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APPENDICES

Appendix A Calculation Algorithm Method of Tray (IFP's Method)

1. Calculate liquid flow on tray by Francis Weir Formula (equation 3.15).
2. Calculate accumulate and composition on tray by equation E.3 and equation E.6
3. Calculate temperature tray by bubble point equation (appendix B).
4. Calculate vapor flow by E.8 (energy equation, steady-state assumption).

Appendix B Calculation Temperature from Bubble Point Equation

1. Assume a value of temperature
2. Calculate vapor pressure from Antoine's equation
3. Calculate vapor composition and sum value of all vapor composition.
4. Calculate new temperature by use Newton's method
5. Go back to step 2 until new temperature convergence.

Appendix C Response Curves of Tuning Parameter

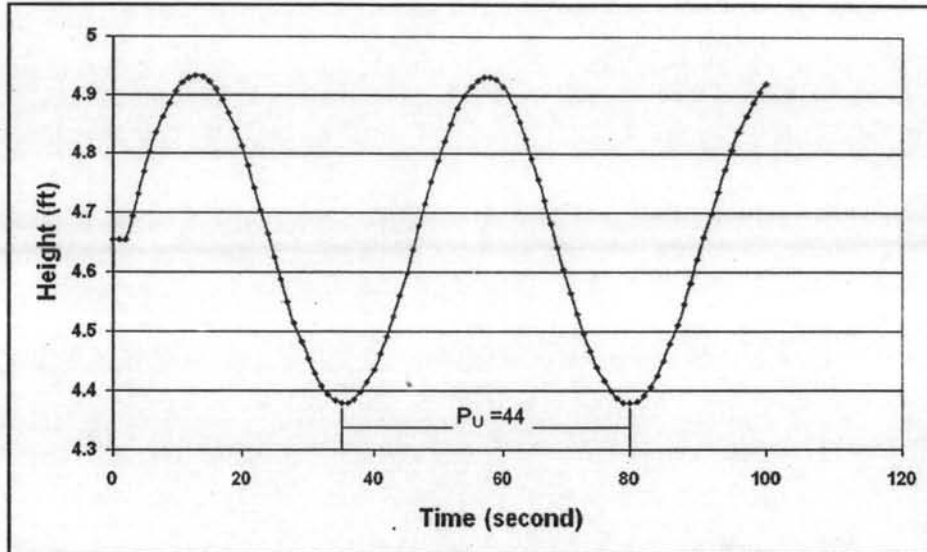


Figure C.1 Response curve of height of gravitational flow tank using feed back control with at $K=0.0193$ with disturbance of changing input volumetric flow rate per tank area from 0.311 to 0.35 ft/s.

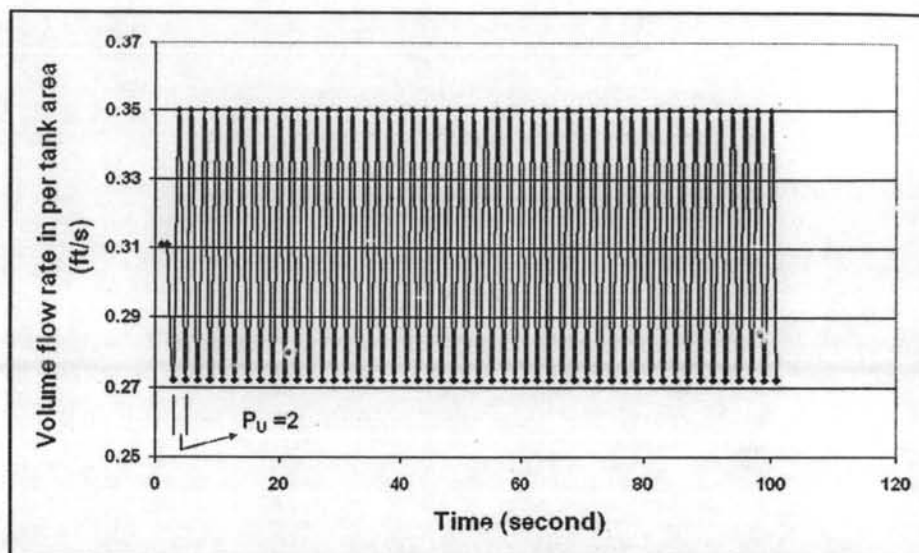


Figure C.2 Response curve of input volumetric flow rate in per tank area of gravitational flow tank with feed forward control at $K=2$ with disturbance of changing input volumetric flow rate per tank area from 0.311 to 0.35 ft/s.

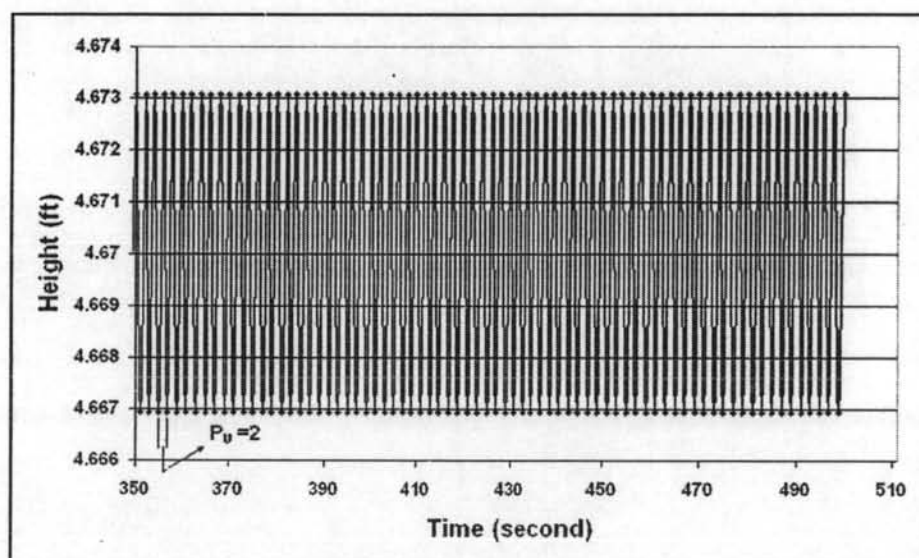


Figure C.3 Response curve of height of gravitational flow tank with cascade control at K of primary controller=0.33339 with disturbance of changing set point from 4.6546 to 4.67 ft/s.

Secondary controller uses the value from feed forward control.

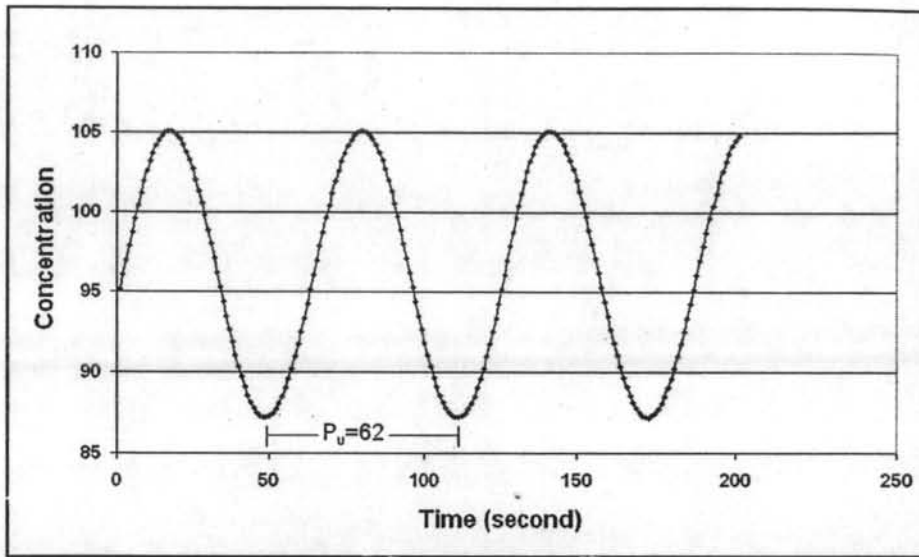


Figure C.4 Response curve of concentration of plug-flow plus CSTR with feedback control at K of controller = 0.1048 after changing feed flowrate from 4 to 5 kmol/s.

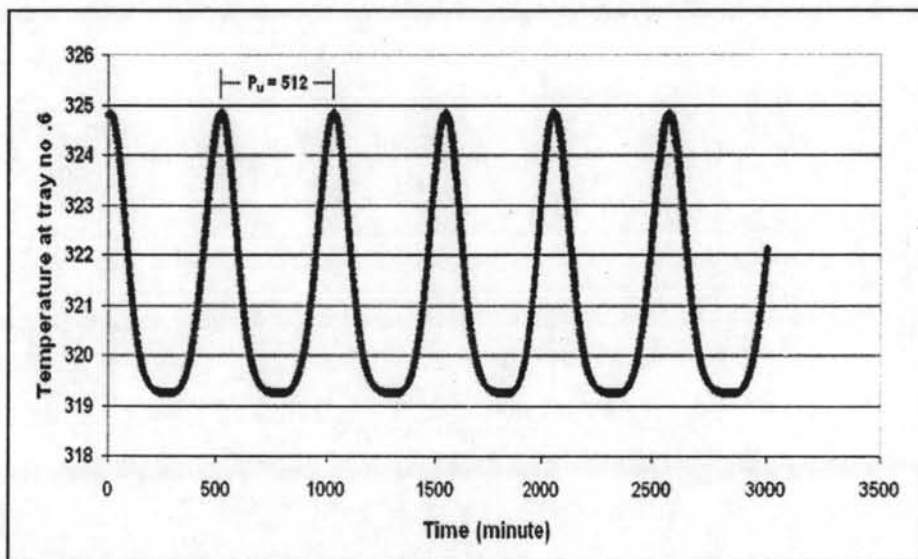


Figure C.5 Response curve of temperature of tray no.6 of top cascade control at $K = 0.00002$ with disturbance of changing disturbance from 0.5:0.5 to 0.3:0.7 (propane:butane).

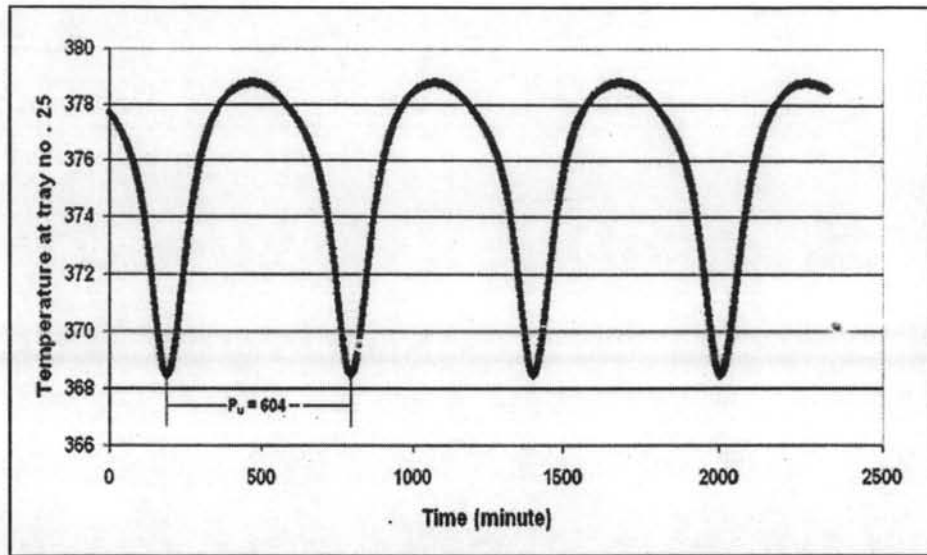


Figure C.6 Response curve of temperature of tray no.6 of bottom cascade control at $K = 0.00001$ with disturbance of changing disturbance from 0.5:0.5 to 0.3:0.7 (propane:butane).

Appendix D Liquid and Vapor Enthalpy

Liquid and vapor enthalpy are calculated from data in table D.1 and D.2 by used cubic splines function in digital visual fortran program.

Table D.1 Liquid enthalpy

Temperature(K)	Propane(Kcal/Kmol)	Butane(Kcal/Kmol)
273.15	902.24	1125.79
273.15	1221.82	1481.22
273.15	1564.33	1847.22
273.15	1938.14	2227.85
273.15	2360.87	2623.56
273.15	2887.39	3036.26
273.15	3675.48	3468.77
273.15	3937.55	3925.29
273.15	4204.17	4412.81
273.15	4475.33	4944.49

Table D.2 Vapor enthalpy

Temperature(K)	Pressure(Bar)	Propane(Kcal/Kmol)	Butane(Kcal/Kmol)
313.15	1	4653.41	6128.56
323.15	1	4840.63	6381.99
333.15	1	5032.22	6641.07
343.15	1	5228.2	6905.82
353.15	1	5428.62	7176.25
363.15	1	5633.48	7452.38
373.15	1	5842.8	7734.19
383.15	1	6056.6	8021.67
393.15	1	6274.86	8314.8

Table D.2 (Con'd) Vapor enthalpy

403.15	1	6497.6	8613.56
313.15	5	4539.02	5966.78
323.15	5	4735.51	6165.19
333.15	5	4935.2	6455.61
343.15	5	5138.41	6740.21
353.15	5	5345.35	7025.55
363.15	5	5556.17	7313.81
373.15	5	5770.99	7605.95
383.15	5	5989.88	7902.47
393.15	5	6212.92	8203.68
403.15	5	6440.13	8509.75
313.15	10	4366.94	5966.78
323.15	10	4580.95	6165.19
333.15	10	4793.92	6361.11
343.15	10	5008.23	6553.18
353.15	10	5224.93	6764.9
363.15	10	5444.61	7097.64
373.15	10	5667.64	7411.93
383.15	10	5894.24	7724.62
393.15	10	6124.6	8039.06
403.15	10	6538.82	8356.61
313.15	15	4175.28	5966.78
323.15	15	4386.16	6165.19
333.15	15	4623.34	6361.12
343.15	15	4853.6	6553.18
353.15	15	5083.22	6739.61
363.15	15	5314.25	6917.97
373.15	15	5547.67	7142.29

Table D.2 (Con'd) Vapor enthalpy

383.15	15	5784.04	7500.3
393.15	15	6023.71	7837.22
403.15	15	6266.9	8171.6
313.15	20	4175.29	5966.78
323.15	20	4246.78	6165.19
333.15	20	4405.16	6361.11
343.15	20	4667.77	6553.18
353.15	20	4916.29	6739.61
363.15	20	5162.5	6917.97
373.15	20	5409.37	7084.84
383.15	20	5658.19	7235.06
393.15	20	5909.66	7578.38
403.15	20	6164.23	7945.05

Appendix E Numerical Method Of Depropanizer Column

Mole balance

$$\frac{d(AM_j)}{dt} = A_j + V_{j+1} + L_{j-1} - V_j - L_j \quad (E.1)$$

Applying implicit Euler method to equation E.1

$$AM_{j,k+1} = AM_{j,k} + (A_{j,k+1} + V_{j+1,k+1} + L_{j-1,k+1} - \dot{V}_{j,k+1} - L_{j,k+1})dt \quad (E.2)$$

Applying BALL hypothesis (1961) which is $V_{j+1,k+1} = V_{j+1,k}$ and $V_{j,k+1} = V_{j,k}$ to equation E.2 and $y_{j+1,k+1} = y_{j+1,k}$ and $y_{j,k+1} = y_{j,k}$ to equation E.5.

$$AM_{j,k+1} = AM_{j,k} + (A_{j,k+1} + V_{j+1,k} + L_{j-1,k+1} - V_{j,k} - L_{j,k+1})dt \quad (E.3)$$

Composition balance

$$\frac{dx_j AM_j}{dt} = A_j z_j + L_{j-1} x_{j-1} + V_{j+1} y_{j+1} - V_j y_j - L_j x_j \quad (E.4)$$

Use implicit Euler method and BALL hypothesis on equation E.4

$$x_{j,k+1} AM_{j,k+1} = x_{j,k} AM_{j,k} + (A_{j,k+1} z_{j,k+1} + L_{j-1,k+1} x_{j-1,k+1} + V_{j+1,k} y_{j+1,k} - V_{j,k} y_{j,k} - L_{j,k+1} x_{j,k+1})dt \quad (E.5)$$

Rearrange equation E.5

$$x_{j,k+1} = \frac{x_{j,k} AM_{j,k} + (A_{j,k+1} z_{j,k+1} + L_{j-1,k+1} x_{j-1,k+1} + V_{j+1,k} y_{j+1,k} - V_{j,k} y_{j,k})dt}{AM_{j,k+1} + L_{j,k+1} dt} \quad (E.6)$$

Energy balance (steady state assumption)

$$0 = h_{A,k+1} A_{j,k+1} + h_{j+1,k+1}^L L_{j+1,k+1} + h_{j-1,k}^V V_{j-1,k} - h_{j,k+1}^L L_{j,k+1} - h_{j,k+1}^V V_{j,k+1} \quad (E.7)$$

Rearrange equation E.7

$$V_{j,k+1} = \frac{h_{A,k+1} A_{j,k+1} + h_{j+1,k+1}^L L_{j+1,k+1} + h_{j-1,k}^V V_{j-1,k} - h_{j,k+1}^L L_{j,k+1}}{h_{j,k+1}^V} \quad (E.8)$$

Where

j is the tray index.

k is the time index

A is the feed flowrate.

AM is the accumulate on tray.

dt is the time step.

h_A is the enthalpy of feed flowrate.

h^L is the enthalpy of liquid.

h^V is the enthalpy of vapor.

L is the liquid flowrate.

V is the vapor flowrate.

x is the liquid composition.

y is the vapor composition.

z is the feed composition.

Appendix F Numerical Methods

F.1 Explicit Euler's method

In the model, Euler's method is used for explicit calculation. This method is used for replacing integration of some equation. For example, material, mass, and component balance equation.

$$y_{i+1} = y_i + f(x_i, y_i) * h \quad (\text{F.1})$$

Where

y_{i+1} is the value at new time step.

y_i is the value at previous time step.

$f(x_i, y_i)$ is the function at previous time step.

h is the step time.

There are many methods of root finding in numerical method. For instant, bisection, regular falsi. In this work, Root finding method used in distillation model is Newton-Raphson convergence.

$$x_{i+1} = x_i - \frac{f_i}{f_i'} \quad (\text{F.2})$$

Where

x_{i+1} is the value at new step time.

x_i is the value at old step time.

f_i is the function.

f_i' is the first derivative of function.

F.2 Implicit Euler's method

Implicit method is faster than explicit method. Implicit method gives stable and converge solution with larger time step compared to explicit method.

$$y_{i+1} = y_i + f'(x_{i+1}, y_{i+1}) * h \quad (\text{F.3})$$

Where

y_{i+1} is the value at new step time.

y_i is the value at old step time.

$f'(x_{i+1}, y_{i+1})$ is the first derivative at new step time.

h is the step time.

F.3 Integral Absolute Error (IAE)

IAE is calculated by equation F.4.

$$\text{IAE} = \int \text{abs}(\text{error})dt \quad (\text{F.4})$$

Appendix G Response Curves of Step Response for DMC

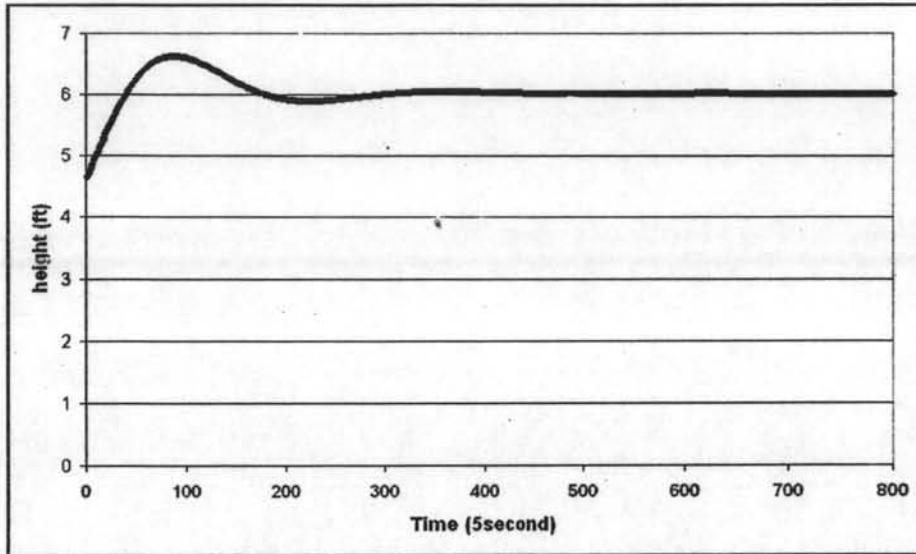


Figure G.1 Response curve of liquid level in gravitational flow tank with step of feed flow rate in per tank area at 0.039 ft/s.

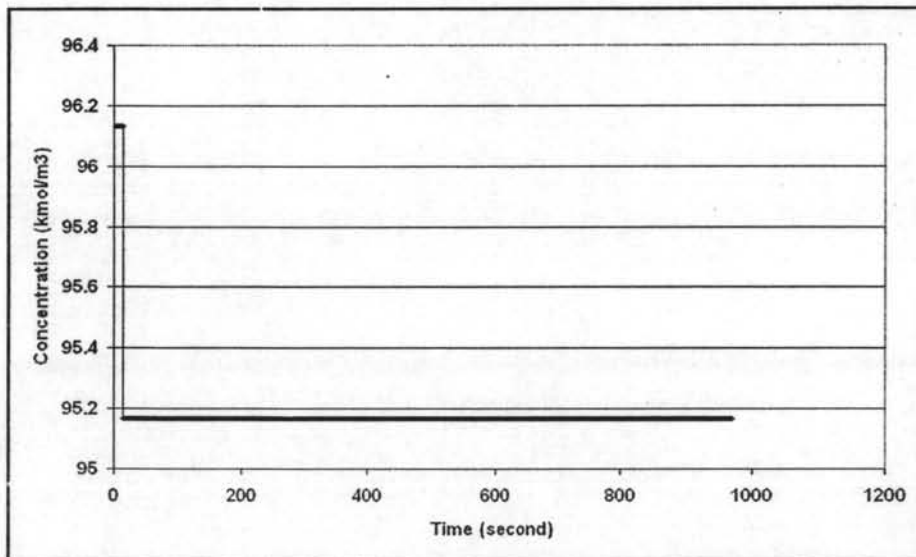


Figure G.2 Response curve of concentration in plug-flow plus CSTR with step of feed flow rate 1 kmol/s.

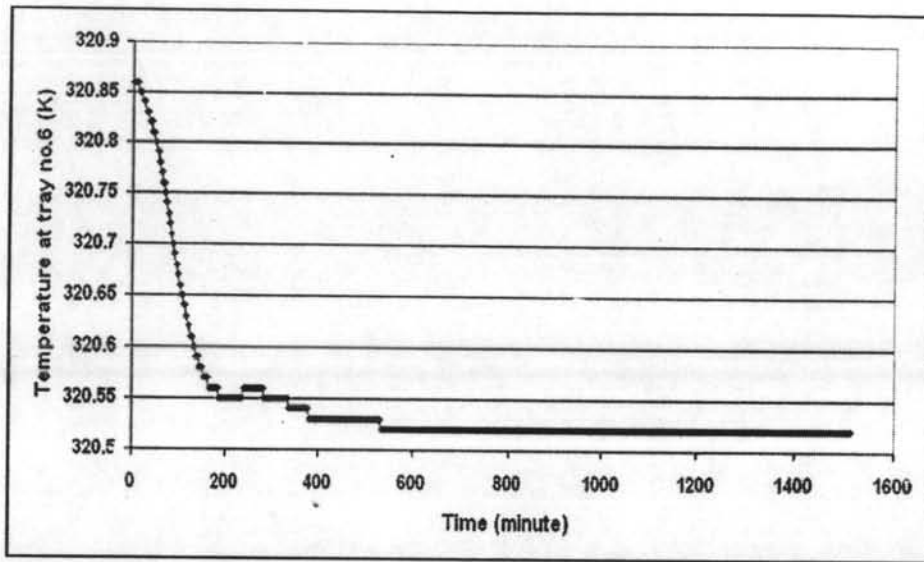


Figure G.3 Response curve of tray no.6 with step of reflux flowrate at 0.001 kmol/minute.

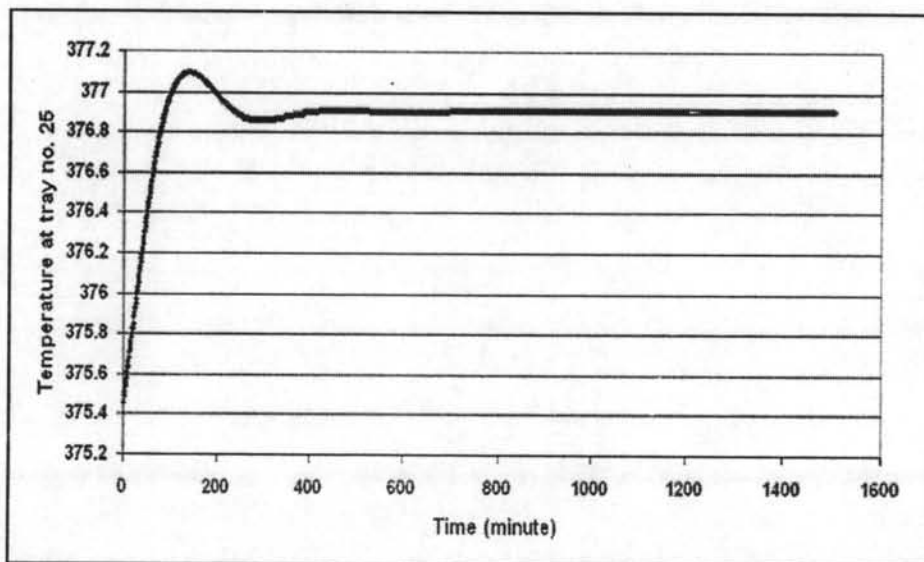


Figure G.4 Response curve of tray no.25 with step of steam flowrate at 0.01 kmol/30 second.

Appendix H Source Code of Gravitational Flow Tank

H.1 Gravitational Flow Tank with Feed Forward Control

```
program gravitytank
    real(8) v           !velocity
    real(8) h           !height
    real(8) f           !feed
    real(8) sp          !set point
    real(8) time        !time
    real(8) delta       !time step
    real(8) vdot        !derivative of velocity
    real(8) hdot        !derivative of height
    real(8) fdot        !derivative of feedin
    real(8) fold        !proportional gain
    real(8) k           !proportional gain
    real(8) ti          !reset time
    real(8) td          !derivative time
    open (1, file = 'output.xls')
    !initial
    h=4.6546
    v=4.98397
    f=0.311
    fold=0.311
    k=0.6*2
    ti=2/2.
    td=2/8.
    sp=0.311
    fdot=0
    time=0
    delta=1
100  vdot=0.0107*h-0.002005*v**2
    if(time.eq.2)then
        f=0.35
    end if
    fdot=k*((sp-f)+1/ti*(sp-fold-fdot*delta/2)*delta-td*fdot)
    fold=f
    f=f+fdot*delta
    if (f.le.0)then
        f=0
    end if
    hdot=f-0.0624*v
3    write (1,3)time,v,h,f
    format(4f10.5)
    v=v+vdot*delta
    if (v.le.0)then
        v=0
    end if
    h=h+hdot*delta
    if (h.le.0)then
        h=0
    end if
    time=time+delta
    if(time.le.3000) goto 100
end program
```

H.2 Gravitational Flow Tank with Feedback Control

```
program gravitytank
    real(8) v           !velocity
    real(8) h           !height
    real(8) hold        !feed
    real(8) f           !feed
    real(8) sp          !set point
    real(8) time        !time
    real(8) delta       !time step
```

```

real(8) vdot           !derivative of velocity
real(8) hdot          !derivative of height
real(8) fdot          !derivative of feedin
real(8) k              !proportional gain
real(8) ti             !reset time
real(8) td             !derivative time
open (1, file = 'output.xls')
!initial
h=4.6546
hold=h
v=4.98397
f=0.311
k=0.6*0.0193
ti=44./2.
td=44./8.
sp=4.6546
fdot=0
time=0
delta=1
100 vdot=0.0107*h-0.00205*v**2
if(time.eq.2)then
!
    f=0.35
    sp=4.7
end if
hdot=f-0.0624*v
write (1,3)time,v,h,f
3 format(4f10.5)
v=v+vdot*delta
hold=h
h=h+hdot*delta
fdot=k*((sp-h)+1/ti*(sp-hold-hdot*delta/2)*delta-td*hdot)
f=f+fdot*delta
time=time+delta
if(time.le.8000) goto 100
end program

```

H.3 Gravitational Flow Tank with Cascade Control

```

program gravitytank
real(8) v              !velocity
real(8) h              !height
real(8) f              !feed
real(8) sp             !set point of height of level in tank
real(8) time           !time
real(8) delta          !time step
real(8) vdot           !derivative of velocity
real(8) hdot           !derivative of height
real(8) hold           !derivative of feed in
real(8) fdot           !derivative of set point of feed in
real(8) fold           !proportional gain of master controller
real(8) spdot          !proportional gain of slave controller
real(8) k1             !integral term of master controller
real(8) k2             !integral term of slave controller
real(3) ti             !derivative term of master controller
real(8) ti1            !derivative term of slave controller
real(8) td             !set point of velocity of feed in
real(8) td1            !set point of velocity of feed in
open (1, file = 'output.xls')
!initial
h=4.6546
hold=4.6546
v=4.98397
f=0.311
fold=0.311
k1=0.6*2
ti1=2./2.
td1=2./8.
k2=0.6*0.33339

```

```

ti=2/2.
td=2/8.
sp=4.6546
sph=0.311
fdot=0
time=0
delta=1
100 vdot=0.0107*h-0.002005*v**2
! if(time.eq.1)then
!     f=0.35
!     sp=4.7
! end if
! fdot=k1*((sph-f)+1/ti1*(sph-fold-fdot*delta/2)*delta-td1*fdot)
! fold=f
! f=f+fdot*delta
! if (f.le.0)then
!     f=0
! end if
! hdot=f-0.0624*v
! write (1,3)time,v,h,f
! format(4f10.5)
! v=v+vdot*delta
! if (v.le.0)then
!     v=0
! end if
! hold=h
! h=h+hdot*delta
! if (h.le.0)then
!     h=0
! end if
! spdot=k2*((sp-h)+1/ti*(sp-hold-hdot*delta/2)*delta-td*hdot)
! sph=sph+spdot*delta
! time=time+delta
! if(time.le.8000) goto 100
end program

```

H.4 Gravitational Flow Tank with DMC

```

program gravitytank
implicit none
integer i,j,k,l,m
real(8) v           !velocity
real(8) h           !height
real(8) f           !feed
real(8) time        !time
real(8) delta       !time step
real(8) vdot        !derivative of velocity
real(8) hdot        !derivative of height
real(8) vsim        !velocity in simulation
real(8) vdotsim     !derivative of velocity in simulation
real(8) hdotsim     !derivative of height in simulation
real(8) sp          !set point
real(8) a1(80,40)
real(8) b1(160)
real(8) x(80)
real(8) dmo(80)
real(8) dm(40)
real(8) xol(80)
real(8) xcl(80)
real(8) df
real(8) ij(80)
real(8) ff
real(8) a1t(40,80)
real(8) ata(40,40)
real(8) ii(40,40)
real(8) atai(40,40)
real(8) aaa(40,80)
real(8) rr(80)
real(8) aa

```

```
real(8) bb
real(8) cc
open (1, file = 'output.xls')
b1( 1 )= 5.01090941
b1( 2 )= 9.998794226
b1( 3 )= 14.88592424
b1( 4 )= 19.60360219
b1( 5 )= 24.09246882
b1( 6 )= 28.30264488
b1( 7 )= 32.19371004
b1( 8 )= 35.73452293
b1( 9 )= 38.90289183
b1( 10 )= 41.68510982
b1( 11 )= 44.07537208
b1( 12 )= 46.07509619
b1( 13 )= 47.69216763
b1( 14 )= 48.9401339
b1( 15 )= 49.83737013
b1( 16 )= 50.40623778
b1( 17 )= 50.67225629
b1( 18 )= 50.66330495
b1( 19 )= 50.40886921
b1( 20 )= 49.93934295
b1( 21 )= 49.28539502
b1( 22 )= 48.47740545
b1( 23 )= 47.5449745
b1( 24 )= 46.51650493
b1( 25 )= 45.41885641
b1( 26 )= 44.27706926
b1( 27 )= 43.11415359
b1( 28 )= 41.95093903
b1( 29 )= 40.80597964
b1( 30 )= 39.69550859
b1( 31 )= 38.63343649
b1( 32 )= 37.63138804
b1( 33 )= 36.69877116
b1( 34 )= 35.84287354
b1( 35 )= 35.06898157
b1( 36 )= 34.38051693
b1( 37 )= 33.77918686
b1( 38 )= 33.26514392
b1( 39 )= 32.83715204
b1( 40 )= 32.49275544
b1( 41 )= 32.22844782
b1( 42 )= 32.03983924
b1( 43 )= 31.92181852
b1( 44 )= 31.86870937
b1( 45 )= 31.87441855
b1( 46 )= 31.93257484
b1( 47 )= 32.03655764
b1( 48 )= 32.18011453
b1( 49 )= 32.35646705
b1( 50 )= 32.55940432
b1( 51 )= 32.78286451
b1( 52 )= 33.02110385
b1( 53 )= 33.26875373
b1( 54 )= 33.52086589
b1( 55 )= 33.77294644
b1( 56 )= 34.02097917
b1( 57 )= 34.2614389
b1( 58 )= 34.49129571
b1( 59 )= 34.70801083
b1( 60 )= 34.90952518
b1( 61 )= 35.09424145
b1( 62 )= 35.26100062
b1( 63 )= 35.40905405
b1( 64 )= 35.53803185
b1( 65 )= 35.64790851
b1( 66 )= 35.73896665
b1( 67 )= 35.81175969
b1( 68 )= 35.86707409
```

bl(69)= 35.90589184
bl(70)= 35.92935388
bl(71)= 35.93872481
bl(72)= 35.93535937
bl(73)= 35.92067113
bl(74)= 35.89610352
bl(75)= 35.86310353
bl(76)= 35.82309816
bl(77)= 35.77747374
bl(78)= 35.72755809
bl(79)= 35.67460556
bl(80)= 35.61978487
bl(81)= 35.5641696
bl(82)= 35.50873122
bl(83)= 35.45433454
bl(84)= 35.40173533
bl(85)= 35.35157991
bl(86)= 35.30440659
bl(87)= 35.26064861
bl(88)= 35.22063849
bl(89)= 35.18461353
bl(90)= 35.15272216
bl(91)= 35.1250311
bl(92)= 35.10153304
bl(93)= 35.08215463
bl(94)= 35.06676475
bl(95)= 35.05518274
bl(96)= 35.04718654
bl(97)= 35.04252071
bl(98)= 35.04090399
bl(99)= 35.04203661
bl(100)= 35.04560695
bl(101)= 35.05129785
bl(102)= 35.0587922
bl(103)= 35.06777801
bl(104)= 35.07795281
bl(105)= 35.08902748
bl(106)= 35.10072942
bl(107)= 35.11280512
bl(108)= 35.12502218
bl(109)= 35.13717074
bl(110)= 35.14906446
bl(111)= 35.16054093
bl(112)= 35.17146173
bl(113)= 35.18171208
bl(114)= 35.19120015
bl(115)= 35.19985605
bl(116)= 35.20763061
bl(117)= 35.214494
bl(118)= 35.22043406
bl(119)= 35.22545467
bl(120)= 35.22957396
bl(121)= 35.23282248
bl(122)= 35.23524141
bl(123)= 35.23688075
bl(124)= 35.23779762
bl(125)= 35.23805452
bl(126)= 35.23771783
bl(127)= 35.2368563
bl(128)= 35.23553969
bl(129)= 35.23383758
bl(130)= 35.23181827
bl(131)= 35.22954782
bl(132)= 35.22708924
bl(133)= 35.22450181
bl(134)= 35.22184053
bl(135)= 35.21915572
bl(136)= 35.21649268
bl(137)= 35.21389155
bl(138)= 35.21138718
bl(139)= 35.20900916

```

b1( 140 )=35.20678152
b1( 141 )=35.20472484
b1( 142 )=35.20285257
b1( 143 )=35.20117521
b1( 144 )=35.19969869
b1( 145 )=35.19842511
b1( 146 )=35.1973531
b1( 147 )=35.19647823
b1( 148 )=35.19579339
b1( 149 )=35.19528921
b1( 150 )=35.19495444
b1( 151 )=35.19477634
b1( 152 )=35.194741
b1( 153 )=35.19483376
b1( 154 )=35.19503945
b1( 155 )=35.19534274
b1( 156 )=35.19572837
b1( 157 )=35.19618141
b1( 158 )=35.19668743
b1( 159 )=35.19723272
b1( 160 )=35.19780438
ii=0.
dm=1
do j=1,40
  ii(j)=1.0
end do
atai=ii
do j=1,80
  do k=1,40
    if (j+1-k.le.0)then
      a1(j,k)=0
    else
      a1(j,k)=b1(j+1-k)
    end if
  end do
end do
a1t=transpose(a1)
ata=matmul(a1t, a1)
ata=ata+20*ii
do i=1,40
  aa=ata(i,i)
  do j=1,40
    ata(i,j)=ata(i,j)/aa
    atai(i,j)=atai(i,j)/aa
  end do
  if (i.ne.40)then
    do j=1,40-i
      bb=ata(41-j,i)
      do l=1,40
        ata(41-j,l)=ata(41-j,l)-bb*ata(i,l)
        atai(41-j,l)=atai(41-j,l)-bb*atai(i,l)
      end do
    end do
  end if
end do
do i=1,39
  if (i.ne.40)then
    do j=1,40-i
      bb=ata(j,41-i)
      do l=1,40
        ata(j,l)=ata(j,l)-bb*ata(41-i,l)
        atai(j,l)=atai(j,l)-bb*atai(41-i,l)
      end do
    end do
  end if
end do
!initial
h=4.654597719
v=4.9839743261
f=0.311
sp=4.654597719

```

```

time=0
delta=1
100 vdot=0.0107*h-0.002005*v**2
    if (cc.eq.0)then
        f=f+df
    end if
    if (f.lt.0)then
        f=0
    end if
    if (time.eq.0)then
        !
        sp=4.7
        f=0.35
    end if
    hdot=f-0.0624*v
!if (cc.eq.0)then
    write (1,3)time,v,h,f,df
3    format(15f15.10)
lend if
    i=i+1
    if (i.eq.60)then
        i=0
    end if
    v=v+vdot*delta
    h=h+hdot*delta
    if (cc.eq.0)then
        do j=1,79
            dmo(81-j)=dmo(80-j)
        end do
        dmo(1)=dm(1)
        if (time.eq.0)then
            dmo(1)=0
        end if
        do j=1,80
            xol(j)=0
            do k=1,80
                xol(j)=xol(j)+(b1(j+k)-b1(k))*dmo(k)
            end do
            xol(j)=h+xol(j)
        end do
        aaa=matmul(atai,a1t)
        do i=1,80
            x(i)=sp-xol(i)
        end do
        dm=matmul(aaa,x)
        df=dm(1)
    end if
    cc=cc+1
    if (cc.eq.5)then
        cc=0
    end if
    time=time+delta
    if(time.le.1000) goto 100
end program

```


Appendix I Source Code of Plug-flow and CSTR

I.1 Plug-flow and CSTR with Feedback Control

```
program gravitytank !this is plug-flow plus CSTR
  implicit none
  integer i !index
  real(8) h !height
  real(8) f !feed
  real(8) time !time
  real(8) delta !time step
  real(8) sp !set point
  real(8) b1(32)
  real(8) ff(16)
  real(8) hold
  real(8) df
  real(8) dv
  real(8) dc(20)
  real(8) con(16) !concentration of substance
  real(8) incon !initial concentration
  real(8) aa
  real(8) bb
  real(8) cc
  real(8) dh
  real(8) k,tari,tard !controller parameter
  OPEN (1, file = 'output.xls')
  !initial
  f=4.0d0
  dv=1.0d0
  incon=100.0d0
  con=0.0d0
  sp=103.8522256042d0
  time=0
  delta=1.0d0
100 f=f+df
  !
  if (time.eq.30) then
    f=6.0d0
    sp=18.00D0
  end if
  !CSTR
  !conversion of CSTR =0.5 per volumn of CSTR
  ff(16)=0.5*ff(15)
  con(16)=con(15)-(ff(15)-ff(16))/10.0 !Volumn of CSTR =10 m3
  hold=h
  h=con(16)
  !plug flow
  !conversion of plug flow =0.2 per dv
  do i=1,15
    if (16-i.eq.1)then
      ff(16-i)=0.8*f
      con(16-i)=incon-(ff(16-i)-f)/dv
    else
      ff(16-i)=0.8*ff(15-i)
      con(16-i)=con(15-i)-(ff(16-i)-ff(15-i))/dv
    end if
  end do
  !if (cc.eq.0) then
  write(i,400) time,h,f,df,sp
  400 format(15f20.10)
  !end if
  if (time.ge.30) then
    k=0.6*0.1052
    tari=62/2.
    tard=62/8.
    dh=df
    df=k*((sp-h)+1/tari*(sp-incon+(ff(15)-f)/1d0+(ff(15)-ff(16))/10.0d0)*delta-tard*dh)
  end if
```

```

time=time+delta
if(time.le.10000) goto 100
end program

```

I.2 Plug-flow and CSTR with DMC

```

program gravitytank !this is plug-flow plus CSTR
implicit none
integer i,j,k,l,m
real(8) h !height
real(8) f !feed (kmol/s)
real(8) time !time
real(8) delta !time step
real(8) sp !set point
real(8) a1(11,4)
real(8) b1(32)
real(8) x(11)
real(8) ff(16)
real(8) dmo(11)
real(8) dm(4)
real(8) xol(11)
real(8) xcl(11)
real(8) df !differential of plug-flow volumn (m3)
real(8) dv
real(8) a1t(4,11)
real(8) ata(4,4)
real(8) ii(4,4)
real(8) atai(4,4)
real(8) aaa(4,11)
real(8) con(16) !concentration of substance (kmol/m3)
real(8) incon !initial concentration of substance (kmol/m3)
real(8) aa
real(8) bb
real(8) cc
OPEN (1, file = 'output.xls')
b1( 1 ) = 0
b1( 2 ) = 0
b1( 3 ) = 0
b1( 4 ) = -0.966574839
b1( 5 ) = -0.966574839
b1( 6 ) = -0.966574839
b1( 7 ) = -0.966574839
b1( 8 ) = -0.966574839
b1( 9 ) = -0.966574839
b1( 10 ) = -0.966574839
b1( 11 ) = -0.966574839
b1( 12 ) = -0.966574839
b1( 13 ) = -0.966574839
b1( 14 ) = -0.966574839
b1( 15 ) = -0.966574839
b1( 16 ) = -0.966574839
b1( 17 ) = -0.966574839
b1( 18 ) = -0.966574839
b1( 19 ) = -0.966574839
b1( 20 ) = -0.966574839
b1( 21 ) = -0.966574839
b1( 22 ) = -0.966574839
b1( 23 ) = -0.966574839
b1( 24 ) = -0.966574839
b1( 25 ) = -0.966574839
b1( 26 ) = -0.966574839
b1( 27 ) = -0.966574839
b1( 28 ) = -0.966574839
b1( 29 ) = -0.966574839
b1( 30 ) = -0.966574839
b1( 31 ) = -0.966574839
b1( 32 ) = -0.966574839
ii=0.

```

```

dm=1
dmo=0
do j=1,4
  ii(j,j)=1.0
end do
atai=ii
do j=1,11
  do k=1,4
    if (j+1-k.le.0)then
      a1(j,k)=0
    else
      a1(j,k)=b1(j+1-k)
    end if
  end do
end do
alt=transpose(a1)
ata=matmul(alt, a1)
ata=ata+40*ii
do i=1,4
  aa=ata(i,i)
  do j=1,4
    ata(i,j)=ata(i,j)/aa
    atai(i,j)=atai(i,j)/aa
  end do
  if (i.ne.4)then
    do j=1,4-i
      bb=ata(5-j,i)
      do l=1,4
        ata(5-j,l)=ata(5-j,l)-bb*ata(i,l)
        atai(5-j,l)=atai(5-j,l)-bb*atai(i,l)
      end do
    end do
  end if
end do
do i=1,3
  if (i.ne.4)then
    do j=1,4-i
      bb=ata(j,5-i)
      do l=1,4
        ata(j,l)=ata(j,l)-bb*ata(5-i,l)
        atai(j,l)=atai(j,l)-bb*atai(5-i,l)
      end do
    end do
  end if
end do
!initial
f=4.0d0
dv=1.0d0
incon=100.0d0
con=0
sp=96.1337006438
time=0
delta=1
cc=0.
100 if (cc.eq.0)then
      f=f+df
    end if
    if (time.eq.30) then
      f=6.0d0
      sp=18.00D0
    end if
!CSTR
!conversion of CSTR =0.5 per volumn of CSTR
ff(16)=0.5*ff(15)
con(16)=con(15)-(ff(15)-ff(16))/10 !Volumn of CSTR =10 m3
h=con(16)
!plug flow
!conversion of plug flow =0.2 per dv
do i=1,15
  if (16-i.eq.1)then
    ff(16-i)=0.8*f
  
```

```

        con(16-i)=incon+(ff(16-i)-f)/dv
    else
        ff(16-i)=0.8*ff(15-i)
        con(16-i)=con(15-i)+(ff(16-i)-ff(15-i))/dv
    end if
end do
!if (cc.eq.0) then
write(1,400) time,h,f,df
400 format(15f20.10)
!end if
if (cc.eq.0.and.time.ge.30)then
do j=1,10
    dmo(12-j)=dmo(11-j)
end do
dmo(1)=dm(1)/10
if (time.eq.0)then
    dmo(1)=0
end if
do j=1,11
    xol(j)=0
    do k=1,11
        xol(j)=xol(j)+(b1(j+k)-b1(k))*dmo(k)
    end do
    xol(j)=h+xol(j)
end do
aaa=matmul(atai,alt)
do i=1,11
    x(i)=sp-xol(i)
end do
dm=matmul(aaa,x)
df=dm(1)
end if
cc=cc+delta
if (cc.eq.5)then
    cc=0
end if
time=time+delta
if(time.le.1000) goto 100
end program

```

Appendix J Source Code of Depropanizer Column

J.1 Depropanizer Column with Cascade Control

```
program distillation
  implicit none
  integer i,ite,j,k
  integer ib,it
  integer h,m,s
  integer tf
  integer n
  real(8) a
  real(8) aa
  real(8) am(200,2)
  real(8) amo
  real(8) b(2)
  real(8) cpn
  real(8) cpw
  real(8) d(2)
  real(8) db
  real(8) dcb
  real(8) dct
  real(8) dd
  real(8) denliq(200)
  real(8) dl1
  real(8) ds
  real(8) dt
  real(8) f
  real(8) finequa
  real(8) ft
  real(8) ha
  real(8) haineq
  real(8) high(200)
  real(8) highold(2)
  real(8) hl(200)
  real(8) hlb
  real(8) hv(200)
  real(8) hvb
  real(8) keep(1000)
  real(8) l(200,2)
  real(8) lo
  real(8) p(200)
  real(8) pb
  real(8) pf
  real(8) qc
  real(8) qcc
  real(8) qr
  real(8) qrc
  real(8) qn
  real(8) qw
  real(8) qwo
  real(8) scond
  real(8) sph
  real(8) sphb
  real(8) spl1
  real(8) spcb
  real(8) spct
  real(8) sps
  real(8) sreb
  real(8) t(200)
  real(8) tb
  real(8) tib
  real(8) tit
  real(8) tnout
  real(8) tnin
  real(8) told(2)
  real(8) twout
  real(8) twin

  !index
  !index of sensitive tray
  !time index
  !tray of feed
  !number if tray and n th tray
  !factor
  !parameter
  !accumulate of liquid in tray (kg-mol/minute)
  !accumulate of liquid in tray at old iteration (kg-mol/minute)
  !bottom product flowrate (kg-mol/minute)
  !heat capacity of cool water (kJ/(C*kg-mol))
  !heat capacity of hot water (kJ/(C*kg-mol))
  !distillate (kg-mol/minute)
  !bottom product flow rate change (kg-mol/s)
  !set point of reboiler change (kg-mol/s)
  !set point of reflux change (kg-mol/s)
  !distillate flow rate change (kg-mol/s)
  !density of liquid (kg-mol/m3)
  !reflux flow rate change (kg-mol/s)
  !steam flow rate change (kg-mol/s)
  !constant step time (1 second)
  !feed (kg-mol/minute)
  !feed in equation
  !feed temperature
  !total feed enthalpy
  !enthalpy of feed in equation
  !high of liquid in tray,bottom column and reflux reboiler (m)
  !high of liquid in bottom column and reflux reboiler at old step time (m)
  !total liquid enthalpy (kj/kg-mol)
  !liquid enthalpy of bottom column (kj/kg-mol)
  !total vapor enthalpy (kj/kg-mol)
  !vapor enthalpy of bottom column (kj/kg-mol)
  !keep value
  !liquid flow (kg-mol/minute)
  !liquid flow of tray No. 1 at old step time (kg-mol/minute)
  !pressure on tray (bar)
  !pressure of bottom column (bar)
  !pressure of feed (bar)
  !heat duty of condenser (kj)
  !heat duty of condenser for minute (kj)
  !heat duty of reboiler (kj)
  !heat duty of reboiler for minute (kj)
  !flowrate of cool water (kg-mol/half-minute)
  !flowrate of hot water (kg-mol/half-minute)
  !flowrate of hot water at old step time (kg-mol/minute)
  !surface area of condenser (m2)
  !set point of liquid level in drum (m)
  !set point of liquid level in bottom column (m)
  !set point of reflux (kg-mol/min)
  !set point of cascade at bottom column (K)
  !set point of cascade at top column (K)
  !setpoint of steam flow rate (kg-mol/s)
  !surface area of reboiler (m2)
  !temperature of tray (K)
  !bottom temperature (K)
  !temperature at tray no. ib th
  !temperature at tray no. it th
  !temperature of nitrogen out of condenser (K)
  !temperature of nitrogen enter condenser (K)
  !temperature of sensitive tray at 30 second ago (K)
  !temperature of hot water out of reboiler (K)
  !temperature of hot water enter reboiler (K)
```

```

real(8) ureb          !over all heat transfer coefficient of reboiler (Kw/m2 C)
real(8) ucond        !over all heat transfer coefficient of condenser (Kw/m2 C)
real(8) unwanted     !unwant parameter
real(8) v(200,2)     !vapor flow (kg-mol/minute)
real(8) x(2,200,2)   !liquid composition (component,tray,time)
real(8) xb(2)        !liquid composition at bottom column
real(8) xx(2)        !keep liquid component value
real(8) y(2,200,2)   !vapor composition (component,tray,time)
real(8) yb(2)        !vapor composition at bottom column
real(8) z(2)         !feed composition
open (1,file='output.xls')
open (2,file='save.dat')
!initial value
n=30
am=0.50312
cpn=6024.96
cpw=6024.96
dt=1./60
f=0.09
unwant=0
ft=323
hl=0
l=0
it=6
ib=25
p=1.01325
pf=2.0265
pb=1.01325
qn=0.5
qw=0.001
scond=1000
sreb=1000
spcb=375.8
spct=321.1
sph=0.4
sphb=0.4
spll=0.315
sps=0.20
t=320
tb=320
tf=n
tmin=288
twin=393
ureb=0.438139514
ucond=0.438139514
v=0
xb=0
yb(1)=0.5
yb(2)=0.5
z(1)=0.5
z(2)=0.5
call enth(pf,ft,unwant,unwant,z(1),z(2),unwant,ha) !calculate enthalpy
do j=1,n
  do i=1,2
    x(i,j,1)=0
    x(i,j,2)=0
  end do
  if (j.lt.n)then
    y(1,j,2)=0.5
    y(2,j,2)=0.5
  end if
  call enth(p(j),t(j),x(1,j,1),x(2,j,1),y(1,j,2),y(2,j,2),hl(j),hv(j)) !calculate enthalpy
  hl(j)=hv(j)
end do
call enth(pb,tb,xb(1),xb(2),yb(1),yb(2),h1b,hvb)
do i=1,1000
  read (2,*) keep(i)
end do
do i=1,n-1
  x(1,i,2)=keep(i)
end do

```

```

xb(1)=keep(30)
do i=1,n-1
    x(2,i,2)=keep(30+i)
end do
xb(2)=keep(60)
do i=1,n
    y(1,i,2)=keep(60+i)
end do
yb(1)=keep(91)
do i=1,n
    y(2,i,2)=keep(91+i)
end do
yb(2)=keep(122)
do i=1,n
    am(i,2)=keep(122+i)
end do
do i=1,n
    am(i,1)=keep(152+i)
end do
do i=1,n
    high(i)=keep(182+i)
end do
do i=1,n-1
    t(i)=keep(212+i)
end do
tb=keep(242)
told(1)=keep(243)
told(2)=keep(244)
do i=1,n-1
    p(i)=keep(244+i)
end do
pb=keep(274)
do i=1,n
    hl(i)=keep(274+i)
end do
h1b=keep(305)
do i=1,n
    hv(i)=keep(305+i)
end do
hvb=keep(336)
ha=keep(337)
ft=keep(338)
f=keep(339)
z(1)=keep(340)
z(2)=keep(341)
do i=1,n
    v(i,2)=keep(341+i)
end do
do i=1,n
    l(i,2)=keep(371+i)
end do
d(2)=keep(402)
b(2)=keep(403)
qw=keep(404)
qwo=keep(405)
qr=keep(406)
qc=keep(407)
qcc=keep(408)
qrc=keep(409)
lo=keep(410)
do i=1,n
    x(1,i,1)=keep(410+i)
end do
do i=1,n
    x(2,i,1)=keep(440+i)
end do
do i=1,n
    y(1,i,1)=keep(470+i)
end do
do i=1,n
    y(2,i,1)=keep(500+i)

```

```

end do
do i=1,n
    v(i,1)=keep(530+i)
end do
do i=1,n
    l(i,1)=keep(560+i)
end do
sreb=keep(591)
spcb=keep(592)
spct=keep(593)
sph=keep(594)
sphb=keep(595)
spl1=keep(596)
sps=keep(597)
tf=keep(598)
it=keep(599)
ib=keep(600)
pf=keep(601)
scond=keep(602)
amo=keep(603)
ucond=keep(604)
ureb=keep(605)
jd=keep(606)
dl1=keep(607)
ds=keep(608)
dcb=keep(609)
dct=keep(610)
db=keep(611)
qn=keep(612)
tnin=keep(613)
tnout=keep(614)
twin=keep(615)
twout=keep(616)
do i=1,n
    denliq(i)=keep(616+i)
end do

do h=1,8000
    do m=1,60
        do s=1,60
            write (6,111) h,high(1),high(n),t(6),t(25),l(1,2),qw,b(2),d(2)
            111 format (1i,15f13.7)
            if (high(n/2).ge.0.03175)then
                tf=n/2
                pf=17.0
                ft=369.0
                f=0.09
                z(1)=0.5
                z(2)=0.5
                if (h.ge.1)then !disturbance occur
                    !z(1)=0.3
                    !z(2)=0.7
                    !f=0.1
                    !spct=323.1
                    !qw=0.02
                end if
                unwanted=0
                call enth(pf,ft,z(1),z(2),unwanted,unwanted,ha,unwanted) !calculate enthalpy
            end if
            if (s.eq.1)then
                told(2)=t(it)
                spl1=spl1+dct
            end if
            !condenser & reflux drum
            call l1control(spl1,l(1,2),dl1,lo) ! call control of reflux flow rate
            lo=l(1,2)
            l(1,2)=l(1,2)+dl1
            if (s.eq.1)then
                d(2)=d(2)+dd
            end if
            if (d(2).lt.0.or.high(1).le.0)then

```



```

        d(2)=0
        dd=0
    end if
    if (l(1,2).lt.0.or.high(1).le.0)then
        l(1,2)=0
    end if
    am(1,2)=am(1,1)+(v(2,2)-l(1,2)-d(2))*dt !calculate accumulate in drum
    if (am(1,2).lt.0)then
        am(1,2)=0
    end if
    call dliq(t(1),x(1,1,2),x(2,1,2),denliq(1))
    if (s.eq.1)then
        highold(1)=high(1)
    end if
    high(1)=am(1,2)/(denliq(1)*1.23)
    if (denliq(1).eq.0.or.high(1).le.0)then
        high(1)=0
    end if
    if (x(1,1,1).eq.0.and.x(2,1,1).eq.0) then
        do i=1,2
            x(i,1,1)=y(i,1,2)
        end do
    end if

x(1,1,2)=(x(1,1,1)*am(1,1)+(v(2,2)*y(1,2,2))*dt)/(am(1,2)+(l(1,2)+d(2))*dt) !calculate composition in drum
if (x(1,1,2).lt.0.000000001)then
    x(1,1,2)=0
end if
x(2,1,2)=1.-x(1,1,2)
a=exp(-(ucond*scond)/(qn*cpn))
tnout=tnin+(1-a)*(t(2)-tnin)
qc=qn*cpn*(tnout-tnin) !calculate heat duty of reboiler
if (t(1).lt.308)then
    qc=0
end if
p(1)=16.00
call bubtp(p(1),x(1,1,2),x(2,1,2),y(1,1,2),y(2,1,2),t(1))
call enth(p(1),t(1),x(1,1,2),x(2,1,2),y(1,1,2),y(2,1,2),hl(1),hv(1))
x(1,1,1)=x(1,1,2)
x(2,1,1)=x(2,1,2)
y(1,1,1)=y(1,1,2)
y(2,1,1)=y(2,1,2)
am(1,1)=am(1,2)
v(1,1)=v(1,2)
l(1,1)=l(1,2)

ltray
do j=2,n-1
    if(j.eq.tf)then
        finequa=f
        haineq=ha
    else
        finequa=0
        haineq=0
    end if
    am(j,2)=am(j,1)
    amo=am(j,2)
    call dliq(t(j),x(1,j,2),x(2,j,2),denliq(j))
    high(j)=am(j,2)/(denliq(j)*0.982)
    if (denliq(j).eq.0.or.high(j).le.0)then
        high(j)=0
    end if
    if (high(j).lt.0.03175) then
        l(j,2)=0
    else
        l(j,2)=denliq(j)*1.17*(am(j,2)/(denliq(j)*0.982)-
        0.03175)**1.5
        if ((am(j,2)/(denliq(j)*0.982).lt.0.03175)then
            l(j,2)=0
        end if
    end if
end do

```



```

if (high(n).ge.0.3)then
  a=exp((ureb*sreb)/(qw*cpw))
  twout=(twin+(a-1)*tb)/a
  qr=qw*cpw*(twin-twout) !calculate heat duty of reboiler
end if
2
if (high(n).lt.0.1.or.qw.le.0.0001)then
  qr=0
end if
bottom column
am(n,2)=am(n,1)+(finequa+l(n-1,2)-v(n,2)-b(2))*dt !calculate accumulate in
if (am(n,2).lt.0)then
  am(n,2)=0
end if
enthalpy
if (high(n).lt.0.3.and.v(n,2).ne.0)then
  unwanted=0
  call enth(pb,tb,unwanted,unwanted,yb(1),yb(2),unwanted,hvb) !calculate
  hv(n)=hvb
  do i=1,2
    y(i,n,2)=yb(i)
  end do
end if
if (xb(1).eq.0.and.xb(2).eq.0)then
  xb(1)=yb(1)
  xb(2)=yb(2)
end if
v(n,2)*yb(1))*dt)/(am(n,2)+b(2)*dt) !calculate liquid composition in bottom column
if (xb(1).lt.0.0000000001)then
  xb(1)=0
end if
xb(2)=1.-xb(1)
pb=p(n-1)+0.065
call bubpt(pb,xb(1),xb(2),yb(1),yb(2),tb)
do i=1,2
  y(i,n,2)=yb(i)
end do
call dliq(t(n),xb(1),xb(2),denliq(n))
if (s.eq.1)then
  highold(2)=high(n)
end if
high(n)=am(n,2)/(denliq(n)*1.23)
if (denliq(n).eq.0.or.high(n).le.0)then
  high(n)=0
end if
call enth(pb,tb,xb(1),xb(2),yb(1),yb(2),h1b,hvb)
v(n,2)=(qr+finequa*haineq+hl(n-1)*l(n-1,2)-h1b*b(2))/hvb
if (v(n,2).lt.0)then
  v(n,2)=0
end if
if (s.eq.1)then
  b(2)=b(2)+db
end if
if (high(n).le.0)then
  high(n)=0
  b(2)=0
  db=0
end if
if (b(2).lt.0)then
  b(2)=0
  db=0
end if
do i=1,2
  x(i,n,2)=xb(i)
  y(i,n,2)=yb(i)
end do
x(1,n,1)=x(1,n,2)
x(2,n,1)=x(2,n,2)
y(1,n,1)=y(1,n,2)
y(2,n,1)=y(2,n,2)
am(n,1)=am(n,2)

```

control of bottom flow rate

```

v(n,1)=v(n,2)
l(n,1)=l(n,2)
call dcontrol(sph,high(1),dd,v(2,2),d(2),l(1,2),denliq(1),highold(1))
call bcontrol(sphb,high(n),db,v(n,2),b(2),l(n-1,2),denliq(n),highold(2)) ! call
if (h.ge.1000.and.m.eq.60.and.s.eq.60)then
  open (2,file='save.dat')
  do i=1,n-1
    keep(i)=x(1,i,2)
  end do
  keep(30)=xb(1)
  do i=1,n-1
    keep(30+i)=x(2,i,2)
  end do
  keep(60)=xb(2)
  do i=1,n
    keep(60+i)=y(1,i,2)
  end do
  keep(91)=yb(1)
  do i=1,n
    keep(91+i)=y(2,i,2)
  end do
  keep(122)=yb(2)
  do i=1,n
    keep(122+i)=am(i,2)
  end do
  do i=1,n
    keep(152+i)=am(i,1)
  end do
  do i=1,n
    keep(182+i)=high(i)
  end do
  do i=1,n-1
    keep(212+i)=t(i)
  end do
  keep(242)=tb
  keep(243)=told(1)
  keep(244)=told(2)
  do i=1,n-1
    keep(244+i)=p(i)
  end do
  keep(274)=pb
  do i=1,n
    keep(274+i)=hl(i)
  end do
  keep(305)=h1b
  do i=1,n
    keep(305+i)=hv(i)
  end do
  keep(336)=hvb
  keep(337)=ha
  keep(338)=ft
  keep(339)=f
  keep(340)=z(1)
  keep(341)=z(2)
  do i=1,n
    keep(341+i)=v(i,2)
  end do
  do i=1,n
    keep(371+i)=l(i,2)
  end do
  keep(402)=d(2)
  keep(403)=b(2)
  keep(404)=qw
  keep(405)=qwo
  keep(406)=qr
  keep(407)=qc
  keep(408)=qcc
  keep(409)=qrc
  keep(410)=lo
  do i=1,n

```

```

        keep(410+i)=x(1,i,1)
    end do
    do i=1,n
        keep(440+i)=x(2,i,1)
    end do
    do i=1,n
        keep(470+i)=y(1,i,1)
    end do
    do i=1,n
        keep(500+i)=y(2,i,1)
    end do
    do i=1,n
        keep(530+i)=v(i,1)
    end do
    do i=1,n
        keep(560+i)=l(i,1)
    end do
    keep(591)=sreb
    keep(592)=spcb
    keep(593)=spct
    keep(594)=sph
    keep(595)=sphb
    keep(596)=sp11
    keep(597)=sps
    keep(598)=tf
    keep(599)=it
    keep(600)=ib
    keep(601)=pf
    keep(602)=scond
    keep(603)=amo
    keep(604)=ucond
    keep(605)=ureb
    keep(606)=dd
    keep(607)=d11
    keep(608)=ds
    keep(609)=dcb
    keep(610)=dct
    keep(611)=db
    keep(612)=qn
    keep(613)=tmin
    keep(614)=tnout
    keep(615)=twin
    keep(616)=twout
    do i=1,n
        keep(616+i)=denliq(i)
    end do
    do i=1,1000
        write(2,*) keep(i)
    end do
    close(2)
end if
end do !s
!DO J=1,N
    !IF (M.GE.53.AND.H.GE.1) THEN !S.EQ.60.AND.
    !IF (H.ge.1.AND.M.GE.1)
    THEN !S.EQ.60.AND.M.GE.53.AND.H.GE.1 !AND.M.GE.60.AND.s.eq.2
    !
    ! if (j.eq.n)then
    ! write(1,402)
    h,m,t(6),t(25),x(1,1,2),xb(2),l(1,2),qw,d(2),b(2),high(1),high(n),spcb,spct
    ! write(1,402)
    H,M,J,TF,xb(1),xb(2),yb(1),yb(2),v(n,2),l(n,2),Tb,Pb,high(n),am(n,2),qr,b(2)
    !
    ! else
    ! WRITE(1,402)
    H,M,J,TF,x(1,j,2),x(2,j,2),y(1,j,2),y(2,j,2),v(j,2),l(j,2),T(J),P(J),high(J),am(J,2),denliq(j),d(2)
    !
    ! end if
    ! 402 FORMAT(2i,2f10.1,20f10.4)
    ! 402 FORMAT(1I,1X,1I,1X,1I,1X,1I,1X,1I,1X,15F12.4)
    ! end if
    !
    ! END DO
    !
    if (high(n).gt.0)then

```

```

tib =t(ib)
call cutdec1(tib)
call cbcontrol(spcb,tib,dcb,finequa,z(1),v(ib+1,2),y(1,ib+1,2),l(ib-1,2),x(1,ib-
1,2),v(ib,2),y(1,ib,2),l(ib,2),x(1,ib,2),told(1),am(ib,2))
else
dcb=0
end if
if (high(1).gt.0)then
tit=t(it)
call cutdec1(tit)
call ctcontrol(spct,tit,dct,finequa,z(1),v(it+1,2),y(1,it+1,2),l(it-1,2),x(1,it-
1,2),v(it,2),y(1,it,2),l(it,2),x(1,it,2),told(2),am(it,2))
else
dct=0
end if
end do !m
end do !h
end program

```

```

subroutine bubpt(pp,x1,x2,y1,y2,tt) !calculate temperature from bubble point equation
integer i !index
real(8) df !differential of function
real(8) f !function
real(8) pp !pressure (bar)
real(8) ps1,ps2 !vapor pressure (bar)
real(8) tt !temperature (K)
real(8) x1,x2 !!liquid composition
real(8) y1,y2 !vapor composition
real(8) yy1,yy2
1 ps1=exp(-369.348/(tt-168.126)+5.23749) !calculate vapor pressure of propane
ps2=exp(-1275.718/(tt-59.782)+6.85137) !calculate vapor pressure of butane
y1=x1*ps1/pp !calculate vapor composition
y2=x2*ps2/pp
if (abs(1-y1-y2).lt.0.00000001) goto 10 !find correct temperature
f=1-y1-y2
df=x1/pp*ps1*369.348/(tt-168.126)**2
df=df+x2/pp*ps2*1275.718/(tt-59.782)**2
tt=tt+f/df
goto 1
10 return
end

```

```

subroutine enth(p,t,x3,x4,y3,y4,h1,ha) ! calculate liquid and vapor enthalpy from pressure,temperature, and composition
use numerical_libraries
implicit real*8 (a-h,o-z)
real(8) t !temperature
real(8) p !pressure
real(8) y3,y4 !vapor composition of propane and butane
real(8) x3,x4 !liquid composition
real(8) ha !total vapor enthalpy
real(8) ha3 !vapor enthalpy of propane
real(8) ha4 !vapor enthalpy of butane
real(8) hll(2) !!iquid enthalpy of propane and butane
real(8) hl !total liquid enthalpy
common/blkd1/popv(5),hvc3(5),hvc4(5)
data popv/1.,5.,10.,15.,20./
parameter (korder=3,ndata=5,nknot=ndata+korder)
dimension x1data(ndata),fl data(ndata)
dimension x1knot(nknot),bscoefl(ndata)
integer i

!calculate vapor enthalpy
t=t-273.15
if (p.eq.1.or.p.eq.5.or.p.eq.10.or.p.eq.15.or.p.eq.20)then
if (p.eq.1)then

ha3=0.00000243589743879133*t**3+0.0216068764561292*t**2+16.7600885781487*t+3948.29071794724
ha4=5171.95353379809+22.7750602176193*t+0.0285385198127802*t**2-
0.0000006546231517426*t**3

```

```

end if
if (p.eq.5)then
    ha3=3785.71550582761+18.240793123538*t+0.0139970279720996*t**2+0.0000212237762234762*t**3
    ha4=13362.9290022956-614.055453861994*t+19.4411005643476*t**2-
0.305859930252696*t**3+0.00264210823154405*t**4-0.0000118981890756778*t**5+0.0000000218680429435476*t**6
end if
if (p.eq.10)then
    ha3=9299.88843643293-489.679087204064*t+18.2134871645406*t**2-
0.335630483024728*t**3+0.00337653409332662*t**4-0.0000176090629930964*t**5+0.0000000372728987837522*t**6
    ha4=52119.620884926-4542.38831847744*t+183.561795154405*t**2-
3.96420633705897*t**3+0.0496691999500929*t**4-0.000361742582892285*t**5+0.00000142214836684578*t**6-
0.0000000233518724898894*t**7
end if
if (p.eq.15)then
    ha3=3499.26966208774+10.0480539969921*t+0.235411990181417*t**2-
0.00185526320973007*t**3+0.00000546197552656038*t**4
    ha4=-41073.9677943845+4570.52957391954*t-
185.978489301388*t**2+4.09239659695254*t**3-0.0523767526218596*t**4+0.000390079118628205*t**5-
0.00000156690531090442*t**6+0.0000000262353582012308*t**7
end if
if (p.eq.20)then
    ha3=4127.1570396016+73.4391303904704*t-
4.99493677579601*t**2+0.125573969112786*t**3-0.00143072973061548*t**4+0.0000077793456208826*t**5-
0.0000000164069371112414*t**6
    ha4=54716.6018791736-4931.18850411005*t+206.110049953317*t**2-
4.63591405624864*t**3+0.0608851762849367*t**4-0.000467220003840682*t**5+0.00000194083612282833*t**6-
0.00000000336865665585238*t**7
end if
else
do i=1,5
    x1 data(i)=popv(i)
end do
do i=1,5
if (i.eq.1)then
    hvc3(i)=2.43589743879133*10**(-
6)*t**3+0.0216068764561292*t**2+16.7600885781487*t+3948.29071794724
    hvc4(i)=5171.95353379809+22.7750602176193*t+0.0285385198127802*t**2-
0.0000006546231517426*t**3
end if
if (i.eq.2)then
    hvc3(i)=3785.71550582761+18.240793123538*t+0.0139970279720996*t**2+0.0000212237762234762*t**3
    hvc4(i)=13362.9290022956-614.055453861994*t+19.4411005643476*t**2-
0.305859930252696*t**3+0.00264210823154405*t**4-0.0000118981890756778*t**5+0.0000000218680429435476*t**6
end if
if (i.eq.3)then
    hvc3(i)=9299.88843643293-489.679087204064*t+18.2134871645406*t**2-
0.335630483024728*t**3+0.00337653409332662*t**4-0.0000176090629930964*t**5+0.0000000372728987837522*t**6
    hvc4(i)=52119.620884926-4542.38831847744*t+183.561795154405*t**2-
3.96420633705897*t**3+0.0496691999500929*t**4-0.000361742582892285*t**5+0.00000142214836684578*t**6-
0.0000000233518724898894*t**7
end if
if (i.eq.4)then
    hvc3(i)=3499.26966208774+10.0480539969921*t+0.235411990181417*t**2-
0.00185526320973007*t**3+0.00000546197552656038*t**4
    hvc4(i)=-41073.9677943845+4570.52957391954*t-
185.978489301388*t**2+4.09239659695254*t**3-0.0523767526218596*t**4+0.000390079118628205*t**5-
0.00000156690531090442*t**6+0.0000000262353582012308*t**7
end if
if (i.eq.5)then
    hvc3(i)=4127.1570396016+73.4391303904704*t-
4.99493677579601*t**2+0.125573969112786*t**3-0.00143072973061548*t**4+0.0000077793456208826*t**5-
0.0000000164069371112414*t**6
    hvc4(i)=54716.6018791736-4931.18850411005*t+206.110049953317*t**2-
4.63591405624864*t**3+0.0608851762849367*t**4-0.000467220003840682*t**5+0.00000194083612282833*t**6-
0.00000000336865665585238*t**7
end if
fl data(i)=hvc3(i)
end do
call dbsnak(ndata,x1data,korder,x1knot)

```

```

        call dbsint(ndata,x1data,fl data,korder,x1knot,bscoef1)
        ncoef=ndata
        ha3=dbsval(p,korder,x1knot,ncoef,bscoef1)
        do i=1,5
            fl data(i)=hvc4(i)
        enddo
        call dbsint(ndata,x1data,fl data,korder,x1knot,bscoef1)
        ha4=dbsval(p,korder,x1knot,ncoef,bscoef1)
    end if
    ha=4.186*(ha3*y3+ha4*y4)
    t=t+273.15
    ! calculate liquid enthalpy
    do i=1,2
        check_component: select case (i) ! select composition
        case (1)
            if(t.le.373)then
                hll(1)=0.000198088*t**4-0.263253174*t**3+131.264949*t**2-
29069.26192*t+2410921.733
            else
                hll(1)=0.0227*t**2+9.0203*t-2851.2
            end if
        case (2)
            hll(2)=0.00000626941753153494*t**4-0.008361954*t**3+4.249105865*t**2-
936.7516086*t+74283.83672
        end select check_component
    end do
    hl=4.186*(x3*hll(1)+x4*hll(2))
end

```

```

subroutine dliq(tt,x11,x22,denliq) !calculate density of liquid
    real(8) a(2) !parameter
    real(8) avmw !average molecular weight
    real(8) b(2) !parameter
    real(8) den(2) !liquid density of i component
    real(8) denliq !mixture liquid density
    real(8) n(2) !parameter
    real(8) m(2) !molecular weight
    real(8) tt !temperature
    real(8) tc(2) !critical temperature
    real(8) x1,x11 !liquid propane composition
    real(8) x2,x22 !liquid butane composition
    data tc(1),tc(2)/369.82,452.15/ ! critical temperature
    data m(1),m(2)/44.097,58.124/ ! molecular weight
    data a(1),a(2)/0.22151,0.22827/ ! parameter for calculate liquid density
    data b(1),b(2)/0.27744,0.27240/ ! parameter for calculate liquid density
    data n(1),n(2)/0.28700,0.28630/ ! parameter for calculate liquid density
    if (x11.eq.0.and.x22.eq.0)then
        denliq=0
        return
    end if
    x1=x11/(x11+x22)
    x2=x22/(x11+x22)
    if (tt.gt.369.8)then
        den(1)=a(1)*b(1)**(-1*(1-369.8/tc(1)))**n(1)
        den(2)=a(2)*b(2)**(-1*(1-tt/tc(2)))**n(2)
        goto 1
    end if
    do i=1,2 ! calculate density of component
        den(i)=a(i)*b(i)**(-1*(1-tt/tc(i)))**n(i)
    end do
    1
    avmw=x1*m(1)+x2*m(2) ! calculate average molecular weight
    denliq=1000*(x1*den(1)/m(1)+x2*den(2)/m(2)) ! calculate density of liquid mixture
end

```

```

subroutine cutdec1(dd) ! cut decimal
    real(8) dd,aa,bb,cc
    aa=(int(dd*100))
    bb=(int(dd*10))
    cc=aa/100-bb/10
end

```



```

        if (cc*100.ge.5)then
            dd=bb/10+0.1d0
        else
            dd=bb/10
        end if
    end

subroutine dcontrol(sph,h,dd,v2,d,l1,den,hold) ! control level in reflux drum (feed back)
    real(8) sph,h,k,tari,tard,dt,dd,dh,v2,d,l1,den,hold
    integer i
    k=0.6*15
    tari=18/2.
    tard=18/8.
    dt=1.
    if (den.eq.0)then
        dd=0
        return
    end if
    dh=(v2-d-l1)/(12.33*den)
    dd=k*((h-sph)+1/tari*(hold+dh*dt/2-sph))*dt+tard*dh)
end

subroutine l1control(sp,l1,dl1,l1o) ! control reflux flow rate
    real(8) sp,l1,k,tari,tard,dt,dl1,l1o
    integer i
    k=0.6*2
    tari=2/2.
    tard=2/8.
    dt=1.
    dl1=k*((sp-l1)+1/tari*(sp-l1o-dl1*dt/2))*dt-tard*dl1)
end

subroutine scontrol(sp,s,ds,so) ! control steam flow rate (feed forward)
    real(8) sp,s,k,tari,tard,dt,ds,so
    integer i
    k=0.6*2
    tari=2/2.
    tard=2/8.
    dt=1.
    ds=k*((sp-s)+1/tari*(sp-so-ds*dt/2))*dt-tard*ds)
end

subroutine bcontrol(sph,h,db,vn,b,lnm1,den,hold) ! control level in bottom column (feed back)
    real(8) sph,h,k,tari,tard,dt,db,dh,vn,b,lnm1,den,d2h,hold
    integer i
    k=0.6*15
    tari=17/2.
    tard=17/8.
    dt=1.
    if (den.eq.0)then
        db=0
        return
    end if
    dh=(lnm1-vn-b)/(12.33*den)
    db=k*((h-sph)+1/tari*(hold+dh*dt/2-sph))*dt+tard*dh)
end

subroutine ctcontrol(spt,t,db,f,z1,vp1,y1p1,lm1,x1m1,v,y1,l,x1,told,am) ! control level in bottom column (feed back)
    real(8) spt,t !set point of temperature and temperature
    real(8) k,tari,tard !tuning parameter
    real(8) dt !time step
    real(8) db !set point of reflux change
    real(8) dtt !differentiate of temperature
    real(8) f,z1,z2 !feed flow rate and composition of feed
    real(8) vp1,y2p1,y1p1 !vapor flow rate and composition from tray below sensitive tray
    real(8) lm1,x2m1,x1m1 !liquid flow rate and composition from tray above sensitive tray
    real(8) v,l !vapor and liquid flow rate of sensitive tray
    real(8) y1,x1,y2,x2 !composition of sensitive tray
    real(8) dx1,dx2 !differentiate of liquid composition

```

```

real(8) k1,k2          !equilibrium coefficient
real(8) am             !accumulate on sensitive tray
real(8) told           !temperature of sensitive tray at 30 second ago
k=0.6*0.00002
tari=512/2.
terd=512/8.
dt=1.
x2=1-x1
y2=1-y1
y2p1=1-y1p1
x2m1=1-x1m1
k1=y1/x1
k2=y2/x2
dx2=(f*(z2-x2)+vp1*(y2p1-x2)+lm1*(x2m1-x2)-v*(y2-x2))/am
dx1=(f*(z1-x1)+vp1*(y1p1-x1)+lm1*(x1m1-x1)-v*(y1-x1))/am
dtt=(-k2*dx2-k1*dx1)/(x1*(k1*369.348/(t-168.126)**2)+x2*(k2*1275.718/(t-59.782)**2))
db=k*((t-spt)+1/tari*(told+dtt*dt/2-spt)*dt+tard*dtt)
end

subroutine cbcontrol(spt,t,db,f,z1,vp1,y1p1,lm1,x1m1,v,y1,l,x1,told,am) ! control level in bottom column (feed back)
real(8) spt,t          !set point of temperature and temperature
real(8) k,tari,tard    !tuning parameter
real(8) dt             !time step
real(8) db             !set point of reflux change
real(8) dtt           !differentiate of temperature
real(8) f,z1,z2       !feed flow rate and composition of feed
real(8) vp1,y2p1,y1p1 !vapor flow rate and composition from tray below sensitive tray
real(8) lm1,x2m1,x1m1 !liquid flow rate and composition from tray above sensitive tray
real(8) v,l           !vapor and liquid flow rate of sensitive tray
real(8) y1,x1,y2,x2   !composition of sensitive tray
real(8) dx1,dx2       !differentiate of liquid composition
real(8) k1,k2         !equilibrium coefficient
real(8) am            !accumulate on sensitive tray
real(8) told          !temperature of sensitive tray at 30 second ago
k=0.6*0.00001
tari=604/2.
tard=604/8.
dt=1.
x2=1-x1
y2=1-y1
y2p1=1-y1p1
x2m1=1-x1m1
k1=y1/x1
k2=y2/x2
dx2=(f*(z2-x2)+vp1*(y2p1-x2)+lm1*(x2m1-x2)-v*(y2-x2))/am
dx1=(f*(z1-x1)+vp1*(y1p1-x1)+lm1*(x1m1-x1)-v*(y1-x1))/am
dtt=(-k2*dx2-k1*dx1)/(x1*(k1*369.348/(t-168.126)**2)+x2*(k2*1275.718/(t-59.782)**2))
db=k*((spt-t)+1/tari*(spt-told-dtt*dt/2)*dt-tard*dtt)
end

```

J.2 Depropanizer Column with DMC

```

program distillation
implicit none
integer iii,ll
integer i,ite,j,k      !index
integer ib,it         !index of sensitive tray
integer h,m,s         !time index
integer tf            !tray of feed
integer n             !number if tray and n th tray
real(8) a             !factor
real(8) aa            !parameter
real(8) aaal(150,521)
real(8) aaa2(150,692)
real(8) am(200,2)     !accumulate of liquid in tray (kg-mol/minute)
real(8) amo           !accumulate of liquid in tray at old iteration (kg-mol/minute)
real(8) amv(200)     !accumulate of vapor (kg-mol/minute)

```

real(8) atal(150,150)	
real(8) ata2(150,150)	
real(8) atail(150,150)	
real(8) atai2(150,150)	inverse matrix of
real(8) a1(521,150)	
real(8) a2(692,150)	
real(8) a1t(150,521)	
real(8) a2t(150,692)	
real(8) bb	!parameter
real(8) b(2)	!bottom product flowrate (kg-mol/minute)
real(8) b1(1042)	
real(8) b2(1384)	
real(8) cpn	!heat capacity of cool water (kJ/(C*kg-mol))
real(8) cpw	!heat capacity of hot water(kJ/(C*kg-mol))
real(8) d(2)	!distillate (kg-mol/minute)
real(8) db	!bottom product flow rate change (kg-mol/s)
real(8) dcb	!set point of reboiler change (kg-mol/s)
real(8) dct	!set point of reflux change (kg-mol/s)
real(8) dd	!distillate flow rate change (kg-mol/s)
real(8) denliq(200)	!density of liquid (kg-mol/m ³)
real(8) dl1	!reflux flow rate change (kg-mol/s)
real(8) dm1(150)	!manipulated variable move
real(8) dm2(150)	!manipulated variable move
real(8) dma1(521)	
real(8) dma2(692)	
real(8) dmo1(521)	
real(8) dmo2(692)	
real(8) ds	!steam flow rate change (kg-mol/s)
real(8) dt	!constant step time (1 second)
real(8) f	!feed (kg-mol/half-minute)
real(8) finequa	!feed in equation
real(8) ft	!feed temperature
real(8) ha	!total feed enthalpy
real(8) haineq	!enthalpy of feed in equation
real(8) high(200)	!high of liquid in tray,bottom column and reflux reboiler (m)
real(8) highold(2)	!high of liquid in bottom column and reflux reboiler at old step time (m)
real(8) hl(200)	!total liquid enthalpy (kj/kg-mol)
real(8) hlb	!liquid enthalpy of bottom column (kj/kg-mol)
real(8) hv(200)	!total vapor enthalpy (kj/kg-mol)
real(8) hvb	!vapor enthalpy of bottom column (kj/kg-mol)
real(8) ii(150,150)	!identity matrix
real(8) keep(1000)	!keep value
real(8) l(200,2)	!liquid flow (kg-mol/half-minute)
real(8) lo	!liquid flow of tray No. 1 at old step time (kg-mol/half-minute)
real(8) p(200)	!pressure on tray (bar)
real(8) pb	!pressure of bottom column (bar)
real(8) pf	!pressure of feed (bar)
real(8) qc	!heat duty of condenser (kj)
real(8) qcc	!heat duty of condenser for minute (kj)
real(8) qr	!heat duty of reboiler (kj)
real(8) qrc	!heat duty of reboiler for minute (kj)
real(8) qn	!flowrate of cool water (kg-mol/minute)
real(8) qw	!flowrate of hot water (kg-mol/minute)
real(8) qwo	!flowrate of hot water at old step time (kg-mol/minute)
real(8) scond	!surface area of condenser (m ²)
real(8) sph	!set point of liquid level in drum (m)
real(8) sphb	!set point of liquid level in bottom column (m)
real(8) spl1	!set point of reflux (kg-mol/minute)
real(8) spcb	!set point of cascade at bottom column (K)
real(8) spct	!set point of cascade at top column (K)
real(8) sps	!setpoint of steam flow rate (kg-mol/s)
real(8) sreb	!surface area of reboiler (m ²)
real(8) t(200)	!temperature of tray (K)
real(8) tb	!bottom temperature (K)
real(8) tib	!temperature at tray no. ib th (K)
real(8) tit	!temperature at tray no. it th (K)
real(8) tnout	!temperature of nitrogen out of Kcondenser (K)
real(8) tmin	!temperature of nitrogen enter condenser (K)
real(8) told(2)	!temperature of sensitive tray at 30 second ago (K)
real(8) twout	!temperature of hot water out of reboiler (K)
real(8) twin	!temperature of hot water enter reboiler (K)

```

real(8) ureb          !over all heat transfer coefficient of reboiler (Kw/m2 C)
real(8) ucond        !over all heat transfer coefficient of condenser (Kw/m2 C)
real(8) unwanted     !unwant parameter
real(8) v(200,2)     !vapor flow (kg-mol/minute)
real(8) x(2,200,2)   !liquid composition (component,tray,time)
real(8) xb(2)        !liquid composition at bottom column
real(8) xol1(521)
real(8) xol2(692)
real(8) xx(2)        !keep liquid component value
real(8) y(2,200,2)   !vapor composition (component,tray,time)
real(8) yb(2)        !vapor composition at bottom column
real(8) z(2)         !feed composition
real(8) cc
open (1,file='output.xls')
open (2,file='save.dat')
!initial value
cc=0
iii=0
n=30
am=0.50312
cpn=6024.96
cpw=6024.96
dt=1./60
f=0.09
unwant=0
ft=323
hl=0
l=0
it=6
ib=25
p=1.01325
pf=2.0265
pb=1.01325
qn=0.5
qw=0.001
scond=1000
sreb=1000
spcb=375.8
spct=321.1
sph=0.4
sphb=0.4
spl1=0.315
sps=0.20
t=320
tb=320
tf=n
tnin=288
twin=393
ureb=0.438139514
ucond=0.438139514
v=0
xb=0
yb(1)=0.5
yb(2)=0.5
z(1)=0.5
z(2)=0.5
call enth(pf,ft,unwant,unwant,z(1),z(2),unwant,ha) !calculate enthalpy
do j=1,n
  do i=1,2
    x(i,j,1)=0
    x(i,j,2)=0
  end do
  if (j.lt.n)then
    y(1,j,2)=0.5
    y(2,j,2)=0.5
  end if
  call enth(p(j),t(j),x(1,j,1),x(2,j,1),y(1,j,2),y(2,j,2),hl(j),hv(j)) !calculate enthalpy
  hl(j)=hv(j)
end do
call enth(pb,tb,xb(1),xb(2),yb(1),yb(2),h1b,hvb)
do i=1,1000

```

```

        read (2,*) keep(i)
    end do
    do i=1,n-1
        x(1,i,2)=keep(i)
    end do
    xb(1)=keep(30)
    do i=1,n-1
        x(2,i,2)=keep(30+i)
    end do
    xb(2)=keep(60)
    do i=1,n
        y(1,i,2)=keep(60+i)
    end do
    yb(1)=keep(91)
    do i=1,n
        y(2,i,2)=keep(91+i)
    end do
    yb(2)=keep(122)
    do i=1,n
        am(i,2)=keep(122+i)
    end do
    do i=1,n
        am(i,1)=keep(152+i)
    end do
    do i=1,n
        high(i)=keep(182+i)
    end do
    do i=1,n-1
        t(i)=keep(212+i)
    end do
    tb=keep(242)
    told(1)=keep(243)
    told(2)=keep(244)
    do i=1,n-1
        p(i)=keep(244+i)
    end do
    pb=keep(274)
    do i=1,n
        hl(i)=keep(274+i)
    end do
    hlb=keep(305)
    do i=1,n
        hv(i)=keep(305+i)
    end do
    hvb=keep(336)
    ha=keep(337)
    ft=keep(338)
    f=keep(339)
    z(1)=keep(340)
    z(2)=keep(341)
    do i=1,n
        v(i,2)=keep(341+i)
    end do
    do i=1,n
        l(i,2)=keep(371+i)
    end do
    d(2)=keep(402)
    b(2)=keep(403)
    qw=keep(404)
    qwo=keep(405)
    qr=keep(406)
    qc=keep(407)
    qcc=keep(408)
    qrc=keep(409)
    lo=keep(410)
    do i=1,n
        x(1,i,1)=keep(410+i)
    end do
    do i=1,n
        x(2,i,1)=keep(440+i)
    end do

```

```

do i=1,n
  y(1,i,1)=keep(470+i)
end do
do i=1,n
  y(2,i,1)=keep(500+i)
end do
do i=1,n
  v(i,1)=keep(530+i)
end do
do i=1,n
  l(i,1)=keep(560+i)
end do
sreb=keep(591)
spcb=keep(592)
spct=keep(593)
sph=keep(594)
sphb=keep(595)
spll=keep(596)
sps=keep(597)
tf=keep(598)
it=keep(599)
ib=keep(600)
pf=keep(601)
scond=keep(602)
amo=keep(603)
ucond=keep(604)
ureb=keep(605)
dd=keep(606)
dl1=keep(607)
ds=keep(608)
dcb=keep(609)
dct=keep(610)
db=keep(611)
qn=keep(612)
tnin=keep(613)
tnout=keep(614)
twin=keep(615)
twout=keep(616)
do i=1,n
  denliq(i)=keep(616+i)
end do

```

b1(1)=	0.0
b1(2)=	0.0
b1(3)=	0.0
b1(4)=	0.0
b1(5)=	0.0
b1(6)=	0.0
b1(7)=	0.0
b1(8)=	0.0
b1(9)=	0.0
b1(10)=	0.0
b1(11)=	0.0
b1(12)=	0.0
b1(13)=	-10.0
b1(14)=	-10.0
b1(15)=	-10.0
b1(16)=	-10.0
b1(17)=	-10.0
b1(18)=	-10.0
b1(19)=	-10.0
b1(20)=	-10.0
b1(21)=	-10.0
b1(22)=	-20.0
b1(23)=	-20.0
b1(24)=	-20.0
b1(25)=	-20.0
b1(26)=	-20.0
b1(27)=	-20.0
b1(28)=	-20.0
b1(29)=	-30.0

bl(30)=	-30.0
bl(31)=	-30.0
bl(32)=	-30.0
bl(33)=	-30.0
bl(34)=	-30.0
bl(35)=	-30.0
bl(36)=	-30.0
bl(37)=	-40.0
bl(38)=	-40.0
bl(39)=	-40.0
bl(40)=	-40.0
bl(41)=	-40.0
bl(42)=	-40.0
bl(43)=	-50.0
bl(44)=	-50.0
bl(45)=	-50.0
bl(46)=	-50.0
bl(47)=	-50.0
bl(48)=	-50.0
bl(49)=	-60.0
bl(50)=	-60.0
bl(51)=	-60.0
bl(52)=	-60.0
bl(53)=	-60.0
bl(54)=	-70.0
bl(55)=	-70.0
bl(56)=	-70.0
bl(57)=	-70.0
bl(58)=	-80.0
bl(59)=	-80.0
bl(60)=	-80.0
bl(61)=	-80.0
bl(62)=	-90.0
bl(63)=	-90.0
bl(64)=	-90.0
bl(65)=	-90.0
bl(66)=	-100.0
bl(67)=	-100.0
bl(68)=	-100.0
bl(69)=	-100.0
bl(70)=	-110.0
bl(71)=	-110.0
bl(72)=	-110.0
bl(73)=	-120.0
bl(74)=	-120.0
bl(75)=	-120.0
bl(76)=	-120.0
bl(77)=	-130.0
bl(78)=	-130.0
bl(79)=	-130.0
bl(80)=	-140.0
bl(81)=	-140.0
bl(82)=	-140.0
bl(83)=	-140.0
bl(84)=	-150.0
bl(85)=	-150.0
bl(86)=	-150.0
bl(87)=	-160.0
bl(88)=	-160.0
bl(89)=	-160.0
bl(90)=	-160.0
bl(91)=	-170.0
bl(92)=	-170.0
bl(93)=	-170.0
bl(94)=	-180.0
bl(95)=	-180.0
bl(96)=	-180.0
bl(97)=	-180.0
bl(98)=	-190.0
bl(99)=	-190.0
bl(100)=	-190.0

b1(101)=	-190.0
b1(102)=	-200.0
b1(103)=	-200.0
b1(104)=	-200.0
b1(105)=	-200.0
b1(106)=	-210.0
b1(107)=	-210.0
b1(108)=	-210.0
b1(109)=	-210.0
b1(110)=	-220.0
b1(111)=	-220.0
b1(112)=	-220.0
b1(113)=	-220.0
b1(114)=	-220.0
b1(115)=	-230.0
b1(116)=	-230.0
b1(117)=	-230.0
b1(118)=	-230.0
b1(119)=	-240.0
b1(120)=	-240.0
b1(121)=	-240.0
b1(122)=	-240.0
b1(123)=	-240.0
b1(124)=	-250.0
b1(125)=	-250.0
b1(126)=	-250.0
b1(127)=	-250.0
b1(128)=	-250.0
b1(129)=	-250.0
b1(130)=	-260.0
b1(131)=	-260.0
b1(132)=	-260.0
b1(133)=	-260.0
b1(134)=	-260.0
b1(135)=	-260.0
b1(136)=	-270.0
b1(137)=	-270.0
b1(138)=	-270.0
b1(139)=	-270.0
b1(140)=	-270.0
b1(141)=	-270.0
b1(142)=	-270.0
b1(143)=	-280.0
b1(144)=	-280.0
b1(145)=	-280.0
b1(146)=	-280.0
b1(147)=	-280.0
b1(148)=	-280.0
b1(149)=	-280.0
b1(150)=	-280.0
b1(151)=	-280.0
b1(152)=	-290.0
b1(153)=	-290.0
b1(154)=	-290.0
b1(155)=	-290.0
b1(156)=	-290.0
b1(157)=	-290.0
b1(158)=	-290.0
b1(159)=	-290.0
b1(160)=	-290.0
b1(161)=	-290.0
b1(162)=	-290.0
b1(163)=	-290.0
b1(164)=	-300.0
b1(165)=	-300.0
b1(166)=	-300.0
b1(167)=	-300.0
b1(168)=	-300.0
b1(169)=	-300.0
b1(170)=	-300.0
b1(171)=	-300.0

b1(243)=	-300.0
b1(244)=	-300.0
b1(245)=	-300.0
b1(246)=	-300.0
b1(247)=	-300.0
b1(248)=	-300.0
b1(249)=	-300.0
b1(250)=	-300.0
b1(251)=	-300.0
b1(252)=	-300.0
b1(253)=	-300.0
b1(254)=	-300.0
b1(255)=	-300.0
b1(256)=	-300.0
b1(257)=	-300.0
b1(258)=	-300.0
b1(259)=	-300.0
b1(260)=	-300.0
b1(261)=	-300.0
b1(262)=	-300.0
b1(263)=	-300.0
b1(264)=	-300.0
b1(265)=	-300.0
b1(266)=	-300.0
b1(267)=	-300.0
b1(268)=	-300.0
b1(269)=	-300.0
b1(270)=	-300.0
b1(271)=	-300.0
b1(272)=	-300.0
b1(273)=	-300.0
b1(274)=	-300.0
b1(275)=	-300.0
b1(276)=	-300.0
b1(277)=	-300.0
b1(278)=	-300.0
b1(279)=	-300.0
b1(280)=	-300.0
b1(281)=	-300.0
b1(282)=	-300.0
b1(283)=	-310.0
b1(284)=	-310.0
b1(285)=	-310.0
b1(286)=	-310.0
b1(287)=	-310.0
b1(288)=	-310.0
b1(289)=	-310.0
b1(290)=	-310.0
b1(291)=	-310.0
b1(292)=	-310.0
b1(293)=	-310.0
b1(294)=	-310.0
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b2(1202)=	1450.0
b2(1203)=	1450.0
b2(1204)=	1450.0
b2(1205)=	1450.0
b2(1206)=	1450.0
b2(1207)=	1450.0
b2(1208)=	1450.0
b2(1209)=	1450.0
b2(1210)=	1450.0
b2(1211)=	1450.0
b2(1212)=	1450.0
b2(1213)=	1450.0
b2(1214)=	1450.0
b2(1215)=	1450.0
b2(1216)=	1450.0
b2(1217)=	1450.0
b2(1218)=	1450.0
b2(1219)=	1450.0
b2(1220)=	1450.0
b2(1221)=	1450.0
b2(1222)=	1450.0
b2(1223)=	1450.0
b2(1224)=	1450.0
b2(1225)=	1450.0
b2(1226)=	1450.0
b2(1227)=	1450.0
b2(1228)=	1450.0
b2(1229)=	1450.0
b2(1230)=	1450.0
b2(1231)=	1450.0
b2(1232)=	1450.0
b2(1233)=	1450.0
b2(1234)=	1450.0
b2(1235)=	1450.0
b2(1236)=	1450.0
b2(1237)=	1450.0
b2(1238)=	1450.0
b2(1239)=	1450.0
b2(1240)=	1450.0
b2(1241)=	1450.0
b2(1242)=	1450.0
b2(1243)=	1450.0
b2(1244)=	1450.0
b2(1245)=	1450.0
b2(1246)=	1450.0
b2(1247)=	1450.0
b2(1248)=	1450.0
b2(1249)=	1450.0
b2(1250)=	1450.0
b2(1251)=	1450.0
b2(1252)=	1450.0

b2(1253)=	1450.0
b2(1254)=	1450.0
b2(1255)=	1450.0
b2(1256)=	1450.0
b2(1257)=	1450.0
b2(1258)=	1450.0
b2(1259)=	1450.0
b2(1260)=	1450.0
b2(1261)=	1450.0
b2(1262)=	1450.0
b2(1263)=	1450.0
b2(1264)=	1450.0
b2(1265)=	1450.0
b2(1266)=	1450.0
b2(1267)=	1450.0
b2(1268)=	1450.0
b2(1269)=	1450.0
b2(1270)=	1450.0
b2(1271)=	1450.0
b2(1272)=	1450.0
b2(1273)=	1450.0
b2(1274)=	1450.0
b2(1275)=	1450.0
b2(1276)=	1450.0
b2(1277)=	1450.0
b2(1278)=	1450.0
b2(1279)=	1450.0
b2(1280)=	1450.0
b2(1281)=	1450.0
b2(1282)=	1450.0
b2(1283)=	1450.0
b2(1284)=	1450.0
b2(1285)=	1450.0
b2(1286)=	1450.0
b2(1287)=	1450.0
b2(1288)=	1450.0
b2(1289)=	1450.0
b2(1290)=	1450.0
b2(1291)=	1450.0
b2(1292)=	1450.0
b2(1293)=	1450.0
b2(1294)=	1450.0
b2(1295)=	1450.0
b2(1296)=	1450.0
b2(1297)=	1450.0
b2(1298)=	1450.0
b2(1299)=	1450.0
b2(1300)=	1450.0
b2(1301)=	1450.0
b2(1302)=	1450.0
b2(1303)=	1450.0
b2(1304)=	1450.0
b2(1305)=	1450.0
b2(1306)=	1450.0
b2(1307)=	1450.0
b2(1308)=	1450.0
b2(1309)=	1450.0
b2(1310)=	1450.0
b2(1311)=	1450.0
b2(1312)=	1450.0
b2(1313)=	1450.0
b2(1314)=	1450.0
b2(1315)=	1450.0
b2(1316)=	1450.0
b2(1317)=	1450.0
b2(1318)=	1450.0
b2(1319)=	1450.0
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b2(1333)=	1450.0
b2(1334)=	1450.0
b2(1335)=	1450.0
b2(1336)=	1450.0
b2(1337)=	1450.0
b2(1338)=	1450.0
b2(1339)=	1450.0
b2(1340)=	1450.0
b2(1341)=	1450.0
b2(1342)=	1450.0
b2(1343)=	1450.0
b2(1344)=	1450.0
b2(1345)=	1450.0
b2(1346)=	1450.0
b2(1347)=	1450.0
b2(1348)=	1450.0
b2(1349)=	1450.0
b2(1350)=	1450.0
b2(1351)=	1450.0
b2(1352)=	1450.0
b2(1353)=	1450.0
b2(1354)=	1450.0
b2(1355)=	1450.0
b2(1356)=	1450.0
b2(1357)=	1450.0
b2(1358)=	1450.0
b2(1359)=	1450.0
b2(1360)=	1450.0
b2(1361)=	1450.0
b2(1362)=	1450.0
b2(1363)=	1450.0
b2(1364)=	1450.0
b2(1365)=	1450.0
b2(1366)=	1450.0
b2(1367)=	1450.0
b2(1368)=	1450.0
b2(1369)=	1450.0
b2(1370)=	1450.0
b2(1371)=	1450.0
b2(1372)=	1450.0
b2(1373)=	1450.0
b2(1374)=	1450.0
b2(1375)=	1450.0
b2(1376)=	1450.0
b2(1377)=	1450.0
b2(1378)=	1450.0
b2(1379)=	1450.0
b2(1380)=	1450.0
b2(1381)=	1450.0
b2(1382)=	1450.0
b2(1383)=	1450.0
b2(1384)=	1450.0

```
ii=0.  
do j=1,150  
  ii(j,j)=i.0  
end do  
atai1=ii  
do j=1,521  
  do k=1,150
```



```

                if (j+1-k.le.0)then
                    a1(j,k)=0
                else
                    a1(j,k)=b1(j+1-k)
                end if
            end do
        end do
        alt=transpose(a1)
        atal=matmul(alt,a1)
        atal=atal+1e8*ii !***** 1.5e10
        do i=1,150
            aa=atal(i,i)
            do j=1,150
                atal(i,j)=atal(i,j)/aa
                atai1(i,j)=atai1(i,j)/aa
            end do
            if (i.ne.150)then
                do j=1,150-i
                    bb=atal(151-j,i)
                    do ll=1,150
                        atal(151-j,ll)=atal(151-j,ll)-bb*atal(i,ll)
                        atai1(151-j,ll)=atai1(151-j,ll)-bb*atai1(i,ll)
                    end do
                end do
            end if
        end do
        do i=1,149
            if (i.ne.150)then
                do j=1,150-i
                    bb=atal(j,151-i)
                    do ll=1,150
                        atal(j,ll)=atal(j,ll)-bb*atal(151-i,ll)
                        atai1(j,ll)=atai1(j,ll)-bb*atai1(151-i,ll)
                    end do
                end do
            end if
        end do
        atai2=ii
        do j=1,692
            do k=1,150
                if (j+1-k.le.0)then
                    a2(j,k)=0
                else
                    a2(j,k)=b2(j+1-k)
                end if
            end do
        end do
        a2t=transpose(a2)
        ata2=matmul(a2t,a2)
        ata2=ata2+1e7*ii !***** 0.2e10
        do i=1,150
            aa=ata2(i,i)
            do j=1,150
                ata2(i,j)=ata2(i,j)/aa
                atai2(i,j)=atai2(i,j)/aa
            end do
            if (i.ne.150)then
                do j=1,150-i
                    bb=ata2(151-j,i)
                    do ll=1,150
                        ata2(151-j,ll)=ata2(151-j,ll)-bb*ata2(i,ll)
                        atai2(151-j,ll)=atai2(151-j,ll)-bb*atai2(i,ll)
                    end do
                end do
            end if
        end do
        do i=1,149
            if (i.ne.150)then
                do j=1,150-i
                    bb=ata2(j,151-i)
                    do ll=1,150

```

```

ata2(j,11)=ata2(j,11)-bb*ata2(151-i,11)
atai2(j,11)=atai2(j,11)-bb*atai2(151-i,11)
end do
end do
end if
end do

do h=1,20000
do m=1,60
do s=1,60
write (6,111) h,t(6),t(25),l(1,2),dm1(1),qw,dm2(1),sps,spct
111 format (1i,15f13.7)
if (high(n/2).ge.0.03175)then
tf=n/2
pf=17.0
ft=369.0
f=0.09
z(1)=0.5
z(2)=0.5
!if (h.ge.1)then !disturbance occur
if (h.eq.1.and.m.eq.1.and.s.eq.1)then
!z(1)=0.3
!z(2)=0.7
!f=0.1
qw=0.02
!spct=323.1
end if
unwant=0
call enth(pf,ft,z(1),z(2),unwant,unwant,ha,unwant) !calculate enthalpy
end if

if (s.eq.1)then
told(2)=t(it)
end if
if (s.eq.1.and.cc.eq.0)then
spl1=spl1+dct
end if
!condenser & reflux drum
call l1control(spl1,l(1,2),dl1,lo) ! call control of reflux flow rate
lo=l(1,2)
l(1,2)=l(1,2)+dl1
if (s.eq.1)then
d(2)=d(2)+dd
end if
if (d(2).lt.0.or.high(1).le.0)then
d(2)=0
dd=0
end if
if (l(1,2).lt.0.or.high(1).le.0)then
l(1,2)=0
end if
am(1,2)=am(1,1)+(v(2,2)-l(1,2)-d(2))*dt !calculate accumulate in drum
if (am(1,2).lt.0)then
am(1,2)=0
end if
call dliq(t(1),x(1,1,2),x(2,1,2),denliq(1))
if (s.eq.1)then
highold(1)=high(1)
end if
high(1)=am(1,2)/(denliq(1)*1.23)
if (denliq(1).eq.0.or.high(1).le.0)then
high(1)=0
end if
if (x(1,1,1).eq.0.and.x(2,1,1).eq.0) then
do i=1,2
x(i,1,1)=y(i,1,2)
end do

```

```

end if

x(1,1,2)=(x(1,1,1)*am(1,1)+v(2,2)*y(1,2,2))*dt/(am(1,2)+(l(1,2)+d(2))*dt) !calculate composition in drum
if (x(1,1,2).lt.0.0000000001)then
  x(1,1,2)=0
end if
x(2,1,2)=1.-x(1,1,2)
a=exp(-(ucond*scond)/(qn*cpn))
tnout=tnin+(1-a)*(t(2)-tnin)
qc=qn*cpn*(tnout-tnin) !calculate heat duty of reboiler
if (t(1).lt.308)then
  qc=0
end if
p(1)=16.00
call bubpt(p(1),x(1,1,2),x(2,1,2),y(1,1,2),y(2,1,2),t(1))
call enth(p(1),t(1),x(1,1,2),x(2,1,2),y(1,1,2),y(2,1,2),hl(1),hv(1))
x(1,1,1)=x(1,1,2)
x(2,1,1)=x(2,1,2)
y(1,1,1)=y(1,1,2)
y(2,1,1)=y(2,1,2)
am(1,1)=am(1,2)
v(1,1)=v(1,2)
l(1,1)=l(1,2)

!tray
do j=2,n-1
  if(j.eq.tf)then
    finequa=f
    haineq=ha
  else
    finequa=0
    haineq=0
  end if
  am(j,2)=am(j,1)
  amo=am(j,2)
  call dliq(t(j),x(1,j,2),x(2,j,2),denliq(j))
  high(j)=am(j,2)/(denliq(j)*0.982)
  if (denliq(j).eq.0.or.high(j).le.0)then
    high(j)=0
  end if
  if (high(j).lt.0.03175) then
    l(j,2)=0
  else
    l(j,2)=denliq(j)*1.17*(am(j,2)/(denliq(j)*0.982)-
0.03175)**1.5
    if ((am(j,2)/(denliq(j)*0.982).lt.0.03175)then
      l(j,2)=0
    end if
    if (l(j,2).lt.0)then
      l(j,2)=0
    end if
  end if
  am(j,2)=am(j,1)+(finequa+v(j+1,2)+l(j-1,2)-l(j,2)-v(j,2))*dt !calculate
accumulate in tray
  if (am(i,2).lt.0)then
    am(j,2)=0
  end if
  if (abs((amo-am(j,2))/amo).gt.0.000001) goto 1
  if (denliq(j).eq.0)then
    am(j,2)=am(j,1)+(finequa+v(j+1,2)+l(j-1,2)-v(j,2))*dt
    if (am(j,2).lt.0)then
      am(j,2)=0
    end if
  end if
  if (x(1,j,1).eq.0.and.x(2,j,1).eq.0) then
    do i=1,2
      x(i,j,1)=y(i,j,2)
    end do
  end if
end if

```

```

1,2)*x(1,j-1,2)-v(j,2)*y(1,j,2))*dt)/(am(j,2)+l(j,2)*dt)
x(1,j,2)=(x(1,j,1)*am(j,1)+(finequa*z(1)+v(j+1,2))*y(1,j+1,2)+l(j-
if (x(1,j,2).lt.0)then
    x(1,j,2)=0
end if
x(2,j,2)=1.-x(1,j,2)
p(j)=p(j-1)+0.065
call bubpt(p(j),x(1,j,2),x(2,j,2),y(1,j,2),y(2,j,2),t(j))
call enth(p(j),t(j),x(1,j,2),x(2,j,2),y(1,j,2),y(2,j,2),hl(j),hv(j))
v(j,2)=(hv(j+1)*v(j+1,2)+hl(j-1)*l(j-1,2)+finequa*haineq-
l(j,2)*hl(j))/hv(j)
if (v(j,2).lt.0)then
    v(j,2)=0
end if
end do
do j=2,n-1
    x(1,j,1)=x(1,j,2)
    x(2,j,1)=x(2,j,2)
    y(1,j,1)=y(1,j,2)
    y(2,j,1)=y(2,j,2)
    am(j,1)=am(j,2)
    v(j,1)=v(j,2)
    l(j,1)=l(j,2)
end do
!reboiler & column bottom
if (s.eq.1)then
    told(1)=t(ib)
end if
if (s.eq.1.and.cc.eq.0)then
    sps=sps+dcb
end if
if (sps.lt.0)then
    sps=0
end if
if (n.eq.tf)then
    finequa=f
    haineq=ha
else
    finequa=0
    haineq=0
end if
if (high(n).ge.0.3)then
    call scontrol(sps,qw,ds,qwo) ! call control of steam flow rate
else
    ds=0
end if
qwo=qw
qw=qw+ds
if (qw.lt.0)then
    qw=0
end if
if (qw.le.0) goto 2
if (high(n).ge.0.3)then
    a=exp((ureb*sreb)/(qw*cpw))
    twout=(twin+(a-1)*tb)/a
    qr=qw*cpw*(twin-twout) !calculate heat duty of reboiler
end if
if (high(n).lt.0.1.or.qw.le.0)then
    qr=0
end if
am(n,2)=am(n,1)+(finequa+l(n-1,2)-v(n,2)-b(2))*dt !calculate accumulate in
bottom column
if (am(n,2).lt.0)then
    am(n,2)=0
end if
if (high(n).lt.0.3.and.v(n,2).ne.0)then
    unwant=0
    call enth(pb,tb,unwant,unwant,yb(1),yb(2),unwant,hvb) !calculate
enthalpy
hv(n)=hvb
do i=1,2

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                                y(i,n,2)=yb(i)
                                end do
                                end if
                                if (xb(1).eq.0.and.xb(2).eq.0)then
                                    xb(1)=yb(1)
                                    xb(2)=yb(2)
                                end if
                                xb(1)=(xb(1)*am(n,1)+(finequa*z(1)+l(n-1,2)*x(1,n-1,2)-
v(n,2)*yb(1))*dt)/(am(n,2)+b(2)*dt) !calculate liquid composition in bottom column
                                if (xb(1).lt.0.000000001)then
                                    xb(1)=0
                                end if
                                xb(2)=1-xb(1)
                                pb=p(n-1)+0.065
                                call bubpt(pb,xb(1),xb(2),yb(1),yb(2),tb)
                                do i=1,2
                                    y(i,n,2)=yb(i)
                                end do
                                call dliq(t(n),xb(1),xb(2),denliq(n))
                                if (s.eq.1)then
                                    highold(2)=high(n)
                                end if
                                high(n)=am(n,2)/(denliq(n)*1.23)
                                if (denliq(n).eq.0.or.high(n).le.0)then
                                    high(n)=0
                                end if
                                call enth(pb,tb,xb(1),xb(2),yb(1),yb(2),h1b,hvb)
                                v(n,2)=(qr+finequa*haineq+hl(n-1)*l(n-1,2)-h1b*b(2))/hvb
                                if (v(n,2).lt.0)then
                                    v(n,2)=0
                                end if
                                if (s.eq.1)then
                                    b(2)=b(2)+db
                                end if
                                if (high(n).le.0)then
                                    high(n)=0
                                    b(2)=0
                                    db=0
                                end if
                                if (b(2).lt.0)then
                                    b(2)=0
                                    db=0
                                end if
                                do i=1,2
                                    x(i,n,2)=xb(i)
                                    y(i,n,2)=yb(i)
                                end do
                                x(1,n,1)=x(1,n,2)
                                x(2,n,1)=x(2,n,2)
                                y(1,n,1)=y(1,n,2)
                                y(2,n,1)=y(2,n,2)
                                am(n,1)=am(n,2)
                                v(n,1)=v(n,2)
                                l(n,1)=l(n,2)
                                cc=cc+1
                                if (cc.eq.120)then
                                    cc=0
                                end if
                                call dcontrol(sph,high(1),dd,v(2,2),d(2),l(1,2),denliq(1),highold(1))
                                call bcontrol(sphb,high(n),db,v(n,2),b(2),l(n-1,2),denliq(n),highold(2)) ! call
control of bottom flow rate
                                if (h.eq.8000.and.m.eq.60.and.s.eq.1)then
                                    open (2,file='save.dat')
                                    do i=1,n-1
                                        keep(i)=x(1,i,2)
                                    end do
                                    keep(30)=xb(1)
                                    do i=1,n-1
                                        keep(30+i)=x(2,i,2)
                                    end do
                                    keep(60)=xb(2)
                                end if

```

```

do i=1,n
    keep(60+i)=y(1,i,2)
end do
keep(91)=yb(1)
do i=1,n
    keep(91+i)=y(2,i,2)
end do
    keep(122)=yb(2)
do i=1,n
    keep(122+i)=am(i,2)
end do
do i=1,n
    keep(152+i)=am(i,1)
end do
do i=1,n
    keep(182+i)=high(i)
end do
do i=1,n-1
    keep(212+i)=t(i)
end do
keep(242)=tb
keep(243)=told(1)
keep(244)=told(2)
do i=1,n-1
    keep(244+i)=p(i)
end do
    keep(274)=pb
do i=1,n
    keep(274+i)=hl(i)
end do
    keep(305)=hlb
do i=1,n
    keep(305+i)=hv(i)
end do
keep(336)=hvb
keep(337)=ha
keep(338)=ft
keep(339)=f
keep(340)=z(1)
keep(341)=z(2)
do i=1,n
    keep(341+i)=v(i,2)
end do
do i=1,n
    keep(371+i)=l(i,2)
end do
keep(402)=d(2)
keep(403)=b(2)
keep(404)=qw
keep(405)=qwo
keep(406)=qr
keep(407)=qc
keep(408)=qcc
keep(409)=qrc
keep(410)=lo
do i=1,n
    keep(410+i)=x(1,i,1)
end do
do i=1,n
    keep(440+i)=x(2,i,1)
end do
do i=1,n
    keep(470+i)=y(1,i,1)
end do
do i=1,n
    keep(500+i)=y(2,i,1)
end do
do i=1,n
    keep(530+i)=v(i,1)
end do
do i=1,n

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        keep(560+i)=l(i,1)
    end do
    keep(591)=sreb
    keep(592)=spcb
    keep(593)=spct
    keep(594)=sph
    keep(595)=sphb
    keep(596)=spl1
    keep(597)=sps
    keep(598)=tf
    keep(599)=it
    keep(600)=ib
    keep(601)=pf
    keep(602)=scond
    keep(603)=amo
    keep(604)=ucond
    keep(605)=ureb
    keep(606)=dd
    keep(607)=dl1
    keep(608)=ds
    keep(609)=dcb
    keep(610)=dct
    keep(611)=db
    keep(612)=qn
    keep(613)=tmin
    keep(614)=inout
    keep(615)=twin
    keep(616)=twout
    do i=1,n
        keep(616+i)=denliq(i)
    end do
    do i=1,1000
        write(2,*) keep(i)
    end do
    close(2)
end if

if (cc.eq.0)then
    do j=1,520
        dmo1(522-j)=dmo1(521-j)
    end do
    dmo1(1)=dm1(1)
    do j=1,521
        xol1(j)=0
        do k=1,521
            xol1(j)=xol1(j)+(b1(j+k)-b1(k))*dmo1(k)
        end do
        tit=t(6)
        call cutdec1(tit)
        xol1(j)=tit+xol1(j)
    end do
    aaal=matmul(atai1,a1t)
    do i=1,521
        dmal(i)=spct-xol1(i)
    end do
    dm1=matmul(aaal,dmal)
    dct=dm1(1)

    do j=1,691
        dmo2(693-j)=dmo2(692-j)
    end do
    dmo2(1)=dm2(1)
    do j=1,692
        xol2(j)=0
        do k=1,692
            xol2(j)=xol2(j)+(b2(j+k)-b2(k))*dmo2(k)
        end do
        tib=t(25)
        call cutdec1(tib)
        xol2(j)=tib+xol2(j)
    end do
end if

```

```

end do
aaa2=matmul(atai2,a2t)
do i=1,692
    dma2(i)=spcb-xol2(i)
end do
dm2=matmul(aaa2,dma2)
dcb=dm2(1)
end if
end do !s
!DO J=1,N
!IF (S.EQ.1.AND.M.GE.53.AND.H.GE.1) THEN
!IF (H.ge.1.AND.M.GE.1) THEN
!if (j.eq.n)then
write(1,402) h,t(6),t(25),x(1,1,2),xb(2),l(1,2),qw,d(2),b(2),high(1),high(n),spcb,spct
!write(1,402) H,M,J,TF,xb(1),xb(2),yb(1),yb(2),Tb,Pb,high(n),am(n,2),qr
!else
!WRITE(1,402) H,M,J,TF,x(1,j,2),x(2,j,2),y(1,j,2),y(2,j,2),T(J),P(J),high(J),am(J,2),denliq(j)
!end if
402 FORMAT(1I,2E0.1,15E0.4)
!402 FORMAT(1I,1X,1I,1X,1I,1X,1I,1X,1I,1X,15F12.4)
END If
!END DO
end do !m
end do !h
end program

subroutine bubpt(pp,x1,x2,y1,y2,tt) !calculate temperature from bubble point equation
integer i !index
real(8) df !differential of function
real(8) f !function
real(8) pp !pressure (bar)
real(8) ps1,ps2 !vapor pressure (bar)
real(8) tt !temperature (K)
real(8) x1,x2 !!liquid composition
real(8) y1,y2 !vapor composition
real(8) yy1,yy2
1 ps1=exp(-369.348/(tt-168.126)+5.23749) !calculate vapor pressure of propane
ps2=exp(-1275.718/(tt-59.782)+6.85137) !calculate vapor pressure of butane
y1=x1*ps1/pp !calculate vapor composition
y2=x2*ps2/pp
if (abs(1-y1-y2).lt.0.00000001) goto 10 !find correct temperature
f=1-y1-y2
df=x1/pp*ps1*369.348/(tt-168.126)**2
df=df+x2/pp*ps2*1275.718/(tt-59.782)**2
tt=tt+f/df
goto 1
10
return
end

subroutine enth(p,t,x3,x4,y3,y4,hl,ha) ! calculate liquid and vapor enthalpy from pressure,temperature, and composition
use numerical_libraries
implicit real*8 (a-h,o-z)
real(8) t !temperature
real(8) p !pressure
real(8) y3,y4 !vapor composition of propane and butane
real(8) x3,x4 !!liquid composition
real(8) ha !total vapor enthalpy
real(8) ha3 !vapor enthalpy of propane
real(8) ha4 !vapor enthalpy of butane
real(8) hll(2) !!liquid enthalpy of propane and butane
real(8) hl !total liquid enthalpy
common/blkd1/popv(5),hvc3(5),hvc4(5)
data popv/1.,5.,10.,15.,20./
parameter (korder=3,ndata=5,nknot=ndata+korder)
dimension x1data(ndata),fldata(ndata)
dimension x1knot(nknot),bscoefl(ndata)
integer i

!calculate vapor enthalpy

```



```

t=t-273.15
if (p.eq.1.or.p.eq.5.or.p.eq.10.or.p.eq.15.or.p.eq.20)then
  if (p.eq.1)then

    ha3=0.00000243589743879133*t**3+0.0216068764561292*t**2+16.7600885781487*t+3948.29071794724
    ha4=5171.95353379809+22.7750602176193*t+0.0285385198127802*t**2-
0.0000006546231517426*t**3
    end if
    if (p.eq.5)then

      ha3=3785.71550582761+18.240793123538*t+0.0139970279720996*t**2+0.0000212237762234762*t**3
      ha4=13362.9290022956-614.055453861994*t+19.4411005643476*t**2-
0.305859930252696*t**3+0.00264210823154405*t**4-0.0000118981890756778*t**5+0.000000218680429435476*t**6
      end if
      if (p.eq.10)then
        ha3=9299.88843643293-489.679087204064*t+18.2134871645406*t**2-
0.335630483024728*t**3+0.00337653409332662*t**4-0.0000176090629930964*t**5+0.000000372728987837522*t**6
        ha4=52119.620884926-4542.38831847744*t+183.561795154405*t**2-
3.96420633705897*t**3+0.0496691999500929*t**4-0.000361742582892285*t**5+0.00000142214836684578*t**6-
0.00000000233518724898894*t**7
        end if
        if (p.eq.15)then
          ha3=3499.26966208774+10.0480539969921*t+0.235411990181417*t**2-
0.00185526320973007*t**3+0.00000546197552656038*t**4
          ha4=-41073.9677943845+4570.52957391954*t-
185.978489301388*t**2+4.09239659695254*t**3-0.0523767526218596*t**4+0.000390079118628205*t**5-
0.00000156690531090442*t**6+0.0000000262353582012308*t**7
          end if
          if (p.eq.20)then
            ha3=4127.1570396016+73.4391303904704*t-
4.99493677579601*t**2+0.125573969112786*t**3-0.00143072973061548*t**4+0.0000077793456208826*t**5-
0.0000000164069371112414*t**6
            ha4=54716.6018791736-4931.18850411005*t+206.110049953317*t**2-
4.63591405624864*t**3+0.0608851762849367*t**4-0.000467220003840682*t**5+0.00000194083612282833*t**6-
0.00000000336865665585238*t**7
            end if
          else
            do i=1,5
              x1 data(i)=popv(i)
            end do
            do i=1,5
              if (i.eq.1)then
                hvc3(i)=2.43589743879133*10**(-
6)*t**3+0.0216068764561292*t**2+16.7600885781487*t+3948.29071794724
                hvc4(i)=5171.95353379809+22.7750602176193*t+0.0285385198127802*t**2-
0.0000006546231517426*t**3
                end if
                if (i.eq.2)then

                  hvc3(i)=3785.71550582761+18.240793123538*t+0.0139970279720996*t**2+0.0000212237762234762*t**3
                  hvc4(i)=13362.9290022956-614.055453861994*t+19.4411005643476*t**2-
0.305859930252696*t**3+0.00264210823154405*t**4-0.0000118981890756778*t**5+0.000000218680429435476*t**6
                  end if
                  if (i.eq.3)then
                    hvc3(i)=9299.88843643293-489.679087204064*t+18.2134871645406*t**2-
0.335630483024728*t**3+0.00337653409332662*t**4-0.0000176090629930964*t**5+0.000000372728987837522*t**6
                    hvc4(i)=52119.620884926-4542.38831847744*t+183.561795154405*t**2-
3.96420633705897*t**3+0.0496691999500929*t**4-0.000361742582892285*t**5+0.00000142214836684578*t**6-
0.00000000233518724898894*t**7
                    end if
                    if (i.eq.4)then
                      hvc3(i)=3499.26966208774+10.0480539969921*t+0.235411990181417*t**2-
0.00185526320973007*t**3+0.00000546197552656038*t**4
                      hvc4(i)=-41073.9677943845+4570.52957391954*t-
185.978489301388*t**2+4.09239659695254*t**3-0.0523767526218596*t**4+0.000390079118628205*t**5-
0.00000156690531090442*t**6+0.0000000262353582012308*t**7
                      end if
                      if (i.eq.5)then
                        hvc3(i)=4127.1570396016+73.4391303904704*t-
4.99493677579601*t**2+0.125573969112786*t**3-0.00143072973061548*t**4+0.0000077793456208826*t**5-
0.0000000164069371112414*t**6

```

```

                                hvc4(i)=54716.6018791736-4931.18850411005*t+206.110049953317*t**2-
4.63591405624864*t**3+0.0608851762849367*t**4-0.000467220003840682*t**5+0.00000194083612282833*t**6-
0.00000000336865665585238*t**7
                                end if
                                fl data(i)=hvc3(i)
                                end do
                                call dbsnak(ndata,x1data,korder,x1knot)
                                call dbsint(ndata,x1data,fl data,korder,x1knot,bscoef1)
                                ncoef=ndata
                                ha3=dbsval(p,korder,x1knot,ncoef,bscoef1)
                                do i=1,5
                                        fl data(i)=hvc4(i)
                                enddo
                                call dbsint(ndata,x1data,fl data,korder,x1knot,bscoef1)
                                ha4=dbsval(p,korder,x1knot,ncoef,bscoef1)
                                end if
                                ha=4.186*(ha3*y3+ha4*y4)
                                t=t+273.15
                                ! calculate liquid enthalpy
                                do i=1,2
                                        check_component: select case (i) ! select composition
                                        case (1)
                                                if(t.le.373)then
                                                        hll(1)=0.000198088*t**4-0.263253174*t**3+131.264949*t**2-
29069.26192*t+2410921.733
                                                else
                                                        hll(1)=0.0227*t**2+9.0203*t-2851.2
                                                end if
                                        case (2)
                                                hll(2)=0.00000626941753153494*t**4-0.008361954*t**3+4.249105865*t**2-
936.7516086*t+74283.83672
                                        end select check_component
                                end do
                                hl=4.186*(x3*hll(1)+x4*hll(2))
                                end

subroutine dliq(tt,x11,x22,denliq) !calculate density of liquid
    real(8) a(2)                !parameter
    real(8) avmw                !average molecular weight
    real(8) b(2)                !parameter
    real(8) den(2)              !liquid density of i component
    real(8) denliq              !mixture liquid density
    real(8) n(2)                !parameter
    real(8) m(2)                !molecular weight
    real(8) tt                  !temperature
    real(8) tc(2)               !critical temperature
    real(8) x1,x11              !liquid propane composition
    real(8) x2,x22              !liquid butane composition
    data tc(1),tc(2)/369.82,452.15/ ! critical temperature
    data m(1),m(2)/44.097,58.124/ ! molecular weight
    data a(1),a(2)/0.22151,0.22827/ ! parameter for calculate liquid density
    data b(1),b(2)/0.27744,0.27240/ ! parameter for calculate liquid density
    data n(1),n(2)/0.28700,0.28630/ ! parameter for calculate liquid density
    if (x11.eq.0.and.x22.eq.0)then
        denliq=0
        return
    end if
    x1=x11/(x11+x22)
    x2=x22/(x11+x22)
    if (tt.gt.369.8)then
        den(1)=a(1)*b(1)**(-1*(1-369.8/tc(1)))**n(1))
        den(2)=a(2)*b(2)**(-1*(1-tt/tc(2)))**n(2))
        goto 1
    end if
    do i=1,2 ! calculate density of component
        den(i)=a(i)*b(i)**(-1*(1-tt/tc(i)))**n(i))
    end do
    !
    avmw=x1*m(1)+x2*m(2) ! calculate average molecular weight
    denliq=1000*(x1*den(1)/m(1)+x2*den(2)/m(2)) ! calculate density of liquid mixture
end

```

```

subroutine cutdec1(dd) ! cut decimal
  real(8) dd,aa,bb,cc
  aa=(int(dd*1000))
  bb=(int(dd*100))
  cc=aa/1000-bb/100
  if (cc*1000.ge.5)then
    dd=bb/100+0.01d0
  else
    dd=bb/100
  end if
end

subroutine dcontrol(sph,h,dd,v2,d,l1,den,hold) ! control level in reflux drum (feed back)
  real(8) sph,h,k,tari,tard,dt,dd,dh,v2,d,l1,den,hold
  integer i
  k=0.6*15
  tari=18/2.
  tard=18/8.
  dt=1.
  if (den.eq.0)then
    dd=0
    return
  end if
  dh=(v2-d-l1)/(12.33*den)
  dd=k*((h-sph)+1/tari*(hold+dh*dt/2-sph)*dt+tard*dh)
end

subroutine l1control(sp,l1,dl1,l1o) ! control reflux flow rate
  real(8) sp,l1,k,tari,tard,dt,dl1,l1o
  integer i
  k=0.6*2
  tari=2/2.
  tard=2/8.
  dt=1.
  dl1=k*((sp-l1)+1/tari*(sp-l1o-dl1*dt/2)*dt-tard*dl1)
end

subroutine scontrol(sp,s,ds,so) ! control steam flow rate (feed forward)
  real(8) sp,s,k,tari,tard,dt,ds,so
  integer i
  k=0.6*2
  tari=2/2.
  tard=2/8.
  dt=1.
  ds=k*((sp-s)+1/tari*(sp-so-ds*dt/2)*dt-tard*ds)
end

subroutine bcontrol(sph,h,db,vn,b,lnm1,den,hold) ! control level in bottom column (feed back)
  real(8) sph,h,k,tari,tard,dt,db,dh,vn,b,lnm1,den,d2h,hold
  integer i
  k=0.6*15
  tari=17/2.
  tard=17/8.
  dt=1.
  if (den.eq.0)then
    db=0
    return
  end if
  dh=(lnm1-vn-b)/(12.33*den)
  db=k*((h-sph)+1/tari*(hold+dh*dt/2-sph)*dt+tard*dh)
end

```

Appendix K Compared Result of Depropanizer Column between results of ProII Program and Fortran Program

Results of liquid composition in table K.1 and Figure K.1 have low error at the top bottom tray. Tray that stays near the centre of the column will have the high error. Results of vapour composition in table K.2 and Figure K.2 have tend like the results of liquid composition. From the Figure K.1 and K.2, Tend of liquid and vapor composition are in the same tending of ProII program.

Table K.1 Liquid compositions (mole fraction) of distillation column at steady-state of ProII and Fortran (implicit method, IFP's method) programs

Tray No.	Fortran		ProII		% Error	
	Propane	Butane	Propane	Butane	Propane	Butane
1	1	0	1	0	0	0
2	1	0	1	0	0	0
3	0.9999	0.0001	0.9999	0.0001	0	0
4	0.9999	0.0001	0.9999	0.0001	0	0
5	0.9997	0.0003	0.9997	0.0003	0	0
6	0.9994	0.0006	0.9994	0.0006	0	0
7	0.9988	0.0012	0.9986	0.0014	0.02	-14.29
8	0.9974	0.0026	0.9969	0.0031	0.05	-16.13
9	0.9947	0.0053	0.9933	0.0067	0.14	-20.90
10	0.989	0.011	0.9856	0.0144	0.34	-23.61
11	0.9775	0.0225	0.9692	0.0308	0.86	-26.95
12	0.9547	0.0453	0.936	0.064	2.00	-29.22
13	0.9117	0.0883	0.8735	0.1265	4.37	-30.20
14	0.8376	0.1624	0.7711	0.2289	8.62	-29.05
15	0.7274	0.2726	0.6342	0.3658	14.70	-25.48
16	0.6828	0.3172	0.5944	0.4056	14.87	-21.79
17	0.6147	0.3853	0.5355	0.4645	14.79	-17.05
18	0.5224	0.4776	0.4573	0.5427	14.24	-12.00
19	0.4142	0.5858	0.3666	0.6334	12.98	-7.52
20	0.306	0.694	0.2754	0.7246	11.11	-4.22
21	0.2123	0.7877	0.1951	0.8049	8.82	-2.14
22	0.1404	0.8596	0.1319	0.8681	6.44	-0.98
23	0.0898	0.9102	0.0861	0.9139	4.30	-0.40
24	0.0562	0.9438	0.0549	0.9452	2.37	-0.15
25	0.0346	0.9654	0.0343	0.9657	0.87	-0.03
26	0.0211	0.9789	0.0211	0.9789	0	0
27	0.0128	0.9872	0.0128	0.9872	0	0
28	0.0076	0.9924	0.0077	0.9924	-1.2987	0
29	0.0045	0.9955	0.0044	0.9956	2.27273	-0.01
30	0.0025	0.9975	0.0025	0.9975	0	0

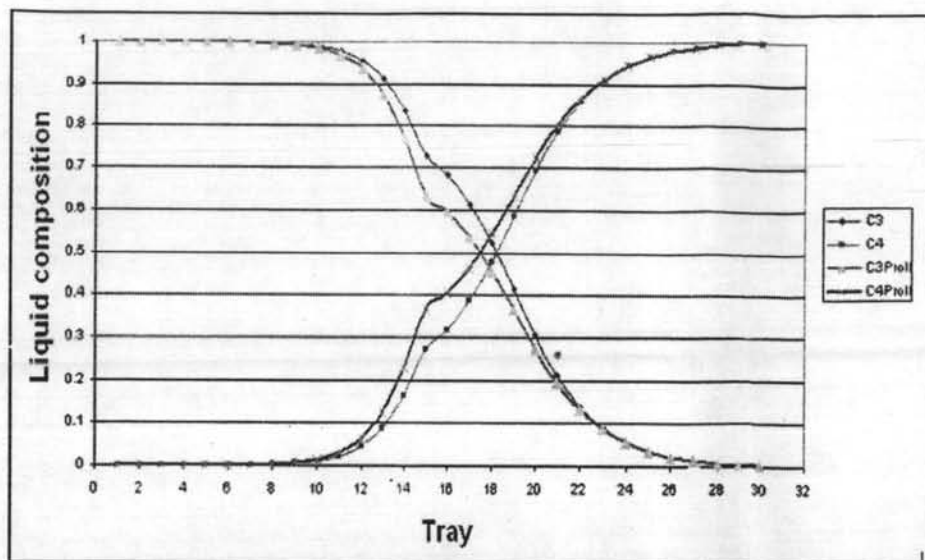


Figure K.1 Liquid composition (mole fraction) from Fortran (implicit method, IFP's method) program compared to one from ProII.

Table K.2 Vapor composition (mole fraction) of distillation column at steady-state from ProII and Fortran (implicit method, IFP's method) programs

Tray No.	Fortran		ProII		% Error	
	Propane	Butane	Propane	Butane	Propane	Butane
1	1	0	1	0	0	0
2	1	0	1	0	0	0
3	1	0	1	0	0	0
4	0.9999	0.0001	1	0.0001	-0.01	0
5	0.9999	0.0001	0.9999	0.0001	0	0
6	0.9998	0.0002	0.9998	0.0003	0	-33.333
7	0.9995	0.0005	0.9994	0.0006	0.01001	-16.667
8	0.9989	0.0011	0.9988	0.0012	0.01001	-8.3333
9	0.9977	0.0023	0.9973	0.0027	0.04011	-14.815
10	0.9953	0.0047	0.9942	0.0058	0.11064	-18.966
11	0.9903	0.0097	0.9875	0.0125	0.28354	-22.4
12	0.9801	0.0199	0.9733	0.0267	0.69865	-25.468
13	0.96	0.04	0.9446	0.0554	1.63032	-27.798
14	0.9223	0.0777	0.8909	0.1091	3.52453	-28.781
15	0.8579	0.1421	0.8038	0.1962	6.73053	-27.574
16	0.8284	0.1716	0.7744	0.2256	6.97314	-23.936
17	0.7793	0.2207	0.7273	0.2727	7.14973	-19.069
18	0.7035	0.2965	0.6569	0.3431	7.09393	-13.582
19	0.5993	0.4007	0.5624	0.4376	6.56117	-8.4324
20	0.4754	0.5246	0.4513	0.5487	5.34013	-4.3922
21	0.3505	0.6495	0.3388	0.6612	3.45337	-1.7695
22	0.2424	0.7576	0.2395	0.7605	1.21086	-0.3813
23	0.1598	0.8402	0.1614	0.8386	-0.9913	0.19079
24	0.1019	0.8981	0.105	0.895	-2.9524	0.34637
25	0.0636	0.9364	0.0665	0.9335	-4.3609	0.31066
26	0.039	0.961	0.0413	0.9587	-5.569	0.23991
27	0.0237	0.9763	0.0252	0.9748	-5.9524	0.15388
28	0.0142	0.9858	0.0151	0.9849	-5.9603	0.09138
29	0.0083	0.9917	0.0088	0.9912	-5.6818	0.05044
30	0.0047	0.9953	0.0049	0.9951	-4.0816	0.0201

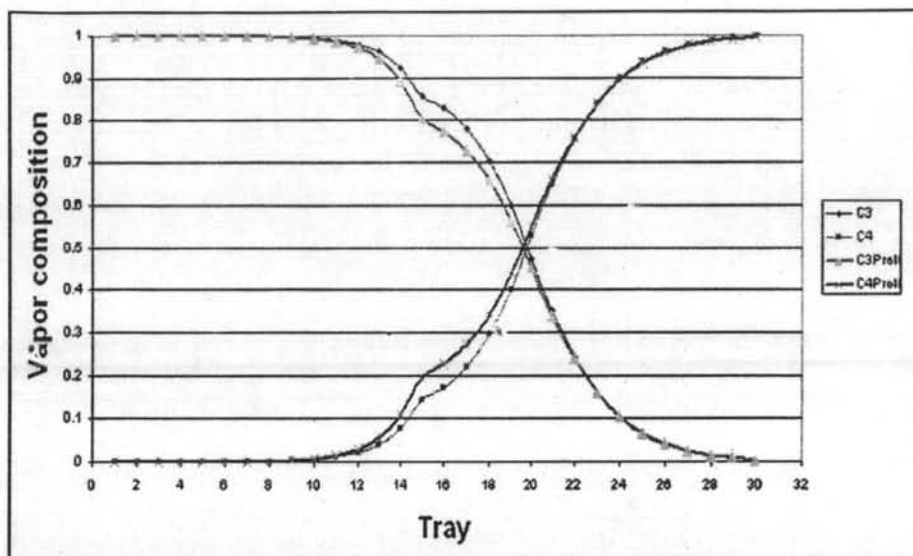


Figure K.2 Vapor composition (mole fraction) from Fortran (implicit method, IFP's method) program compared to ProII.

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