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APPENDIX

A. CALCULATION OF EMPIRICAL THERMAL CONDUCTIVITY

From the empirical thermal diffusivity (D-Emp.) could be calculated the empirical thermal conductivity (K-Emp.) by this equation below ;

$$D = K/\rho C_p \quad (A-1)$$

This value was represented quantity of heat flux transport through the tire. This experiment, the changing of tread compound properties during tire curing process were simulated to measure by thermal analyser. Those measurings were specific heat and density change with temperature. (see Fig. A.1 and A.2) The details of calculation shown in table 5.6 and 5.7. The empirical value had some correlation with temperature. But the literatures presented, thermal conductivity was calculated from overall range of temperature during curing process. This work also, calculating had been done based on vulcanizing temperature 125-150 °C. It found that the value as follows.

- For ideal boundary condition : 0.24 - 0.26 W/m.°C.
- For actual boundary condition : 1.25 - 1.36 W/m.°C.

Curve 1: TMA in Expansion
 File info: uvsam Thu Feb 23 15:36:25 1995
 Sample Height: 13.101 mm
 non-vulcanisated sample
 (Subtracted)

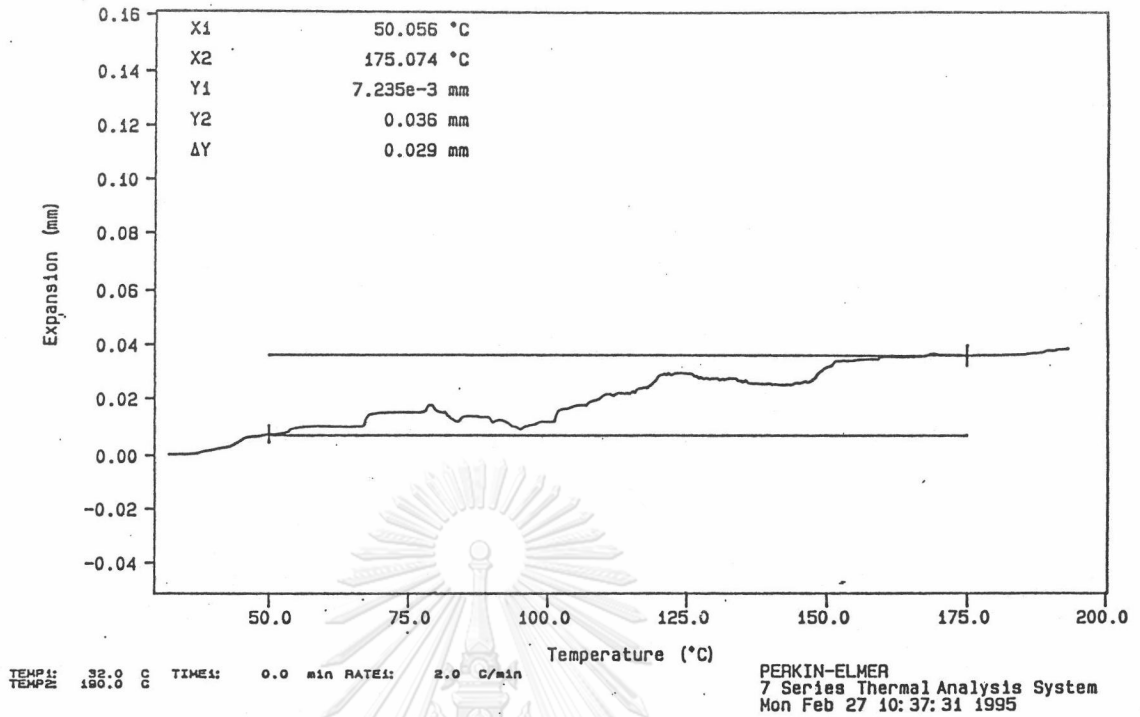


Figure A.1 The expansion of tread compound during tire curing ; Simulation by TMA.

Curve 1: DSC
 File info: tu5 Wed Mar 8 11:09:34 1995
 Sample Weight: 5.120 mg
 unvulcanize

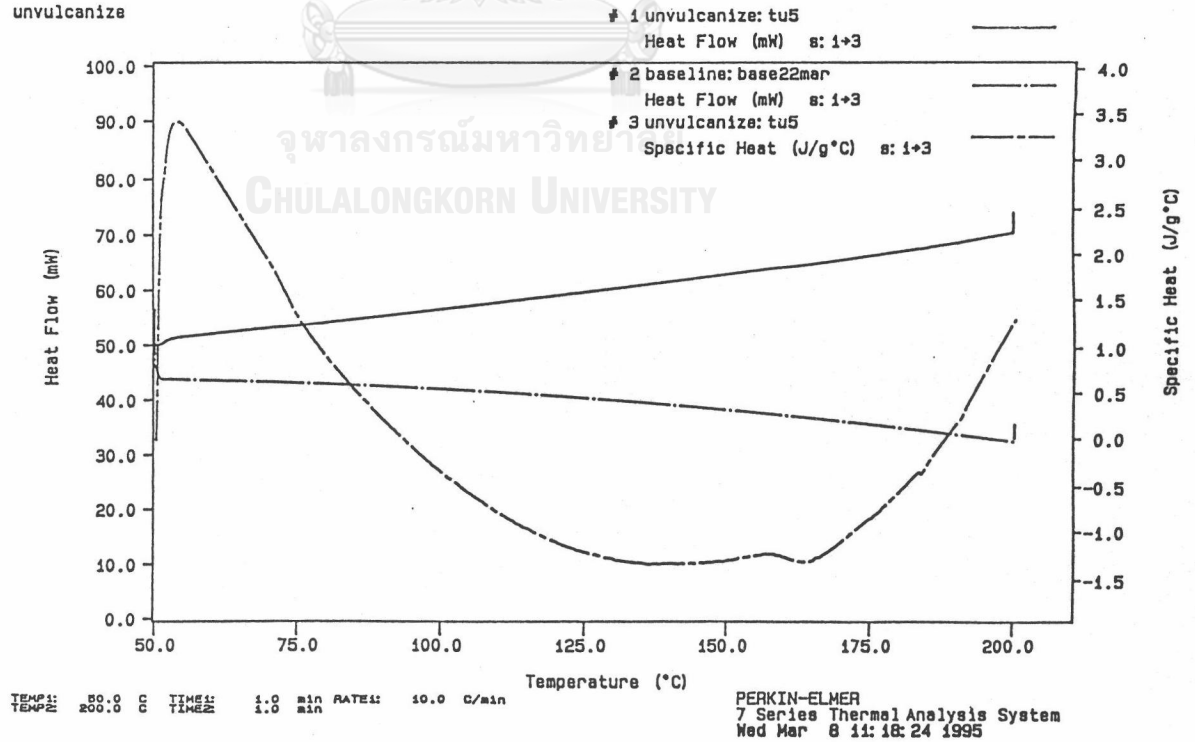
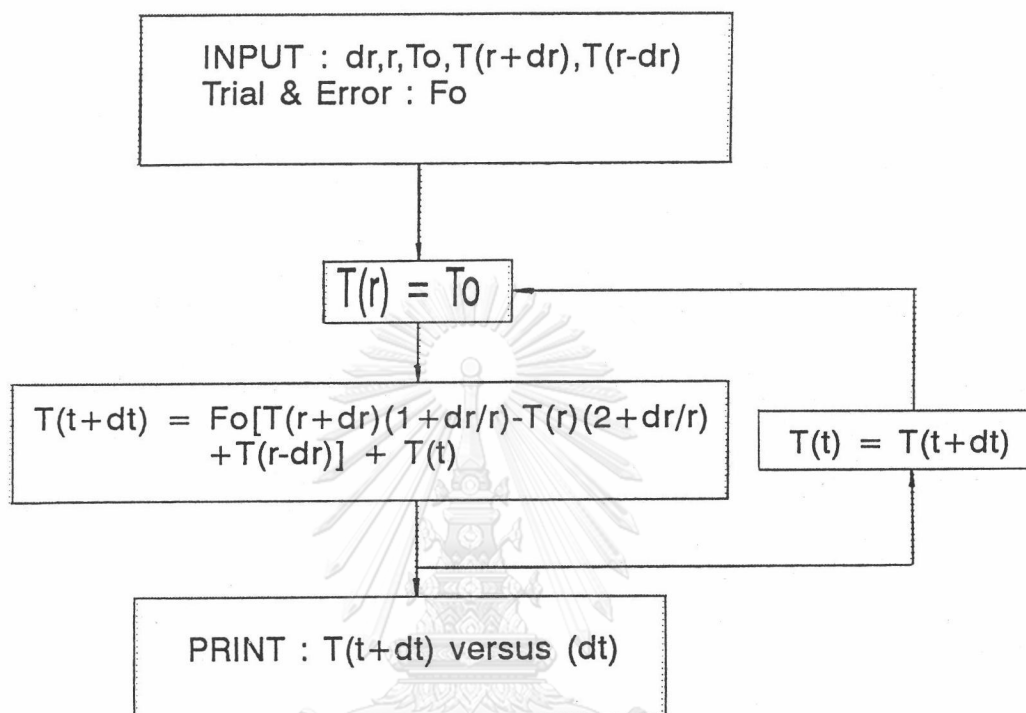


Figure A.2 The specific heat versus temperature profile for tread compound ; Measured by DSC.

B. Sample calculation by computer aided

Calculation flow chart



From this flow chart, the calculation had been done on computer by using *LOTUS 123* application. Input data for calculation are including ;

- Initial and boundary condition : T_0 , $T(r+\Delta r)$, $T(r-\Delta r)$
- Time interval : Δt
- Dimension for specified under tread position : Δr , r
- Trial and Error : F_0

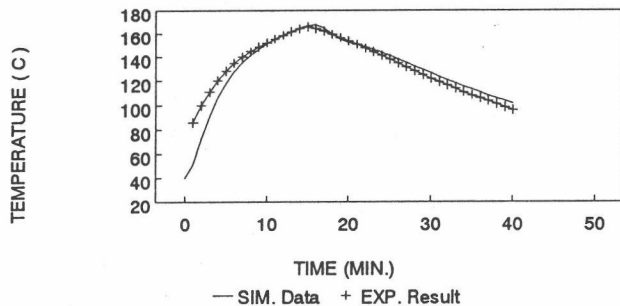
The running results are shown at next page.

$T(r+dr)$	$T(r+dr) \times (1+dr/r)$	$T(r)=T(t)$	$T(r) \times (2+dr/r)$	$T(r-dr) = T(r+dr)$	CURING TIME				
40.0	41.4	40.0	81.4	40.0	10.7	50.7	0.0		
75.3	77.9	50.7	103.2	65.7	21.5	72.2	1.0	85.8	
95.5	98.8	72.2	146.8	76.7	18.8	90.9	2.0	99.7	
110.5	114.3	90.9	185.0	93.0	15.1	106.1	3.0	110.9	
122.2	126.4	106.1	215.7	106.9	12.1	118.1	4.0	120.4	
130.8	135.3	118.1	240.3	118.3	9.5	127.6	5.0	128.4	
137.8	142.5	127.6	259.6	127.7	7.6	135.2	6.0	135.0	
143.6	148.5	135.2	275.1	135.3	6.4	141.6	7.0	140.3	
148.3	153.4	141.6	288.1	141.9	5.2	146.9	8.0	144.9	
152.3	157.5	146.9	298.8	147.3	4.5	151.4	9.0	148.9	
155.8	161.1	151.4	307.9	152.0	3.9	155.2	10.0	152.3	
159.1	164.6	155.2	315.8	156.0	3.6	158.8	11.0	155.6	
162.0	167.6	158.8	323.1	159.8	3.3	162.1	12.0	158.7	
164.3	169.9	162.1	329.7	163.3	2.7	164.8	13.0	161.7	
166.3	172.0	164.8	335.2	166.2	2.3	167.0	14.0	164.3	
168.0	173.8	167.0	339.8	168.6	0.6	167.6	15.0	166.1	
167.9	173.7	167.6	341.0	167.5	-2.7	164.9	16.0	164.6	
162.5	168.1	164.9	335.5	160.8	-5.0	159.9	17.0	162.3	
156.2	161.6	159.9	325.3	155.4	-4.4	155.5	18.0	159.4	
152.3	157.5	155.5	316.3	153.2	-2.8	152.7	19.0	156.6	
150.3	155.5	152.7	310.6	152.1	-1.9	150.8	20.0	153.7	
148.4	153.5	150.8	306.7	150.6	-2.0	148.8	21.0	150.8	
146.3	151.3	148.8	302.7	148.5	-2.2	146.6	22.0	147.6	
143.9	148.8	146.6	298.1	146.0	-2.6	144.0	23.0	144.6	
141.4	146.3	144.0	292.9	143.1	-2.8	141.2	24.0	141.4	
138.7	143.5	141.2	287.2	139.9	-2.0	138.3	25.0	138.0	
135.9	140.6	138.3	281.3	136.8	-3.0	135.3	26.0	134.8	
133.0	137.6	135.3	275.2	133.5	-3.0	132.3	27.0	131.5	
130.2	134.7	132.3	269.0	130.4	-2.9	129.3	28.0	128.2	
127.4	131.8	129.3	263.1	127.4	-2.9	126.4	29.0	125.0	
124.7	129.0	126.4	257.2	124.4	-2.9	123.6	30.0	122.0	
122.1	126.3	123.6	251.4	121.4	-2.8	120.8	31.0	119.0	
119.4	123.5	120.8	245.8	118.5	-2.7	118.2	32.0	116.3	
117.1	121.1	118.2	240.4	115.9	-2.5	115.6	33.0	113.8	
114.7	118.6	115.6	235.2	113.2	-2.6	113.0	34.0	110.8	
112.1	115.9	113.0	230.0	110.4	-2.6	110.5	35.0	108.1	
109.8	113.6	110.5	224.8	107.9	-2.4	108.1	36.0	105.7	
107.6	111.3	108.1	219.9	105.5	-2.3	105.8	37.0	103.4	
105.4	109.0	105.8	215.3	103.2	-2.3	103.6	38.0	100.7	
103.3	106.8	103.6	210.7	100.9	-2.1	101.5	39.0	98.2	
101.2	104.7	101.5	206.4	98.8	-2.1	99.4	40.0	96.0	
99.3	102.7	99.4	202.1	96.7	-1.9	97.4	41.0	93.9	
97.5	100.8	97.4	198.2	94.8	-1.8	95.7	42.0	92.2	
95.9	99.2	95.7	194.6	93.1	-1.1	94.5	43.0		
95.6	98.9	94.5	192.3	92.7	-0.2	94.4	44.0		
94.7	97.9	94.4	191.9	93.0	-1.2	93.2	45.0		
92.9	96.1	93.2	189.6	91.2		93.2	46.0		
	0.0	93.2	189.6	96.2		93.2	47.0		
						0.0	48.0		
						0.0	49.0		

dr = 11.4 MM.
r = 332.25 MM.

dr/r = 0.0343

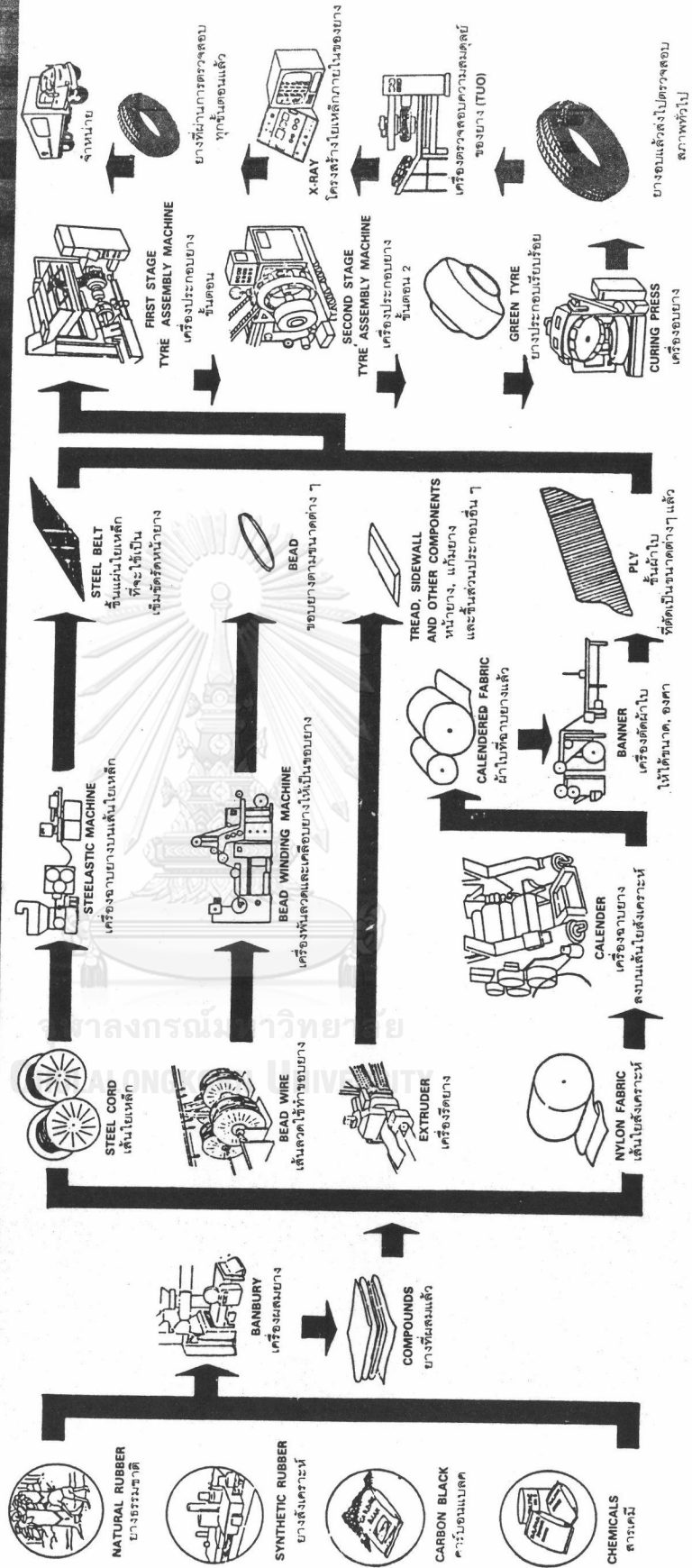
GRAPH SHOWN SIMULATION vs. EXPERIMENTAL
SPECIMEN : Tire No. # 1



Fo = 0.4175

บริษัท ยางสยาม จำกัด

STEELBELTED RADIAL TYRE PROCESS กรรมวิธีการผลิตยางเรเดียลเสริมใยเหล็ก

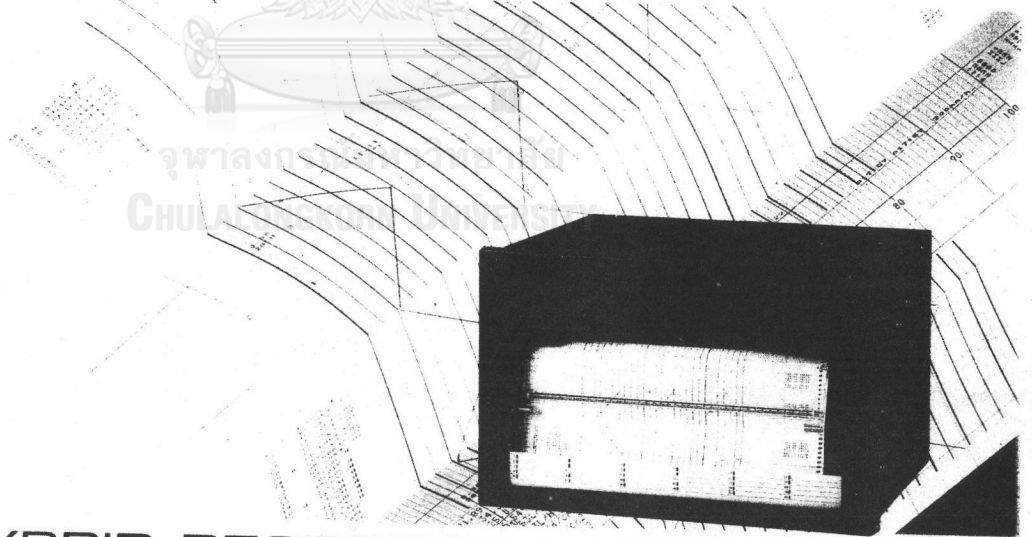


Appendix C. FIGURE SHOWS STEELBELTED RADIAL TYRE PROCESS

YOKOGAWA 

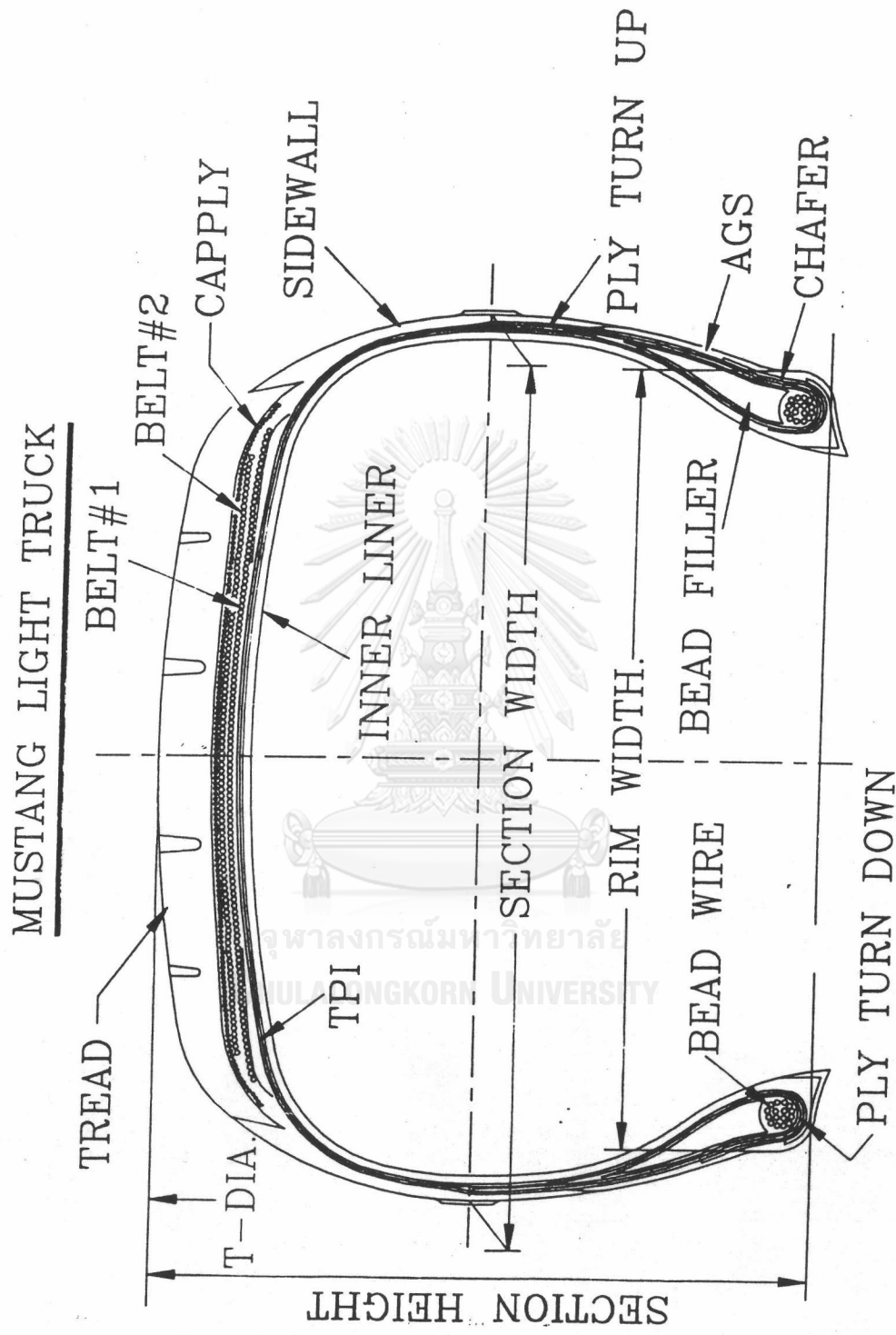
High-speed scanning of 30 points/s
High-speed recording of 60 points/2 s
Ten-color analog traces

HR



HYBRID RECORDER HR 2400

Appendix D. FIGURE SHOWS DATA RECORDER YOKOGAWA HR-2400



Appendix E. FIGURE SHOWS CROSS-SECTION TIRE OF LIGHT TRUCK RADIAL

VITA.

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