# Chapter 4 

## Geostatistical Analysis

### 4.1 Background

A relatively new theory was developed by Professor G. Matheron in France during the 1950's, which has overcome most of the problems which the statistical and conventional methods are incapable of solving. This method under the title of "The Theory of Regionalized Variables" applies variables which are spatially correlated with each other in a geological of other manner. Practically, the theory, however, is not restricted to only geological variables.

The method accounts for the relationship between the samples which have arisen from common geological process and captures this spatial correlation in a mathematical expression called the "variogram function" (Fig.4.1) This allows an estimation variance or mean squared error to be calculated for any estimate (David, 1977, Gershon, 1986; Whitchurch et al., 1987).

The semivariogram is therefore defined as half the mean squared difference of pairs of values at some distance, $h$, apart.

Semivariogram (or expressed as $\gamma(h)=\left\{\sum\left(x_{i}\right)-\left(x_{i}-h\right)\right\} / 2 n$ )

When $\gamma(h)$ is called the semi-variogram (although some authors sloppily call it the variogram), h is stand for grade, x denoteds the position of one sample in the pair, $\mathrm{x}+\mathrm{h}$ is the position of the other, and $n$ is the number of pairs.

To illustrate the method of calculation, consider a set of samples taken at regular intervals of 1 metre along a straight line must be considered (Fig. 4.2). To generate semivariogram, it would be required to calculate the half mean squared differences of all the samples 1 metre apart (i.e. $\mathrm{N}-1$ pair). Then the process for samples which are 2 metre apart ( $\mathrm{N}-2$ pairs) is repeated.

The aim of geostatistical method of interpolation of variable values (such as an ore grade) is called "kriging" after the South African mining engineer, Krige, D.G., who pioneered the theory in South African underground gold mines (Davis, 1976 ; Dagbert \& David, 1986).

The estimator (also known as the "Best Linear Unbias Estimator" or BULE, in which the values of the samples are multiplied by weighting factors which are determined from a set of linear equation.

### 4.2 Definition of Some Important Geostatistical Terms

In the following context, several geostatistical terms are applied. To be familiar with these technical terms, some of them can be defined herein mostly following Clark (1979), journel (1974), and Evans (1951) (see also in Fig. 4.1).

Range is an increase in the separation distance can no longer cause a corresponding increase in the average squared difference between pair of values. Therefore, range is a distance (a) beyond which the variogram or co-variance value remains essentially constant, another word - the point at which the sill value is reached.

Sill is the plateau the variogram reaches at the range. The upper limit of any variogram model which has such a limit, i.e., which tends to 'level off' at large distances. Sill can also be defined as the variogram value ( $\mathrm{C}+\mathrm{Co}$ ) for very large distance $\gamma(\mathrm{h})$.


Fig. 4.1. Typical variogram plots (Royal and others, 1980).


Fig. 4.2. Process of variogram generation (David, 1977).
nugget effect is the value of the variogram or covariance (Co) which provides a discontinuity near the origin and is generally attributable to difference in sample values over very small distance, e.g., two halves of core, and can include inaccuracies in sampling and assaying, and the associated random errors. The vertical jump from the value of zero at the origin to the value of the variogram at extremely small separation distances is call the "nugget effect". The ratio of the nugget effect and is usually quoted in percentage. The ratio of the nugget to sill is referred to as the relative nugget effect (quoted in \%).

Cross validation is defined as a technique for testing the validity of a variogram model by kriging each sampled location with all of the other samples in the search neighborhood, and comparing the estimator with the true sample values. Interpretation of results, however, can often be difficult: Unusually large differences between estimation and true values may indicate the presence of "spatial outliners", or points which do not seem to belong with their surrounding

Geostatistics means a methodology for the analysis of spatially correlated data. The characteristic feature is the use of variograms or related techniques to quantify and model the spatial correlation structure. Also includes the various techniques, such as kriging, which utilize spatial correlation models.

Kriging means a weighted-moving-average interpolation methods where the set of weights assigned to samples minimized the estimation variance, which is computed as a function of the variogram model and locations of the samples relative to each other, and to the point or block being estimated.

Kriging standard deviation is the standard error of estimation computed for kriging estimate. By definition, kriging is the weighted linear estimation with the particular set of weights which minimizes the computed estimation variance (standard error squared).

The relationship of the kriging standard deviation to the underlying assumptions. Therefore, kriging standard deviations should be interpreted with caution.

Lag is a distance class interval used for variogram computation.

Semivariogram is almost identical in meaning to the term 'variogram' (see variogram).

Variogram is a plot of variance (one-half the mean squared difference) of paired samples measured as a junction of the distance (and optionally of the direction) between samples. Typically, all possible sample pairs are examined, and grouped into classes (lag) of approximately, equal distance and direction. Variogram provides a means of quantifying the commonly observed relationship. The samples close together will tend to have more similar values than samples for apart.

### 4.3 Variogram Analysis

### 4.3.1 Variogram Model

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Having calculated the experimental semi-variograms, an equation that best describes the values is found by fitting a curve to these experimental values to simplify further calculations. This curve is called a model variogram. The following observation (see Figs. 4.3 to 4.9 ) serve as an addition support for the argument that even with regularly gridded and well-behaved sample data, the exercise of fitting a function to the variogram model involves essential choices on the practitioners. The theoretical models developed to date can be simply divided into two main groups (Clark, 1976) :-
A) Variogam model with sill (see Figs. 4.3 to 4.6); and
B) Variogram model without sill (see Figs. 4.7 to 4.9).

## Varioaram Model with Sill

In cases where the semi-variogram increases with distance and levels off to a constant value after a certain distance, hence developing a sill, the following modeling methods are most commonly applied :-

1. The spherical model or Matheron model (Fig. 4.3)

The equation of spherical model is

2. Exponential Model (Fig. 4.4)

The equation of exponential model is $\gamma(\mathrm{h}) \quad=\mathrm{Co}+\mathrm{C}[1-\exp (-\mathrm{h} / \mathrm{a})]$;
3. Pure Nugget Effect Model (Fig. 4.5)

This model is shown by variance = sill. The equation of exponential model is

$$
\gamma(h)=0 ; h=0 \text { and } \quad \gamma(h)=\text { วิทย } C o ; h>0 \text {; and }
$$

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4. Gaussian Model (Fig. 4.6)

This model is almost similar to the spherical model. It shows parabola in the first step and continues to spherical model in the end. The equation of gaussian model is

$$
\gamma(h)=C o+C\left[1-\operatorname{ex}\left(-h^{2} / a^{2}\right)\right]
$$

when partial range $=1.73 \mathrm{a}(95 \%$ of sill), Effective range $=a$.

## Variogram Model without Sill

Only three models are briefly described including :

1. De Wijsian Model (see Fig. 4.7)

Variogram will be increase when distance increase. The equation of De Wijsan model is
when $A=3 \alpha$ (coefficient of intrinsic dispersion from
$[\gamma(h 2)-\gamma(h 1)] /\left[1_{n}(h 2)-1_{n}(h 1)\right]$ and $B=Y$-intercept $=C o$;
2. Power model or linear model (Fig. 4.8)
when $\lambda=1$
The equation of power model is $\gamma(h)=A h^{2}+B$ when $A=$ slope, $B=Y-$ intercept, $\quad \lambda=0<\lambda<2$; and

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3. Hole effect model (Fig. 4.9)

The equation is $\gamma(h)=C o+C\{[1-\sin (a h)] / a h\}$.


Fig. 4.3. Spherical variogram model.


Fig. 4.4.
Exponential variogram model.

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Fig. 4.5. Pure nugget effect variogram model, noting that variance (or h) = sill (or Co).


Fig. 4.6. Gaussian variogram model, showing parabola curve in the step and switching to spherical model at the end.


Fig. 4.7. De Wijsian variogram model, depicting the constant increase of variance at a constant distance increment.

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Fig. 4.8. $\quad$ Power variogram model.


Fig. 4.9. The Hole Effect variogram model, illustrating the fluctuation of variance with increasing distance.


### 4.3.2 Measurement of Basic Statistical Values

All stored and treated data in FoxPro database were rearranged into a new format in the form of Geo_EAS. Then basic statistical values of individual variables from Sin Pun and Saba Yoi areas can be determined.

## Sin Pun Area

It is observed statistically that the ash content of Nong Wa P1-P4 coal seam falls within the average range of $26-28 \%$ whereas that of the $M$ seam averages a little higher at $30 \%$. Variance measured from coal samples becomes quite high. This is probably due to the contrast in analyzed values up to $30 \%$. Sulphur contents fall in the average range of $4-5 \%$ for $P$ seams and increase up to $6.5 \%$ in $M$ seam.

From these statistical values, it is likely that both ash and sulphur contents increase as depth increases. Statistical values of individual variables for Sin Pun area are depicted in Table 4.1-4.5.


## Saba Yoi Area

Arithmetic mean of ash content from coal seams of Saba Yoi area ranges from 28 to $36 \%$. Variances of analytical coal values for the S1, S2, and S4 seam are not high, as compared with those of the P seams in the Sin Pun area.

As stated in Tables 4.6-4.9, the contrast between the minimum and maximum values of coal data for the $\mathrm{S} 1, \mathrm{~S} 2$, and S 4 seams is approximately $8 \%$, which is much lower than that of the S3 seam-up to $51 \%$. This is due essentially caused by the difference in coal values of about $20 \%$. However, the sulphur contents of Saba Yoi individual coal seams are averaged at $2 \%$.

Table 4.1. Statistic values for P1 seam, Nong Wa deposit, Sin Pun area.

| Value | Easting |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (UTM) | Northing <br> $($ UTM $)$ | Ash <br> $(\%)$ | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |  |
| Mean | 536323.7 | 909653.3 | 27.206 | 2017.867 | 28.032 | 4.179 | 1.435 |
| Variance | 156858.2 | 44089.16 | 99.992 | 695662.6 | 50.612 | 3.184 | 0.008 |
| Std. Dev. | 396.053 | 209.974 | 10 | 834.064 | 7.114 | 1.784 | 0.091 |
| Coef. Var. | 0.074 | 0.023 | 36.755 | 41.334 | 25.379 | 42.696 | 6.33 |
| Skewness | 0.063 | 0.481 | -0.695 | 0.306 | 1.018 | 0.005 | 0.148 |
| Kurtosis | 1.988 | 2.336 | 2.425 | 1.758 | 2.599 | 1.822 | 3.531 |
| Minimum | 535707.8 | 909400 | 6.8 | 823 | 20 | 1.52 | 1.26 |
| 25th \%tile | 535916.6 | 909456.9 | 18.365 | 1402.25 | 23.042 | 2.26 | 1.392 |
| Median | 536398.2 | 909599 | 28.07 | 1726 | 25.25 | 4.2 | 1.44 |
| 75th \%tile | 536528.1 | 909797.7 | 35.375 | 2784 | 29.645 | 5.465 | 1.47 |
| Maximum | 537006.9 | 910098.6 | 39.66 | 3347 | 42.23 | 6.86 | 1.64 |

Table 4.2. Statistic values for P2 seam, Nong Wa deposit, Sin Pun area.

| Value | Easting <br> (UTM) | Northing (UTM) | Ash <br> (\%) | CV (kcal/kg) | Moisture <br> (\%) | Sulphur (\%) | Density (g/cc) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 536296.1 | 909660.8 | 23.564 | 2501.471 | 28.146 | 5.091 | 1.385 |
| Variance | 186627 | 41652.84 | 83.612 | 567879.5 | 32.348 | 2.839 | 0.008 |
| Std. Dev. | 432.004 | 204.09 | 9.144 | 753.578 | 5.688 | 1.685 | 0.087 |
| Coef. Var. | 0.081 | 0.022 | 38.806 | 30.125 | 20.207 | 33.096 | 6.268 |
| Skewness | 0.336 | 0.141 | -0.625 | -0.207 | 0.683 | -0.53 | -0.363 |
| Kurtosis | 1.842 | 2.691 | 2.465 | 2.023 | 1.948 | 2.523 | 2.045 |
| Minimum | 535707.8 | 909300 | 4.26 | 1100 | 22.11 | 1.46 | 1.22 |
| 25th \%tile | 535909.4 | 909482.1 | 15.997 | 1845.25 | 23.245 | 3.835 | 1.322 |
| Median | 536282 | 909695.8 | 25.55 | 2592 | 26.08 | 5.2 | 1.39 |
| 75th \%tile | 536578.3 | 909795.4 | 30.688 | 3063.75 | 31.628 | 6.335 | 1.447 |
| Maximum | 537006.9 | 910098.6 | 37.13 | 3659 | 38.06 | 7.59 | 1.51 |

Table 4.3. Statistic values for P3 seam, Nong Wa deposit, Sin Pun area.

| Value | Easting <br> $($ UTM $)$ | Northing <br> $($ UTM $)$ | Ash <br> $(\%)$ | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 536265 | 909671.4 | 27.647 | 2131.25 | 27.718 | 4.81 | 1.433 |
| Variance | 192824.8 | 37174.43 | 110.076 | 878453.9 | 22.776 | 5.519 | 0.013 |
| Std. Dev. | 439.118 | 192.807 | 10.492 | 937.259 | 4.772 | 2.349 | 0.112 |
| Coef. Var. | 0.082 | 0.021 | 37.948 | 43.977 | 17.218 | 48.843 | 7.819 |
| Skewness | 0.703 | 0.419 | -0.727 | 0.046 | 1.263 | -0.18 | -0.153 |
| Kurtosis | 2.615 | 2.666 | 2.558 | 2.177 | 3.338 | 1.513 | 1.714 |
| Minimum | 535707.8 | 909398.1 | 5.47 | 494 | 23.3 | 1.13 | 1.25 |
| 25th \%tile | 535905.7 | 909507.8 | 20.51 | 1492 | 24.45 | 2.09 | 1.31 |
| Median | 536240.9 | 909675.8 | 28.97 | 2157 | 26.325 | 5.265 | 1.455 |
| 75th \%tile | 536499.6 | 909797.4 | 36.94 | 2652 | 28.34 | 6.99 | 1.53 |
| Maximum | 537208.7 | 910098.6 | 39.53 | 3659 | 38.89 | 7.89 | 1.58 |

Table 4.4. Statistic values for P4 seam, Nong Wa deposit, Sin Pun area.

| Value | Easting <br> $($ UTM $)$ | Northing <br> $($ UTM $)$ | Ash <br> $(\%)$ | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 536400.7 | 909615.1 | 27.909 | 2142.294 | 28.266 | 5.141 | 1.365 |
| Variance | 219061.7 | 47934.23 | 67.994 | 612670.6 | 28.895 | 5.488 | 0.019 |
| Std. Dev. | 468.04 | 218.939 | 8.246 | 782.733 | 5.375 | 2.343 | 0.138 |
| Coef. Var. | 0.087 | 0.024 | 29.545 | 36.537 | 19.017 | 45.568 | 10.124 |
| Skewness | 0.259 | 0.525 | -0.511 | 0.008 | 0.683 | -0.356 | 0.255 |
| Kurtosis | 2.029 | 2.464 | 2.349 | 2.198 | 2.596 | 1.848 | 1.572 |
| Minimum | 535707.8 | 909300 | 11.08 | 842 | 19.91 | 0.8 | 1.22 |
| 25th \%tile | 536000.1 | 909404.4 | 19.472 | 1442.75 | 25.135 | 3.31 | 1.22 |
| Median | 536398.2 | 909597.2 | 30.72 | 2392 | 26.85 | 5.81 | 1.36 |
| 75th \%tile | 536578.3 | 909773.4 | 32.563 | 2593.25 | 28.485 | 7.318 | 1.467 |
| Maximum | 537208.7 | 910098.6 | 40.34 | 3659 | 39.2 | 7.92 | 1.61 |

Table 4.5. Statistic values for $M$ seam, Nong Wa deposit, Sin Pun area.

| Value | Easting |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (UTM) | Northing <br> $($ UTM $)$ | Ash <br> $(\%)$ | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |  |
| Mean | 536421.4 | 909592.1 | 30.628 | 2152.333 | 24.684 | 6.936 | 1.372 |
| Variance | 201625.9 | 31720.29 | 54.787 | 1026495 | 20.602 | 8.746 | 0.014 |
| Std. Dev. | 449.028 | 178.102 | 7.402 | 1013.161 | 4.539 | 2.957 | 0.117 |
| Coef. Var. | 0.084 | 0.02 | 24.167 | 47.073 | 18.388 | 42.641 | 8.544 |
| Skewness | -0.413 | -0.332 | -0.635 | -0.932 | -0.17 | -0.898 | 0.043 |
| Kurtosis | 2.017 | 1.782 | 2.067 | 2.665 | 1.475 | 3.926 | 1.791 |
| Minimum | 535707.8 | 909300 | 18.09 | 160 | 18.09 | 0.46 | 1.22 |
| 25th \%tile | 535917.8 | 909417.9 | 22.507 | 1181.5 | 19.945 | 6.092 | 1.237 |
| Median | 536503 | 909650.3 | 29.95 | 2337 | 24.78 | 7.18 | 1.39 |
| 75th \%tile | 536675.9 | 909700.1 | 36.693 | 2906 | 28.778 | 7.65 | 1.425 |
| Maximum | 536998.1 | 909798.4 | 38.11 | 3091 | 29.94 | 11.14 | 1.54 |

Table 4.6. Statistic values for S1 seam, Ban Khok Tok deposit, Saba Yoi area.

| Value | Easting <br> (UTM) | Northing <br> (UTM) | Ash <br> (\%) | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 710260.5 | 726240.3 | 36.402 | 2196.556 | 22.461 | 1.936 | 1.368 |
| Variance | 106653.4 | 101839.4 | 5.83 | 8181.778 | 10.785 | 0.056 | 0.008 |
| Std. Dev. | 326.578 | 319.123 | 2.415 | 90.453 | 3.284 | 0.236 | 0.089 |
| Coef. Var. | 0.046 | 0.044 | 6.633 | 4.118 | 14.621 | 12.183 | 6.475 |
| Skewness | 0.039 | -0.28 | 0.135 | 0.512 | -1.064 | -0.03 | -0.362 |
| Kurtosis | 1.962 | 1.822 | 2.62 | 2.261 | 3.646 | 2.782 | 2.367 |
| Minimum | 709766.1 | 725751.9 | 32.37 | 2091 | 15.3 | 1.52 | 1.21 |
| 25th \%tile | 709966.9 | 725879.3 | 34.803 | 2104.5 | 20.557 | 1.777 | 1.29 |
| Median | 710271.4 | 726228.1 | 35.82 | 2195 | 23.47 | 1.97 | 1.37 |
| 75th \%tile | 710485 | 726426.8 | 37.78 | 2243.25 | 24.195 | 2.05 | 1.408 |
| Maximum | 710780.6 | 726627.3 | 40.71 | 2363 | 26.73 | 2.35 | 1.48 |

Table 4.7. Statistic values for $S 2$ seam, Ban Khok Ok deposit, Saba Yoi area.

| Value | Easting |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (UTM) | Northing <br> $($ UTM $)$ | Ash <br> $(\%)$ | CV <br> $(\mathrm{kcal} / \mathrm{kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |  |
| Mean | 712218.6 | 725434.1 | 33.797 | 2261.111 | 24.312 | 1.491 | 1.35 |
| Variance | 44995.78 | 98519.49 | 6.028 | 70356.86 | 2.878 | 0.043 | 0.004 |
| Std. Dev. | 212.122 | 313.878 | 2.455 | 265.249 | 1.696 | 0.207 | 0.066 |
| Coef. Var. | 0.03 | 0.043 | 7.265 | 11.731 | 6.978 | 13.913 | 4.871 |
| Skewness | -0.307 | -0.806 | 0.508 | -0.996 | 0.818 | -0.167 | -0.45 |
| Kurtosis | 1.476 | 2.769 | 2.04 | 3.679 | 2.184 | 1.436 | 1.589 |
| Minimum | 711936.5 | 724801.6 | 30.75 | 1683 | 22.59 | 1.2 | 1.26 |
| 25th \%tile | 711961.1 | 725202 | 31.628 | 2125.75 | 23.003 | 1.273 | 1.265 |
| Median | 712266.8 | 725438.4 | 33.08 | 2307 | 23.55 | 1.5 | 1.37 |
| 75th \%tile | 712369.9 | 725643.5 | 34.86 | 2336.5 | 24.823 | 1.673 | 1.398 |
| Maximum | 712458.8 | 725770 | 38 | 2579 | 27.29 | 1.72 | 1.43 |

Table 4.8. Statistic values for S 3 seam, Ban Sao deposit, Saba Yoi area.

| Value | Easting <br> (UTM) | Northing <br> (UTM) | Ash <br> (\%) | CV <br> $(\mathrm{kcal/kg})$ | Moisture <br> $(\%)$ | Sulphur <br> $(\%)$ | Density <br> $(\mathrm{g} / \mathrm{cc})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 709343.7 | 728719.4 | 28.198 | 2453.241 | 27.52 | 1.475 | 1.351 |
| Variance | 214902.4 | 407153 | 51.024 | 167788.2 | 14.965 | 0.032 | 0.004 |
| Std. Dev. | 463.576 | 638.085 | 7.143 | 409.62 | 3.868 | 0.179 | 0.062 |
| Coef. Var. | 0.065 | 0.088 | 25.332 | 16.697 | 14.057 | 12.158 | 4.568 |
| Skewness | -0.311 | 0.618 | -0.073 | -0.204 | -0.579 | 0.867 | 0.088 |
| Kurtosis | 2.304 | 2.585 | 1.676 | 2.48 | 2.342 | 3.075 | 1.608 |
| Minimum | 708458.2 | 727828.9 | 18.34 | 1661.85 | 19.56 | 1.25 | 1.27 |
| 25th \%tile | 708963.8 | 728227.5 | 19.965 | 2139.058 | 24.54 | 1.32 | 1.29 |
| Median | 709405.3 | 728616.6 | 28.45 | 2501.55 | 27.85 | 1.45 | 1.35 |
| 75th \%tile | 709705.4 | 728970.8 | 32.982 | 2611.647 | 30.275 | 1.54 | 1.395 |
| Maximum | 710096.9 | 730031.7 | 38.19 | 3123.28 | 32.18 | 1.88 | 1.45 |

Table 4.9. Statistic values for S4 seam, Ban Sao deposit, Saba Yoi area.

| Value | Easting <br> (UTM) | Northing <br> (UTM) | Ash <br> (\%) | $\begin{gathered} \text { CV } \\ (\mathrm{kcal} / \mathrm{kg}) \end{gathered}$ | Moisture <br> (\%) | Sulphur <br> (\%) | Density (g/cc) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean | 709612.9 | 728484.4 | 36.256 | 1936.896 | 25.159 | 1.803 | 1.387 |
| Variance | 58753.38 | 213325.1 | 12.479 | 226344.6 | 16.871 | 0.291 | 0.003 |
| Std. Dev. | 242.391 | 461.871 | 3.533 | 475.757 | 4.107 | 0.539 | 0.051 |
| Coef. Var. | 0.034 | 0.063 | 9.744 | 24.563 | 16.326 | 29.899 | 3.645 |
| Skewness | 1.252 | 0.785 | 0.073 | 0.653 | -1.26 | 1.126 | -0.421 |
| Kurtosis | 3.292 | 1.978 | 1.625 | 2.647 | 3.572 | 2.913 | 2.625 |
| Minimum | 709405.3 | 728018.6 | 31,68 | 1378.58 | 16.82 | 1.31 | 1.3 |
| 25th \%tile | 709436.9 | 728171.8 | 32.88 | 1477.865 | 21.792 | 1.438 | 1.337 |
| Median | 709559.9 | 728227.5 | 37.26 | 1991.3 | 26.59 | 1.52 | 1.39 |
| 75th \%tile | 709612.5 | 728580.3 | 37.842 | 2082.212 | 27.035 | 1.862 | 1.41 |
| Maximum | 710096.9 | 729231.4 | 41.22 | 2802.81 | 29.48 | 2.84 | 1.46 |

### 4.3.3 Varioaram Parameters

Several parameters involved in the variogram construction and analysis in this study include number of pairs, direction, tolerance angel, and lag spacing. After all the data are stored in the form of Geo_EAS format, the Geo_EAS software program can sort the number of pairs in all directions (isotropic) search using Prevar subprogram created by Englund (1991). Prevar is a preprocessor program for variogram analysis. All variogram calculation use the distance and relative direction between pair of points in the sample area. The output of Prevar is a "pair comparison file" (pcf). The pcf contains the input data file content along with distances and relative directions between pair of sample points. Limits may be imposed on the $X$ and $Y$ coordinate values or on the distance between points in a pair. If no limits are specified, all sample points are used for calculation. The pair comparison file can become quite large if there are many points in the data file. It is recommended that some limits on the distance between points be specified. In a situation like those of Sin Pun and Saba Yoi areas where the samples are not regularly spaced (see Figs 3.2 \& 3.8), approximation must be introduced into calculation (see Clark, 1979, Isaaks \& Srivasta va, 1989, Evan, 1995). Supported that one needs to calculate the experimental variogram value for a distance in a specified direction (e.g., north-east, south-west). The chance of finding any pairs at exactly this separation with irregular sampling is quite small, a 'tolerance' or each specification is, therefore, placed. Fig. 4.10 illustrates the size of the tolerance, lag spacing and search area (-area which related sample data are counted). This is rather a circular argument, since the structure still becomes unknown until the semivariogram is constructed (Journal, 1974; Thomas, 1992). For a good practice, a narrow range of ' $\delta$ h' values and tolerance-angle values are simulated. In general case, the $\gamma(\mathrm{h})$ or variogram is frequently small relative to the sample spacing. In this investigation, the tolerance angles used for analysis are selected $-5^{\circ}, 15^{\circ}, 25^{\circ}, 35^{\circ}$, and $45^{\circ}$ (see in Fig. 4.11). One may agree, from an example shown in Table 4.10, that with specific direction and lag spacing (i.e., $157.5^{\circ}$ and 280 m , respectively, numbers of pairs at $25^{\circ}, 35^{\circ}$, and $45^{\circ}$ tolerance angles are
almost similar. But if also taking into account on Table 4.11, one may realize that the $45^{\circ}$ tolerance Zscore for these specific direction and spacing is closer to 0 than those of the others. However, the good result after changing orientation is that of $45^{\circ}$ at $\mathrm{E}-\mathrm{W}$ direction (Tables 4.10 and 4.11). This is probably due to the limited amount of drilled-holes. However, according to Isaaks \& Srivastava (1985), the angular tolerance of $40^{\circ}$ was applied to their variogram analysis. In this study, determination on the samples mutually related to each other in several directions is applied by using Geo_EAS computed designed software. The angle $0^{0}$ is assigned to represent easting direction, then the direction is moved clockwise to every $22.5^{\circ}$ (Table 4.11).

Lag spacing applied in the variogram analysis was simulated at a given distance, e.g. $200 \mathrm{~m}, 400 \mathrm{~m}, 600 \mathrm{~m}, 800 \mathrm{~m}$ etc., until variogram models of individual parameters can be figured out. It should be pointed out again that there are 3 main parameters in the variogram construction -lag spacing, direction, and tolerance angle. For analyzing the variogram model with the application of Geo_EAS software, simulation was able to perform with respect to these 3 variogram parameters simultaneously. Followings are the examples of analyzing the variogram models of the P1 seam ash data ( 15 bore-holes), Nong Wa deposit, Sin Pun area. As shown in Figs. 4.13 and 4.14 and Table 4.13, the variogram model becomes pure nugget for every tolerance angle and lag spacing. Therefore, it is quite probable that there is no relationship among paired samples, using these parameters, unless sampling pattern and analysis are regarded incorrect. So simulation was done continuously, but in this case the direction was changed from $0^{\circ}$ to $22.5^{\circ}$ with similar varying lag spacing and tolerance angles (Table 4.12). Similar situation was encountered for Saba Yoi ash content data when using the parameters quoted in Table 4.14, being pure nugget model. Once again, simulation was performed using the varying direction as $45^{\circ}, 67.5^{\circ}, 90^{\circ}, 112.5^{\circ}, 135^{\circ}$, and $157.5^{\circ}$, respectively with the same values of the other variogram parameters, and the result became clearly the pure-nugget effect variance. In this case, it is regarded that there is no mutual relationship of samples with respect to these parameters applied.


Fig.4.10. Search area defined by tolerances on angle ( $\theta$ ) and distance between pairs in experimental variogram.


Fig. 4.11. Tolerance angle testing applied in this study with $22.5^{\circ}$ for individual divisions as sectors.
(see also Table 4.12).

 models

$$
\text { sill }=70, \text { and R-major }=500 \mathrm{~m} .
$$



Tolerance angle $45^{\circ}$ with spherical model,
nugget $=0$, sill $=130$, and range $=900 \mathrm{~m}$.

Fig. 4.12. Test of tolerance angles for ash content (\%), P1 seam, Sin Pun area, at fixed direction $157.5^{\circ}$ and lag spacing 280 m . Noted that x -axis is distance ( m ) and y -axis indicates variance.

Table 4.10. Numbers of pairs at various tolerance angle testing for ash content (\%), P1 seam, Sin Pun area, at fixed direction $157.5^{\circ}$ and lag spacing 280 m .

| pair no. | $5^{\circ}$ | $15^{\circ}$ | $25^{\circ}$ | $35^{\circ}$ | $45^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | - | 1 | 7 | 9 | 9 |
| 2 | 4 | 9 | 18 | 22 | 24 |
| 3 | 3 | 15 | 25 | 27 | 31 |
| 4 | 5 | 9 | 11 | 13 | 13 |
| 5 | 2 | 4 | 5 | 5 | 5 |

Table 4.11. The result of cross validation of tolerance angle testing for ash content (\%), P1 seam, Sin Pun area, fixed direction $157.5^{\circ}$ and lag spacing 280 m .

| angle ( ${ }^{\circ}$ ) | R-minor (m) | Mean of difference | Zscore |
| :---: | :---: | :---: | :---: |
| 5 | - | - | - |
| 15 | 210 | 0.739 | 0.049 |
| 25 | 450 | 0.061 | 0.007 |
| 35 | 450 | 0.065 | 0.004 |
| 45 | 490 | 0.018 | -0.001 |

Table 4.12. A comparison between angles used in the variogarm analysis and the direction for related samples, ash content, Nong Wa P1 seam (see also Fig. 4.11).


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Trials and errors were also done for all the ash data of 17 drill-holes of the P2 seam with three involving variogram parameters using the variable values of tolerance angle and lag spacing. All the results of variogram analysis point to the pure nugget effect model. Simulation was done so far for the data of seams P3, P4, M, S1, S2, S3, and S4. As a result, the pure nugget effect models were virtually encountered.

A great care was taken into account for the data in the FoxPro database system. It is obvious that the concentration of Sin Pun data occurs mostly in the northern and central parts of the Nong Wa deposit area, and only few are in the south. A new selection for variogram analysis was applied to the Nong Wa area without the drill-hole data in the south. For the Saba Yoi area, it is observed that individual coal seams occur discontinuously in various sub-basins (deposits).

Data of seams S1 and S2 are more concentrated in the Ban Khok Tok and Ban Khok Ok deposit, respectively (see also Figs 3.10 and 3.11), and those of S3 and S4 are in Ban Sao deposit (see Figs 3.12 and 3.13). So a new selection have been made for the uses of the coal seam data which appear more in the coal sub-basins (or deposits). Therefore, a new data set were selected from the FoxPro database system and reformatted It using the Geo_EAS software for variogram analysis utilizing the same parameters as previously analyzed. After a specific direction to which samples are mostly related was identified, calculation was applied to the variogram model of each parameter in the data set, including ash content (\%), calorific value (kcal/kg), moisture content (\%), sulphur content (\%), and density (\%).

As a result (see Tables 4.15 and 4.16), lag-spacing appropriate to individual data sets and variables were determined in order to make a configuration of curve fitting of those variables with the variogram model assigned, as previously described. It is quite important to note herein also that variogram construction had to be performed in accordance with the cross validation analysis.

The reason beyond this application is to check the level of confidence of the model being used, and to compare between the values computerized and the values from the actual analysis with variable lag spacing. Theoretically, if variogram model is changed, the result of cross-validation remained unchanged. Then, the variogram model after cross-validation was applied successfully for the geostatistical estimation (see also Gurba, 1994, Gillies et al., 1987).



Fig. 4.13. Examples of variogram model from testing direction $0^{\circ}$ (east-west) of S1 seam, Saba Yoi area.


Fig. 4.14. Examples of variogram model (mostly nugget-effect) from testing direction $22.5^{\circ}$ with lag spacing at 200 and 400 m and tolerance angle at $25^{\circ}$ and $35^{\circ}$, S1 seam, Saba Yoi area.

Table 4.13. Results of variogram model with fixed direction (at $0^{\circ}$ ) and varying lag spacings and tolerance angle, comuted by Geo_EAS program.

| Direction | Tolerance angle (degree) | lag spacing <br> (m.) | Variogram model |
| :---: | :---: | :---: | :---: |
| 0 | 5 | 200 | pure nugget effect |
| 0 | 5 | 400 | pure nugget effect |
| 0 | 5 | 600 | pure nugget effect |
| 0 | 5 | 800 | pure nugget effect |
| 0 | 15 | 200 | pure nugget effect |
| 0 |  | 400 | pure nugget effect |
| 0 |  | 600 | pure nugget effect |
| 0 |  | 800 | pure nugget effect |
| 0 |  | 200 | pure nugget effect |
| 0 | 25 | - 400 | pure nugget effect |
| 0 | 25 | 600 | pure nugget effect |
| 0 | $25$ | $800$ | pure nugget effect |
| 0 | $35$ | $200$ | pure nugget effect |
| 0 | 35 | 400 | pure nugget effect |
| 0 | 35 | 600 | pure nugget effect |
| 0 | 35 | 800 | pure nugget effect |
| 0 | 45 | 200 | pure nugget effect |
| 0 | 45 | 400 | pure nugget effect |
| 0 | 45 | 600 | pure nugget effect |
| 0 | 45 | 800 | pure nugget effect |

Table 4.14. Result of variogram model with fixed direction at $22.5^{\circ}$ and varying tolerance angles and lag spacing computed by Geo_EAS program.

| Direction | Tolerance angle (degree) | Lag spacing <br> (m.) | Variogram model |
| :---: | :---: | :---: | :---: |
| 22.5 | 5 | 200 | pure nugget effect |
| 22.5 | 5 | 400 | pure nugget effect |
| 22.5 | 5 | 600 | pure nugget effect |
| 22.5 | 5 | 800 | pure nugget effect |
| 22.5 | 15 | 200 | pure nugget effect |
| 22.5 |  | 400 | pure nugget effect |
| 22.5 |  | 600 | pure nugget effect |
| 22.5 |  | 800 | pure nugget effect |
| 22.5 |  | 200 | pure nugget effect |
| 22.5 | 25 | $\pm 400$ | pure nugget effect |
| 22.5 | 25 | 600 | pure nugget effect |
| 22.5 | $25$ | $800$ | pure nugget effect |
| 22.5 | ALO | $200$ | pure nugget effect |
| 22.5 | 35 | 400 | pure nugget effect |
| 22.5 | 35 | 600 | pure nugget effect |
| 22.5 | 35 | 800 | pure nugget effect |
| 22.5 | 45 | 200 | pure nugget effect |
| 22.5 | 45 | 400 | pure nugget effect |
| 22.5 | 45 | 600 | pure nugget effect |
| 22.5 | 45 | 800 | pure nugget effect |

Table 4.15. A summary of values of variogram parameters used for variogram analysis of Sin Pun coal seams, calculated by Geo_EAS software.

| Seam | Variable | Direction <br> (degree) | Tolerance angle (degree) | Lag spacing <br> (m) |
| :---: | :---: | :---: | :---: | :---: |
| P1 | Ash | 157.5 | 45 | 280 |
|  | CV | 157.5 | 45 | 280 |
|  | Moisture | 157.5 | 45 | 150 |
|  | Sulphur | 0 | 45 | 180 |
|  | Density | 157.5 | 45 | 190 |
| P2 | Ash | 157.5 | 45 | 140 |
|  | CV | 191 | 45 | 240 |
|  | Moisture | 157.5 | 45 | 170 |
|  | Sulphur | 157.5 | 45 | 240 |
|  | Density | -157.5 | 45 | 260 |
| P3 | Ash | 157.5 | 45 | 160 |
|  | CV | 157.5 | 45 | 160 |
|  | Moisture | 0 | 45 | 190 |
|  | Sulphur | 157.5 | 45 | 210 |
|  | Density | 22.5 | 45 | 280 |
| P4 | Ash 1 บก | รณ冂157.5 ทย | ลย 45 | 250 |
|  | CV | 157.5 | 45 | 200 |
|  | Moisture | 157.5 | 45 | 310 |
|  | Sulphur | 22.5 | 45 | 280 |
|  | Density | 157.5 | 45 | 150 |
| M | Ash | 157.5 | 45 | 170 |
|  | CV | 157.5 | 45 | 220 |
|  | Moisture | 157.5 | 45 | 350 |
|  | Sulphur | 157.5 | 45 | 200 |
|  | Density | 0 | 45 | 330 |

Table 4.16. A summary of values of variogram parameters used for variogram analysis of Saba Yoi coal seams, calculated by Geo_EAS software.


### 4.4 Results of Variogram Analysis

Results of variogram analysis from several variable of coal seams indicate mostly the spherical models (see Tables 4.15 and 4.16). Few are regarded as gaussian and linear models. However, some variables of specific coal seems (e.g. S4 seam) cannot define any relationship of data to each other, giving rise to pure nugget model. The overall selections of the variogram results from the start to the end (variogram model) are exhibited in Appendix D.

### 4.4.1 Variogram Analvsis of Ash Contents (\%)

The example of ash content is made by using P1 seam as a representative for the Sin Pun area (see Table 4.15). After simulation 5 lag numbers are identified it is discovered that first lag spacing, or herein called lag no. 1, is assigned at a distance between 0 and 280 m , lag no. 2 (the second lag spacing) is from 280 to 560 m , lag no. 3 from 560 to 840 m , lag no. 4 from 840 to $1,120 \mathrm{~m}$, and lag no. 5 from 1,120 to $1,400 \mathrm{~m}$. These ranges of lag spacing are applied to variogram analysis in this study. As shown in Table 4.17, lag no. 1 consists of 9 numbers of pair with the average distance of 185.249 m (computed from distance-column 4 in Table 4.18).

The variogram value estimated based upon these parameters is 21.117 . It is also noted that the orientation used in this study is based upon the direction or trend, another word E-W orientation means samples being concerned or related are aligned more or less in the E-W trend. Therefore, the orientation of related samples at $0^{\circ}$ is automatically applied to $180^{\circ}$ for computer calculation. The analysis of P1-seam ash content shows mostly mutual relationships in the WSW - ENE direction ( $157.5^{\circ}$ ) at the tolerance angel of $45^{\circ}$ and with lag spacing 280 m . These variogram values of parameters are then applied for variogram-model construction shown in Table 4.17. In this model, the nugget effect (Co) equals 0 , sill (C) equals 130, and range is 900 m . Table 4.17 shows a result of variogram parameter values plotted as variogram in Fig. 4.15. The spherical model
variogram is encountered occur as a result of relationship among samples, shown in Tables 4.17 and 4.18. It is noted that on the table 4.18, pair means relationship between the first and the second data sample points (as 15: 10 in the first row in the table, respectively). The $1^{\text {st }}$ value of the second column means value of ash content of the first sample, $2^{\text {nd }}$ value of the third column indicates value of the second sample, distance in the fourth column is the length between two given samples, direction in the fifth column is orientation of the second sample as viewed from the first, and difference ${ }^{2}$ of the last column means square of difference in values [( $1^{\text {st }}-2^{\text {nd }}$ values $\left.)^{2}\right]$ (see also equation 4.1 ). It is noted that the value in the last column (difference ${ }^{2}$, in Table 4.18) are arranged in an increasing order from the top row. Result from Table 4.18 reveals that selected lag results can give rise to the orientation with maximum related sample values at $157.5^{\circ}$ and its opposite direction, as compared with those of the other orientations (not shown herein).

Parameters obtained from variogarm model were then tested by cross validation method in order to check values obtained from kriging estimation (column3; estimate, Table 4.19) diviating form the actual values, P1 seam, cross validation test is shown in Table 4.19. It was found from Table 4.19 that 'Zscore' (the last column) indicates the ratio of kriging standard (the fifth column or kriging of standard diviation, see also chapters 1 and 3) and their difference (the forth column). Zscore is very close to zero (0), then the result of analysis is quite reliable. If it is not, the result become unreliable. So small values in 'Difference may give rise to the decreases in Zscore. As a result, a group of data analyzed are regarded reliable. Since after estimation, the mean of P1 seam ash content (27.206) expressed as estimate in the $3^{\text {rd }}$ column is different from the mean from the analysis (27.244) expressed as variable in the $2^{\text {nd }}$ column, giving rise to the value of difference ( 0.038 ) expressed as difference in the $4^{\text {th }}$ column and Zscore of 0.000 .

Although the Zscore of the maximum value is rather high (1.505), the rest values of Zscore are close to 0 , giving rise to the reliable result. Furthermore, the result of cross validation can indicate the search distance used for estimation, since values of the mean
of difference and Zscore can be changed based upon the change in search values. For the ash content of Nong Wa P1 seam, the most appropriate search distance after simulation is 470 m .

For the Saba Yoi area, is made by using S1 seam as a representative for the ash content (see also Table 4.16). It is discovered that lag no. 1 is between 0 and 240 m , lag no. 2 is between 240 and 480 m , lag no. 3 is between 480 and 720 m , lag no. 4 is between 720 and 960 m, and lag no. 5 is between 960 and 1200 m . It is observed, after simulation, that the analysis of S1 seam ash content shows mostly mutual relationships in the N-S direction $\left(90^{\circ}\right)$ at the tolerance angle of $45^{\circ}$ and with lag spacing of 240 m . Fig. 4.16 shows a spherical model simulated from 5 lags and 19 concerned pairs, and the average distances and variogram values are shown in Table 4.20.

The nugget effect (Co) at 3, sill (C) of 2.1, and the range at 380 m are used for S1 seam data. Table 4.20 shows result of variogram parameters values plotted as variogram in Fig. 4.16 occur as a result of relationship among samples, shown in Tables 4.20 and 4.21. Result from Table 4.21 reveals that selected lag result can give rise to the maximum related sample value at 90 direction (and opposite), compared to those of the other orientations.

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Parameters obtained from variogarm model were then tested by cross validation method. After estimation, the mean of S1 seam ash content (36.402) is different from the mean from the analysis (36.525), giving rise to the value of difference (-0.382). As the results for the ash content of Ban Khok Tok S1 seam, the most appropriate search distance after simulation is 270 m .

Table 4.17. Results of lag spacing, numbers of pair average distance at direction $157.5^{\circ}$ and variogram value for ash content (\%), P1 seam, Sin Pun area.

| Lag no. | Pair <br> (no.) | Avg. distance <br> $(\mathrm{m})$ | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 9 | 185.249 | 21.117 |
| 2 | 24 | 398.774 | 74.991 |
| 4 | 31 | 689.91 | 120.31 |
| 5 | 5 | 978.584 | 133.457 |



Fig. 4.15. Variogram spherical model of ash content (\%), P1 seam, Nong Wa deposit, Sin Pun area.

Table 4.18. $\quad$ Selected lag results of ash content (\%) at 157.5 orientation for P1 seam Nong Wa deposit, Sin Pun area, using Geo_EAS software.

Lag 1 for ash content (\%)

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $15: 10$ | 26.33 | 27.9 | 113.136 | 148.233 | 2.465 |
| $15: 13$ | 26.33 | 28.07 | 205.549 | 356.601 | 3.028 |
| $13: 01$ | 28.07 | 29.96 | 149.668 | 133.917 | 3.572 |
| $10: 01$ | 27.9 | 29.96 | 200.827 | 10.345 | 4.244 |
| $9: 08$ | 19.07 | 16.25 | 170.66 | 310.961 | 7.952 |
| $14: 01$ | 35.23 | 29.96 | 134.492 | 318.353 | 27.773 |
| $8: 06$ | 16.25 | 10.95 | 212.701 | 177.508 | 28.09 |
| $12: 01$ | 36.6 | 29.96 | 200.572 | 181.536 | 44.09 |
| $8: 04$ | 16.25 | 32.34 | 279.639 | 2.177 | 258.888 |

Lag 2 for ash content (\%)

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $4: 02$ | 32.34 | 37.78 | 303.259 | 359.563 | 29.594 |
| $15: 04$ | 26.33 | 32.34 | 435.41 | 117.113 | 36.12 |
| $14: 13$ | 35.23 | 28.07 | 283.948 | 316.017 | 51.266 |
| $12: 10$ | 36.6 | 27.9 | 400.213 | 185.943 | 75.69 |
| $11: 01$ | 39.66 | 29.96 | 518.268 | 168.198 | 94.09 |
| $14: 03$ | 35.23 | 25.34 | 510.922 | 11.13 | 97.812 |
| $15: 12$ | 26.33 | 36.6 | 318.323 | 18.499 | 105.473 |
| $13: 11$ | 28.07 | 39.66 | 403.504 | 0.257 | 134.328 |
| $10: 08$ | 27.9 | 16.25 | 496.399 | 140.256 | 135.722 |
| $3: 02$ | 25.34 | 37.78 | 410.164 | 165.655 | 154.754 |

Lag 2 for ash content (\%) (cont.)

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $9: 04$ | 19.07 | 32.34 | 408.789 | 343.186 | 176.093 |
| $14: 08$ | 35.23 | 16.25 | 515.792 | 158.153 | 360.24 |
| $15: 05$ | 26.33 | 6.8 | 526.74 | 159.228 | 381.421 |
| $10: 05$ | 27.9 | 6.8 | 416.241 | 162.199 | 445.21 |
| $6: 04$ | 10.95 | 32.34 | 491.939 | 0.16 | 457.532 |
| $14: 05$ | 35.23 | 6.8 | 493.378 | 179.789 | 808.265 |
| $13: 10$ | 28.07 | 27.9 | 309.798 | 166.609 | 0.029 |
| $12: 02$ | 36.6 | 37.78 | 345.878 | 124.732 | 1.392 |
| $14: 12$ | 35.23 | 36.6 | 312.501 | 344.407 | 1.877 |
| $4: 01$ | 32.34 | 29.96 | 418.467 | 315.762 | 5.664 |
| $14: 04$ | 35.23 | 32.34 | 284.178 | 134.537 | 8.352 |
| $12: 11$ | 36.6 | 39.66 | 326.402 | 340.049 | 9.364 |
| $7: 04$ | 35.81 | 32.34 | 359.151 | 303.696 | 12.041 |
| $6: 05$ | 10.95 | 6.8 | 280.9 | 314.784 | 17.222 |

Lag 3 for ash content (\%)

| Pair * $^{\text {st }}$Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $11: 10$ | 39.66 | 27.9 | 708.336 | 174.334 | 138.298 |
| $13: 08$ | 28.07 | 16.25 | 786.125 | 150.331 | 139.712 |
| $15: 11$ | 26.33 | 39.66 | 608.776 | 359.023 | 177.689 |
| $8: 01$ | 16.25 | 29.96 | 643.947 | 334.096 | 187.964 |
| $15: 06$ | 26.33 | 10.95 | 791.049 | 150.778 | 236.544 |
| $14: 09$ | 35.23 | 19.07 | 672.13 | 151.49 | 261.146 |
| $10: 06$ | 27.9 | 10.95 | 678.043 | 151.202 | 287.303 |

Lag 3 for ash content (\%) (cont.)

| Pair * | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 9:02 | 19.07 | 37.78 | 704.948 | 350.153 | 350.064 |
| 12:08 | 36.6 | 16.25 | 827.135 | 160.512 | 414.122 |
| 13:05 | 28.07 | 6.8 | 725.513 | 164.08 | 452.413 |
| 8:02 | 16.25 | 37.78 | 582.747 | 0.817 | 463.541 |
| 5:01 | 6.8 | 29.96 | 600.835 | 351.271 | 536.386 |
| 14:06 | 35.23 | 10.95 | 719.933 | 163.772 | 589.518 |
| 6:02 | 10.95 | 37.78 | 795.188 | 359.932 | 719.849 |
| 12:05 | 36.6 | 6.8 | 798.997 | 173.835 | 888.04 |
| 5:02 | 6.8 | 37.78 | 629.412 | - 18.377 | 959.76 |
| 14:07 | 35.23 | 35.81 | 640.491 | 128.483 | 0.336 |
| 11:02 | 39.66 | 37.78 | 640.632 | 141.862 | 3.534 |
| 7:02 | 35.81 | 37.78 | 585.818 | 329.068 | 3.881 |
| 10:03 | 27.9 | 25.34 | 638.95 | 20.529 | 6.554 |
| 12:04 | 36.6 | 32.34 | 576.568 | 150.197 | 18.148 |
| 13:04 | 28.07 | 32.34 | 568.078 | 135.276 | 18.233 |
| 14:11 | 35.23 | 39.66 | 638.441 | 342.181 | 19.625 |
| 7:01 | 35.81 | 29.96 | 773.336 | 310.191 | 34.223 |
| 4:03 | 32.34 | 25.34 | 708.293 | 351.562 | 49 |
| 15:09 | 26.33 | 19.07 | 776.95 | 139.381 | 52.708 |
| 10:07 | 27.9 | 35.81 | 695.555 | 115.688 | 62.568 |
| 10:09 | 27.9 | 19.07 | 665.389 | 137.882 | 77.969 |
| 15:07 | 26.33 | 35.81 | 793.263 | 120.088 | 89.87 |
| 15:08 | 26.33 | 16.25 | 608.643 | 141.734 | 101.606 |
| 9:01 | 19.07 | 29.96 | 803.684 | 329.311 | 118.592 |

Lag 4 for ash content (\%)

| Pair * | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12:07 | 36.6 | 35.81 | 912.169 | 140.078 | 0.624 |
| 9:03 | 19.07 | 25.34 | 1114.314 | 348.498 | 39.313 |
| 11:04 | 39.66 | 32.34 | 899.892 | 153.755 | 53.582 |
| 13:07 | 28.07 | 35.81 | 922.739 | 130.795 | 59.908 |
| 13:09 | 28.07 | 19.07 | 948.815 | 146.911 | 81 |
| 8:03 | 16.25 | 25.34 | 984.495 | 354.561 | 82.628 |
| 7:03 | 35.81 | 25.34 | 985.892 | 335.889 | 109.621 |
| 13:06 | 28.07 | 10.95 | 980.171 | 156.019 | 293.094 |
| 12:09 | 36.6 |  | 979.218 | 155.581 | 307.301 |
| 5:03 | 6.8 | 25.34 | 999.388 | 5.559 | 343.732 |
| 6:01 | 10.95 | 29.96 | $843.383$ | 339.847 | 361.38 |
| 12:06 | 36.6 | 10.95 | 1032.42 | 163.965 | 657.922 |
| 11:05 | 39.66 | 6.8 | 1118.703 | 169.848 | 1079.78 |

Lag 5 for ash content (\%)

| Pair * | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 11:07 | 39.66 | 35.81 | 1224.031 | 145.304 | 14.822 |
| 6:03 | 10.95 | 25.34 | 1196.965 | 355.085 | 207.072 |
| 11:09 | 39.66 | 19.07 | 1304.876 | 156.698 | 423.948 |
| 11:08 | 39.66 | 16.25 | 1153.529 | 160.381 | 548.028 |
| 11:06 | 39.66 | 10.95 | 1358.243 | 163.024 | 824.264 |

Table 4.19. Cross validation for ash content (\%) at $157.5^{\circ}$, P1 seam, Nong Wa deposit, Sin Pun area, tested using Geo_EAS program.

Ash content (\%)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 6.8 | 13.868 | -9.600 | 5.974 | -.840 |
| 25th \%tile | 16.25 | 21.520 | -5.785 | 6.471 | -.751 |
| Median | 27.9 | 27.297 | -2.876 | 7.278 | -.444 |
| 75th \%tile | 35.23 | 31.518 | 2.918 | 8.972 | .368 |
| Maximum | 39.66 | 38.426 | 14.720 | 11.425 | 1.505 |
| Mean | 27.206 | 27.244 | .038 | 8.173 | .000 |
| Std. Dev. | 10 | 6.477 | 7.059 | 1.737 | .745 |

Table 4.20. Results of lag spacing, numbers of pair average distance at direction $90^{\circ}$ and variogram value for ash content (\%), S1 seam, Saba Yoi area.
\(\left.$$
\begin{array}{|c|c|c|c|}\hline \text { Lag no. } & \begin{array}{c}\text { Pair } \\
\text { (no.) }\end{array}
$$ \& \begin{array}{c}Avg. distance <br>

(m)\end{array} \& Estimate\end{array}\right]\)| 186.733 |
| :---: |
| 1 |
| 2 |



Fig. 4.16. Variogram spherical model of ash content (\%), S1 seam,
Ban Khok Tok deposit, Saba Yoi area.

Table 4.21. Selected lag results of ash content (\%) at 90 orientation for S 1 seam Ban Khok Tok deposit, Saba Yoi area, using Geo_EAS software.
lag 1 for ash content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $9: 06$ | 37.75 | 34.77 | 186.733 | ลัย 86.45 | 8.88 |

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lag 2 for ash content (\%)

| Pair $^{\star}$ | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3:02 | 35.82 | 35.62 | 287.887 | 132.959 | 0.04 |
| $7: 03$ | 37.79 | 35.82 | 415.161 | 255.261 | 3.881 |
| $2: 01$ | 35.62 | 37.89 | 444.395 | 117.253 | 5.153 |
| $7: 05$ | 37.79 | 40.71 | 406.596 | 77.446 | 8.526 |
| $9: 05$ | 37.75 | 40.71 | 434.534 | 112.593 | 8.762 |
| $6: 05$ | 34.77 | 40.71 | 279.297 | 129.725 | 35.284 |

lag 3 for ash content (\%)

| Pair* $^{1^{\text {st }} \text { Value }}$(\%) | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $4: 02$ | 34.9 | 35.62 | 590.011 | 270.352 | 0.518 |
| $6: 03$ | 34.77 | 35.82 | 692.316 | 237.449 | 1.102 |
| $9: 03$ | 37.75 | 35.82 | 536.688 | 227.738 | 3.725 |
| $8: 06$ | 32.37 | 34.77 | 701.353 | 110.206 | 5.76 |
| $7: 04$ | 37.79 | 34.9 | 502.636 | 127.421 | 8.352 |
| $5: 02$ | 40.71 | 35.62 | 705.424 | 236.418 | 25.908 |
| $9: 08$ | 37.75 | 32.37 | 535.75 | 298.278 | 28.944 |

lag 4 for ash content (\%)

| Pair* | $1^{\text {st }}$ Value |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $(\%)$ | $2^{\text {nd }}$ Value | Distance | Direction | Difference $^{2}$ |  |
| $(\%)$ | $(\mathrm{m})$ | (degree) |  |  |  |
| $4: 03$ | 34.9 | 35.82 | 825.243 | 284.012 | 0.846 |
| $3: 01$ | 35.82 | 37.89 | 725.729 | 123.418 | 4.285 |
| $5: 03$ | 40.71 | 35.82 | 821.607 | 256.342 | 23.912 |

lag 5 for ash content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 8:04 | 32.37 | 34.9 | 1195.694 | 132.941 | 6.401 |
| 8:05 | 32.37 | 40.71 | 969.102 | 115.732 | 69.556 |

Table 4.22. Cross validation for ash content (\%) at $90^{\circ}$, S 1 seam, Ban Khok Tok deposit, Saba Yoi area, tested using Geo_EAS program.

Ash Content (\%)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 32.37 | 34.77 | -5.94 | 2.661 | -1.863 |
| 25th \%tile | 34.77 | 34.9 | -2.99 | 2.712 | -0.939 |
| Median | 35.62 | 35.82 | -0.2 | 3.183 | -0.063 |
| 75 th \%tile | 37.75 | 37.75 | 0.2 | 3.188 | 0.063 |
| Maximum | 40.71 | 39.157 | 4.387 | 3.19 | 1.617 |
| Mean | 36.402 | 36.525 | -0.382 | 3.051 | -0.101 |
| Std. Dev. | 2.415 | 1.576 | 3.239 | 0.227 | 1.074 |

A Bo

### 4.4.2 Varioaram Analvsis of Calorific Value (kcal/ka)

The example of calorific value is made by using P2 seam as a representative for the Sin Pun area (see Table 4.15). After simulation it is discovered that lag no. 1 is assigned at a distance between 0 and 240 m , lag no. 2 (the second lag spacing ) is from 240 to 480 m , lag no. 3 from 480 to 720 m , lag no. 4 from 720 to 960 m , lag no. 5 from 960 to 1,200 m, and lag no. 6 from 1,200 to $1,440 \mathrm{~m}$ (see Table 4.24). These ranges of lag spacing are applied to variogram analysis in this study. As shown in Table 4.23, lag no. 1 consists of 6 numbers of pair with the average distance of 185.249 m (computed from distance-column 4 in Table 4.24). The variogram value as estimated based upon these parameters is 279064.400 . It is also noted that the orientation used in this study is based upon the direction or trend, another word N-S orientation means samples being concerned are aligned more or less in the N-S trend. Therefore, the orientation of related samples at $90^{\circ}$ is automatically applied to $270^{\circ}$ for computer calculation. The analysis of P2-seam ash content shows mostly mutual relationships in the N-S direction (90 ) at the tolerance angel of $45^{\circ}$ and with lag spacing of 240 m . These variogram values of parameters are then applied for variogram-model construction as shown in Table 4.23.

In this model, the nugget effect (Co) equals 0 , sill (C) equals 675000, and range is 600 m . Table 4.23 shows a result of variogram parameter values plotted as variogram in Fig. 4.17. Spherical model variogram is obtained from this analysis and it may occur as a result of relationship among samples, shown in Tables 4.23 and 4.24. It is noted that on Table 4.24, pair means relationship between the first and the second data sample points (as 7:06 in the first row in the table, respectively). The $1^{\text {st }}$ value of the second column means value of calorific value of the first sample, the $2^{\text {nd }}$ value of the third column indicates value of the second sample, distance in the forth column is length between two given samples, direction in the fifth column is orientation of the second sample as viewed from the first, and difference ${ }^{2}$ of the last column means square of difference in values [( $1^{\text {st }}-2^{\text {nd }}$ values $\left.)^{2}\right]$ (see also equation 4.1 ).

It is noted that the value in the last column (difference ${ }^{2}$, in Table 4.24 ) are arranged in an increasing order from the top row. Result from Table 4.24 reveals that selected lag results can give rise to the orientation with maximum related sample values at $90^{\circ}$ and its opposite direction, as compared with those of the other orientations (not shown herein). Parameters obtained from variogarm model were then tested by cross validation method (see Table 4.25). Since after estimation, the mean of P2 seam calorific value (2501.000) is different from the mean from the analysis (2488.024), giving rise to the value of difference $(-0.032)$. Except for the Zscores of the minimum value (13.446 ) and the maximum value ( 0.949 ), the other Zscores show rather good result, i.e., close to zero (see Table 4.25). Furthermore, the result of cross validation (Table 4.25) can indicate the search distance used for estimation, since values of the mean of difference and Zscore can be changed basically upon the change in search values. For the ash content of Nong Wa P2 seam, the most appropriate search distance after simulation is 250 m .

For the Saba Yoi area, calorific value is made by using S 2 seam as a representative for the Saba Yoi area (see also Table 4.16). It is discovered that lag no. 1 is between 0 and 180 m , lag no. 2 is between 180 and 360 m , lag no. 3 is between 360 and 540 m , and lag no. 4 is between 540 and 620 m . It is observed, after simulation, that the analysis of S2 seam calorific value shows mostly mutual relationships in the SW-NE direction $\left(45^{\circ}\right)$ at the tolerance angle of $45^{\circ}$ and with lag spacing 180 m . These variogram values of parameters are then applied for variogram model construction.

Fig. 4.18 shows a spherical model simulated from 4 lags and 20 concerned pairs, and average distance and variogram values shown in Table 4.26. In this model, the nugget effect (Co) equals 4000, sill (C) equals 6200, range is 400 m . Table 4.26 shows result of variogram parameters values plotted as variogram in Fig. 4.18 occur as a result of relationship among samples, shown in Tables 4.26 and 4.27. Result from Table 4.27 reveals that selected lag result can give rise to the maximum related sample value at 45
direction (and its opposite direction), compared to those of the other orientations. Parameters obtained from variogarm model were then tested by cross validation method.

After estimation, the mean of S 2 seam calorific value (2225.000) is different from the mean from the analysis (2214.804), giving rise to the value of difference (-14.196). For the calorific value of Ban Khok Ok S2 seam, the most appropriate search distance after simulation is 260 m .

Table 4.23. Result of lag spacing, number of pair average distance at direction $90^{\circ}$ and variogram value for calorific value (kcal/kg), P2 seam, Sin Pun area.

| Lag no. | Pair <br> (no.) | Avg. distance <br> (m) | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 6 | 185.249 | 279064.400 |
| 2 | 27 | 178.210 | 561594.600 |
| 3 | 31 | 610.446 | 680836.400 |
| 4 | พาลิ 15 | 840.604 | 1235443.000 |
| 5 | 8 | 15 | 1072.767 |
| 6 | 8 | 1300.370 | 148247.200 |



Fig. 4.17. Variogram spherical model of calorific value (kcal/kg), P2 seam, Nong Wa deposit, Sin Pun area.

Table 4.24. Selected lag results of calorific value (kcal/kg) at 90 orientation for P 2 seam, Nong Wa deposit, Sin Pun area, using Geo_EAS software.

Lag 1 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 06$ | 3556 | 3659 | 149.852 | 136.842 | 10609 |
| $13: 03$ | 2892 | 2435 | 222.743 | 26.263 | 208849 |
| $10: 08$ | 2592 | 3291 | 212.701 | 177.508 | 488601 |
| $13: 06$ | 2892 | 3659 | 203.625 | 179.912 | 588289 |
| $17: 04$ | 1831 | 2787 | 128.553 | 155.591 | 913936 |
| $10: 06$ | 2592 | 3659 | 151.785 | 215.261 | 1138489 |

Lag 2 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 17:15 | 1831 | 1100 | 312.501 | 344.407 | 534361 |
| 7:04 | 3556 | 2787 | 379.795 | 7.765 | 591361 |
| 15:02 | 1100 | 1888 | 271.066 | 42.355 | 620944 |
| 4:01 | 2787 | 1976 | 265.493 | 33.653 | 657721 |
| 11:09 | 3124 | 2279 | 263.611 | 43.232 | 714025 |
| 17:13 | 1831 | 2892 | 412.392 | 165.393 | 1125721 |
| 7:03 | 3556 | 2435 | 356.052 | 34.32 | 1256641 |
| 13:12 | 2892 | 1761 | 379.27 | 322.775 | 1279161 |
| 6:03 | 3659 | 435 | 415.168 | 13.689 | 1498176 |
| 16:04 | 1398 | 87 | 407.355 | 142.086 | 1929321 |
| 16:05 | 1398 | 835 | 407.219 | 345.785 | 2064969 |
| 15:04 | 1100 | 2787 | 439.977 | 161.84 | 2845969 |
| 16:14 | 1398 | 3121 | $403.504$ | 0.257 | 2968729 |
| 15:05 | 1100 | 2835 | 366.456 | 324.426 | 3010225 |
| 12:07 | 1761 | 3556 | 416.241 | 162.199 | 3222025 |
| 15:14 | 1100 | 3121 | 326.402 | 340.049 | 4084441 |
| 2:01 | 1888 | 1976 ณั่ | ท1410.164 | ลัย 165.655 | 7744 |
| 13:04 | 2892 | 2787 | 286.552 | SI 349.773 | 11025 |
| 10:03 | 2592 | 2435 | 279.639 | 2.177 | 24649 |
| 10:04 | 2592 | 2787 | 387.41 | 339.004 | 38025 |
| 16:12 | 1398 | 1761 | 309.798 | 166.609 | 131769 |
| 13:08 | 2892 | 3291 | 307.927 | 161.602 | 159201 |
| 17:16 | 1831 | 1398 | 283.948 | 316.017 | 187489 |
| 3:01 | 2435 | 1976 | 303.259 | 359.563 | 210681 |
| 16:02 | 1398 | 1888 | 419.183 | 44.885 | 240100 |
| 15:12 | 1100 | 1761 | 400.213 | 185.943 | 436921 |
| 11:03 | 3124 | 2435 | 408.789 | 343.186 | 474721 |

lag 3 for calorific value ( $\mathrm{kcal} / \mathrm{kg}$ )

| Pair* | $1^{\text {st }} \text { Value }$ <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12:05 | 1761 | 2835 | 716.999 | 346.141 | 1153476 |
| 14:01 | 3121 | 1976 | 640.632 | 141.862 | 1311025 |
| 11:01 | 3124 | 1976 | 704.948 | 350.153 | 1317904 |
| 17:14 | 1831 | 3121 | 638.441 | 342.181 | 1664100 |
| 17:11 | 1831 | 3124 | 672.13 | 151.49 | 1671849 |
| 15:03 | 1100 | 2435 | - 576.568 | 150.197 | 1782225 |
| 14:12 | 3121 | 1761 | 708.336 | 174.334 | 1849600 |
| 12:11 | 1761 | 3124 | 665.389 | 137.882 | 1857769 |
| 17:08 | 1831 | 291 | 719.933 | 163.772 | 2131600 |
| 16:13 | 1398 | 2892 | 674.37 | 153.473 | 2232036 |
| 12:08 | 1761 | 3291 | 678.043 | 151.202 | 2340900 |
| 7:01 | 3556 | 1976 | 629.412 | 18.377 | 2496400 |
| 6:01 | 3659 | 1976 | 713.108 | 7.732 | 2832489 |
| 17:07 | 1831 | 3556 | 493.378 | 179.789 | 2975625 |
| 17:06 | 1831 | 3659 | 611.648 | 170.181 | 3341584 |
| 12:06 | 1761 | 3659 | 555.375 | 155.564 | 3602404 |
| 17:02 | 1831 | 1888 | 510.922 | 11.13 | 3249 |
| 12:02 | 1761 | 1888 | 638.95 | 20.529 | 16129 |
| 9:01 | 2279 | 1976 | 585.818 | 329.068 | 91809 |
| 11:04 | 3124 | 2787 | 543.984 | 330.522 | 113569 |
| 8:04 | 3291 | 2787 | 592.97 | 345.54 | 254016 |
| 3:02 | 2435 | 1888 | 708.293 | 351.562 | 299209 |
| 10:01 | 2592 | 1976 | 582.747 | 0.817 | 379456 |
| 17:10 | 1831 | 2592 | 515.792 | 158.153 | 579121 |
| 12:10 | 1761 | 2592 | 496.399 | 140.256 | 690561 |
| 8:03 | 3291 | 2435 | 491.939 | 0.16 | 732736 |
| 6:04 | 3659 | 2787 | 488.315 | 353.983 | 760384 |

lag 3 for calorific value (kcal/kg) (cont.)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $4: 02$ | 2787 | 1888 | 620.047 | 4.208 | 808201 |
| $13: 01$ | 2892 | 1976 | 512.126 | 10.833 | 839056 |
| $17: 05$ | 1831 | 2835 | 668.727 | 333.615 | 1008016 |
| $16: 03$ | 1398 | 2435 | 568.078 | 135.276 | 1075369 |
| $12: 05$ | 1761 | 2835 | 716.999 | 346.141 | 1153476 |

Lag 4 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value | $2^{\text {nd }}$Value <br> $(\%)$ | Distance <br> $(\%)$ | Direction <br> $($ (degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 04$ | 2835 | 2787 | 797.216 | 153.933 | 2304 |
| $14: 04$ | 3121 | 2787 | 766.287 | 161.077 | 111556 |
| $5: 03$ | 2835 | 2435 | 941.888 | 147.955 | 160000 |
| $14: 03$ | 3121 | 2435 | 899.892 | 153.755 | 470596 |
| $13: 02$ | 2892 | 1888 | 900.391 | 359.658 | 1008016 |
| $15: 09$ | 1100 | 2279 | 912.169 | 140.078 | 1390041 |
| $16: 10$ | 1398 | 2592 | 786.125 | 150.331 | 1425636 |
| $8: 01$ | 3291 | 1976 | 795.188 | 359.932 | 1729225 |
| $15: 10$ | 1100 | 2592 | 827.135 | 160.512 | 2226064 |
| $16: 11$ | 1398 | 3124 | 948.815 | 146.911 | 2979076 |
| $15: 13$ | 1100 | 2892 | 724.867 | 164.968 | 3211264 |
| $16: 07$ | 1398 | 3556 | 725.513 | 164.08 | 4656964 |
| $16: 06$ | 1398 | 3659 | 861.482 | 159.514 | 5112121 |
| $15: 07$ | 1100 | 3556 | 798.997 | 173.835 | 6031936 |
| $15: 06$ | 1100 | 3659 | 923.099 | 168.229 | 6548481 |

Lag 5 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 13:05 | 2892 | 2835 | 1075.735 | 338.103 | 3249 |
| 14:13 | 3121 | 2892 | 1050.439 | 163.441 | 52441 |
| 10:05 | 2592 | 2835 | 1183.606 | 335.591 | 59049 |
| 9:02 | 2279 | 1888 | 985.892 | 335.889 | 152881 |
| 14:07 | 3121 | 3556 | 1118.703 | 169.848 | 189225 |
| 14:10 | 3121 | 2592 | 1153.529 | 160.381 | 279841 |
| 10:02 | 2592 | 1888 | 984.495 | 354.561 | 495616 |
| 7:05 | 3556 | 2835 | 1132.617 | 344.693 | 519841 |
| 11:02 | 3124 | 1888 | 1114.314 | 348.498 | 1527696 |
| 8:02 | 3291 | 888 | 1196.965 | 355.085 | 1968409 |
| 7:02 | 3556 | 1888 | 999.388 | 5.559 | 2782224 |
| 6:02 | 3659 | 1888 | $\bigcirc 1104.015$ | 359.705 | 3136441 |
| 16:08 | 1398 | 3291 | 980.171 | 156.019 | 3583449 |
| 15:11 | 1100 | 3124 | $979.218$ | 155.581 | 4096576 |
| 15:08 | 1100 | 3291 | 1032.42 | 163.965 | 4800481 |

Lag 6 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | ล $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14:11 | 3121 | 3124 | 1304.876 | 156.698 | 9 |
| 14:08 | 3121 | 3291 | 1358.243 | 163.024 | 28900 |
| 11:05 | 3124 | 2835 | 1340.627 | 332.55 | 83521 |
| 8:05 | 3291 | 2835 | 1383.215 | 338.881 | 207936 |
| 14:06 | 3121 | 3659 | 1247.046 | 166.095 | 289444 |
| 9:05 | 2279 | 2835 | 1277.872 | 321.324 | 309136 |
| 6:05 | 3659 | 2835 | 1267.046 | 341.526 | 678976 |
| 14:09 | 3121 | 2279 | 1224.031 | 145.304 | 708964 |

Table 4.25. Cross validation for calorific value (kcal/kg) at $90^{\circ}, \mathrm{P} 2$ seam, Nong Wa deposit, Sin Pun area, tested using Geo_EAS program.

Calorific value (kcal/kg)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1100 | 1639.002 | -970.625 | 590.402 | -1.272 |
| 25th \%tile | 1831 | 1918.116 | -482.823 | 621.723 | -0.773 |
| Median | 2435 | 2268.661 | -146.979 | 759.91 | -0.217 |
| 75th \%tile | 2892 | 2968.329 | 334.813 | 797.559 | 0.567 |
| Maximum | 3659 | 3226.813 | 845 | 1125.591 | 0.949 |
| Mean | 2501 | 2488.024 | -13.446 | 753.657 | -0.032 |
| Std. Dev | 753.578 | 542.7 | 519.159 | 136.825 | 0.692 |

Table 4.26. Results of lag spacing, numbers of pair average distance at direction $45^{\circ}$ and variogram value for calorific value ( $\mathrm{kcal} / \mathrm{kg}$ ), S2 seam, Saba Yoi area.

| Lag no. | Pair (no.) | Avg. distance (m) | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 3 | 126.7 .7 | 65142.670 |
| 2 | 6 | 265.607 | 92681.340 |
| 3 | 6 | 461.921 | 102521.500 |
| 4 | 5 | 620.738 | 13366.500 |



Fig. 4.18. Variogram spherical model of calorific value (kcal/kg), S2 seam, Ban Khok Ok deposit, Saba Yoi area.

Table 4.27. Selected lag results of calorific value ( $\mathrm{kcal} / \mathrm{kg}$ ) at 45 orientation for S 2 seam, Ban Khok Ok deposit, Saba Yoi area, using Geo_EAS software.
lag 1 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 05$ | 2323 | 2341 | 121.048 | 83.954 | 324 |
| $5: 04$ | 2341 | 2307 | 108.283 | 190.947 | 1156 |
| $4: 01$ | 2307 | 1683 | 150.88 | 235.395 | 389376 |

lag 2 for calorific value ( $\mathrm{kcal} / \mathrm{kg}$ )

| Pair $^{\star}$ | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 03$ | 2112 | 2167 | 266.047 | 217.613 | 3025 |
| $7: 04$ | 2112 | 2307 | 359.122 | 63.854 | 38025 |

lag 2 for calorific value (kcal/kg) (cont.)

| Pair* $^{\text {nt }}$ Value |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |  |
| $7: 06$ | 2112 | 2323 | 336.071 | 41.472 | 44521 |
| $7: 01$ | 2112 | 1683 | 211.054 | 69.891 | 184041 |
| $6: 01$ | 2323 | 1683 | 180.9 | 187.744 | 409600 |
| $5: 01$ | 2341 | 1683 | 240.451 | 217.013 | 432964 |

lag 3 for calorific value (kcal/kg)

| Pair* | $1^{\text {st }}$ Value | $2^{2^{\text {nd }} \text { Value }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $(\%)$ | $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| $6: 02$ | 2323 | 2288 | 473.799 | 261.473 | 1225 |
| $7: 05$ | 2112 | 2341 | 433.128 | 52.351 | 52441 |
| $8: 06$ | 2579 | 2323 | 535.722 | 23.224 | 65536 |
| $8: 04$ | 2579 | 2307 | 505.729 | 37.958 | 73984 |
| $3: 01$ | 2167 | 1683 | 458.553 | 51.841 | 234256 |
| $8: 01$ | 2579 | 1683 | 364.596 | 30.834 | 802816 |

lag 4 for calorific value ( $\mathrm{kcal} / \mathrm{kg}$ )

| Pair* $^{*}$ | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 02$ | 2341 | 2288 | 594.757 | 261.978 | 2809 |
| $4: 03$ | 2307 | 2167 | 609.216 | 232.721 | 19600 |
| $6: 03$ | 2323 | 2167 | 601.781 | 219.767 | 24336 |
| $5: 03$ | 2341 | 2167 | 693.731 | 226.752 | 30276 |
| $8: 05$ | 2579 | 2341 | 604.205 | 33.289 | 56644 |

Table 4.28. Cross validation for calorific value (kcal/kg) at $45^{\circ}, \mathrm{S} 2$ seam, Ban Khok Ok deposit, Saba Yoi area, tested using Geo_EAS program.

Calorific Value (kcal/kg)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1683 | 2021.234 | -557.766 | 932.835 | -0.507 |
| 25th \%tile | 2112 | 2021.234 | -557.766 | 932.835 | -0.507 |
| Median | 2288 | 2161.012 | -145.988 | 990.465 | -0.156 |
| 75th \%tile | 2323 | 2246.145 | 134.145 | 1083.494 | 0.124 |
| Maximum | 2579 | 2362.603 | 633.170 | 1211.865 | 0.616 |
| Mean | 2225 | 2201.804 | -14.196 | 1047.997 | -0.018 |
| Std. Dev | 258.834 | 112.880 | 378.723 | 92.525 | 0.359 |

### 4.4.3 Variogram Analysis of Moisture Contents (\%)

The example of moisture content is made by using P4 seam as a representative for the Sin Pun area (see Table 4.15). After simulation it is discovered that the lag no. 1 is assigned at a distance between 0 and 310 m , lag no. 2 (the second lag spacing ) is from 310 to 620 m, lag no. 3 from 620 to 930 m, lag no. 4 from 930 to 1,240 m, lag no. 5 from 1,240 to $1,550 \mathrm{~m}$, and lag no. 6 from 1,550 to $1,860 \mathrm{~m}$. These ranges of lag spacing are applied to variogram analysis in this study. As shown in Table 4.29, lag no. 1 consists of 20 numbers of pair with the average distance of 219.096 m (computed from distancecolumn 4 in Table 4.30). The variogram value as estimated based upon these parameters is 18.459 . It is also noted that the orientation used in this study is based upon the direction or trend, another word E-W orientation means samples being concerned are aligned more or less in the E-W trend. Therefore, the orientation of related samples at $0^{\circ}$ is automatically applied to $180^{\circ}$ for computer calculation. The analysis of P4-seam moisture content shows mostly mutual relationships in the WSW - ENE direction (157.5 ) at the tolerance angel of $45^{\circ}$ and with lag spacing of 310 m . These variogram values of parameters are then applied for variogram-model construction and shown in Table 4.29. In this model, the nugget effect (Co) equals 5, sill (C) equals 22.5 , and range is 550 m . Table 4.29 shows a result of variogram parameter values plotted as variogram in Fig. 4.19. Spherical model variogram is encountered using these parameter and occur as a result of relationship among samples, shown in Tables 4.29 and 4.30. It is noted that on the Table 4.30, pair means relationship between the first and the second data sample points (as 17:04 in the first row in the table, respectively). The $1^{\text {st }}$ value of the second column means value of moisture content of the first sample, the $2^{\text {nd }}$ value of the third column indicates value of the second sample, distance in the forth column is length between two given samples, direction in the fifth column is orientation of the second sample as viewed from the first, and difference ${ }^{2}$ of the last column means square of difference in values $\left[\left(1^{\text {st }}-2^{\text {nd }} \text { values }\right)^{2}\right]$ (see also equation 4.1).

It is noted that the value in the last column (difference ${ }^{2}$, in Table 4.31) are arranged in an increasing order from the top row. Result from Table 4.31 reveals that selected lag results can give rise to the orientation with maximum related sample values at $157.5^{\circ}$ and its opposite direction, as compared with those of the other orientations (not shown herein). Parameters obtained from variogarm model were then tested by cross validation method (see Table 4.31).in order to check values obtained from kriging estimation (column3; estimate, Table 4.31). Since after estimation, the mean of P4 seam moisture content (28.266) is different from the mean from the analysis (28.315), giving rise to the value of difference (0.064). Howeyer, for the maximum and minimum values, it is figured out that the cross-validation analysis reveals the rather high Zscores (i.e., 2.271 and -2.361 , respectively, quite large), compared to those of the median and mean values (-0.373 and 0.007 , respectively). Furthermore, the result of cross validation (Table 4.31) can indicate the search distance used for estimation, since values of the mean of difference and Zscore can be changed based upon the change in search values. For the moisture content of Nong Wa P4 seam, the most appropriate search distance after simulation is 150 m .

For the Saba Yoi moisture content is made by using S 3 seam as a representative for the Saba Yoi area (see also Table 4.16). After simulation it is discovered that the lag no. 1 is assigned at a distance between 0 and 330 m , lag no. 2 is from 330 to 660 m , lag no. 3 from 660 to 990 m , lag no. 4 from 990 to 1,320 m, lag no. 5 from 1,320 to 1,650 m, lag no. 6 from 1,650 to 1,980 m, and lag no. 7 from 1,980 to 2,310 m.

It is observed, after simulation, that the analysis of S 3 seam moisture content shows mostly mutual relationships in the SSW-NNE direction (112.5 ${ }^{\circ}$ ) at the tolerance angle of $45^{\circ}$ and with lag spacing 330 m . These variogram values of parameters are then applied for variogram model construction. Fig. 4.20 show a spherical model simulated from 7 lags and 42 concerned pairs, and average distance and variogram values shown in Table 4.32.

In this model, the nugget effect (Co) equals 0, sill (C) equals 26, range is 1400 m . Table 4.32 shows result of variogram parameters values plotted as variogram in Fig. 4.20. After simulation, it is observed that the most appropriate model is gaussian which may occur as a result of relationship among samples, shown in Tables 4.32 and 4.33. Result from Table 4.33 reveals that selected lag result can give rise to the maximum related sample value at 112.5 direction (and its opposite direction), compared to those of the other orientations. Parameters obtained from variogarm model were then tested by cross validation method.

After estimation, the mean of S3 seam moisture content (27.520) is different from the mean from the analysis $(27.890)$, giving rise to the value of difference $(0.37)$. Moreover, the result of cross validation can indicate the search distance used for estimation, since values of the mean of difference and Zscore can be changed based upon the change in search values. It is important to note that the Zscore of the minimum and maximum value are quite high (much deviating from zero).

This gives rise to the high Zscore of the standard deviation (Table 4.34). For the moisture content of Ban Sao S3 seam, the most appropriate search distance after simulation is 150 m .

Table 4.29. Result of lag spacing, number of pair average distance at direction $157.5^{\circ}$ and variogram value for moisture content (\%), P4 seam, Sin Pun area.

| Lag no. | Pair <br> (no.) | Avg. distance <br> $(\mathrm{m})$ | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 20 | 219.096 | 18.459 |
| 2 | 29 | 501.354 | 26.497 |
| 4 | 39 | 749.776 | 42.393 |
| 5 | 10 | 1032.843 | 28.169 |
| 6 | 1 | 1339.982 | 24.162 |



Fig. 4.19. Variogram spherical model of moisture content (\%), P4 seam, Nong Wa deposit, Sin Pun area.

Table 4.30. Selected lag results of moisture content (\%) at 157.5 orientation for P4 seam, Nong Wa deposit, Sin Pun area, using Geo_EAS software.

Lag 1 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 17:04 | 27.97 | 26.51 | 264.959 | 116.009 | 2.132 |
| 4:01 | 26.51 | 24.91 | 260.076 | 326.776 | 2.56 |
| 7:06 | 37.25 | 35.07 | 131.256 | 312.433 | 4.752 |
| 11:09 | 26.11 | 28.41 | 289.316 | 131.462 | 5.29 |
| 15:01 | 27.28 | 24.91 | 149.668 | 133.917 | 5.617 |
| 10:01 | 21.96 | 4.91 | 200.827 | 10.345 | 8.703 |
| 16:01 | 19.91 | 4.91 | 134.492 | 318.353 | 25 |
| 15:10 | 27.28 | 21.96 | 309.798 | 166.609 | 28.302 |
| 17:10 | 27.97 | 21.96 | 113.136 | 148.233 | 36.12 |
| 16:04 | 19.91 | 26.51 | - 128.553 | 155.591 | 43.56 |
| 16:03 | 19.91 | 26.85 | 284.178 | 134.537 | 48.164 |
| 16:15 | 19.91 | 27.28 | 283.948 | 316.017 | 54.317 |
| 11:06 | 26.11 | $35,07$ | $203.625$ | 179.912 | 80.282 |
| 14:12 | 35.25 | 25.81 | 152.376 | 316.895 | 89.114 |
| 11:07 | 26.11 | 37.25 | 307.927 | 161.602 | 124.1 |
| 13:12 | 39.2 | 25.81 | 201.846 | 358.953 | 179.292 |
| 4:03 | 26.51 | 26.85 | 170.577 | 118.828 | 0.116 |
| 11:04 | 26.11 | 26.51 | 286.552 | 349.773 | 0.16 |
| 3:02 | 26.85 | 26.3 | 303.259 | 359.563 | 0.303 |
| 17:15 | 27.97 | 27.28 | 205.549 | 356.601 | 0.476 |

Lag 2 for moisture content (\%)


Lag 3 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14:04 | 35.25 | 26.51 | 828.771 | 169.709 | 76.388 |
| 6:02 | 35.07 | 26.3 | 713.108 | 7.732 | 76.913 |
| 14:02 | 35.25 | 26.3 | 663.695 | 153.592 | 80.103 |
| 17:07 | 27.97 | 37.25 | 791.049 | 150.778 | 86.118 |
| 6:01 | 35.07 | 24.91 | 729.375 | 344.6 | 103.226 |
| 7:02 | 37.25 | 26.3 | 795.188 | 359.932 | 119.903 |
| 7:01 | 37.25 | 24.91 | - 843.383 | 339.847 | 152.276 |
| 13:03 | 39.2 | 26.85 | -899.892 | 153.755 | 152.523 |
| 13:04 | 39.2 | 26.51 | 766.287 | 161.077 | 161.036 |
| 13:02 | 39.2 | . 3 | 640.632 | 141.862 | 166.41 |
| 14:10 | 35.25 | . 96 | 796.022 | 182.196 | 176.624 |
| 10:07 | 21.96 | 7.25 | , 678.043 | 151.202 | 233.784 |
| 16:14 | 19.91 | 35,25 | 704.798 | 352.259 | 235.316 |
| 13:10 | 39.2 | 21.96 | $708.336$ | 174.334 | 297.218 |
| 16:07 | 19.91 | 37.25 | 719.933 | 163.772 | 300.676 |
| 16:13 | 19.91 | 39.2 | 638.441 | 342.181 | 372.104 |
| 9:02 | 28.41 | 26.3 | 704.948 | 350.153 | 4.452 |
| 17:12 | 27.97 | 25.81 | 810.622 | 359.006 | 4.666 |
| 5:02 | 23.23 | 26.3 | 701.85 | 134.867 | 9.425 |
| 5:04 | 23.23 | 26.51 | 797.216 | 153.933 | 10.758 |
| 16:05 | 19.91 | 23.23 | 668.727 | 333.615 | 11.022 |
| 9:01 | 28.41 | 24.91 | 803.684 | 329.311 | 12.25 |
| 8:01 | 28.51 | 24.91 | 773.336 | 310.191 | 12.96 |
| 12:10 | 25.81 | 21.96 | 909.672 | 175.358 | 14.823 |
| 16:12 | 19.91 | 25.81 | 833.738 | 346.187 | 34.81 |
| 10:09 | 21.96 | 28.41 | 665.389 | 137.882 | 41.603 |
| 10:08 | 21.96 | 28.51 | 695.555 | 115.688 | 42.903 |
| 17:06 | 27.97 | 35.07 | 667.742 | 154.325 | 50.41 |
| 17:14 | 27.97 | 35.25 | 705.026 | 7.339 | 52.998 |
| 15:06 | 27.28 | 35.07 | 861.482 | 159.514 | 60.684 |

Lag 3 for moisture content (\%) (cont.)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $16: 09$ | 19.91 | 28.41 | 672.13 | 151.49 | 72.25 |
| $16: 08$ | 19.91 | 28.51 | 640.491 | 128.483 | 73.96 |
| $17: 09$ | 27.97 | 28.41 | 776.95 | 139.381 | 0.194 |
| $12: 02$ | 25.81 | 26.3 | 810.83 | 150.497 | 0.24 |
| $17: 08$ | 27.97 | 28.51 | 793.263 | 120.088 | 0.292 |
| $12: 01$ | 25.81 | 24.91 | 717.558 | 171.207 | 0.81 |
| $15: 11$ | 27.28 | 26.11 | 674.37 | 153.473 | 1.369 |
| $15: 08$ | 27.28 | 28.51 | 922.739 | 130.795 | 1.513 |
| $10: 05$ | 21.96 | 23.23 | 716.999 | 346.141 | 1.613 |

Lag 4 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |  |
| $12: 04$ | 25.81 | 26.51 | 960.39 | 164.776 | 0.49 |
| $12: 03$ | 25.81 | 26.85 | 1085.936 | 158.294 | 1.082 |
| $15: 09$ | 27.28 | 28.41 | 948.815 | 146.911 | 1.277 |
| $11: 05$ | 26.11 | 23.23 | 1075.735 | 338.103 | 8.294 |
| $5: 03$ | 23.23 | 26.85 | 941.888 | 147.955 | 13.104 |
| $14: 03$ | 35.25 | 26.85 | 945.7 | 161.664 | 70.56 |
| $14: 11$ | 35.25 | 26.11 | 1115.323 | 169.725 | 83.54 |
| $15: 07$ | 27.28 | 37.25 | 980.171 | 156.019 | 99.401 |
| $13: 08$ | 39.2 | 28.51 | 1224.031 | 145.304 | 114.276 |
| $13: 11$ | 39.2 | 26.11 | 1050.439 | 163.441 | 171.348 |

Lag 5 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 35.25 | 35.07 | 1316.231 | 171.2932 | 0.180 | 0.032 |
| 25.81 | 26.11 | 1246.103 | 165.924 | 0.300 | 0.090 |
| 39.2 | 37.25 | 1358.243 | 163.0242 | 1.950 | 3.803 |
| 35.25 | 37.25 | 1420.826 | 167.9704 | 2.000 | 4.000 |
| 25.81 | 28.41 | 1493.643 | 159.6314 | 2.600 | 6.760 |
| 25.81 | 28.51 | 1396.542 | 149.8973 | 2.700 | 7.290 |
| 39.2 | 35.07 | 1247.046 | 166.0947 | 4.130 | 17.057 |
| 28.41 | 23.23 | 1340.627 | 332.5497 | 5.180 | 26.83 |
| 28.51 | 23.23 | 1277.872 | 321.324 | 5.280 | 27.879 |
| 35.25 | 28.51 | 1248.543 | 151.4708 | 6.740 | 45.428 |
| 35.25 | 28.41 | 1354.389 | 162.1236 | 6.840 | 46.786 |
| 25.81 | 35.07 | 1444.529 | 167.8766 | 9.260 | 85.748 |
| 39.2 | 28.41 | 1304.876 | 156.6976 | 10.790 | 116.424 |
| 35.07 | 23.23 | 1267.046 | 341.5257 | 11.840 | 140.186 |
| 37.25 | 23.23 | 1383.215 | 338.8813 | 14.020 | 196.560 |

Lag 6 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | Lnd $^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 25.81 | 37.25 | 1553.327 | 165.068 | 11.440 | 130.874 |

Table 4.31. Cross validation for moisture content (\%) at $157.5^{\circ}$, P4 seam, Nong Wa deposit, Sin Pun area, tested using Geo_EAS program.

Moisture Content (\%)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 19.91 | 22.969 | -11.848 | 4.788 | -2.361 |
| 25th \%tile | 24.91 | 25.361 | -3.387 | 5.018 | -0.665 |
| Median | 26.51 | 26.85 | -1.919 | 5.146 | -0.373 |
| 75th \%tile | 28.41 | $\underbrace{30.464}$ | 4.446 | 5.933 | 0.903 |
| Maximum | 39.2 | 37.892 | 12.082 | 6.592 | 2.271 |
| Mean | 28.266 | 28.315 | 0.64 | 5.435 | 0.007 |
| Std. Dev | 5.375 | 3.958 | 6.052 | 0.575 | 1.147 |

Table 4.32. Results of lag spacing, numbers of pair average distance at direction $112.5^{\circ}$ and variogram value for moisture content (\%), S3 seam, Saba Yoi area.

| Lag no. | Pair <br> (no.) | Avg. distance <br> $(\mathrm{m})$. | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 2 | 246.065 | 3.880 |
| 2 | 9 | 538.301 | 4.498 |
| 3 | 8 | 809.871 | 16.943 |
| 4 | 11 | 1160.084 | 22.731 |
| 5 | 5 | 1471.897 | 26.377 |
| 6 | 5 | 1784.327 | 24.812 |
| 7 | 2 | 2112.986 | 63.128 |



Fig. 4.20. Variogram gaussian model of moisture content (\%), S3 seam, Ban Sao deposit, Saba Yoi area.

Table 4.33. Selected lag results of moisture content (\%) at 90 orientation for S 3 seam, Ban Sao deposit, Saba Yoi area, using Geo_EAS software.
lag 1 for moisture content (\%)

| Pair $^{\star}$ | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $11: 06$ | 30.26 | 32.18 | 275.721 | 132.988 | 3.686 |
| $13: 03$ | 27.85 | 31.29 | 216.409 | 254.9 | 11.834 |

lag 2 for moisture content (\%)

| Pair $^{\star}$ | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $9: 08$ | 25.92 | 26.35 | 399.191 | 89.749 | 0.185 |
| $6: 03$ | 32.18 | 31.29 | 440.787 | 248.681 | 0.792 |
| $11: 07$ | 30.26 | 31.61 | 608.5 | 89.929 | 1.823 |
| $12: 05$ | 24.2 | 22.69 | 508.143 | 307.142 | 2.28 |
| $12: 09$ | 24.2 | 25.92 | 548.376 | 337.108 | 2.958 |
| $13: 09$ | 27.85 | 25.92 | 632.157 | 142.015 | 3.725 |

lag 3 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $8: 05$ | 26.35 | 22.69 | 623.905 | 251.291 | 13.396 |
| $4: 02$ | 30.01 | 25.56 | 530.89 | 130.522 | 19.803 |
| $2: 01$ | 25.56 | 19.56 | 552.755 | 134.139 | 36 |
| $13: 08$ | 27.85 | 26.35 | 931.585 | 122.206 | 2.25 |
| $11: 09$ | 30.26 | 25.92 | 880.72 | 153.784 | 18.836 |
| $10: 09$ | 30.28 | 25.92 | 811.737 | 104 | 19.01 |
| $9: 03$ | 25.92 | 31.29 | 743.544 | 306.461 | 28.837 |
| $8: 06$ | 26.35 | 32.18 | 839.348 | 315.667 | 33.989 |
| $7: 02$ | 31.61 | 25.56 | 799.003 | 90.161 | 36.603 |
| $10: 05$ | 30.28 | 22.69 | 714.769 | 123.523 | 57.608 |
| $5: 03$ | 22.69 | 31.29 | 758.261 | 327.604 | 73.96 |
| $11: 04$ | 30.26 | 30.01 | 1061.056 | 71.115 | 0.063 |
| $13: 12$ | 27.85 | 24.2 | 1170.36 | 149.023 | 13.322 |
| $11: 08$ | 30.26 | 26.35 | 1114.842 | 135.005 | 15.288 |

lag 4 for moisture content (\%)

| Pair* | $1{ }^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10:08 | 30.28 | 26.35 | 1202.665 | 99.313 | 15.445 |
| 8:03 | 26.35 | 31.29 | 1089.997 | 293.815 | 24.404 |
| 12:10 | 24.2 | 30.28 | 1222.32 | 305.027 | 36.966 |
| 6:02 | 32.18 | 25.56 | 1220.15 | 81.208 | 43.824 |
| 8:01 | 26.35 | 19.56 | 1092.558 | 68.415 | 46.104 |
| 12:03 | 24.2 | 31.29 | 1247.059 | 319.415 | 50.268 |
| 4:01 | 30.01 | 19.56 | 1083.105 | 132.367 | 109.203 |
| 7:01 | 31.61 | 19.56 | 1256.815 | 107.943 | 145.203 |

lag 5 for moisture content (\%)

| Pair* $^{2^{\text {st }} \text { Value }}$Value <br> $(\%)$ | Distance <br> $(\%)$ | Direction <br> $(\mathrm{m})$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (degree) |  |  |  |

lag 6 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 01$ | 22.69 | 19.56 | 1715.962 | 69.46 | 9.797 |
| $10: 02$ | 30.28 | 25.56 | 1900.69 | 71.844 | 22.278 |
| $3: 02$ | 31.29 | 25.56 | 1653.211 | 77.893 | 32.833 |
| $13: 01$ | 27.85 | 19.56 | 1806.664 | 93 | 68.724 |
| $11: 01$ | 30.26 | 19.56 | 1845.109 | 102.089 | 114.49 |

lag 7 for moisture content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $10: 01$ | 30.28 | 19.56 | 2212.484 | 84.623 | 114.918 |
| $3: 01$ | 31.29 | 19.56 | 2013.487 | 91.087 | 137.593 |

Table 4.34. Cross validation for moisture content (\%) at $112.5^{\circ}$, S3 seam, Ban Sao deposit, Saba Yoi area, tested using Geo_EAS program.

Moisture Content (\%)

| Value | Variable | Estimate | Difference | Kriging Sta. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 19.56 | 25.415 | -4.66 | 1.474 | -1.906 |
| 25th \%tile | 24.2 | 26.503 | -2.314 | 2.417 | -0.643 |
| Median | 26.35 | 27.25 | -0.145 | 3.404 | -0.028 |
| 75th \%tile | 30.26 | 28.036 | 0.811 | 4.525 | 0.294 |
| Maximum | 32.181 | 30.773 | 8.476 | 5.615 | 1.87 |
| Mean | 27.52 | 27.89 | 0.37 | 3.629 | 0.023 |
| Std. Dev. | 3.868 | 1.672 | 3.452 | 1.352 | 1.122 |

### 4.4.4 Varioaram Analysis of Sulphur Contents (\%)

The example of sulphur content is made by using P3 seam as a representative for the Sin Pun area (see Table 4.15). After simulation six lag numbers are recognized and it is discovered that the lag no. 1 is assigned at a distance between 0 and 210 m , lag no. 2 (the second lag spacing ) is from 210 to 420 m , lag no. 3 from 420 to 630 m , lag no. 4 from 630 to 840 m , lag no. 5 from 840 to 1,050 m, lag no. 6 from 1,050 to 1,260 m, lag no. 7 from 1,260 to 1,470 m, lag no. 8 from 1,470 to 1,680 m, lag no. 9 from 1,680 to 1,890 m, lag no. 10 from 1,890 to 2,100 m, and lag no. 11 from 2,100 to $2,310 \mathrm{~m}$. These ranges of lag spacing are applied to variogram analysis in this study. As shown in Table 4.35, lag no. 1 consists of 11 numbers of pair with the average distance of 164.630 m (computed from distance-column 4 in Table 4.36).

The variogram value as estimated based upon these parameters is 3.957 . It is also noted that the orientation used in this study is based upon the direction or trend, another word E-W orientation means samples being concerned are aligned more or less in the E-W trend. Therefore, the orientation of related samples at $0^{\circ}$ is automatically applied to $180^{\circ}$ for computer calculation. The analysis of P3-seam sulphur content show mostly mutual relationships in the WSW - ENE direction ( $157.5^{\circ}$ ) at the tolerance angel of $45^{\circ}$ and with lag spacing 310 m . These variogram values of parameters are then applied for variogram-model construction.

As shown in Table 4.35. In this model, the nugget effect (Co) equals 2.3, sill (C) equals 3 , and range is 650 m . Table 4.35 shows a result of variogram parameter values plotted as variogram in Fig. 4.21. Spherical model is considered to be the most appropriate and may occur as a result of relationship among samples, shown in Tables 4.35 and 4.36. It is noted that on Table 4.36, pair means relationship between the first and the second data sample points (as $6: 05$ in the first row in the table, respectively). The $1^{\text {st }}$ value of the second column means value of sulphur content of the first sample, the $2^{\text {nd }}$ value of the third column indicates value of the second sample, distance in the
forth column is length between two given samples, direction in the fifth column is orientation of the second sample as viewed from the first, and difference ${ }^{2}$ of the last column means square of difference in values $\left[\left(1^{\text {st }}-2^{\text {nd }} \text { values }\right)^{2}\right]$ (see also equation 4.1 ). It is noted that the value in the last column (difference ${ }^{2}$, in Table 4.37 ) are arranged in an increasing order from the top row. Result from Table 4.37 reveals that selected lag results can give rise to the orientation with maximum related sample values at $157.5^{\circ}$ and its opposite direction, as compared with those of the other orientations (not shown herein). Parameters obtained from variogarm model were then tested by cross validation method. Since after estimation, the mean of P3 seam sulphur content (4.81) is different from the mean from the analysis (4.57), giving rise to the value of difference ( -0.087 ). Furthermore, the result of cross validation (Table 4.37) can indicate the search distance used for estimation, since values of the mean of difference and Zscore can be changed based upon the change in search values. For the sulphur content of Nong Wa P3 seam, the most appropriate search distance after simulation is 200 m .

For the Saba Yoi, sulphur content data is made by using S 1 seam as a representative for the Sâba Yoi area (see also Table 4.16). It is observed, after simulation, that the analysis of S4 seam sulphur content shows mostly mutual relationships in the SSW-NNE direction $\left(112.5^{\circ}\right)$ at the tolerance angle of $45^{\circ}$ and with lag spacing 160 m . These variogram values of parameters are then applied for variogram model construction. Fig. 4.20 shows a spherical model simulated from 5 lags and 15 concerned pairs, and average distance and variogram values shown in Table 4.32. In this model, the nugget effect (Co) equals 0.21 , sill (C) equals 0.02 , range is 610 m . Table 4.38 shows result of variogram parameters values plotted as variogram in Fig. 4.22. After simulation, the spherical model is encountered and may occur as a result of relationship among samples, shown in Tables 4.38 and 4.39. Result from Table 4.38 reveals that selected lag result can give rise to the maximum related sample value at 90 direction (and opposite), compared to those of the other orientations.

Parameters obtained from variogarm model were then tested by cross validation method. After estimation, the mean of S4 seam sulphur content (4.810) is different from
the mean from the analysis (4.570), giving rise to the value of difference ( -0.240 ). For the sulphur content of Ban Khok Ok S4 seam, the most appropriate search distance after simulation is 150 m .

Table 4.35. Result of lag spacing, number of pair average distance at direction $157.5^{\circ}$ and variogram value for sulphur content (\%), P3 seam, Sin Pun area.

| Lag no. | Pair (no.) | Avg. distance <br> (m) | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 11 | 164.630 | 3.957 |
| 2 | 22 | 339.374 | 4.844 |
| 3 | 20 | 541.101 | 6.053 |
| 4 |  | $0 \times 726.172$ | 5.116 |
| 5 |  | $\bigcirc 932.530$ | 10.800 |
| 6 |  | 1160.827 | 6.516 |
| 7 |  | 1361.497 | 5.494 |
| 8 | จชา 2 งกรถ | มทา 1523.485 ย | . 934 |



Fig. 4.21. Variogram spherical model of sulphur content (\%), P3 seam, Nong Wa deposit, Sin Pun area.

Table 4.36. Selected lag results of sulphur content (\%) at 157.5 orientation for P3 seam, Nong Wa deposit, Sin Pun area, using Geo_EAS software.

Lag 1 for sulphur content (\%)
$\left.\begin{array}{|c|c|c|c|c|c|}\hline \text { Pair* } & 1^{\text {st }} \text { Value } & 2^{\text {nd }} \text { Value } \\ (\%) & \text { Distance } \\ (\%) & \begin{array}{c}\text { Direction } \\ (m)\end{array} & \text { Difference }^{2} \\ \text { (degree) }\end{array}\right]$

Lag 2 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 15:14 | 1.13 | 2.09 | 326.402 | 340.049 | 0.922 |
| 4:01 | 5.09 | 3.73 | 260.076 | 326.776 | 1.85 |
| 12:11 | 2.01 | 3.4 | 379.27 | 322.775 | 1.932 |
| 8:03 | 5.44 | 6.99 | 359.151 | 303.696 | 2.402 |
| 9:04 | 2.94 | 5.09 | - 387.41 | 339.004 | 4.623 |
| 15:11 | 1.13 | 3.4 | 400.213 | 185.943 | 5.153 |
| 6:04 | 7.89 | 5.0 | 379.795 | 7.765 | 7.84 |
| 12:04 | 2.01 | 5.09 | 286.552 | 349.773 | 9.486 |
| 3:01 | 6.99 | . 73 | 418.467 | 315.762 | 10.628 |
| 9:03 | 2.94 | 6.99 | 279.639 | 2.177 | 16.402 |
| 9:07 | 2.94 | 7.16 | $212.701$ | 177.508 | 17.808 |
| 11:06 | 3.4 | $\underline{7.89}$ | 416.241 | 162.199 | 20.16 |
| 12:10 | 2.01 | 7.01 | 289.316 | 131.462 | 25 |
| 12:07 | 2.01 | 7.16 | 307.927 | 161.602 | 26.522 |
| 16:03 | 1.8 | 6.99 | 284.178 | 134.537 | 26.936 |
| 15:02 | 1.13 | 6.97 | 345.878 | 124.732 | 34.106 |
| 3:02 | 6.99 | 6.97 | 303.259 | 359.563 | 0 |
| 10:03 | 7.01 | 6.99 | 408.789 | 343.186 | 0 |
| 16:12 | 1.8 | 2.01 | 412.392 | 165.393 | 0.044 |
| 5:03 | 7.59 | 6.99 | 415.168 | 13.689 | 0.36 |
| 16:15 | 1.8 | 1.13 | 312.501 | 344.407 | 0.449 |
| 7:06 | 7.16 | 7.89 | 280.9 | 314.784 | 0.533 |

Lag 3 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }}$ Value <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 16:09 | 1.8 | 2.94 | 515.792 | 158.153 | 1.3 |
| 8:02 | 5.44 | 6.97 | 585.818 | 329.068 | 2.341 |
| 14:01 | 2.09 | 3.73 | 518.268 | 168.198 | 2.69 |
| 12:01 | 2.01 | 3.73 | 535.683 | 338.839 | 2.958 |
| 10:04 | 7.01 | 5.09 | ) 543.984 | 330.522 | 3.686 |
| 7:04 | 7.16 | 5.09 | 592.97 | 345.54 | 4.285 |
| 5:04 | 7.59 | 5.09 | 488.315 | 353.983 | 6.25 |
| 15:04 | 1.13 |  | 439.977 | 161.84 | 15.682 |
| 9:02 | 2.94 | 6.97 | 582.747 | 0.817 | 16.241 |
| 6:01 | 7.89 | 3.73 | 600.835 | 351.271 | 17.306 |
| 11:05 | 3.4 | 7.59 | $555.375$ | 155.564 | 17.556 |
| 15:13 | 1.13 | 5.72 | 521.477 | 347.253 | 21.068 |
| 12:02 | 2.01 | 6.97 | 512.126 | 10.833 | 24.602 |
| 16:05 | 1.8 | 7.59 | 611.648 | 170.181 | 33.524 |
| 15:03 | 1.13 | 6.99 | 576.568 | 150.197 | 34.34 |
| 16:06 | 1.8 | 7.89 | 493.378 | 179.789 | 37.088 |
| 7:03 | 7.16 | 6.99 | 491.939 | 0.16 | 0.029 |
| 8:04 | 5.44 | 5.09 | 529.311 | 302.129 | 0.122 |
| 11:09 | 3.4 | 2.94 | 496.399 | 140.256 | 0.212 |
| 6:02 | 7.89 | 6.97 | 629.412 | 18.377 | 0.846 |

Lag 4 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value | $2^{\text {nd }}$ Value | Distance | Direction | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14:11 | 2.09 | 3.4 | 708.336 | 174.334 | 1.716 |
| 8:01 | 5.44 | 3.73 | 773.336 | 310.191 | 2.924 |
| 15:09 | 1.13 | 2.94 | 827.135 | 160.512 | 3.276 |
| 13:01 | 5.72 | 3.73 | 717.558 | 171.207 | 3.96 |
| 11:08 | 3.4 | 5.44 | 695.555 | 115.688 | 4.162 |
| 14:04 | 2.09 | 5.09 | 766.287 | 161.077 | 9 |
| 10:01 | 7.01 | 3.73 | 803.684 | 329.311 | 10.758 |
| 11:10 | 3.4 | 7.01 | 665.389 | 137.882 | 13.032 |
| 16:08 | 1.8 | 44 | 640.491 | 128.483 | 13.25 |
| 11:07 | 3.4 | 16 | 678.043 | 151.202 | 14.138 |
| 5:01 | 7.59 |  | $729.375$ | 344.6 | 14.9 |
| 16:13 | 1.8 | 5.72 | $833.738$ | 346.187 | 15.366 |
| 14:02 | 2.09 | 6.97 | ( 640.632 | 141.862 | 23.814 |
| 16:10 | 1.8 | 7.01 | 672.13 | 151.49 | 27.144 |
| 16:07 | 1.8 | 7.16 | 719.933 | 163.772 | 28.73 |
| 15:06 | 1.13 | 7.89 | 798.997 | 173.835 | 45.698 |
| 10:02 | 7.01 | 6.97 | 704.948 | 350.153 | 0.002 |
| 7:02 | 7.16 | 6.97 | 795.188 | 359.932 | 0.036 |
| 16:14 | 1.8 | 2.09 | 638.441 | 342.181 | 0.084 |
| 5:02 | 7.59 | 6.97 | 713.108 | 7.732 | 0.384 |
| 9:01 | 2.94 | 3.73 | 643.947 | 334.096 | 0.624 |
| 15:12 | 1.13 | 2.01 | 724.867 | 164.968 | 0.774 |
| 13:02 | 5.72 | 6.97 | 810.83 | 150.497 | 1.563 |

Lag 5 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value | $2^{\text {nd }}$ Value | Distance | Direction | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $13: 04$ | 5.72 | 5.09 | 960.39 | 164.776 | 0.397 |
| $13: 11$ | 5.72 | 3.4 | 909.672 | 175.358 | 5.382 |
| $7: 01$ | 7.16 | 3.73 | 843.383 | 339.847 | 11.765 |
| $15: 08$ | 1.13 | 5.44 | 912.169 | 140.078 | 18.576 |
| $14: 03$ | 2.09 | 6.99 | 899.892 | 153.755 | 24.01 |
| $15: 10$ | 1.13 | 7.01 | 979.218 | 155.581 | 34.574 |
| $15: 07$ | 1.13 | 7.16 | 1032.42 | 163.965 | 36.361 |
| $15: 05$ | 1.13 | 7.59 | 923.099 | 168.229 | 41.732 |

Lag 6 for sulphur content (\%)

| Pair* | $1^{\text {st }}$Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $14: 12$ | 2.09 | 2.01 | 1050.439 | 163.441 | 0.006 |
| $14: 09$ | 2.09 | 2.94 | 1153.529 | 160.381 | 0.723 |
| $13: 03$ | 5.72 | 6.99 | 1085.936 | 158.294 | 1.613 |
| $14: 08$ | 2.09 | 5.44 | 1224.031 | 145.304 | 11.223 |
| $13: 12$ | 5.72 | 2.01 | 1246.103 | 165.924 | 13.764 |
| $14: 05$ | 2.09 | 7.59 | 1247.046 | 166.095 | 30.25 |
| $14: 06$ | 2.09 | 7.89 | 1118.703 | 169.848 | 33.64 |

Lag 7 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $13: 08$ | 5.72 | 5.44 | 1396.542 | 149.897 | 0.078 |
| $13: 05$ | 5.72 | 7.59 | 1444.529 | 167.877 | 3.497 |
| $13: 06$ | 5.72 | 7.89 | 1318.393 | 171.236 | 4.709 |
| $13: 09$ | 5.72 | 2.94 | 1346.399 | 163.118 | 7.728 |

Lag 7 for sulphur content (\%) (cont.)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $14: 10$ | 2.09 | 7.01 | 1304.876 | 156.698 | 24.206 |
| $14: 07$ | 2.09 | 7.16 | 1358.243 | 163.024 | 25.705 |

Lag 8 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> (\%) | $2^{\text {nd }} \text { Value }$ <br> (\%) | Distance <br> (m) | Direction <br> (degree) | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 13:10 | 5.72 |  | 1493.643 | 159.631 | 1.664 |
| 13:07 | 5.72 |  | 1553.327 | 165.068 | 2.074 |

Table 4.37 Cross validation for sulphur content (\%) at $157.5^{\circ}$, P3 seam, Nong Wa deposit, Sin Pun area, tested using Geo_EAS program.

Sulphur Content (\%)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1.13 | 1.753 | -3.967 | 2.256 | -1.504 |
| 25th \%tile | 2.09 | 3.911 | -2.709 | 2.319 | -1.144 |
| Median | 5.09 | 4.428 | -1.185 | 2.389 | -0.525 |
| 75th \%tile | 6.99 | 5.305 | 2.053 | 2.854 | 0.815 |
| Maximum | 7.89 | 6.97 | 3.991 | 3.406 | 1.765 |
| Mean | 4.81 | 4.57 | -0.24 | 2.499 | -0.087 |
| Std. Dev. | 2.349 | 1.403 | 2.585 | 0.285 | 1.068 |

Table 4.38. Results of lag spacing, numbers of pair average distance at direction $90^{\circ}$ variogram value for sulphur content (\%),

S2 seam, Ban Khok Ok deposit, Saba Yoi area.

| Lag no. | Pair <br> $($ no. $)$ | Avg. distance <br> $(\mathrm{m})$. | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 3 | 136.246 |  |
| 2 | 3 | 231.006 | .016 |
| 3 | 5 | 436.394 | .047 |
| 4 | 3 | 590.942 | .066 |
| 5 | 1 | 693.731 | .077 |



Fig. 4.22. Variogram spherical model of sulphur content (\%), S2 seam, Ban Khok Ok deposit, Saba Yoi area.

Table 4.39. Selected lag results of sulphur content (\%) at 90 orientation for S2 seam, Ban Khok Ok deposit, Saba Yoi area, using Geo_EAS software.
lag 1 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 04$ | 1.720 | 1.690 | 136.808 | 133.149 | 0.001 |
| $4: 01$ | 1.690 | 1.620 | 150.880 | 235.395 | 0.005 |
| $6: 05$ | 1.720 | 1.420 | 121.048 | 83.954 | 0.09 |

lag 2 for sulphur content (\%)

| Pair* $^{1^{\text {st }} \text { Value }}$(\%d <br> $(\%)$ | $2^{\text {Value }}$ <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $8: 03$ | 1.280 | 1.270 | 176.217 | 279.720 | 0.000 |
| $7: 01$ | 1.720 | 1.620 | 211.054 | 69.891 | 0.01 |
| $7: 02$ | 1.720 | 1.200 | 305.747 | 306.430 | 0.27 |

lag 3 for sulphur content (\%)

| Pair* $^{\text {1st }}$Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 04$ | 1.720 | 1.690 | 359.122 | 63.854 | 0.001 |
| $7: 05$ | 1.720 | 1.420 | 433.128 | 52.351 | 0.090 |
| $3: 01$ | 1.270 | 1.620 | 458.553 | 51.841 | 0.123 |
| $2: 01$ | 1.200 | 1.620 | 457.366 | 103.787 | 0.176 |
| $6: 02$ | 1.720 | 1.200 | 473.799 | 261.473 | 0.27 |

lag 4 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 02$ | 1.420 | 1.200 | 594.757 | 261.978 | .048 |
| $4: 03$ | 1.690 | 1.270 | 609.216 | 232.721 | .176 |
| $4: 02$ | 1.690 | 1.200 | 658.853 | 272.349 | .240 |

lag 5 for sulphur content (\%)

| Pair* | $1^{\text {st }}$ Value |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $(\%)$ | $\sum^{2^{\text {nd }} \text { Value }}$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference ${ }^{2}$ |  |
| $5: 03$ | 1.420 | 1.270 | 693.731 | 226.752 | .022 |

Table 4.40. Cross validation for sulphur content (\%) at $90^{\circ}$, S2 seam, Ban Khok Ok deposit, Saba Yoi area, tested using Geo_EAS program.

Sulphur Content (\%)

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1.200 | 1.270 | -.236 | .191 | -.993 |
| 25th \%tile | 1.270 | 1.280 | -.190 | .206 | -.752 |
| Median | 1.420 | 1.500 | -.010 | .239 | -.027 |
| 75th \%tile | 1.690 | 1.668 | .048 | .321 | .199 |
| Maximum | 1.720 | 1.695 | .492 | .368 | 1.532 |
| Mean | 1.490 | 1.581 | .028 | .279 | .074 |
| Std. Dev | .222 | .171 | .249 | .072 | .941 |

### 4.4.5 Varioaram Analvsis of Density (g/cc)

The example of density is made by using $M$ seam as a representative for the Sin Pun area (see Table 4.15). After simulation it is discovered the lag no. 1 is assigned at a distance between 0 and 190 m , lag no. 2 (the second lag spacing) is from 190 to 380 m , lag no. 3 from 380 to 570 m , lag no. 4 from 570 to 760 m , lag no. 5 from 760 to 950 m , lag no. 6 from 950 to $1,140 \mathrm{~m}$, lag no. 7 from 1,140 to 1,330 m, and lag no. 8 from 1,330 to $1,520 \mathrm{~m}$ (see Table 4.41). These ranges of lag spacing are applied to variogram analysis in this study. As shown in Table 4.15, lag no. 1 consists of 1 number of pair with the average distance of 131.256 m (computed from distance-column 4 in Table 4.16).

The variogram value as estimated based upon these parameters is 0.002 . It is also noted that the orientation used in this study is based upon the direction or trend, another word E-W orientation means samples being concerned are aligned more or less in the E-W trend. Therefore, the orientation of related samples at $0^{\circ}$ is automatically applied to $180^{\circ}$ for computer calculation. The analysis of M -seam density show mostly mutual relationships in the WSW - ENE direction (157.5 ${ }^{\circ}$ ) at the tolerance angel of $45^{\circ}$ and with lag spacing 190 m . These variogram values of parameters are then applied for variogram-model construction. As shown in Table 4.41. In this model, the nugget effect (Co) equals 0 , sill (C) equals 0.012 , and range is 700 m . Table 4.41 shows a result of variogram parameter values plotted as variogram in Fig. 4.23. Spherical model is recognized from the analysis and the model may occur as a result of relationship among samples, shown in Tables 4.41 and 4.42. It is noted that on the table 4.42, pair means relationship between the first and the second data sample points (as $6: 05$ in the first row in the table, respectively). The $1^{\text {st }}$ value of the second column means value of density of the first sample, $2^{\text {nd }}$ value of the third column indicates value of the second sample, distance in the forth column is length between two given samples, direction in the fifth column is orientation of the second sample as viewed from the first, and difference ${ }^{2}$ of the last column means square of difference in values $\left[\left(1^{\text {st }}-2^{\text {nd }} \text { values }\right)^{2}\right]$ (see also
equation 4.1 ). It is noted that the value in the last column (difference ${ }^{2}$, in Table 4.43 ) are arranged in an increasing order from the top row.

Result from Table 4.43 reveals that selected lag results can give rise to the orientation with maximum related sample values at $157.5^{\circ}$ and its opposite direction, as compared with those of the other orientations (not shown herein). Parameters obtained from variogarm model were then tested by cross validation method (see Table 4.43). Since after estimation, the mean of $M$ seam density (1.372) is different from the mean from the analysis (1.393), giving rise to the value of difference (0.021). It is also visualized from Table 4.43 that only the Zscore of the maximum value is deviate from zero, the rest of the values are satisfied, giving rise to the more reliable of the analysis. Furthermore, the result of cross validation can indicate the search distance used for estimation, since values of the mean of difference and Zscore can be changed based upon the change in search values. For the density of Nong Wa M seam, the most appropriate search distance after simulation is 420 m .

For the Saba Yoi density is made by using S4 seam as a representative for the Saba Yoi area (see also Table 4.16). After simulation it is discovered the lag no. 1 is between 0 and 320 m , lag no. 2 is between 320 and 640 m , lag no. 3 is between 640 and 960 m , lag no. 4 is between 960 and 1,280 m, and lag no. 5 is between 1,280 and 1,600 m . It is observed, after simulation, that the analysis of S4 seam density shows mostly mutual relationships in the N -S direction $\left(90^{\circ}\right)$ at the tolerance angle of $45^{\circ}$ and with lag spacing 320 m . These variogram values of parameters are then applied for variogram model construction. Fig. 4.24 shows a spherical model simulated from 5 lags and 10 concerned pairs, and average distance and variogram values shown in Table 4.44.

In this model, the nugget effect (Co) equals 0.0001 , sill (C) equals 0.0018 , range is 1100 m . Table 4.44 shows result of variogram parameters values plotted as variogram in Fig. 4.24, After simulation, it is found out that the most satisfied model is spherical, which may occur as a result of relationship among samples, shown in Tables 4.44 and 4.45 .

Result from Table 4.21 reveals that selected lag result can give rise to the maximum related sample value at 90 direction (and opposite), compared to those of the other orientations. Parameters obtained from variogarm model were then tested by cross validation method. After estimation, the mean of S4 seam density (27.388) is different from the mean from the analysis (27.206), giving rise to the value of difference (0.182). For the density of Ban Sao S4 seam, the most appropriate search distance after simulation is 270 m .

Table 4.41. Result of lag spacing, number of pair average distance at direction $157.5^{\circ}$ and variogram value for density ( $\mathrm{g} / \mathrm{cc}$ ), M seam, Sin Pun area.

| Lag no. | Pair | Avg. distance | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 1 | $(\mathrm{~m})$ |  |
| 2 | 3 | 131.256 | 0.002 |
| 3 | 7 | 340.711 | 0.015 |
| 4 | 7 | 444.088 | 0.009 |
| 5 | 3 | 665.995 | 0.011 |
| 7 | 2 | 1038.869 | 0.012 |
| 8 | 1 | 1232.005 | 0.027 |
|  |  | 1383.215 | 0.012 |



Fig. 4.23. Variogram spherical model of density ( $\mathrm{g} / \mathrm{cc}$ ), M seam, Nong Wa deposit, Sin Pun area.

Table 4.42. Selected lag results of density ( $\mathrm{g} / \mathrm{cc}$ ) at 0 orientation for $M$ seam Nong Wa deposit, Sin Pun area, using Geo_EAS software.

Lag 1 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 05$ | 1.220 | 1.290 | 131.256 | 312.433 | 0.005 |

Lag 2 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $8: 04$ | 1.430 | 1.390 | 366.456 | 324.426 | 0.002 |
| $9: 07$ | 1.540 | 1.330 | 309.798 | 166.609 | 0.044 |
| $8: 1$ | 1.430 | 1.220 | 345.878 | 124.732 | 0.044 |

Lag 3 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $9: 03$ | 1.54 | 1.52 | 407.355 | 142.086 | 0 |
| $7: 05$ | 1.33 | 1.29 | 555.375 | 155.564 | 0.002 |
| $8: 03$ | 1.43 | 1.52 | 439.977 | 161.84 | 0.008 |
| $8: 07$ | 1.43 | 1.33 | 400.213 | 185.943 | 0.01 |
| $9: 04$ | 1.54 | 1.39 | 407.219 | 345.785 | 0.022 |
| $2: 01$ | 1.41 | 1.22 | 410.164 | 165.655 | 0.036 |
| $5: 03$ | 1.29 | 1.52 | 488.315 | 353.983 | 0.053 |

Lag 4 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ <br> Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 04$ | 1.33 | 1.39 | 716.999 | 346.141 | 0.004 |
| $7: 01$ | 1.29 | 1.22 | 713.108 | 7.732 | 0.005 |
| $7: 02$ | 1.33 | 1.41 | 638.950 | 20.529 | 0.006 |
| $7: 06$ | 1.33 | 1.22 | 678.043 | 151.202 | 0.012 |
| $3: 02$ | 1.52 | 1.41 | 620.047 | 4.208 | 0.012 |
| $4: 01$ | 1.39 | 1.22 | 701.850 | 134.867 | 0.029 |
| $6: 03$ | 1.22 | 1.52 | 592.970 | 345.540 | 0.090 |

Lag 5 for density (g/cc)

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 01$ | 1.220 | 1.220 | 795.188 | 359.932 | 0.000 |
| $4: 03$ | 1.390 | 1.520 | 797.216 | 153.933 | 0.017 |
| $8: 05$ | 1.430 | 1.290 | 923.099 | 168.229 | 0.020 |
| $9: 09$ | 1.540 | 1.290 | 861.482 | 159.514 | 0.063 |

Lag 6 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 02$ | 1.220 | 1.410 | 1104.015 | 359.932 | 0.014 |
| $8: 06$ | 1.430 | 1.220 | 1032.420 | 163.965 | 0.044 |
| 8.06 | 1.540 | 1.220 | 980.171 | 156.019 | 0.120 |

Lag 7 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $5: 04$ | 1.290 | 1,390 | 1267.046 | 341.526 | 0.010 |
| $6: 02$ | 1.220 | 1.410 | 196.965 | 355.085 | 0.036 |

Lag 8 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair * | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 04$ | 1.220 | 1.390 | 1383.215 | 338.881 | 0.029 |

Table 4.43. Cross validation for density (g/cc) at $0^{\circ}$, M seam, Nong Wa deposit, Sin Pun area, tested using Geo_EAS program.

Density ( $\mathrm{g} / \mathrm{cc}$ )

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1.220 | 1.281 | -.239 | .085 | -2.566 |
| 25th \%tile | 1.220 | 1.289 | -.163 | .086 | -1.884 |
| Median | 1.330 | 1.341 | -.001 | .092 | -.014 |
| 75th \%tile | 1.410 | 1.476 |  | .086 | .096 |
| Maximum | 1.540 | 1.498 | .265 | .124 | .694 |
| Mean | 1.372 | 1.393 | .021 | .098 | 2.500 |
| Std. Dev | 0.117 | 0.092 | .158 | .013 | .157 |

Table 4.44. Results of lag spacing, numbers of pair average distance at direction $112.5^{0}$ and variogram value for density (g/cc), S4 seam, Saba Yoi area.

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| Lag no. | Pair (no.) | Avg. distance (m.) | Estimate |
| :---: | :---: | :---: | :---: |
| 1 | 3 | 232.840 | 0.001 |
| 2 | 2 | 528.237 | 0.001 |
| 3 | 3 | 828.838 | 0.003 |
| 4 | 2 | 1038.402 | 0.002 |



Fig. 4.24. Variogram linear modet of density ( $\mathrm{g} / \mathrm{cc}$ ), S 4 seam, Ban Sao deposit, Saba Yoi area.

Table 4.45. Selected lag results of density ( $\mathrm{g} / \mathrm{cc}$ ) at 0 orientation for S 4 seam Ban Sao deposit, Saba Yoi area, using Geo_EAS software.
lag 1 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6: 01$ | 1.410 | 1.390 | 216.409 | 254.900 | 0.000 |
| $5: 03$ | 1.390 | 1.410 | 275.721 | 132.988 | 0.000 |
| $4: 03$ | 1.460 | 1.410 | 206.389 | 88.438 | 0.003 |

lag 2 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $3: 01$ | 1.410 | 1.390 | 440.787 | 248.681 | 0.000 |
| $7: 03$ | 1.350 | 1.410 | 615.688 | 281.061 | 0.004 |

lag 3 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$ Value <br> $(\%)$ | Distance <br> $(m)$ | Direction <br> (degree) | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 05$ | 1.350 | 1.390 | 862.118 | 290.799 | 0.002 |
| $7: 06$ | 1.350 | 1.410 | 806.063 | 271.902 | 0.004 |
| $7: 04$ | 1.350 | 1.460 | 818.332 | 277.902 | 0.012 |

lag 4 for density ( $\mathrm{g} / \mathrm{cc}$ )

| Pair | $1^{\text {st }}$ Value <br> $(\%)$ | $2^{\text {nd }}$Value <br> $(\%)$ | Distance <br> $(\mathrm{m})$ | Direction <br> $($ degree $)$ | Difference $^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $7: 01$ | 1.35 | 1.39 | 1015.749 | 267.623 | 0.002 |
| $5: 02$ | 1.39 | 1.30 | 1061.056 | 71.115 | 0.008 |

Table 4.46. Cross validation for density ( $\mathrm{g} / \mathrm{cc}$ ) at $112.5^{\circ}, \mathrm{S} 4$ seam, Ban Sao deposit, Saba Yoi area, tested using Geo_EAS program.

Density ( $\mathrm{g} / \mathrm{cc}$ )

| Value | Variable | Estimate | Difference | Kriging Std. | Zscore |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum | 1.300 | 1.398 | -. 057 | . 019 | -3.021 |
| 25th \%tile | 1.300 | 1.398 | -. 057 | . 019 | $-3.021$ |
| Median | 1.390 | 1.407 | . 028 | . 027 | . 659 |
| 75th \%tile | 1.410 | 1.418 | 033 | . 036 | . 772 |
| Maximum | 1.460 | 1.443 | . 057 | . 073 | 1.861 |
| Mean | 1.387 | 1.418 | . 016 | . 037 | . 250 |
| Std. Dev | 0.051 | 0.019 | . 043 | . 020 | 1.775 |

### 4.5 Summary of the Variogram Result

Based upon the results shown in section 4.4 and the overall results and analyses [including the details of lag results, results from variogram-parameter values, variogram model for the other variables, not shown in section 4.5 in the Appendices $B, C$, and $D$, the followings (see Tables 4.47 and 4.48 ) are the summary of such variogram results.

It is observed that most of the variogram results fit fairly well with the spherical model, particularly those of $\operatorname{Sin}$ Pun coal quality data (about $96 \%$ of 25 models). However, for the 20 models of Saba Yoi, it is found that about $40 \%$ is spherical, $35 \%$ is linear, $20 \%$ is nugget-effect, and $5 \%$ is gaussian.

Table 4.47. Summary of result of Variogram for Sin Pun Area.

| Seam | Variable | direction (degree) | tolerance angle | lag spacing <br> (m) | nugget | sill | range (m) | model |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | Ash | 157.5 | 45 | 280 | 0 | 130 | 900 | Spherical |
|  | CV | 157.5 | 45 | 280 | 0 | 690000 | 600 | Spherical |
|  | Moisture | 135 | 45 | 150 | 0 | 63 | 800 | Spherical |
|  | Sulphur | 157.5 | 45 | 180 | 0 | 4 | 500 | Spherical |
|  | Density | 157.5 | 45 | 190 | 0 | 0.009 | 700 | Spherical |
| P2 | Ash | 157.5 | 45 | 140 | 15 | 72 | 750 | Spherical |
|  | CV | 0 | 45 | 24 | 0 | 675000 | 600 | Spherical |
|  | Moisture | 157.5 | 45 | 170 | 12 | 19 | 600 | Spherical |
|  | Sulphur | 157.5 |  | 350 | 0.5 | - | 420 | Linear |
|  | Density | 157.5 |  | 260 | 0.004 | 0.0045 | 400 | Spherical |
| P3 | Ash | 157.5 |  | 160 | 0 | 100 | 530 | Spherical |
|  | CV | 157.5 |  | 160 | 0 | 960000 | 650 | Spherical |
|  | Moisture | 0 | 45 | 2-3 190 | 0 | 22 | 350 | Spherical |
|  | Sulphur | 157.5 | 45 | 210 | 2.8 | 3 | 650 | Spherical |
|  | Density | 22.5 | 45 | 280 | 0.006 | 0.013 | 850 | Spherical |
| P4 | Ash | 157.5 | 45 | 300 | 18 | - | 500 | Linear |
|  | CV | 157.5 | $45 \cap$ | 200 | 250000 | 280000 | 450 | Spherical |
|  | Moisture | 157.5 | 45 | 310 | 8 | 18.5 | 550 | Spherical |
|  | Sulphur | 0 | 45 | 280 | 2.3 | 2.6 | 500 | Spherical |
|  | Density | 157.5 | 45 | 150 | 0 | 0.021 | 420 | Spherical |
| M | Ash | 157.5 | 45 | 170 | 18 | - | 550 | Linear |
|  | CV | 157.5 | 45 | 220 | 0 | - | 400 | Linear |
|  | Moisture | 157.5 | 45 | 350 | 0 | 17 | 600 | Spherical |
|  | Sulphur | 157.5 | 45 | 300 | 2.8 | 4.2 | 850 | Spherical |
|  | Density | 157.5 | 45 | 190 | 0 | 0.0115 | 700 | Spherical |

Table 4.48. Summary of result of Variogram for Saba Yoi Area.

| Seam | Variable | direction <br> (degree) | tolerance angle | lag spacing <br> (m) | nugget | sill | range (m) | model |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S1 | Ash | 90 | 45 | 240 | 2.2 | 3 | 380 | Spherical |
|  | CV | 90 | 45 | 300 | 2500 | - | 530 | Linear |
|  | Moisture | 112.5 | 45 | 260 | 0 | 9 | 450 | Spherical |
|  | Sulphur | 112.5 | 45 | 200 | 0 | 0.07 | 600 | Spherical |
|  | Density | 90 | 45 | - 260 | 0 | 0.007 | 700 | Spherical |
| S2 | Ash | 67.5 | 45 | 130 | 3 | 5 | 250 | Spherical |
|  | CV | 45 |  | 180 | 40000 | 62000 | 400 | Spherical |
|  | Moisture | - |  | 200 | - | 2.5 | - | Pure nugget |
|  | Sulphur | 90 |  | 160 | 0 | 0.072 | 550 | Spherical |
|  | Density | 67.5 |  | 150 V | 0 | - | 550 | Linear |
| S3 | Ash | 112.5 | 45 | 320 | - | 40 | - | Pure nugget |
|  | CV | 112.5 | 45 | 330 | 0 | 130000 | 1000 | Spherical |
|  | Moisture | 112.5 | 45 | 330 | 1 | 26 | 1500 | Gaussian |
|  | Sulphur | 112.5 | ลง 45 รถ | 330 /ยา | ล1 0 | - | 1200 | Linear |
|  | Density | 112.5 |  | 400 | 0.0026 | - | 1600 | Linear |
| S4 | Ash | - | 45 | - | - | 10 | - | Pure nugget |
|  | CV | - | 45 | - | - | 190000 | - | Pure nugget |
|  | Moisture | - | 45 | - | - | 15 | - | Pure nugget |
|  | Sulphur | - | 45 | - | - | 0.3 | - | Pure nugget |
|  | Density | 112.5 | 45 | 350 | 0.0001 | - | 1100 | Linear |

