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## APPENDIX A

### REVIEW OF PARAMETER ESTIMATION METHODS FOR NONLINEAR MODEL

#### Introduction

Parameter estimation arises in fitting models containing several unknown parameters to experimental data through adjustment of these parameters. Model formulation is not a unique process; many different formulations may be used to fit the data and optimize model parameters. Of particular concern are formulations that are sufficiently accurate to represent physical or chemical phenomena.

Model formulation can be grouped into linear and nonlinear. The term "nonlinear" as applied to models means the model is nonlinear in the parameters (coefficients) to be estimated. The nonlinear estimation problem appears as simply an optimization problem in parameter space.



## Numerical Methods for Nonlinear Model

Suppose  $N$  data points  $(X_i, Y_i)$  are being fitted with a nonlinear model,

$$y = y(x; b) \quad (A-1)$$

where  $b$  is vector of parameters to be estimated.

The objective is to minimize the sum of squares function,  $f(b)$  to obtain the desired parameter estimates.

$$f(b) = \sum_{i=1}^n (Y_i - y_i(x_i, b))^2 \quad (A-2)$$

The nonlinear estimation problem appears as simply an optimization problem in parameter space. The optimization techniques fall into two broad classes: (1) derivative-free methods (direct method) and (2) derivative methods (indirect method). If in the search for a minimum of  $f(b)$ , the partial derivatives of  $f(b)$  must be calculated, then the method is derivative type; otherwise, the method will be termed a derivative-free method of estimation. There are five more effective optimization techniques, namely:

1. **Direct search method** Direct method do not require the use of derivatives in determining the search

direction. A direct search method simply selects a starting vector  $b^0$ , evaluates  $f(b^0)$ . Each  $b^0$  is changed by  $+\Delta b^0$  and, if  $f(b)$  is improved,  $b^0 + \Delta b^0$  is adopted as a new estimate of  $b^1$ . If  $f$  is not improved,  $b^0 - \Delta b^0$  is tested. If no improvement is experienced for either  $\pm \Delta b^0$ ,  $b^1 = b^0$ . This process is continued to complete an "exploratory move". The new estimated parameters define a vector in parameter space that represents a successful direction to reduce  $f(b)$ . A series of accelerating steps is made along this vector as long as  $f(b)$  is reduced. The magnitude of the pattern move in each coordinate direction is proportional to the number of prior successful moves in that direction. If  $f(b)$  is not improved by one of these pattern moves, a new exploratory move is made in order to define a new successful direction, the  $\Delta b$  are reduced gradually until either a new successful direction can be defined or each  $\Delta b$  becomes smaller than some predetermined tolerance. Failure to improve  $f(b)$  for a very small  $\Delta b$  indicates that a local optimum has been reached. Two basic tests have been employed to determine when the search should terminate. One test is made on the fractional change in the individual estimated parameters on the step sizes. Minimum desirable values of the fraction change in the variables are read into the computer program, and the test is conducted after each exploratory search failure. Another test occurs after each exploratory search or pattern move; the change in

the value of  $f(b)$  is compared to a specified fraction read into the computer program. If the value of  $f(b)$  has not decreased from the value on the previous move by an amount greater than the specified fraction, and exploratory search or pattern move is considered a failure. The calculations terminate when both tests are satisfied on a specified number of cycles. The disadvantage of direct search method is that they are slow in comparison with derivative of simplex methods, especially as the number of parameters becomes large.

2. **Simplex method** The second derivative-free method of minimization of a nonlinear objective function is by using of regular geometric patterns of search involving simplexes. In the search for a minimum of the sum of the squares of the deviations,  $f(b)$ , trial values of the model parameters can be selected at points in parameter space located at the vertices of the simplex. The sum of the squares of the deviations is evaluated at each of the vertices of the simplex: a projection is made from the point yielding the highest value of the objective function, point A in Figure A-1 through the centroid of the simplex. Point A is deleted and a new simplex, termed a reflection, is formed composed of the remaining old points and one new point, B, located along the projected line at the proper distance from the centroid. Continuation of this procedure, always deleting

the vertex that yields the highest value of the objective function, plus rules for reducing the size of the simplex and rules to prevent cycling in the vicinity of the extremum, permits a derivative-free search in which the step size is, in essence, fixed at successively reduced levels but the direction of search is permitted to change.

Nelder and Mead (1965) described a more efficient version of the simplex method called 'Downhill simplex method' that permitted the geometric figures to expand and contract continuously during the search. This method minimized a function of  $n$  variables using  $(n+1)$  vertices of a flexible polyhedron. The algorithm and step of calculation are summarized in Figure A-2.

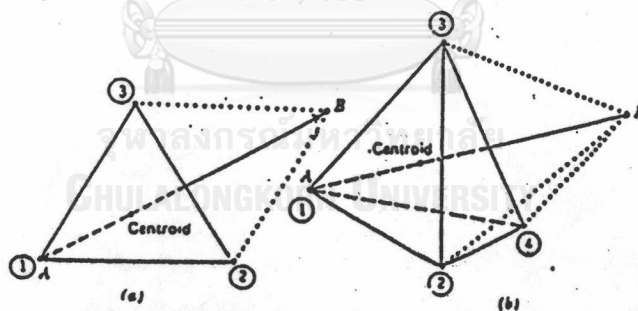


Figure A-1 Regular simplexes of two and three independent parameters.

(a) two variable simplex

(b) three variable simplex



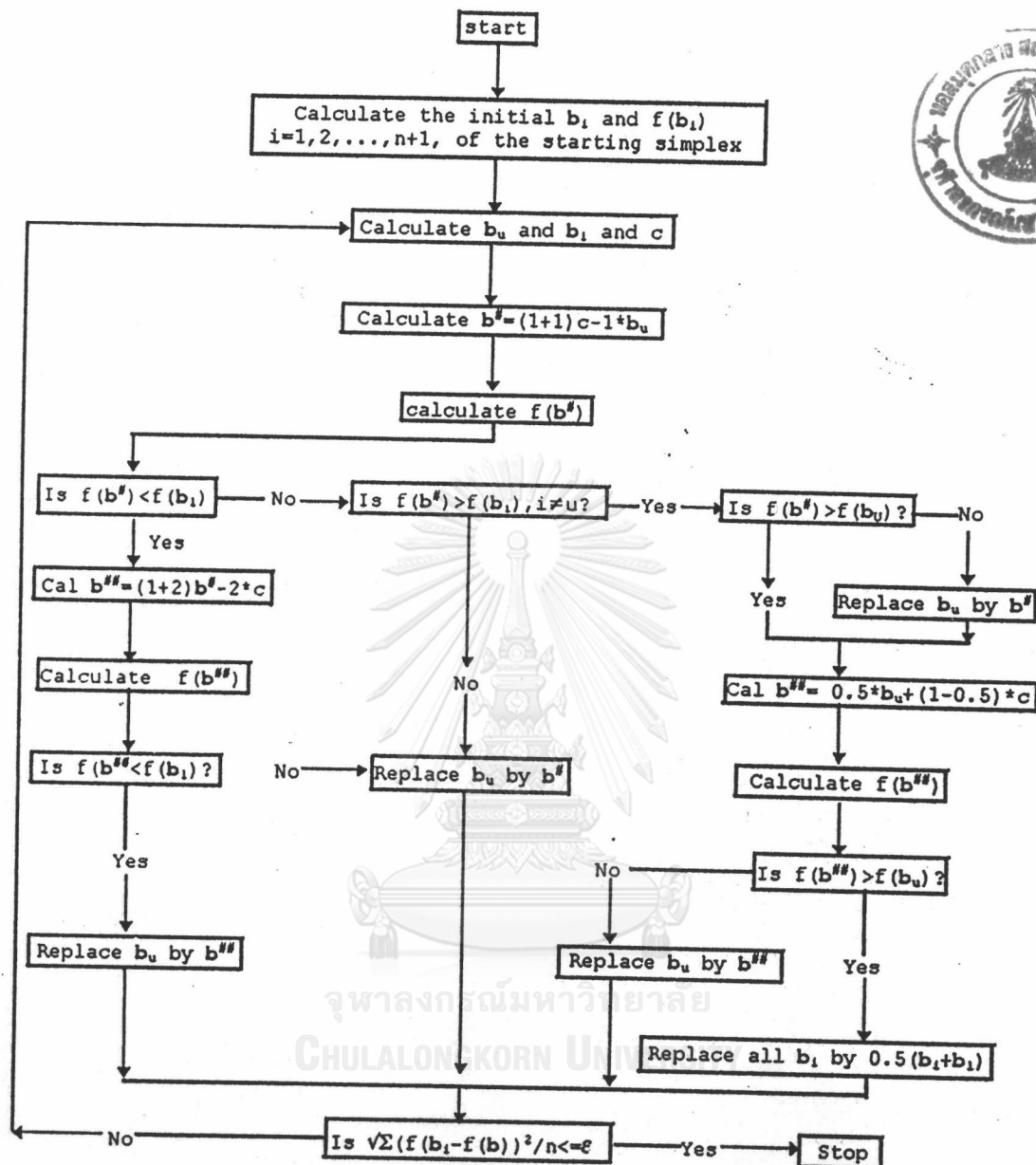


Figure A-2 Flow chart for downhill simplex method

This techniques have proved very successful in finding an extremum of and unconstrained objective function, as well as a constrained extremum, and are especially effective as the number of model parameters

increases and also very effective and easily implemented on a digital computer.

3. **Newton's methods.** Newton's method makes use of the second-order approximation of  $f(b)$  at  $b^k$ , and thus employs second-order information about  $f(b)$ , that is, information obtained from the second partial derivatives of  $f(b)$  with respect to the independent variables.

The minimum of  $f(b)$  in the direction of  $b^k$  is obtained by differentiating the approximation of  $f(b)$  with respect to each of the components of  $b$  and equating the resulting expressions to zero to give

$$\nabla f(b^k) = \nabla f(b^k) + \mathbf{H}(b^k) \Delta b^k = 0 \quad (\text{A-3})$$

or

$$b^{k+1} - b^k = \Delta b^k = -[\mathbf{H}(b^k)]^{-1} \nabla f(b^k) \quad (\text{A-4})$$

where  $[\mathbf{H}(b^k)]^{-1}$  is the inverse of the Hessian matrix  $\mathbf{H}(b^k)$ .

Note that both the direction and step length are specified as a result of Eq. (A-3). If  $f(b)$  is actually quadratic, only one step is required to reach the minimum of  $f(b)$ . However, for a general nonlinear objective function, the minimum of  $f(b)$  will not be reached in one step, so that Eq. (A-4) can be modified to

$$b^{k+1} - b^k = -\lambda^k [\mathbf{H}(b^k)]^{-1} \nabla f(b^k) \quad (\text{A-5})$$

where  $\lambda^k$  is the step length. The search direction  $\mathbf{s}$  is given (for minimization) by

$$\mathbf{s}^k = -[\mathbf{H}(b^k)]^{-1}\nabla f(b^k) \quad (\text{A-6})$$

For the initial estimates of the parameters far from the final estimates, it is a characteristically slow method but converges rapidly near termination (in contrast to the gradient method which converges very slowly).

**4. Gradient Method** This gradient (steepest-descent /ascent) method uses only the first derivatives of the  $f(b)$  in the calculations.

The gradient is the vector at a point  $b$  that gives the (local) direction of the greatest increase in  $f(b)$  and is orthogonal to the contour of  $f(b)$  at  $b$ . For maximization, the search direction is simply the gradient (when used the algorithm is called steepest ascent); for minimization, the search direction is the negative of the gradient (steepest descent).

$$\mathbf{s}^k = \nabla f(b^k) \quad (\text{A-7})$$

In steepest descent at the  $k$ th stage, the transition from point  $b^k$  to another point  $b^{k+1}$  can be viewed as given by the following expression:

$$b^{k+1} = b^k + \Delta b^k = b^k + \lambda^k \mathbf{s}^k = b^k - \lambda^k \nabla f(b^k) \quad (\text{A-8})$$

where  $\Delta b^k$  = vector from  $b^k$  to  $b^{k+1}$

$s^k$  = search direction, the direction of steepest descent

$\lambda^k$  = scalar that determines the step length in direction  $s^k$

The negative of the gradient gives the direction for minimization but not the magnitude of the step to be taken, so that various steepest descent procedures are possible, depending upon the choice of  $\lambda^k$ .

5. **Marquardt's method** Marquardt, Levenberg, and others have suggested that the Hessian matrix of  $f(b)$  be modified on each stage of the search as needed to ensure that the modified  $H(b)$ ,  $H(b)$ , is positive definite and well-conditioned. The procedure adds elements to the diagonal element of  $H(x)$

$$H(b) = [H(b) + \beta I] \quad (A-9)$$

where  $\beta$  is a positive constant large enough to make  $H(b)$  positive definite when  $H(b)$  is not. Also it is possible to use

$$[H(b)]^{-1} = [H^{-1}(b) + \gamma I] \quad (A-9)$$

Marquardt's method has been recommended as being quite effective. It is definitely superior to either the

Newton's method or the method of steepest descent. Because either analytical or numerical derivatives at the minimum of  $f(b)$  are available, it is superior to the simplex method in that subsequent estimates of the precision of the parameters are easy to make. On the other hand, the simplex method has the advantage that the partial derivatives of  $f(b)$  need not be calculated at all, thus saving considerable computer time in estimation. Moreover, it can more easily treat problems involving functions with discontinuities, points of inflection, and end points. For very complex models, the simplex method has proved the more effective in estimating the parameters in simulation studies.

The model in this study is too complex to use Marquard's method, because the model in this study are composed of 7 simultaneous differential equations, 6 simultaneous algebraic equations and a nonlinear-algebraic equation to find the root of equation at every step of the calculation. Thus the optimization method to be used in this study is the downhill simplex method (William et.al (1992)).

### Step of Parameter Estimation

The models in this study consisting of 7 simultaneous differential equations, 6 simultaneous algebraic equations and a nonlinear-algebraic equation as can be shown in the general form:

$$d[A_1]/dt = f(m, k, A_1^-, t) \quad (A-10)$$

$$A_1^- = f(A_1, K_1, A_1^-) \quad (A-11)$$

$$f(m) = 0 \quad (A-12)$$

where  $d[A_1]/dt$  = vector of derivatives of  $A_1$

$f$  = vector of functions

$t$  = independent variable

$A_1$  = vector of dependent variables

$k$  = vector of parameters

$K_1$  = vector of known constants

let  $A_1^*$  = vector of experimental observations of the dependent variable

$A_1$  = vector of calculated values of the dependent variables obtained from integrating Eq. (A-10)

- (1) Assume initial guesses for the parameter  $k$
- (2) Use the vector  $k$  and the initial condition to integrate the differential equations by 4th order Rung-Kutta and solve algebraic equations by Newton-Rapson (Constantinides, (1988)) to obtain the profiles of  $A_1$ .

(3) Let  $err_i$  is error between observation with calculated value.

$$err_i^2 = (A_i - A_i^*)^2 \quad (A-13)$$

(4) Let  $E$  is total error

$$E_1^2 = \sum err_i^2 \quad (A-14)$$

(5) The procedure from step (1) to (4) are called objective function to calculate the sum of square error. The main procedure to optimize the  $E$  value (objective function,  $f(k)$ ) is downhill simplex method as the algorithm described in the preceding section. All problems are solved by writing program in MATLAB program.



APPENDIX B

**Table B-1** Initial condition input used in the simulation

Case	Phenol (mole/l)	Formaldehyde (mole/l)	NaOH (mole/l)	Temperature (°C)
1	1.003	2.119	0.03138	30
2	4.71	9.189	0.09369	30
3	0.9583	2.030	0.01250	57
4	4.68	9.456	0.09615	57
5	5.375	5.375	0.1000	40
6	5.375	5.375	0.1000	50
7	5.375	5.375	0.0500	60
8	5.375	5.375	0.0500	70
9	0.600	0.100	0.0045	90
10	0.200	0.0500	0.0500	30
11	0.400	0.09602	0.200	31
12	4.770	8.4700	0.2860	30
13	4.694	7.2700	0.04388	57
14	4.680	9.4600	0.0953	57
15	4.800	8.5300	0.0462	57
16	4.950	7.0100	0.0489	57
17	2.000	0.2000	0.1300	30
18	2.000	0.2000	0.6000	30
19	1.804	5.9400	1.8040	30
20	4.420	9.3000	0.0937	45



**Table B-2** References of Each Case

Case	Reference
1,12,13,20	Zavitsas et.al (1968)
2,4	Zavitsas (1966)
3,14,15,16	Zavitsas et.al (1967)
5,6,7,8	Debing et.al (1952)
9	DeJong et.al (1956)
10	Dijkstra et.al (1962)
11	Dijkstra et.al (1957)
17,18	Peer et.al (1959)
19	Freeman et.al (1954)



## APPENDIX C

### EQUILIBRIUM CONSTANT

#### Appendix C-1 Equilibrium constant of phenolic species

The equilibrium constant of all phenolic species at each temperature can be calculated from the relationship between temperature and equilibrium constant which were determined by Sprengling et.al(1965) and Zavitsas et.al(1966) individually. The results were in good agreement that  $pK_1$  of each species were linear with temperature as the following equations:

$$pK_1 = -0.0108 \cdot \text{temp} + 10.125 \quad (\text{c-1})$$

$$pK_2 = -0.0117 \cdot \text{temp} + 10.1275 \quad (\text{c-2})$$

$$pK_3 = -0.0105 \cdot \text{temp} + 9.9925 \quad (\text{c-3})$$

$$pK_4 = -0.0107 \cdot \text{temp} + 9.8375 \quad (\text{c-4})$$

$$pK_5 = -0.0108 \cdot \text{temp} + 9.95 \quad (\text{c-5})$$

$$pK_6 = -0.0105 \cdot \text{temp} + 9.7125 \quad (\text{c-6})$$

**Appendix C-2** The equilibrium constant of formaldehyde equilibrium

The constant value of  $Q_1 = 45$  and  $Q_2 = 400$  are used to calculate the methylene glycol fraction at all studied temperature as the average value found by Zavitsas et.al (1968). Because from the studies of Iliceto et.al (1951) and Zavitsas (1968) found that the fraction of formaldehyde in methylene glycol form were not affect by temperature from 20-100 °C and pH of the solution as shown in Figure C-1

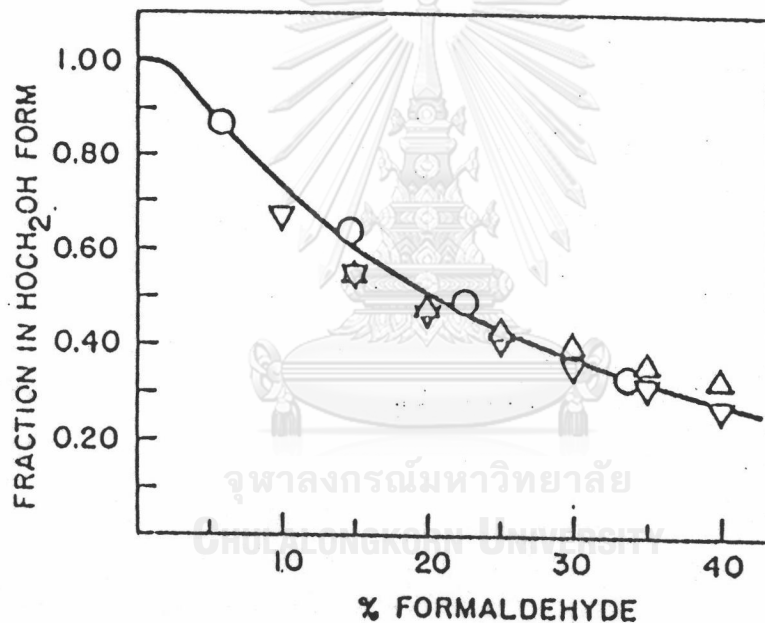


Figure C-1 Fraction of formaldehyde vs. wt.% formaldehyde in water: (-) curve calculated according to equation of formaldehyde equilibrium ;  
 (o) experiment at 20 °C (Iliceto et.al(1951))  
 (Δ) experimental at 35 °C.(Zavitsas (1967))  
 (∇) experimental at 100 °C. (Zavitsas (1967))

**Table C-1** Rate Constants Obtained from Zavitsas' Model  
(Zavitsas et.al (1968))

Temp., (°C)	30	57	30	57	30
[P] <sub>0</sub> , (M.)	1.003	0.9583	4.71	4.68	1.804
[F] <sub>0</sub> , (M.)	2.119	2.030	9.189	9.456	5.94
[NaOH] <sub>0</sub> , (M.)	0.03138	0.0125	0.09369	0.09615	1.804
k <sub>1</sub> , (l/mole.min) × 10 <sup>3</sup>	2.322	30.6	5.01	87.78	3
k <sub>2</sub> , (l/mole.min) × 10 <sup>3</sup>	1.65	20.34	2.847	46.68	1.98
k <sub>3</sub> , (l/mole.min) × 10 <sup>3</sup>	2.892	29.7	5.088	81.06	3.3
k <sub>4</sub> , (l/mole.min) × 10 <sup>3</sup>	2.094	21.6	4.656	61.32	3.18
k <sub>5</sub> , (l/mole.min) × 10 <sup>3</sup>	2.49	33.48	4.608	80.7	3
k <sub>6</sub> , (l/mole.min) × 10 <sup>3</sup>	6.174	64.68	9.318	128.04	7.5
k <sub>7</sub> , (l/mole.min) × 10 <sup>3</sup>	1.476	15.96	3.714	50.58	2.7

**Table C-2** Activation Parameters for the NaOH-Catalyzed  
Hydroxymethylation from Zavitsas' Model

Rate Constant	Dilute Systems		Concentrate Systems	
	E <sub>a</sub> , (kcal)	ln A	E <sub>a</sub> , (kcal)	ln A
k <sub>1</sub>	19	25.45	21.1	29.7
k <sub>2</sub>	18.	2429	20.6	28.25
k <sub>3</sub>	17.	22.62	20.4	28.55
k <sub>4</sub>	17.	22.35	19.0	26.14
k <sub>5</sub>	19.	25.77	21.0	29.61
k <sub>6</sub>	17.	23.62	19.3	27.35
k <sub>7</sub>	17.	22.58	19.2	26.32



APPENDIX D

COMPUTER PROGRAM WRITTEN BY USING MATLAB

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```

function [s]=downhill(p)
% The routine for finding the parameters which make the
% minimum of the objective function by downhill simplex
% method. The objective function named "object(p)"
% where p is the matrix of initial guess parameters.

mp=8;np=7; % mp are numbers of vectors which are the
           % vertics of the starting simplex.
           % np are numbers of parameter in a vector
           % of vertic.

p=zeros(mp,np);
y=zeros(mp,1);
nmax=20;alpha=1;beta=0.5;gamma=2;itmax=500;ftol=0.01;
pbar=zeros(1,np);
pr=zeros(1,np);
prr=zeros(1,np);
mpts=mp;
iter=0;
for i=1:mp
    q=p(i,:);
    [a]=object(q);
    y(i)=a; % y is the vector of objective value
end
y
ilo=1;
if y(1)>y(2),
    ihi=1;
    inhi=2;
else
    ihi=2;
    inhi=1;
end
for j=1:mp
    if y(j)<y(ilo),ilo=j;end
    if y(j)>y(ihi),inhi=ihi;ihi=j;
        elseif y(j)>y(inhi)
            if j~=ihi,inhi=j;end
    end
end
end

%Compute the fractional range from highest to lowest
%and return if satisfactory.

%rtol=2.*abs(y(ihi)-y(ilo))/(abs(y(ihi))+abs(y(ilo)));
rtol=abs(y(ihi)-y(ilo));

while (rtol>ftol) ; (iter==itmax)
    iter=iter+1
    pbar=(sum(p)-p(ihi,:))/np;
    pr=(1+alpha)*pbar-alpha*p(ihi,:);
    [ypr]=object(pr);
    if ypr<=y(ilo)
        prr=gamma*pr+(1-gamma)*pbar;

```

```

[ypr] = object(pr);
if ypr < y(ilo)
    p(ihi,:) = pr;
    y(ihi) = ypr;
else
    p(ihi,:) = pr;
    y(ihi) = ypr;
end
elseif ypr >= y(inhi)
    if ypr < y(ihi)
        p(ihi,:) = pr;
        y(ihi) = ypr;
    end
    pr = beta * p(ihi,:) + (1 - beta) * pbar;
    [ypr] = object(pr);
    if ypr < y(ihi)
        p(ihi,:) = pr;
        y(ihi) = ypr;
    else
        for i = 1:mp
            if i ~= ilo
                pr = 0.5 * (p(i,:) + p(ilo,:));
                p(i,:) = pr;
                [c] = object(pr);
                y(i) = c;
            end
        end
    end
else
    p(ihi,:) = pr;
    y(ihi) = ypr;
end

ilo = 1;
if y(1) > y(2),
    ihi = 1;
    inhi = 2;
else
    ihi = 2;
    inhi = 1;
end
for j = 1:mp
    if y(j) < y(ilo), ilo = j; end
    if y(j) > y(ihi), inhi = ihi; ihi = j;
    elseif y(j) > y(inhi)
        if j ~= ihi, inhi = j; end
    end
end

%rtol = 2 * abs(y(ihi) - y(ilo)) / (abs(y(ihi)) + abs(y(ilo)))
rtol = abs(y(ihi) - y(ilo))
end
s = p(ilo,:);

```



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```

function [sumerr]=object302(p)

% funtion to calculate the objective function
% by using Rung-Kutta algorithm to solve differential
% equation and Newton-Rapstson to find the root of
% m fraction in the model
% This is the example of calculating objective function
% of Simple model with Zavitsas data at 30 C at
% concentrate run

[tepx,yexp]=dat302;
steps=1;y0=[4.71 0 0 0 0 0 9.189]';
least=0;unit=ones(size(y0'));
i=length(tepx);
y=y0;
t0=0;
count=0;tm=max(tepx);

for t=t0:steps:tm
    yold=y; count=count+1;
    t1=t;
    temp=feval('modell',t1,yold,p);
    b1=temp;
    y=yold+0.5*steps*temp;
    t2=t1+0.5*steps;
    temp=feval('modell',t2,y,p);
    b2=temp;
    y=yold+0.5*steps*temp;
    temp=feval('modell',t2,y,p);
    b3=temp;
    y=yold+steps*temp;
    t3=t1+steps;
    temp=feval('modell',t3,y,p);
    y=yold+steps*(b1+temp+2*(b2+b3))/6;
    for j=1:i
        %disp('t');disp(t);disp(tepx(j));
        if t3==tepx(j)
            %disp(t3);disp(tepx(j));
            %a=(yexp(j,:)./y');
            %b=(unit-a).^2;
            b=(yexp(j,:)-y').^2;
            err=sum(b);
            least=least+err;
        end
    end
    %if count==100
    %fprintf('%8.2f%8.2f%8.2f\n',t3,y(1),y(2));
    %count=0;
    %end
end
sumerr=least;

```



```

function [tout,yout]=simnew(phe,f,oh,temp,time)
% Function for simulating the simple model which
% concern water concentration.
% phe is initial phenol concentration
% f is initial fomaldehyde concentration
% oh is initial base concentration
% temp is reaction temperature
% time is a vector of reaction time

steps=1;y0=[phe 0 0 0 0 0 f]';
least=0;unit=ones(size(y0'));
i=length(time);ho=h2o(phe,f,oh);
tout=zeros(i+1,1);
yout=zeros(i+1,length(y0));
y=y0;yout(1,:)=y0';
t0=0.00;tout(1)=t0;
count=0;tm=max(time);

% Calculate rate constant p which relate to
% water concentration as  $p=A*\exp(b/[H2O])$ 
c1=46.9;c2=15;
k1=energyd(temp);
k2=energyc(temp);

ln=k1./k2;lnk=log(ln);
eel=1/c1;ee2=1/c2;
ee=eel-ee2;
slop=lnk/ee;
k01=k1./(exp(slop/c1));
lnk01=log(k1./(exp(slop/c1)));
p=exp(lnk01+slop/ho)

for t=t0:steps:tm
    yold=y; count=count+1;
    t1=t;
    temp=feval('modell',t1,yold,p);
    b1=temp;
    y=yold+0.5*steps*temp;
    t2=t1+0.5*steps;
    temp=feval('modell',t2,y,p);
    b2=temp;
    y=yold+0.5*steps*temp;
    temp=feval('modell',t2,y,p);
    b3=temp;
    y=yold+steps*temp;
    t3=t1+steps;
    temp=feval('modell',t3,y,p);
    y=yold+steps*(b1+temp+2*(b2+b3))/6;
    for j=1:i
        if t3==time(j)
            tout(j+1)=time(j);
            yout(j+1,:)=y';
        end
    end
end
end
end

```

```

function [tout,yout]=zavnew(phe,f,NaOH,Temp,time)
% Function for simulating Zavitsas model which
% concern water concentration.
% phe is initial phenol concentration
% f is initial fomaldehyde concentration
% oh is initial base concentration
% temp is reaction temperature
% time is a vector of reaction time

steps=1;y0=[phe 0 0 0 0 0 f]';
yion=[NaOH 0 0 0 0 0 f]';oh=NaOH;
ho=h2o(phe,f,NaOH);
mf=raptson(f,f,ho,1);

% Calculate equilibrium constant
aa=[-.0108 -.0117 -.0105 -.0107 -.0108 -.0105];
cc=[10.125 10.1275 9.9925 9.8375 9.95 9.7125];
dd=-1*(Temp*aa+cc);k=10.^dd;
a=zeros(1,6);
tm=max(time);
i=length(time);
tout=zeros(i+1,1);
yout=zeros(i+1,length(y0));
y=y0;yout(1,:)=y0';
t0=0.00;tout(1)=t0;
count=0;d=1;option=2;

% Calculate rate constant p which relate to
% water concentration as  $p=A*\exp(B/[H2O])$ 
c1=47;c2=21;
k1=parazd(Temp);
k2=parazc(Temp);
ln=k1./k2;lnk=log(ln);
eel=1/c1;ee2=1/c2;
ee=eel-ee2;
slop=lnk/ee;
k01=k1./(exp(slop/c1));
lnk01=log(k1./(exp(slop/c1)));
p=exp(lnk01+slop/ho)

%slope=(k2-k1)/(c2-c1);inter=k2-slope*c2;
%p=slope.*ho+inter
%ratio=p(1)/(p(1)+p(2))
for t=t0:steps:tm
yold=y; count=count+1;
t1=t;
temp=feval('model3',t1,yion,p,mf);
b1=temp;
y=yion+0.5*steps*temp;
t2=t1+0.5*steps;
temp=feval('model3',t2,y,p,mf);
b2=temp;
y=yion+0.5*steps*temp;
temp=feval('model3',t2,y,p,mf);
b3=temp;

```



```

y=yion+steps*temp;
t3=t1+steps;
temp=feval('model3',t3,y,p,mf);
y=yold+steps*(b1+temp+2*(b2+b3))/6;

    if option==1
        for n=1:6
            a(n)=[k(n)*y(n)]/[k(1)*y(1)];
        end
        yion(1)=oh/sum(a);
        for m=1:6
            yion(m)=[k(m)*y(m)*yion(1)]/[k(1)*y(1)];
        end
    end
    if option==2
        n=y(1:6);
        yi=rapt(1,n,oh,k);
        for l=1:6
            yion(l)=(k(l)/k(1))*y(l)*yi/[(y(l)-yi)+yi*(
k(1)/k(1))];
        end
    end
    yion(7)=y(7);
    mf=raptson(y0(7),y(7),ho,1);

    for j=1:i
        if t3==time(j)
            tout(j+1)=time(j);
            yout(j+1,:)=y';
        end
    end
end
end

```

```

function [tout,yout]=zav(phe,f,NaOH,Temp,time)
% Function for simulating Zavitsas model which
% concern water concentration.
% phe is initial phenol concentration
% f is initial fomaldehyde concentration
% oh is initial base concentration
% temp is reaction temperature
% time is a vector of reaction time

steps=1;y0=[phe 0 0 0 0 0 f]';
yion=[NaOH 0 0 0 0 0 f]';oh=NaOH;
ho=h2o(phe,f,NaOH);
mf=raptson(f,f,ho,1);

% Calculate equilibrium constant
aa=[-.0108 -.0117 -.0105 -.0107 -.0108 -.0105];
cc=[10.125 10.1275 9.9925 9.8375 9.95 9.7125];
dd=-1*(Temp*aa+cc);k=10.^dd;
a=zeros(1,6);
tm=max(time);
i=length(time);
tout=zeros(i+1,1);
yout=zeros(i+1,length(y0));
y=y0;yout(1,:)=y0';
t0=0.00;tout(1)=t0;
count=0;d=1;option=2;

% Calculate rate constant p which relate to
% water concentration as  $p=A+B*[H2O]$ 
c1=47;c2=21;
k1=parazd(Temp);
k2=parazc(Temp);
slope=(k2-k1)/(c2-c1);inter=k2-slope*c2;
p=slope.*ho+inter
%ratio=p(1)/(p(1)+p(2))
for t=t0:steps:tm
    yold=y; count=count+1;
    t1=t;
    temp=feval('model3',t1,yion,p,mf);
    b1=temp;
    y=yion+0.5*steps*temp;
    t2=t1+0.5*steps;
    temp=feval('model3',t2,y,p,mf);
    b2=temp;
    y=yion+0.5*steps*temp;
    temp=feval('model3',t2,y,p,mf);
    b3=temp;
    y=yion+steps*temp;
    t3=t1+steps;
    temp=feval('model3',t3,y,p,mf);
    y=yold+steps*(b1+temp+2*(b2+b3))/6;

    if option==1
        for n=1:6
            a(n)=[k(n)*y(n)]/[k(1)*y(1)];

```

```

end
yion(1)=oh/sum(a);
for m=1:6
    yion(m)=[k(m)*y(m)*yion(1)]/[k(1)*y(1)];
end
end
if option==2
    n=y(1:6);
    yi=rapt(1,n,oh,k);
    for l=1:6
        yion(l)=(k(l)/k(1))*y(l)*yi/[(y(l)-yi)+y
i*(k(1)/k(l))];
    end
end
yion(7)=y(7);
mf=raptson(y0(7),y(7),ho,1);

for j=1:i
    if t3==time(j)
        tout(j+1)=time(j);
        yout(j+1,:)=y';
    end
end
end
end

```



```

function [tout,yout]=gennew(phe,f,NaOH,Temp,time,option)
% Main program for simulating all datas by inputting the
% initial condition: phe is the input concentration of
% phenol in mole/l; f is the input concentration of
% formaldehyde in mole/l; NaOH is the input concentration
% of base in mole/l; Temp is reaction temperature;
% time is the vector of time in minute;
steps=1;y0=[phe 0 0 0 0 0 f]';
yion=[NaOH 0 0 0 0 0 f]';oh=NaOH;
ho=h2o(phe,f,NaOH);
% h2o is the function for calculating water concentration
mf=raptson(f,f,ho,1);
% raptson is the function for calculating fraction of
% formaldehyde in methylene glycol form.

% calculate equilibrium constant
aa=[-.0108 -.0117 -.0105 -.0107 -.0108 -.0105];
cc=[10.125 10.1275 9.9925 9.8375 9.95 9.7125];
dd=-1*(Temp*aa+cc);k=10.^dd;

a=zeros(1,6);
tm=max(time);
i=length(time);
tout=zeros(i+1,1);
yout=zeros(i+1,length(y0));
y=y0;yout(1,:)=y0';
t0=0.00;tout(1)=t0;
count=0;d=1;

% calculate rate constant which relate to water
% concentration as  $p=A*\exp(B/[H2O])$ 
c1=47;c2=15;
k1=energyzd(Temp); %calculate k at dilute concentration
k2=energyzc(Temp); %calculate k at high concentration
ln=k1./k2;lnk=log(ln);
eel=1/c1;ee2=1/c2;
ee=eel-ee2;
slop=lnk/ee;
k01=k1./(exp(slop/c1));
lnk01=log(k1./(exp(slop/c1)));
p=exp(lnk01+slop/ho)

% routine for calculating the profile of output
% concentration
for t=t0:steps:tm
    yold=y; count=count+1;
    t1=t;
    temp=feval('model3',t1,yion,p,mf);
    b1=temp;
    y=yion+0.5*steps*temp;
    t2=t1+0.5*steps;
    temp=feval('model3',t2,y,p,mf);
    b2=temp;
    y=yion+0.5*steps*temp;
    temp=feval('model3',t2,y,p,mf);

```

```

b3=temp;
y=yion+steps*temp;
t3=t1+steps;
temp=feval('model3',t3,y,p,mf);
y=yold+steps*(b1+temp+2*(b2+b3))/6;

    if option==1
        for n=1:6
            a(n)=[k(n)*y(n)]/[k(1)*y(1)];
        end
        yion(1)=oh/sum(a);
        for m=1:6
            yion(m)=[k(m)*y(m)*yion(1)]/[k(1)*y(1)];
        end
    end
    if option==2
        n=y(1:6);
        yi=rapt(1,n,oh,k);
        for l=1:6
            yion(l)=(k(l)/k(1))*y(l)*yi/[(y(l)-yi)+yi*(
k(1)/k(l))];
        end
    end
    yion(7)=y(7);
    mf=raptson(y0(7),y(7),ho,1);

    for j=1:i
        if t3==time(j)
            tout(j+1)=time(j);
            yout(j+1,:)=y';
        end
    end
end
end

```



APPENDIX E

จุฬาลงกรณ์มหาวิทยาลัย  
CHULALONGKORN UNIVERSITY



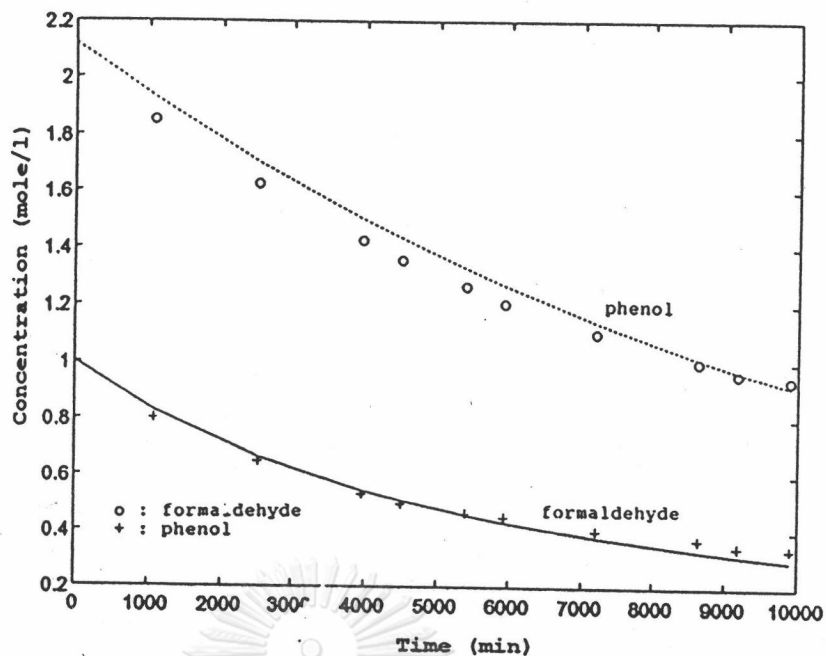


Figure E-1 Reactant concentration vs. time at 30°C,  $[P]_0 = 1.003$  M,  $[F]_0 = 2.119$  M,  $[\text{NaOH}]_0 = 0.03138$  M.: Curve calculated with rate constants from Table 5-1 by Simple model. Point: experimental data (Zavitsas (1966)).

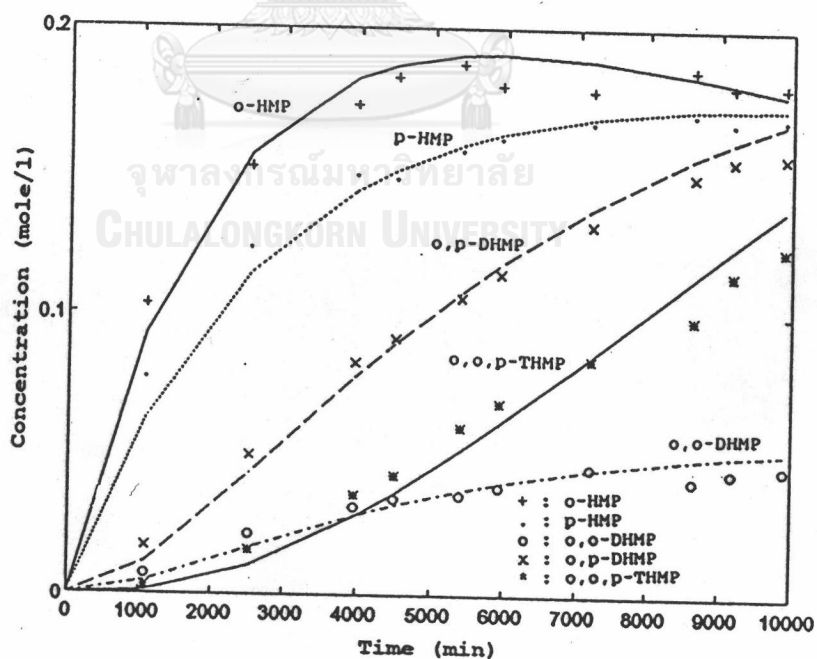


Figure E-2 Product concentration vs. time at 30°C,  $[P]_0 = 1.003$  M,  $[F]_0 = 2.119$  M,  $[\text{NaOH}]_0 = 0.03138$  M.: Curve calculated with rate constants from Table 5-1 by Simple model. Point: experimental data (Zavitsas (1966)).

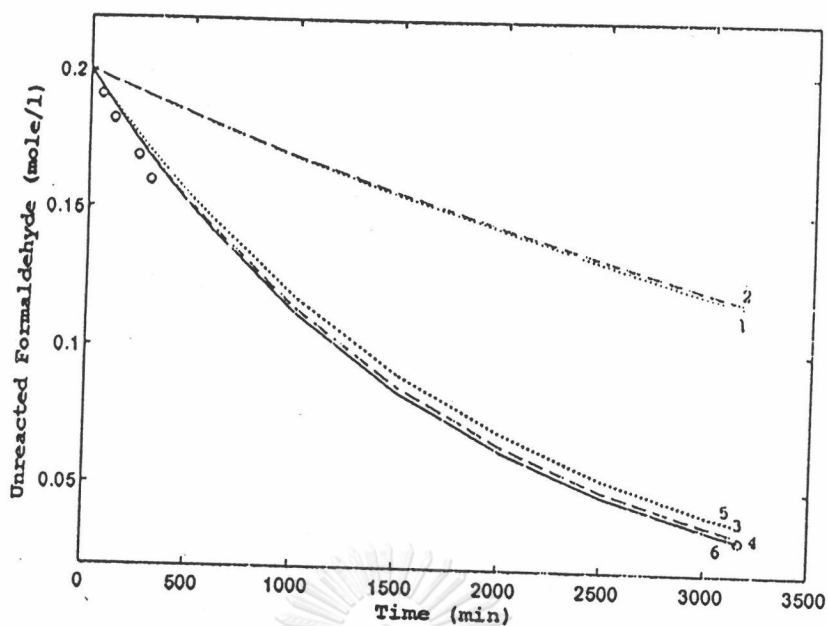


Figure E-3 Formaldehyde concentration vs. time at 30°C,  
 $[P]_0 = 2 \text{ M.}$   $[F]_0 = 0.2 \text{ M.}$   $[\text{NaOH}] = 0.13 \text{ M.}$   
 Curve calculated compare between 6 models  
 described in Page 58 . Point: experimental data  
 (Peer et.al (1959)).

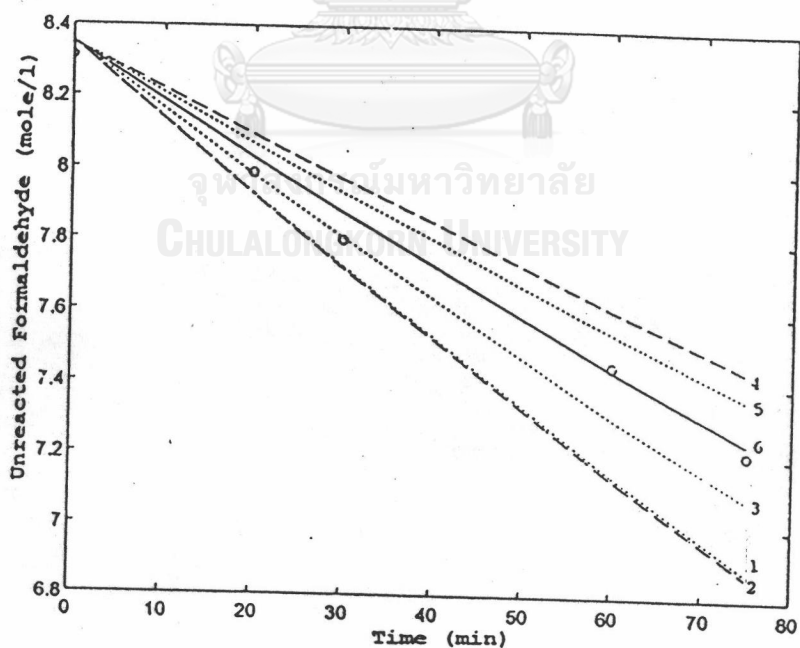


Figure E-4 Formaldehyde concentration vs. time at 57°C,  
 $[P]_0 = 4.8 \text{ M.}$   $[F]_0 = 8.53 \text{ M.}$   $[\text{NaOH}] = 0.0462 \text{ M.}$   
 Curve calculated compare between 6 models  
 described in Page 58 . Point: experimental data  
 (Zavitsas et.al (1967)).

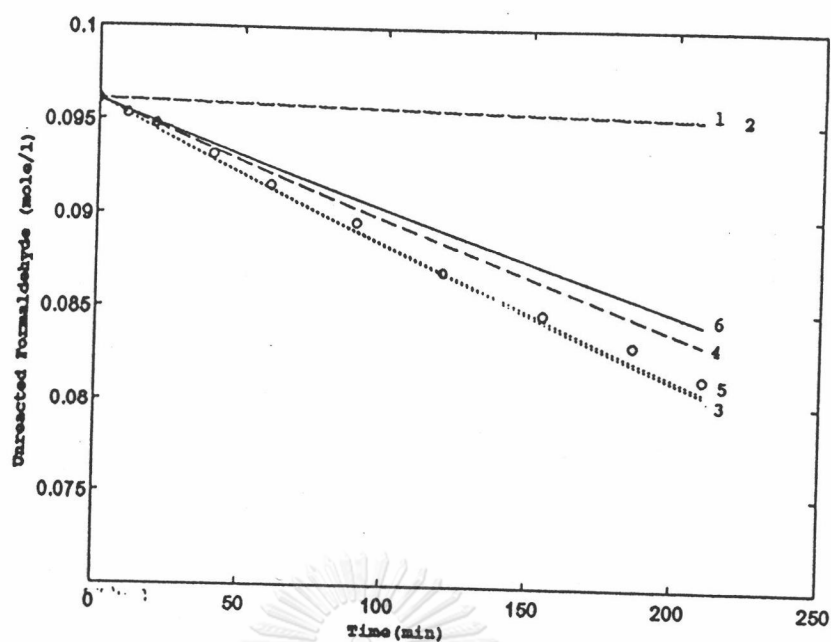


Figure E-5 Formaldehyde concentration vs. time at 31°C,  $[P]_0 = 0.4$  M.  $[F]_0 = 0.09602$  M.  $[NaOH] = 0.2$  M.: Curve calculated compare between 6 models described in Page 58. Point: experimental data (Dijkstra et.al (1959)).

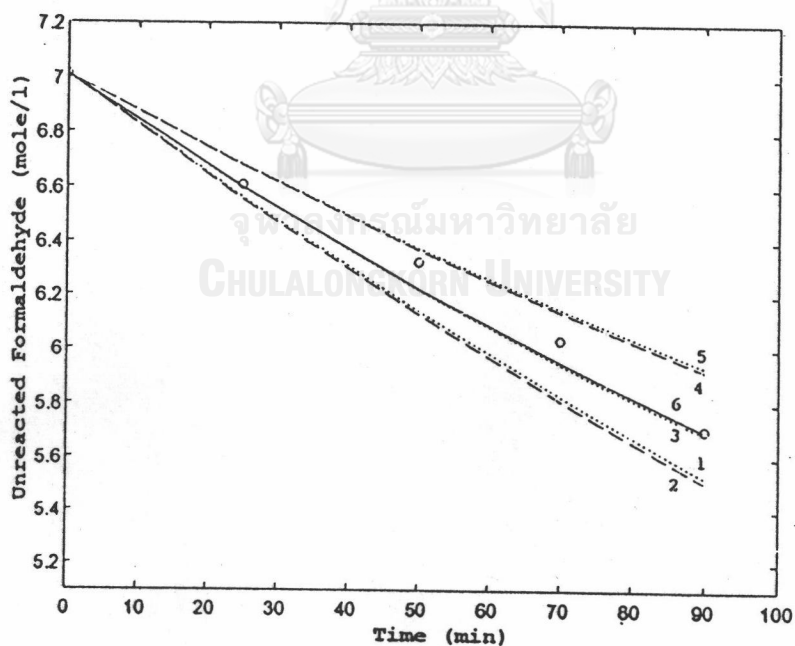


Figure E-6 Formaldehyde concentration vs. time at 57°C,  $[P]_0 = 4.95$  M.  $[F]_0 = 7.01$  M.  $[NaOH] = 0.0489$  M.: Curve calculated compare between 6 models described in Page 58. Point: experimental data (Zavitsas et.al (1967)).

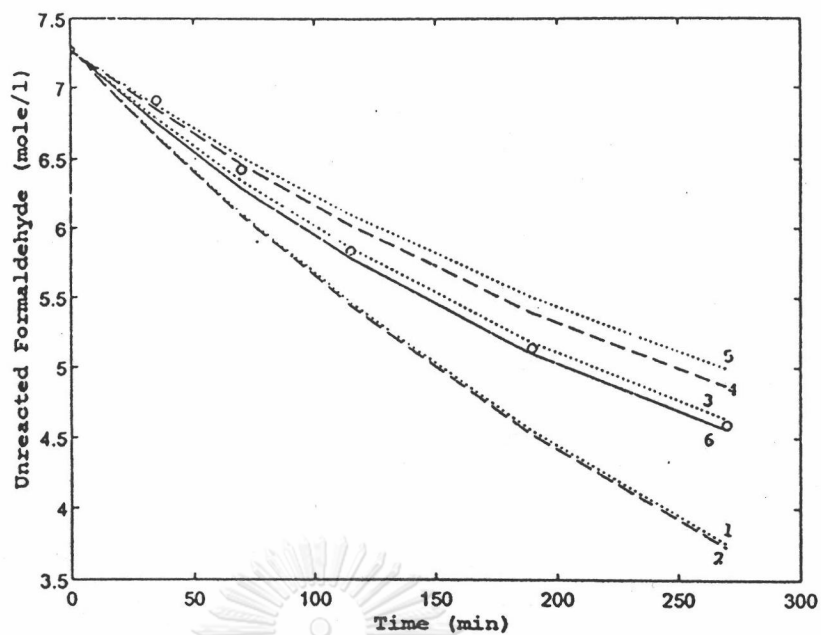


Figure E-7 Formaldehyde concentration vs. time at 57°C,  $[P]_0 = 4.694$  M.  $[F]_0 = 7.27$  M.  $[\text{NaOH}] = 0.04388$  M.: Curve calculated compare between 6 models described in Page 58 . Point: experimental data (Zavitsas et.al (1968)).

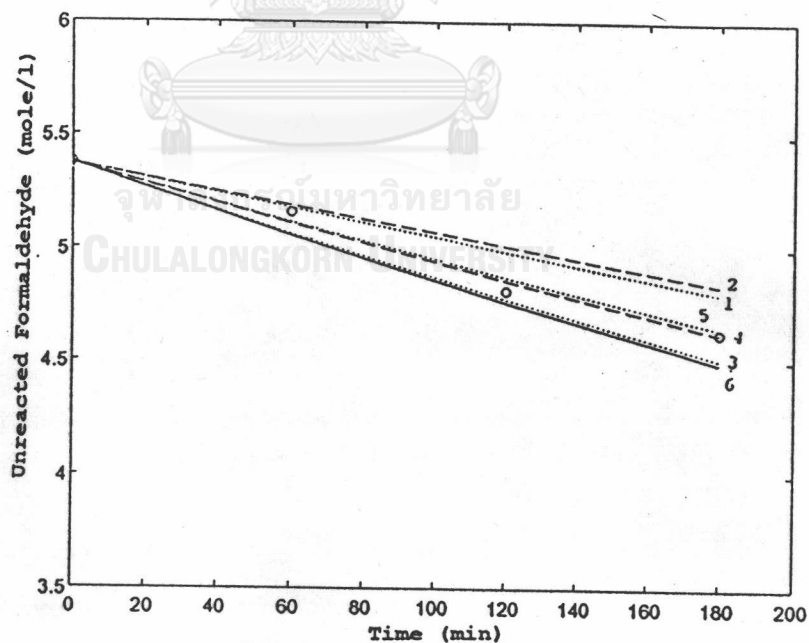


Figure E-8 Formaldehyde concentration vs. time at 40°C,  $[P]_0 = 5.375$  M.  $[F]_0 = 5.375$  M.  $[\text{NaOH}] = 0.1$  M.: Curve calculated compare between 6 models described in Page 58 . Point: experimental data (Dejong et.al (1952)).



## VITA

Miss Surat Atthajariyakul was born on December 6, 1968 in Bangkok, Thailand. She finished her primary school from Singfha and secondary school from Sainampheung. She graduated her B.Sc (Agro-Industrial Product Development) with first class honours from the Faculty of Agro-Industry, Kasetsart University, Bangkok. She then pursues her post-graduate study at the Department of Chemical Engineering, Faculty of Engineering, Chulalongkorn University.



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