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OXIDATION OF NITROBENZENE BY FLUIDIZED-BED FENTON
PROCESS IN THE PRESENCE OF CHLORIDE IONS

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A Thesis Submitted in Partial Fulfillment of the Requirements
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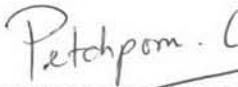
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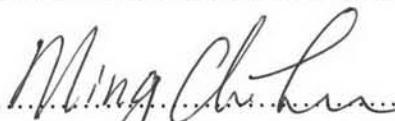
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สมบูรณ์ ชินพิดนันท์ : การออกซิเดชันของไนโตรเบนซินด้วยกระบวนการฟลูอิไดซ์เฟนดันที่มีคลอไรด์อ่อน (OXIDATION OF NITROBENZENE BY FLUIDIZED-BED FENTON PROCESS IN THE PRESENCE OF CHLORIDE IONS) อ.ที่ปรึกษา : ผศ.ดร. ชวัลิต รัตนธรรมสกุล, อ.ที่ปรึกษาร่วม : PROF. MING-CHUN LU, PH.D., 124 หน้า.

งานวิจัยนี้ศึกษาผลของการออกซิเดชันของไนโตรเบนซินด้วยกระบวนการฟลูอิไดซ์เฟนดันที่มีคลอไรด์อ่อน โดยการศึกษาผลกระทบที่เกี่ยวข้องในกระบวนการเฟนดันนี้ได้ใช้ค่าของ พีเอช เฟอร์สติอ่อน ไชโตรเจนเปอร์ออกไซด์ และความเข้มข้นของคลอไรด์อ่อน จากผลการทดลองแสดงให้เห็นว่าอะลูมิเนียมออกไซด์ ซึ่งใช้เป็นตัวกลางโดยมีค่าพีเอช ห้อบอฟซีโรชาร์จ เท่ากับ 9.16 และมีขนาดเท่ากับ 2.50 มิลลิเมตร เป็นตัวกลางที่มีประสิทธิภาพต่อการออกซิเดชันของไนโตรเบนซินด้วยกระบวนการฟลูอิไดซ์เฟนดัน และค่าพีเอช ที่เหมาะสมคือ 2.8 โดยที่กระบวนการฟลูอิไดซ์เฟนดันมีประสิทธิภาพต่อการออกซิเดชันของไนโตรเบนซินที่ต่ำกว่ากระบวนการเฟนดัน การยับยั้งการออกซิเดชันของไนโตรเบนซินด้วยกระบวนการฟลูอิไดซ์เฟนดันโดยคลอไรด์อ่อนจะไม่สามารถทำได้เมื่อค่าความเข้มข้นของคลอไรด์อ่อนต่ำ ที่ค่าความเข้มข้นของคลอไรด์อ่อนสูงการออกซิเดชันของไนโตรเบนซินจะถูกยับยั้งและผลที่มาจากการเกิดปฏิกิริยาที่ซับซ้อนระหว่างเฟอร์สต์และคลอไรด์ ใน การศึกษาได้ทำการใช้ค่าความเข้มข้นของคลอไรด์อ่อนที่ 0.2 โมลาริต เพื่อศึกษาความเข้มข้นของเฟอร์สต์ที่ใช้ในกระบวนการเฟนดันพบว่าเมื่ออัตราส่วนระหว่างความเข้มข้นของคลอไรด์อ่อนต่อกว่าความเข้มข้นของเฟอร์สต์ค่าน้อยกว่าหรือเท่ากับ 200 จะทำให้มีผลต่อการยับยั้งการออกซิเดชันของไนโตรเบนซิน และในทางเดียวกันการเติมเฟอร์สติอ่อนจะมีความสำคัญมากกว่าการเติมไชโตรเจนเปอร์ออกไซด์ที่จะสามารถหยุดการยับยั้งการออกซิเดชันของไนโตรเบนซินที่ พีเอช 2.8 ได้ และผลของการเพิ่มความเข้มข้นของไชโตรเจนเปอร์ออกไซด์ไม่มีผลต่อการยับยั้งการออกซิเดชันของไนโตรเบนซิน การยับยั้งการออกซิเดชันของไนโตรเบนซินยังเงื่อนกับผลของพีเอชด้วยโดยที่ช่วงของการยับยั้งจะลดลงเมื่อเพิ่มค่าพีเอชที่น้อยกว่า 6

ภาควิชา วิศวกรรมสิ่งแวดล้อม
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ลายมือชื่อนิสิต.....
ลายมือชื่ออาจารย์ที่ปรึกษา.....
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SOMBOON CHINTITANUN: OXIDATION OF NITROBENZENE BY FLUIDIZED-BED FENTON PROCESS IN THE PRESENCE OF CHLORIDE IONS. THESIS ADVISOR: ASST. PROF. CHAVALIT RATANATAMSKUL, PH.D., THISIS CO-ADVISOR: PROF. MING-CHUN LU, PH.D., 124 pp.

The objective of this study was to experimentally probe the chloride ions specifically affecting nitrobenzene oxidation by Fenton's reagent. Fluidized-bed experiments were carried out to investigate the effects of pH, Fe^{2+} , H_2O_2 and chloride concentration on the oxidation reaction. Results show that the best efficiency for nitrobenzene oxidation by fluidized-bed Fenton process was used Al_2O_3 as the carrier which has pH_{pzc} of 9.16 and size of 2.50 mm. Optimum pH for nitrobenzene was 2.8. The removal efficiency oxidation of nitrobenzene by fluidized-bed Fenton process was better than Fenton process. The inhibition caused by chloride ions can be overcome by extending the reaction time if the concentration of chloride ions was low. At a high concentration of chloride ions, however, the oxidation of nitrobenzene was inhibited, and actually ceased due to the complexation of Fe–Cl. In this study, the chloride ion concentration was kept at 0.2 M in the experiments when studying the effect of ferrous ion concentration on the Fenton reaction. If the ratio of $[\text{Cl}^-]/[\text{Fe}^{2+}]$ was ≤ 200 , the inhibition effect was very significant. In other words, adding more ferrous ions rather than hydrogen peroxide can break the inhibition originating from the chloride ions at an initial stage of pH 2.8. The inhibition effect of chloride ions on the nitrobenzene reaction depended on the reaction pH; the extent of inhibition decreased with increasing the initial pH as long as the pH was less than 6.

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NOMENCLATURES

AOPs = advanced oxidation processes

UV = ultraviolet

TOC = total organic carbon

$C_6H_5NO_2$ = nitrobenzene (NB)

H_2O_2 = hydrogen peroxide

Fe^{2+} = ferrous ion

Fe^{3+} = ferric ion

OH^{\cdot} = hydroxyl radical

OH^- = hydroxide ion

min = minute

M = molar

k = rate constant

r = initial rate

FB = fluidized-bed

FBR = fluidized-bed Fenton reactor

Γ = surface concentration

s = specific surface area

γ = mass concentration