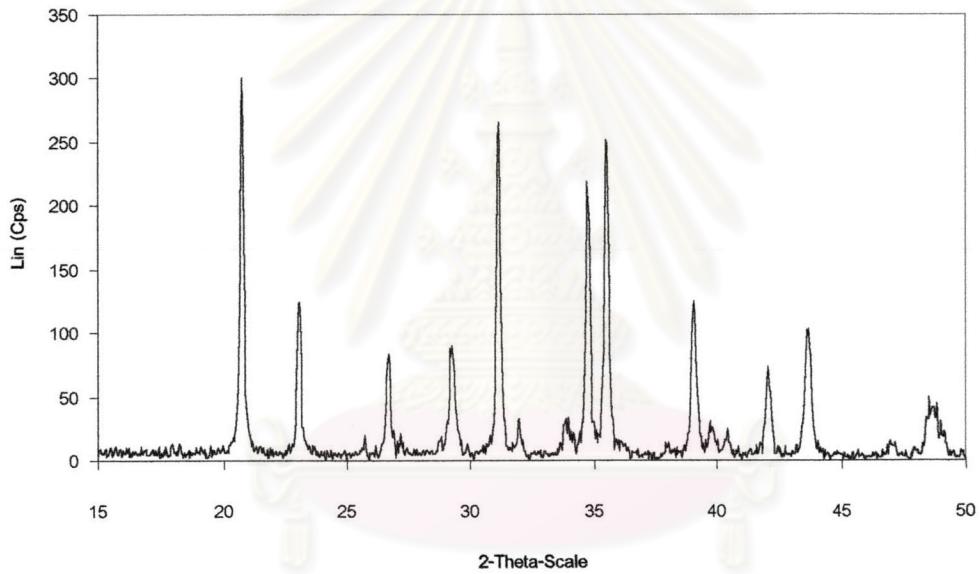


Fig E-2 X-ray diffraction pattern of the Mix powder A raw material

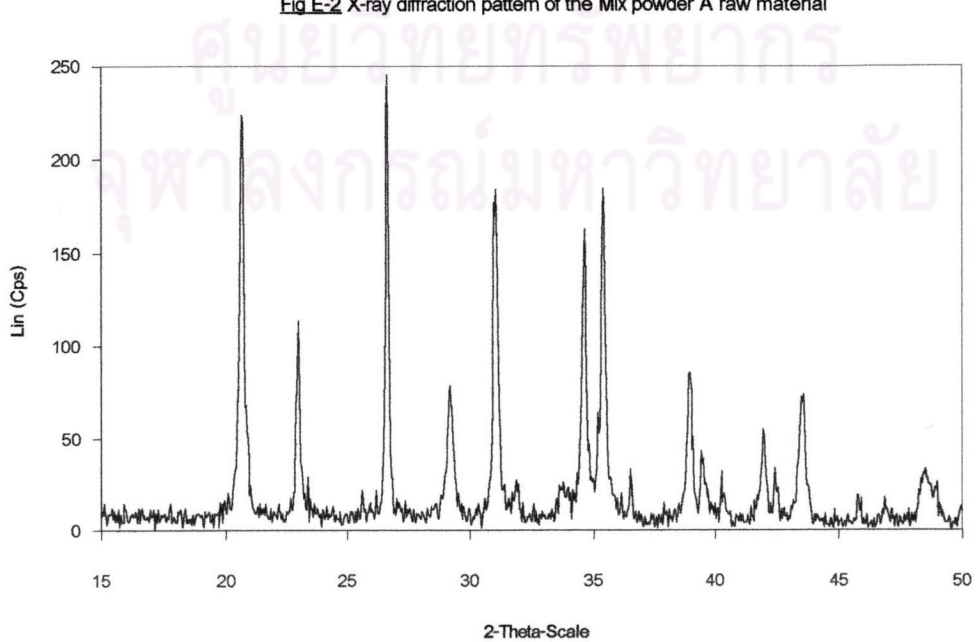


Fig E-3 X-ray diffraction pattern of Mix powder B raw material

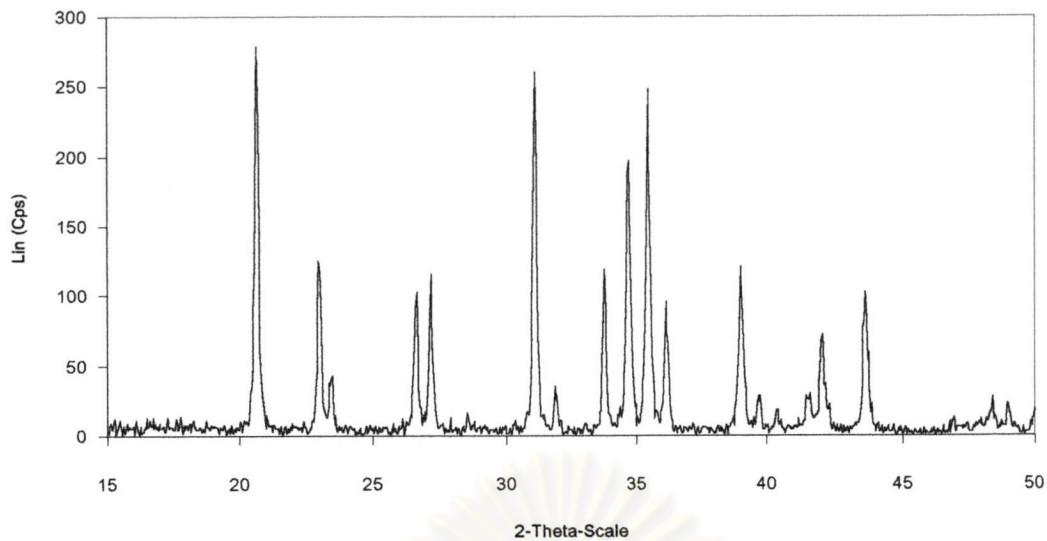


Fig E-4 X-ray diffraction of the SN-7 packing powder raw material

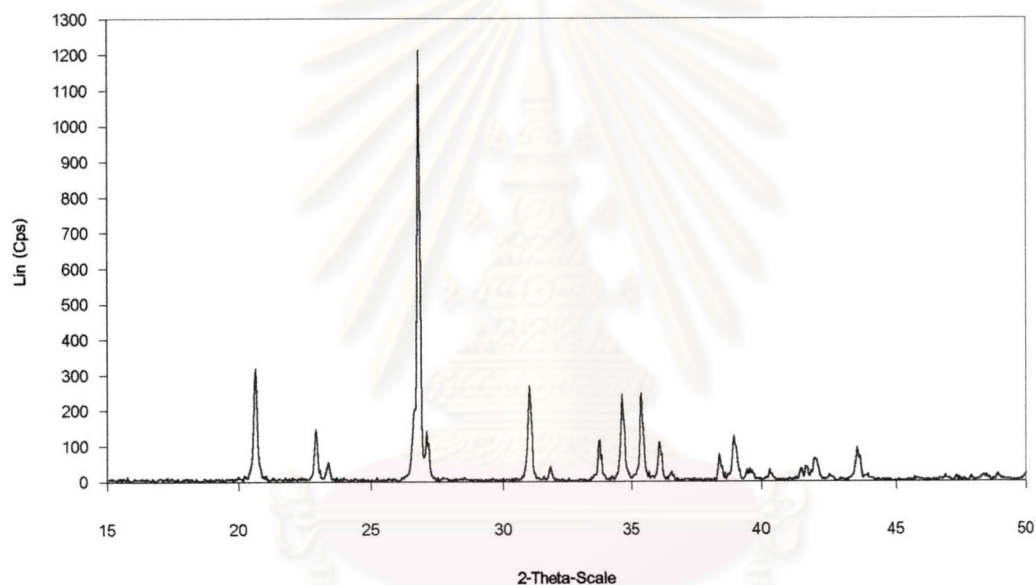


Fig E-5 X-ray diffraction of the SN-7+10 mass % BN packing powder raw material

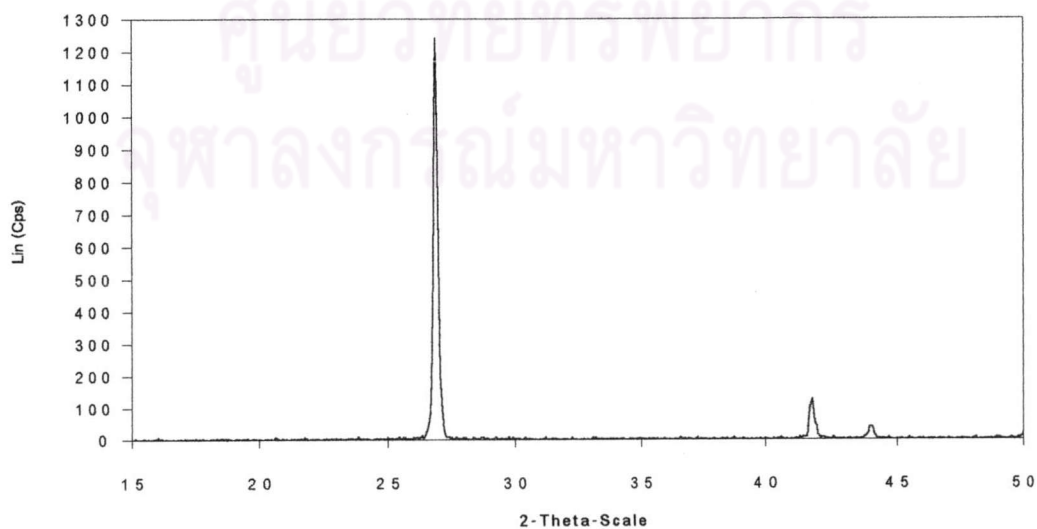


Fig E-6 X-ray diffraction pattern of boron nitride raw material raw material



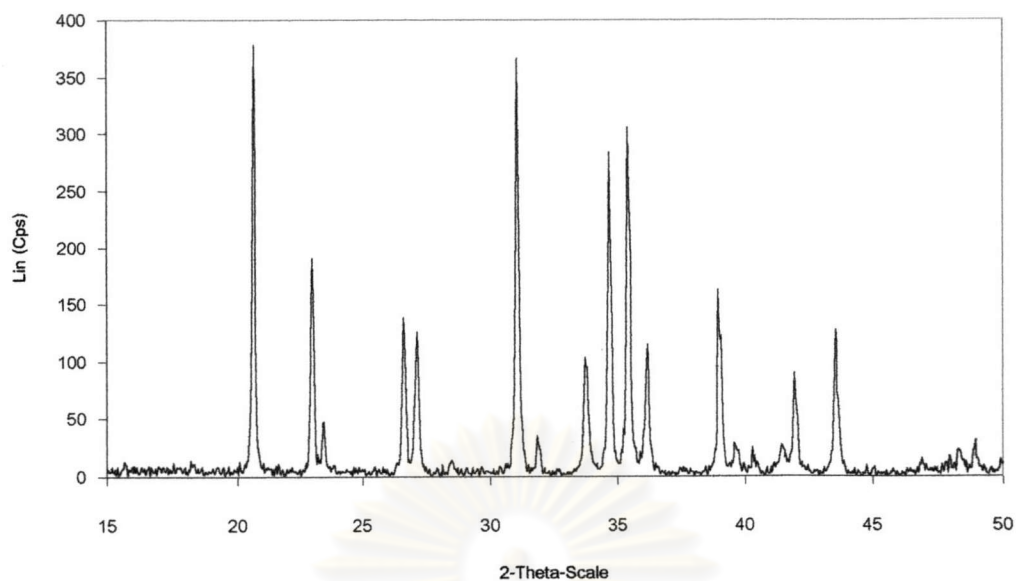


Fig E-7 X-ray diffraction pattern of SN-KO5 packing powder raw material

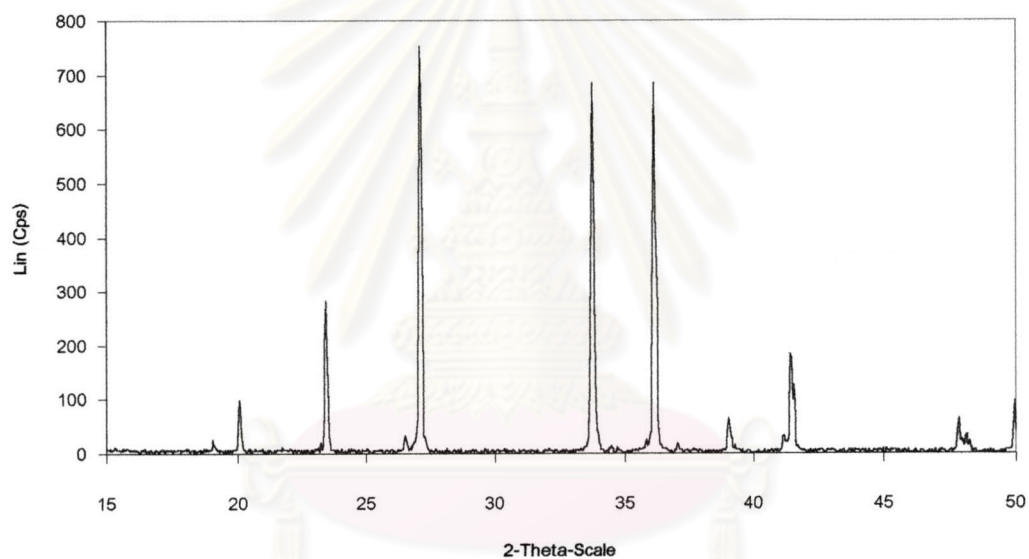


Fig E-8 X-ray diffraction pattern of SN-F2 packing powder raw material

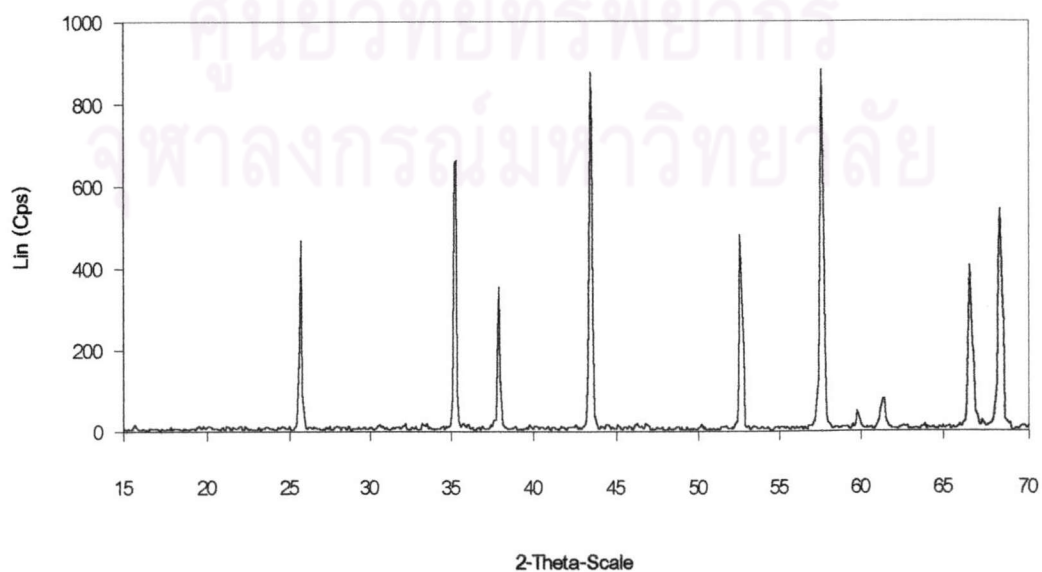
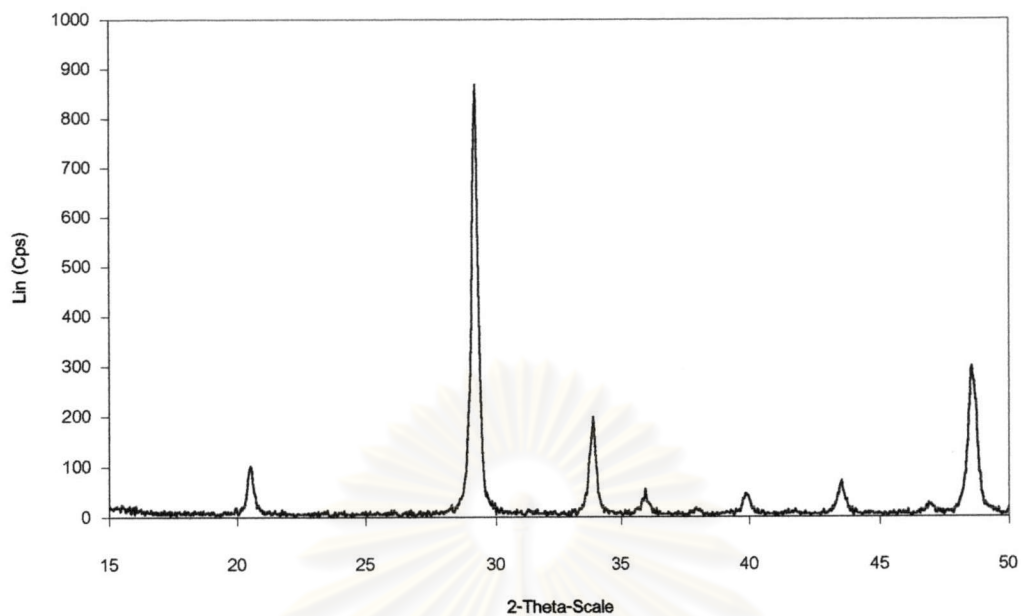
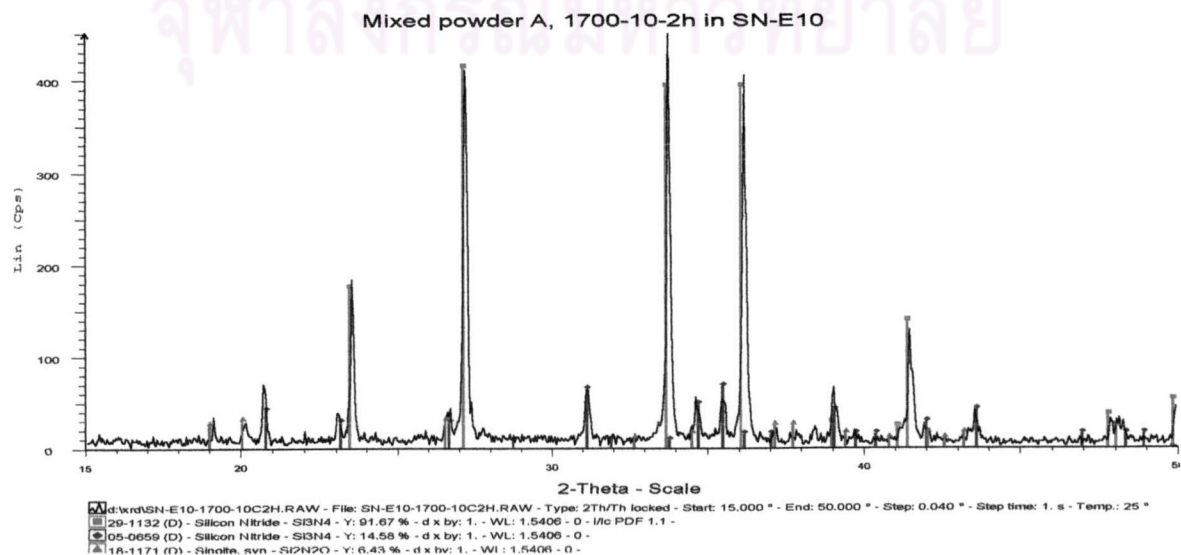
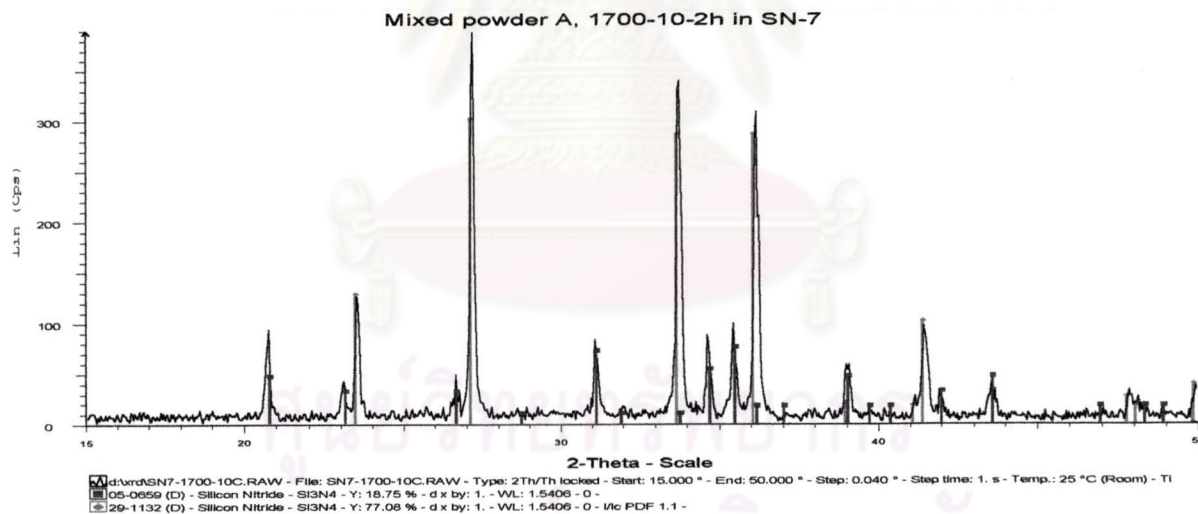
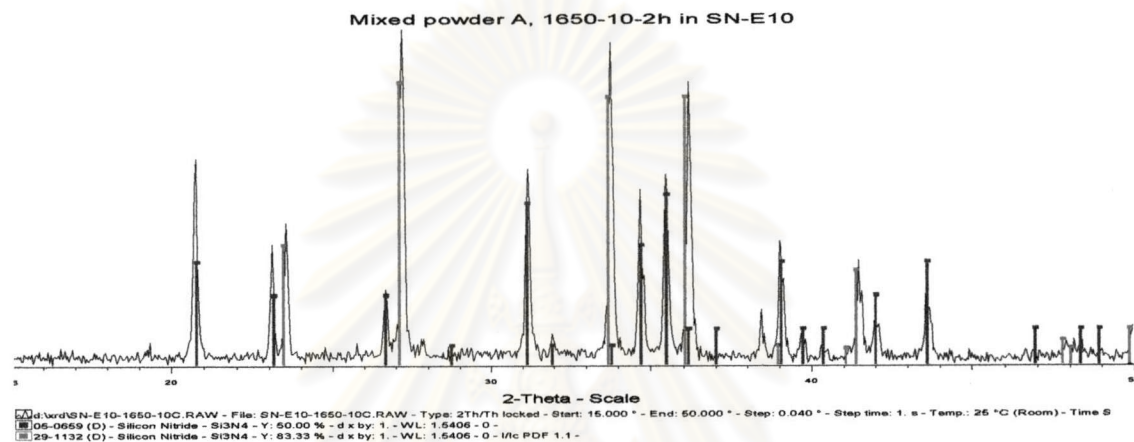
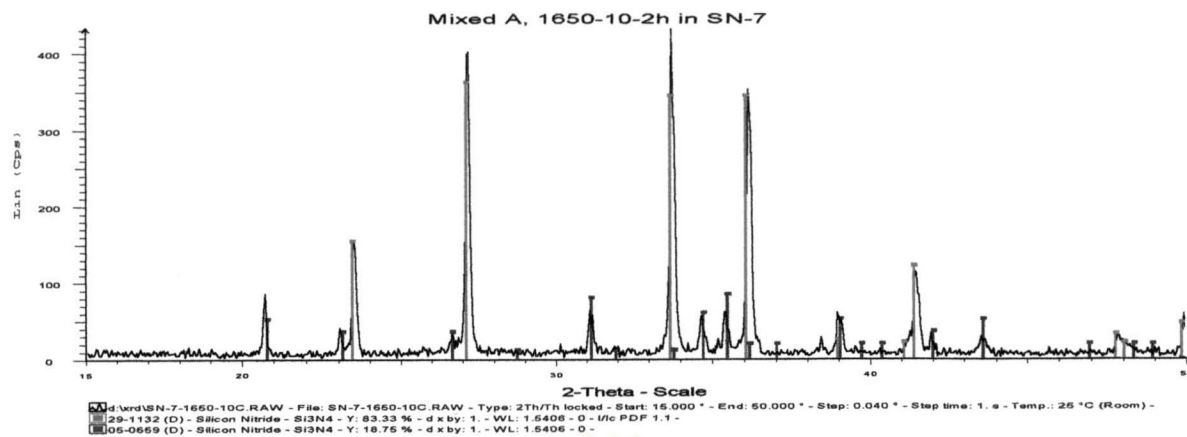


Fig E-9 X-ray diffraction pattern of A-11 packing powder after sintering

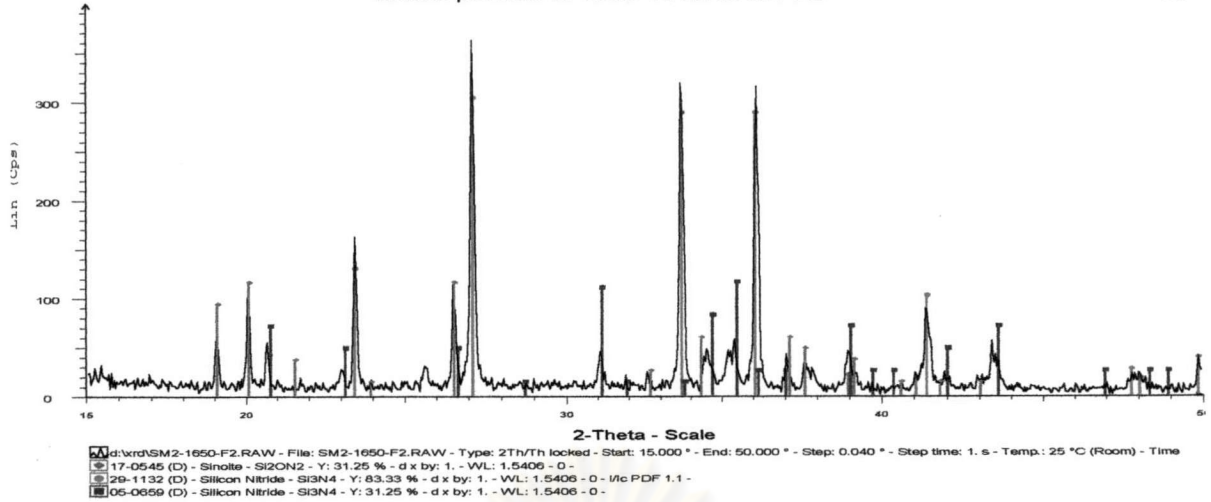


Appendix E-10 X-ray diffraction patten of  $Y_2O_3$  raw material

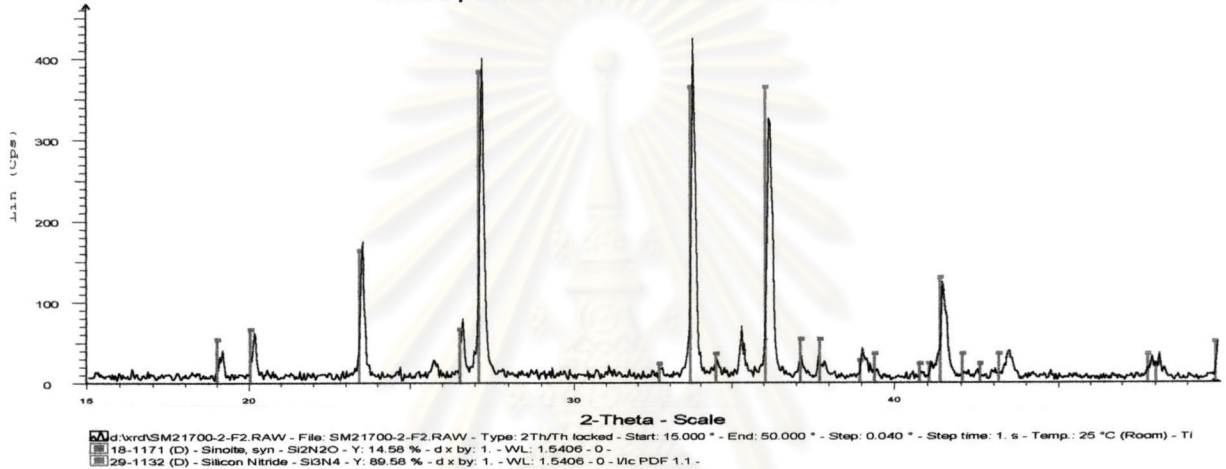
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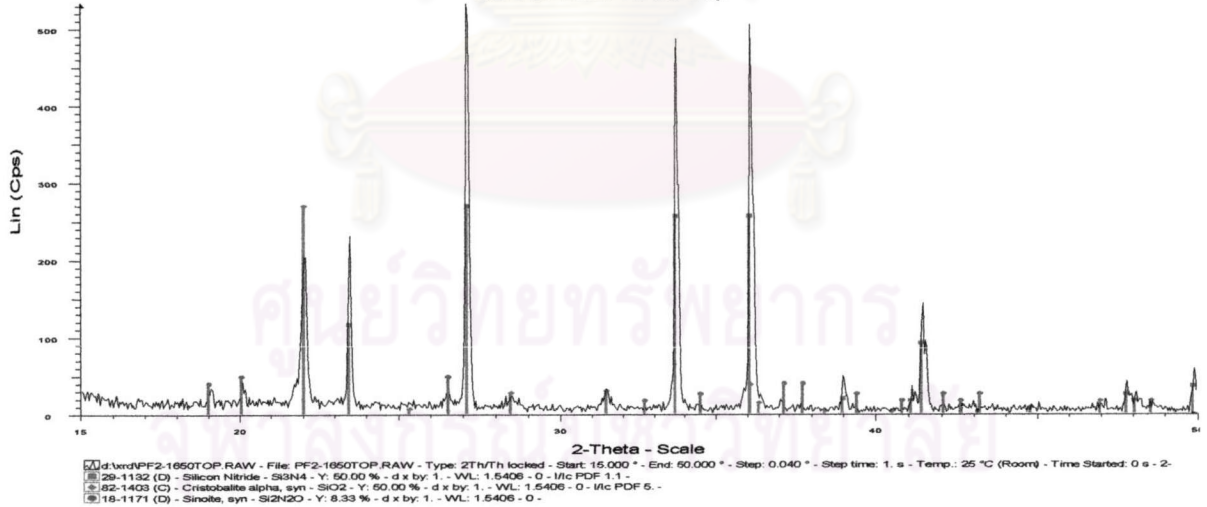
Mixed powder B 1650-10-2h in SN-F2



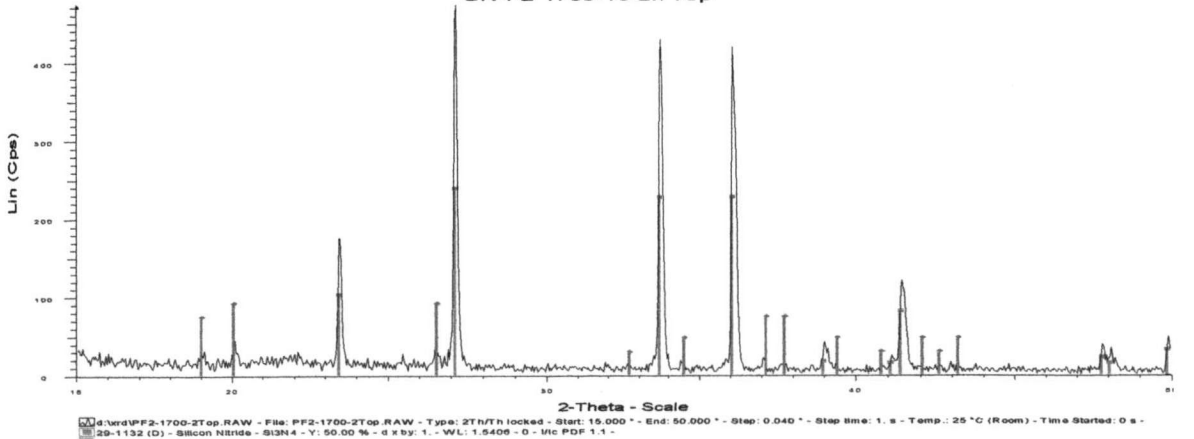
Mixed powder B 1700-10-2h in SN-F2



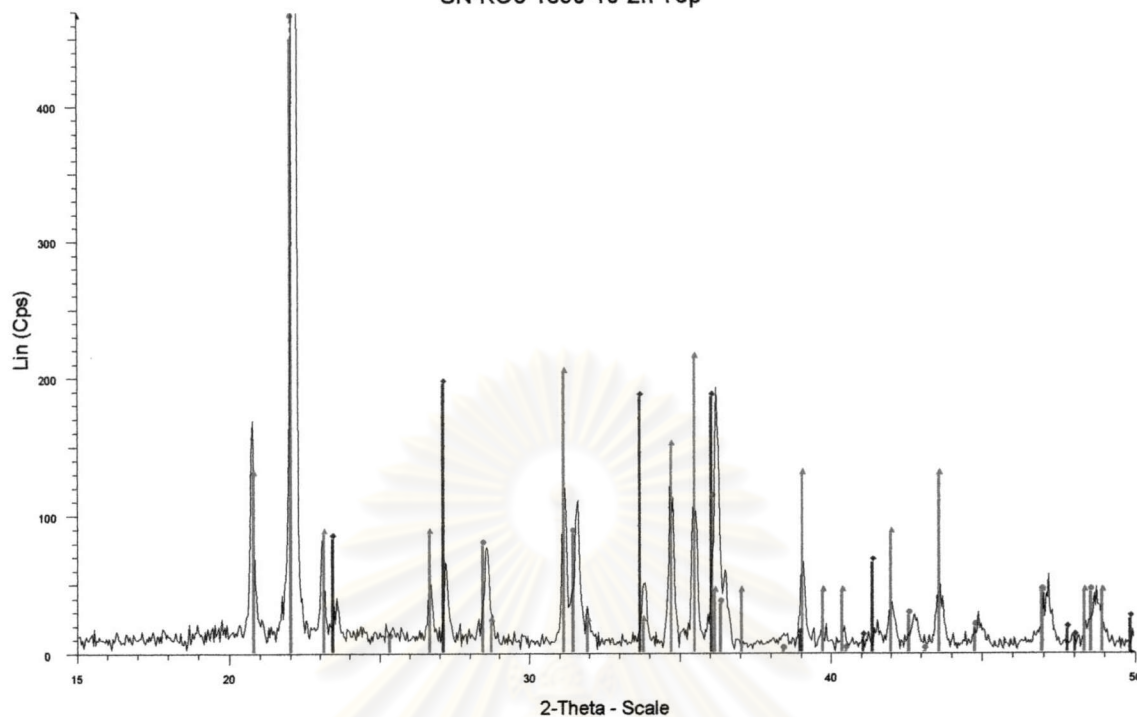
SN-F2 1650-10-2h Top



SN-F2 1700-10-2h Top



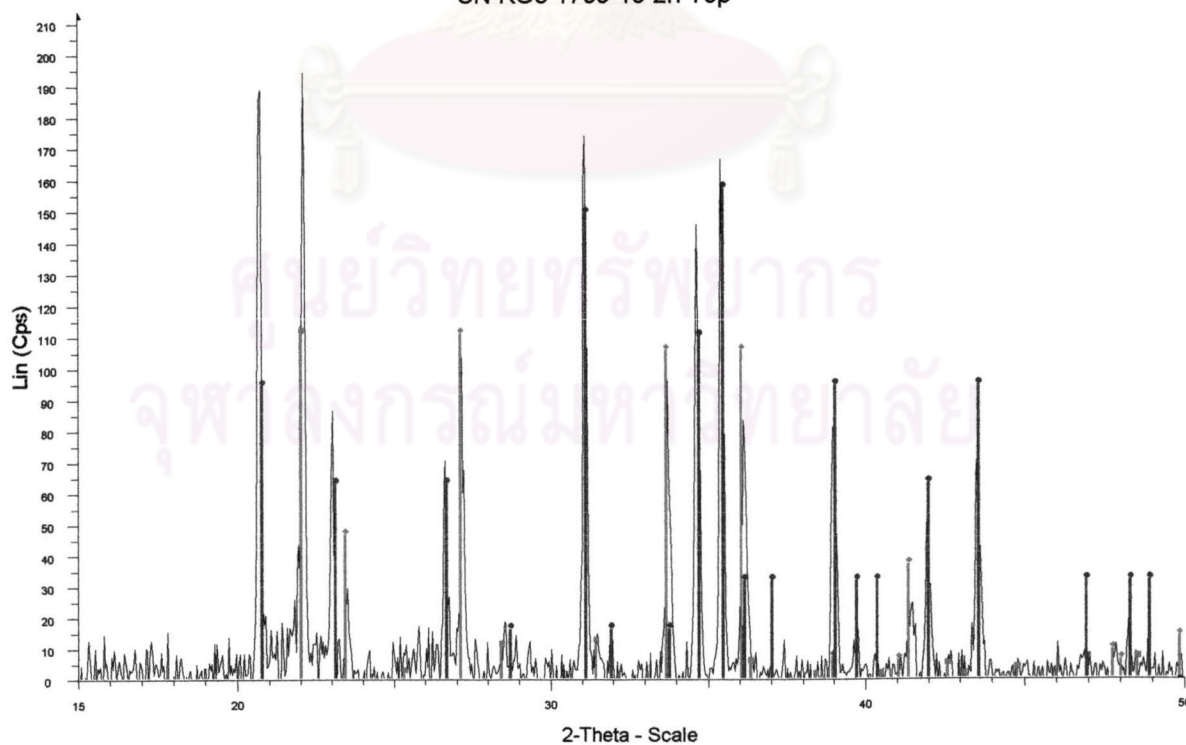
## SN-KO5 1650-10-2h Top



d:\vrd\PKO5-1650-Top.RAW - File: PKO5-1650-Top.RAW - Type: 2Th/Th locked - Start: 15.000 ° - End: 50.000 ° - Step: 0.040 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time Started: 0 s

- 29-1132 (D) - Silicon Nitride - Si3N4 - Y: 15.20 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 1.1 -
- 82-1403 (C) - Cristobalite alpha, syn - SiO2 - Y: 66.67 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 5. -
- ▲ 05-0659 (D) - Silicon Nitride - Si3N4 - Y: 16.67 % - d x by: 1. - WL: 1.5406 - 0 -

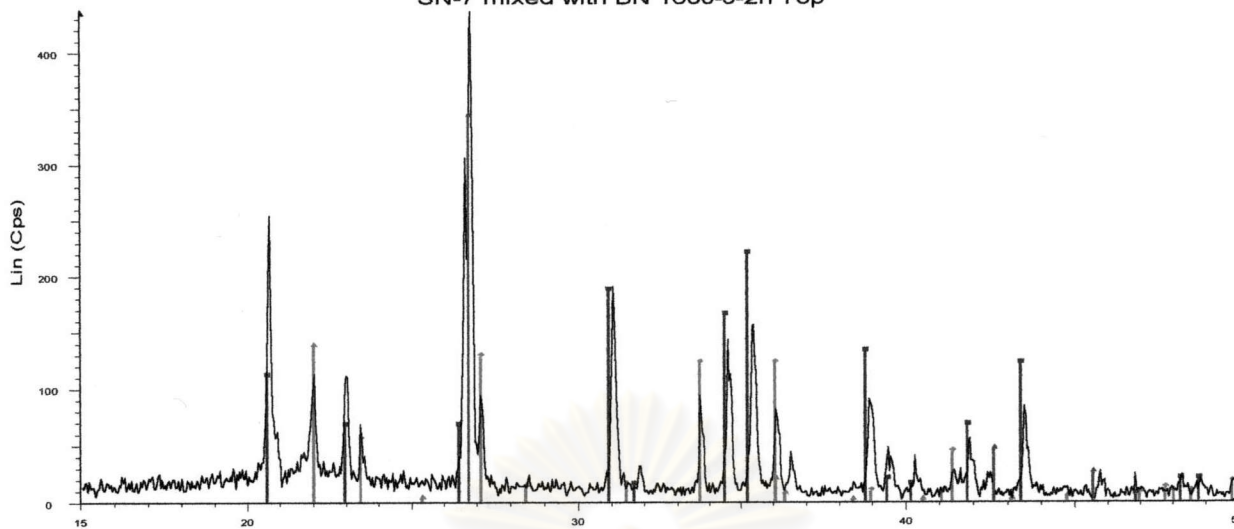
## SN-KO5 1700-10-2h Top



d:\vrd\PKO5-1700-2TOP.RAW - File: PKO5-1700-2TOP.RAW - Type: 2Th/Th locked - Start: 15.000 ° - End: 50.000 ° - Step: 0.040 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time Started:

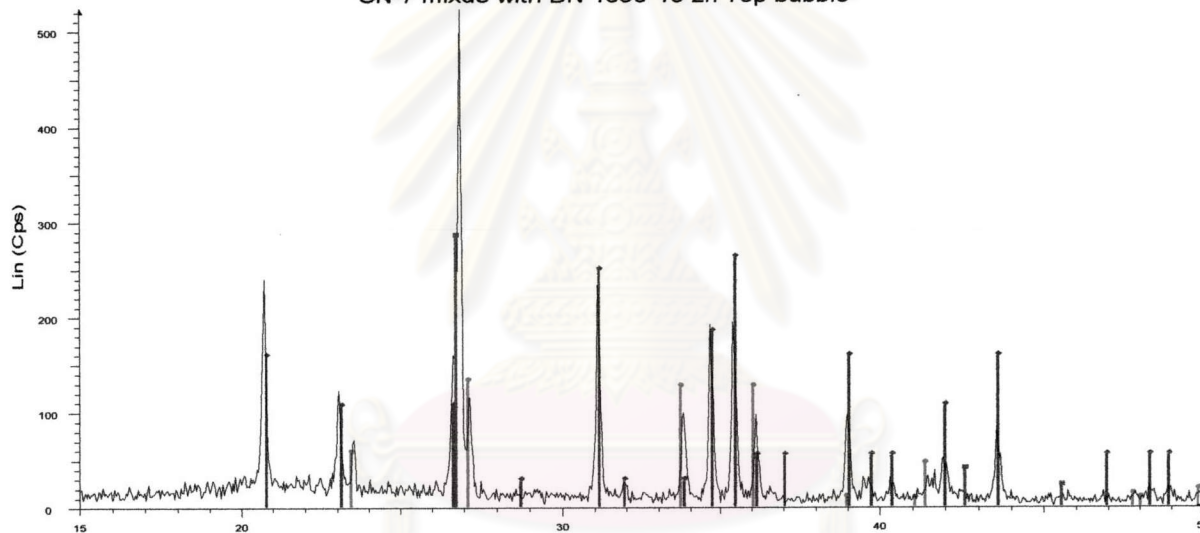
- 82-1403 (C) - Cristobalite alpha, syn - SiO2 - Y: 50.00 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 5. -
- 29-1132 (D) - Silicon Nitride - Si3N4 - Y: 50.00 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 1.1 -
- 05-0659 (D) - Silicon Nitride - Si3N4 - Y: 70.83 % - d x by: 1. - WL: 1.5406 - 0 -

SN-7 mixed with BN 1600-5-2h Top



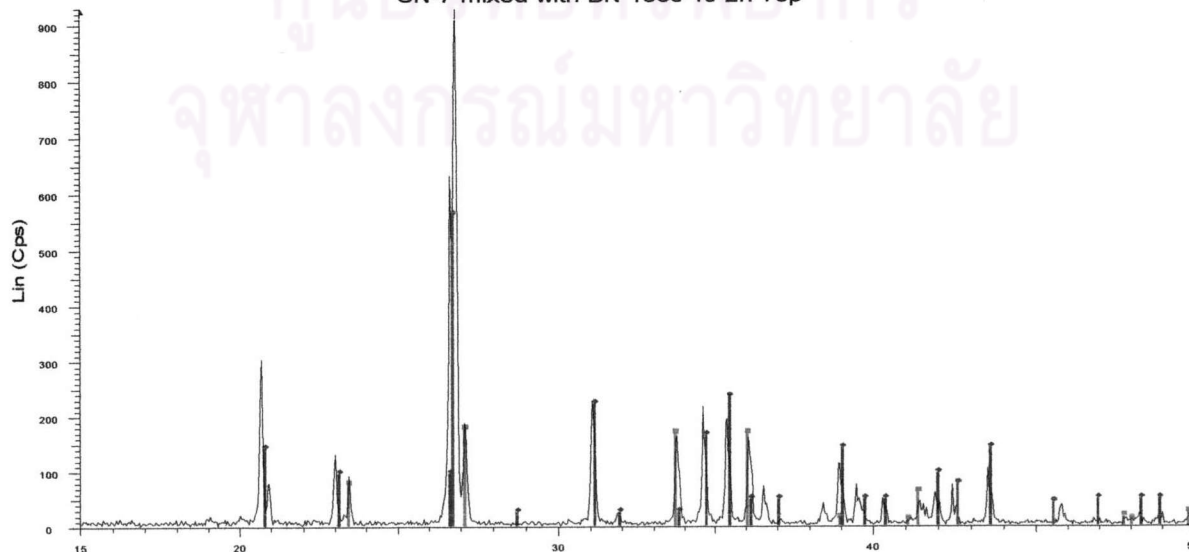
d:\vrd\SN-7,1600 Top (5 c).RAW - File: SN-7,1600 Top (5 c).RAW - Type: 2Th/Th locked - Start: 15.000 ° - End: 50.000 ° - Step: 0.040 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time Star  
 09-0250 (D) - Silicon Nitride - Si3N4 - Y: 50.00 % - d x by: 1. - WL: 1.5406 - 0 -  
 29-1132 (D) - Silicon Nitride - Si3N4 - Y: 29.17 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 1.1 -  
 82-1403 (C) - Cristobalite alpha, syn - SiO2 - Y: 31.25 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 5. -  
 45-1171 (I) - Boron Nitride - BN - Y: 78.33 % - d x by: 1. - WL: 1.5406 - 0 -

SN-7 mixde with BN 1650-10-2h Top bubble



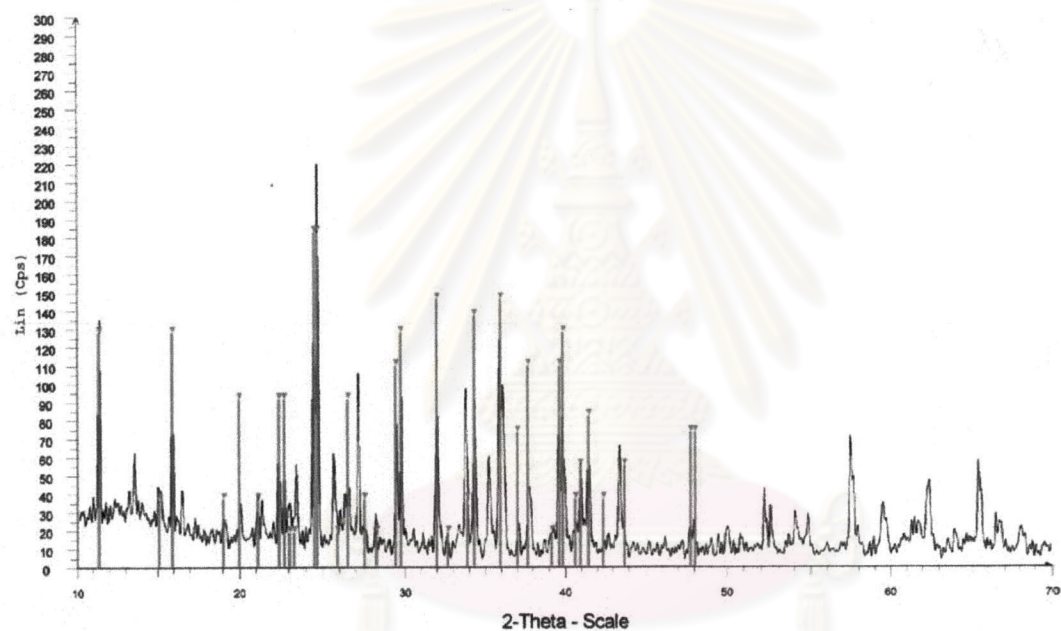
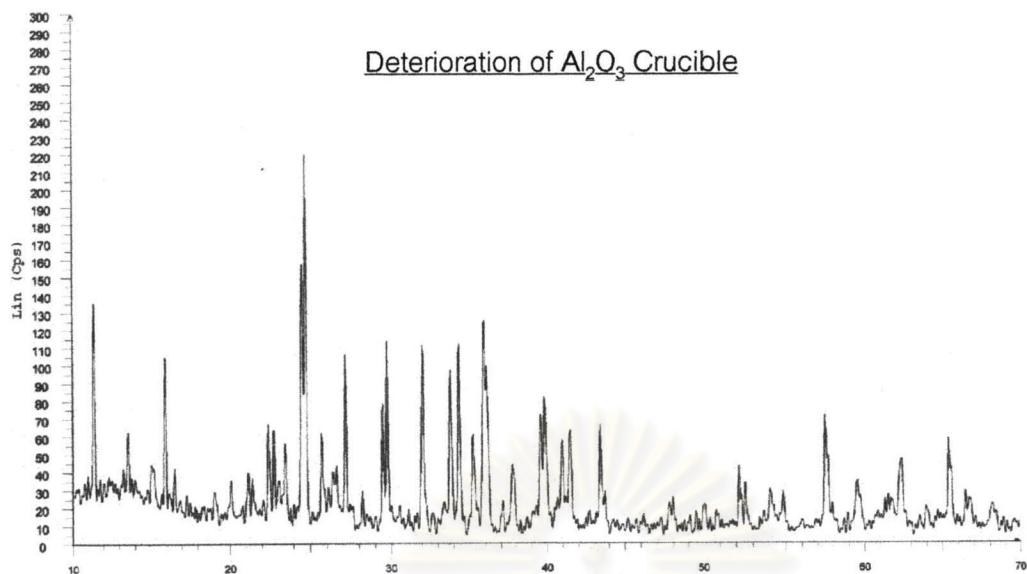
d:\vrd\SN-7,1650 Top bubble(10 c).RAW - File: SN-7,1650 Top bubble(10 c).RAW - Type: 2Th/Th locked - Start: 15.000 ° - End: 50.000 ° - Step: 0.040 ° - Step time: 1. s - Temp.: 25 °C (Ro  
 45-1171 (I) - Boron Nitride - BN - Y: 54.17 % - d x by: 1. - WL: 1.5406 - 0 -  
 05-0659 (D) - Silicon Nitride - Si3N4 - Y: 50.00 % - d x by: 1. - WL: 1.5406 - 0 -  
 29-1132 (D) - Silicon Nitride - Si3N4 - Y: 25.00 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 1.1 -

SN-7 mixed with BN 1650-10-2h Top

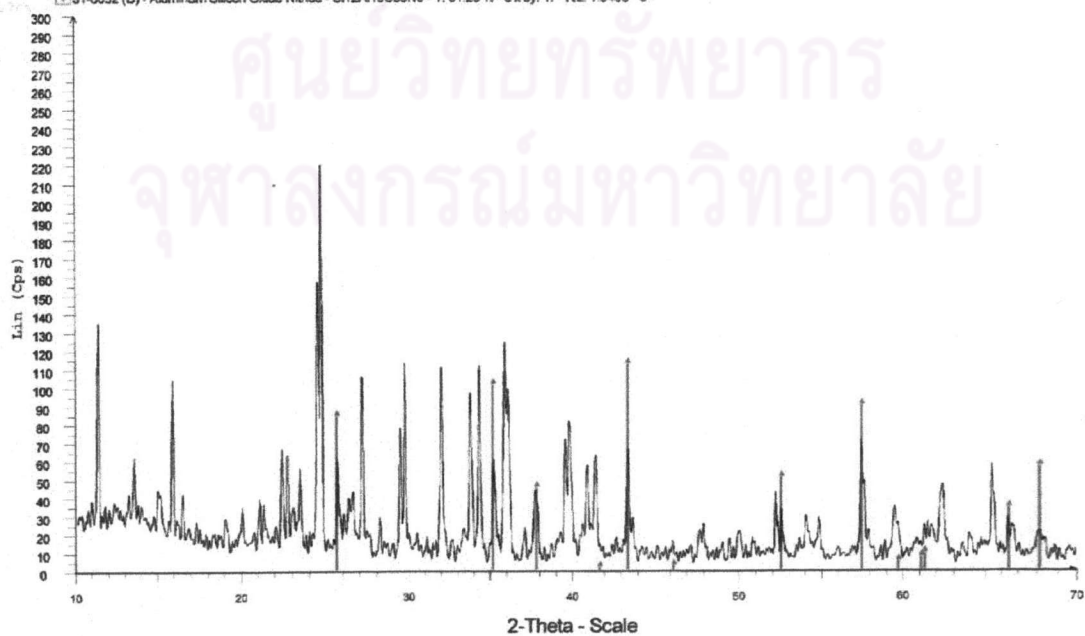


d:\vrd\SN-7,1650c(10c) Top.RAW - File: SN-7,1650c(10c) Top.RAW - Type: 2Th/Th locked - Start: 15.000 ° - End: 50.000 ° - Step: 0.040 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time St  
 29-1132 (D) - Silicon Nitride - Si3N4 - Y: 18.75 % - d x by: 1. - WL: 1.5406 - 0 - I/c PDF 1.1 -  
 05-0659 (D) - Silicon Nitride - Si3N4 - Y: 25.00 % - d x by: 1. - WL: 1.5406 - 0 -  
 45-1171 (I) - Boron Nitride - BN - Y: 60.42 % - d x by: 1. - WL: 1.5406 - 0 -

### Deterioration of $\text{Al}_2\text{O}_3$ Crucible



d:\word\MS1.RAW - File: is1.raw - Type: 2Th/Th locked - Start: 10.000 ° - End: 70.000 ° - Step: 0.050 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time Started: 0 s - 2-Theta: 31-0032 (D) - Aluminum Silicon Oxide Nitride - Si12Al18O39N8 - Y: 81.25 % - d x by: 1. - WL: 1.5406 - 0 -



d:\word\MS1.RAW - File: is1.raw - Type: 2Th/Th locked - Start: 10.000 ° - End: 70.000 ° - Step: 0.050 ° - Step time: 1. s - Temp.: 25 °C (Room) - Time Started: 0 s - 2-Theta: 10-0173 (I) - Corundum, syn - Al2O3 - Y: 50.00 % - d x by: 1. - WL: 1.5406 - 0 - Wc PDF 1. -

## APPENDIX F

**Table F-1** Results of fracture toughness ( $K_{IC}$ ) and Vickers hardness (Hv) of sintered specimens at 1700 °C. (Crack length was measured by SEM)

Conditions (Soaking time)	Sample No. (Piece)	c ( $\mu\text{m}$ )	A ( $\mu\text{m}$ )	$K_{IC}$ ( $\text{MPa} \cdot \text{m}^{(1-2)}$ )	HV (GPa)
1 h	1	95.60	51.45	4.90	17.16
	2	88.20	52.95	5.18	16.22
	3	126.50	50.00	4.33	18.18
	4	120.60	50.00	4.40	18.18
	5	123.50	51.45	4.50	17.16
Average				4.66	17.38
2 h	1	102.90	54.40	5.05	15.35
	2	97.10	54.40	5.15	15.35
	3	97.10	52.95	5.01	16.24
	4	105.90	52.95	4.87	16.24
	5	102.90	52.95	4.91	16.24
Average				5.00	15.88

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**Table F-2** Results of fracture toughness ( $K_{IC}$ ) and Vickers hardness (Hv) of sintered specimens at 1700 °C. (Crack length was measured by Optical microscope, OM)

Conditions (Soaking time)	Sample No. (Piece)	c ( $\mu\text{m}$ )	a ( $\mu\text{m}$ )	$K_{IC}$ ( $\text{MPa} \cdot \text{m}^{(1-2)}$ )	HV (GPa)
1 h	1	93.20	51.40	5.29	17.21
	2	102.30	53.50	5.13	15.88
	3	108.90	51.40	5.05	17.21
	4	90.40	52.30	5.40	16.62
	5	105.00	53.50	4.99	15.88
Average				5.17	16.56
2 h	1	85.00	54.80	5.47	15.14
	2	93.70	54.30	4.90	15.42
	3	96.40	53.60	5.07	15.82
	4	96.20	52.90	5.24	16.25
	5	97.40	53.20	5.01	16.06
Average				5.13	15.74

Note: Scale 1 mm = 20  $\mu\text{m}$

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**Table F-3** Calculation results of flexural strength, S.

Lot of powder B	Sample No. (Piece)	Diameter, c (mm)	Thickness, d (mm)	P (N)	S (MPa)
Lot 3	1	2.71	1.48	762.00	487.26
	2	2.71	1.48	715.80	457.72
	3	2.71	1.48	791.40	506.06
	4	2.71	1.48	577.20	369.09
	5	2.71	1.48	542.60	346.97
	6	2.73	1.47	678.80	434.06
	7	2.71	1.46	608.10	388.85
Average					427.14
Lot 4	1	2.73	1.44	621.20	397.23
	2	2.71	1.48	740.20	473.32
	3	2.71	1.48	582.90	372.74
	4	2.73	1.51	391.00	250.03
	5	2.71	1.49	730.50	467.12
	6	2.71	1.50	684.00	437.38
	7	2.70	1.49	530.60	339.29
Average					414.51

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### Appendix G

Properties of TOSHIBA's specimen (standard bars)

1. Chemical composition

Composition ( mass %)			
Si <sub>3</sub> N <sub>4</sub>	Y <sub>2</sub> O <sub>3</sub>	Al <sub>2</sub> O <sub>3</sub>	TiO <sub>2</sub>
89.5	4.5	5.0	1.0

2. Estimated real density:

$$3.31 \text{ g/cm}^3$$

The calculation was performed assuming that 1 % of Si<sub>3</sub>N<sub>4</sub> is oxygen. Then, the contents of Si<sub>3</sub>N<sub>4</sub> and SiO<sub>2</sub> are 87.82 g and 1.67 g, respectively. Densities of SiO<sub>2</sub>, Y<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub> and Si<sub>3</sub>N<sub>4</sub> are 2.20, 4.84, 4.00, 4.25 and 3.21 g/cm<sup>3</sup>, respective.

3. Bulk density and relative density

Measured bulk density was 3.19 g/cm<sup>3</sup>. Then, relative density is 96.4 %

4. Vickers' Hardness

16.0 GPa

5. Fracture Toughness

Crack length was measured by optical microscope. K<sub>1C</sub> was calculated by two equations.

Crack	K <sub>1C</sub> (MPa.m <sup>1/2</sup> )
Median crack	5.0
Palmqvist crack	5.9

$$K_{1C} = 0.026 \{E^{1/2} P^{1/2} (a/c)^{-3/2}\} \quad \text{for Median cracks}$$

$$K_{1C} = 0.018 H(a^{1/2})(E/H^{0.4})\{(c/a)-1\}^{-1/2} \quad \text{for Median cracks}$$

Young's Modulus, E = 280 GPa.

## BIOGRAPHY

Miss. Piyaporn Chaiyapuck was born in Sisaket on 12<sup>th</sup> of July 1977. She was received a Bachelor Degree in Ceramic Engineering from Faculty of Engineer, Suranaree University in 2000. After graduating, she worked at Casday Co. Ltd. for a year and continued study in Master Degree in the field of Ceramic Technology at Chulalongkorn University and graduated in June 2003.



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