

เอกสารอ้างอิง

ภาษาไทย

- กองเศรษฐกิจอุตสาหกรรม. รายงานภาวะเศรษฐกิจอุตสาหกรรม เฉพาะประเภทอุตสาหกรรม ประกอบรถยนต์ กระทรวงอุตสาหกรรม,ในสภาวะปี 2534-2535.
- เกษม เลิศรัตน์, มัทลีโอะ มียากาวา,ดร. การทำแม่พิมพ์อัดโลหะ. กรุงเทพฯ : ดวงกมล, 2537.
- ขันดีพล วัชรานาถ, มนูญ เลิศวิจิตรพันธุ์, วันชัย โกมลหิรัญ. การตรวจสอบชิ้นงานเชื่อม. กรุงเทพฯ : บริษัท ซีเอ็ดยูเคชั่น จำกัด, 2521.
- จารุณี เหลืองเพชรงาม. การศึกษาระบบการควบคุมคุณภาพสำหรับอุตสาหกรรมคอนกรีตผสมเสร็จแบบหลายโรงผสม. วิทยานิพนธ์ปริญญาโท ภาควิชาวิศวกรรมอุตสาหการ บัณฑิตวิทยาลัย จุฬาลงกรณ์มหาวิทยาลัย, 2536.
- ชาญ ถนัดงาน และคนอื่น ๆ. คู่มือการออกแบบและสร้างแม่พิมพ์ขนาดเล็ก. กรุงเทพฯ : สวัสดิการสถาบันฯ และชมรมอุตสาหกรรมแม่พิมพ์ไทย, 2533.
- ชาญชัย ททรัพย์ากร, ประสิทธิ์ สวัสดิสรพร, วิรุฬ ประเสริฐวรรณันท์. การออกแบบแม่พิมพ์. กรุงเทพฯ : สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น) 2526.
- คารงค์ ทวีแสงสกุลไทย,ผศ. การควบคุมคุณภาพสำหรับนักบริหารและกรณีศึกษา. กรุงเทพฯ : บริษัท เอ็มแอนด์อี จำกัด, 2533.
- ถาวรธรรม ทองประเสริฐ. "เปิดโฉมอุตสาหกรรมชิ้นส่วนยานยนต์ไทย", ผู้ส่งออก ปีที่ 7 ฉบับที่ 148 (ตุลาคม 2536) : 43-50.
- เบงคิจ ฌมรียามา. เทคนิคเครื่องมือวัดเชิงกล การใช้และการบำรุงรักษา. กรุงเทพฯ : สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น), 2536.
- พงษ์เพ็ญ จันทนะ. การศึกษาเพื่อพัฒนาองค์การและระบบข้อมูลในอุตสาหกรรมการผลิตชิ้นส่วนรถยนต์. วิทยานิพนธ์ปริญญาโท ภาควิชาวิศวกรรมอุตสาหการ บัณฑิตวิทยาลัย จุฬาลงกรณ์มหาวิทยาลัย, 2535.
- พิชิต สุขเจริญพงษ์,ดร. การควบคุมคุณภาพเชิงวิศวกรรม. กรุงเทพฯ : บ.ซีเอ็ดยูเคชั่น จก. , 2535.

- มานพ ตันตระกูล. งานทดสอบวัสดุอุตสาหกรรม. กรุงเทพฯ : สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น), 2535.
- วชิระ มีทอง. การออกแบบจิ๊กและฟิกซ์เจอร์. กรุงเทพฯ : สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น), 2536.
- สมบูรณ์ เต็งหงษ์เจริญ, เจริญ พรหมคชสุด, บัณฑิต ใจชื่น. เชื่อมโลหะ 1. กรุงเทพฯ, 2532.
- สมชาย วิศวะวิรัชศักดิ์. การพัฒนากระบวนการควบคุมคุณภาพของอุตสาหกรรมเครื่องใช้ประจำโต๊ะอาหาร. วิทยานิพนธ์ ปริญญาโท ภาควิชาวิศวกรรมอุตสาหกรรม, บัณฑิตวิทยาลัย จุฬาลงกรณ์มหาวิทยาลัย, 2534.
- สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น). เทคโนโลยีเครื่องอัดขึ้นรูปและแม่พิมพ์. เอกสารประกอบการสัมมนา. กรุงเทพฯ.
- สุนันท์ วิเศษสรราชค. การเพิ่มผลผลิตในอุตสาหกรรมผลิตภัณฑ์ขึ้นส่วนโลหะของรถยนต์. วิทยานิพนธ์ ปริญญาโท ภาควิชาวิศวกรรมอุตสาหกรรม, บัณฑิตวิทยาลัย จุฬาลงกรณ์มหาวิทยาลัย, 2534.
- เสรี ยูนิพันธ์, รศ., จรุง มหิธาพองกุล, รศ., คารงค์ ทวีแสงสกุลไทย, ผศ., เทคนิคการควบคุมคุณภาพ. กรุงเทพฯ : ภาควิชาวิศวกรรมอุตสาหกรรม, คณะวิศวกรรมศาสตร์, จุฬาลงกรณ์มหาวิทยาลัย, มิถุนายน 2528.
- อดิศักดิ์ พงษ์พูลผลศักดิ์, รศ. การควบคุมคุณภาพ. กรุงเทพฯ : ศูนย์สื่อเสริม กรุงเทพฯ.
- ฮิโตชิ คูเมะ. วิธีทางสถิติเพื่อการพัฒนาคุณภาพ. กรุงเทพฯ. สมาคมส่งเสริมเทคโนโลยี (ไทย-ญี่ปุ่น), 2535.

ภาษาอังกฤษ

Asian Automotive Component Center. Supplier Development Workshop.

August 1994.

Feigenbaum, A.v. Total Quality Control. Third Edition, Revised,

McGraw-Hill International Editions, New York, 1991.

Japanese Standard Association. JIS Handbook 1989 Ferrous Material

and Metallurgy. Japan 1989.

Juran, J.M., Grya, F.M. Quality Planning and Analysis.

Secound Edition, Mc Graw-Hill Book Co.,Inc.,

New York, 1970.

Kaoruishikawa, D.R. Guide to Quality Control. Asian Productivity,

Oranization, 1972.

Mitsubihi Motor Corporation. Manual For Quality Assurance at Parts

Suppliers. July 1989.

Montgomery, D.C. Introduction to Statistical Quality Control.

John Wiley & Sons Inc., New York, 1985.

Taylor, J.R. Quality Control System. Mc.Graw - Hill Book Co.,Inc.,

New York, 1975.

ภาคผนวก

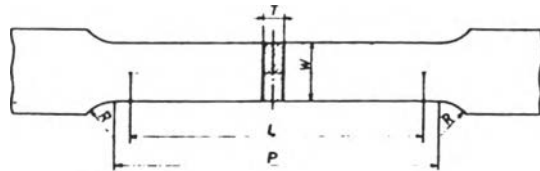
ข้อกำหนดตามมาตรฐานอุตสาหกรรมญี่ปุ่น

4. Form and Dimensions of Test Piece

4.1 The forms and dimensions of the test pieces Nos. 1 to 14 shall be as follows:

- (1) **No. 1 Test Piece** The form and dimensions of this test piece shall conform to Fig. 1.

Fig. 1

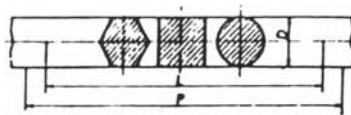


Unit: mm

Type of test piece	Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
1 A	40	200	220 approx.	25 min.	Thickness of material
1 B	25	200	220 approx.	25 min.	Thickness of material

- (2) **No. 2 Test Piece** The form and dimensions of this test piece shall conform to Fig. 2.

Fig. 2

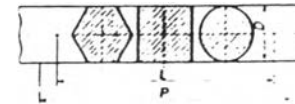


Dia. or width across flats D	Gauge length L	Distance between grips P
Size of material	8 D	(L + 2 D) approx.

Remark: This test piece shall be applied to bars of not more than 25 mm in nominal diameter (or width across flats).

- (3) **No. 3 Test Piece** The form and dimensions of this test piece shall conform to Fig. 3.

Fig. 3

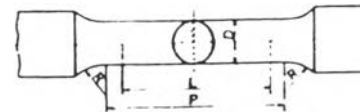


Dia. or width across flats D	Gauge length L	Distance between grips P
Size of material	4 D	(L + 2 D) approx.

- Remarks 1. This test piece shall be applied to bars of over 25 mm in nominal diameter (or width across flats).
2. This test piece may be machined into the test piece with reduced parallel portion. In this case, the diameter of reduced parallel portion shall be not less than 25 mm and the length of the part P shall be approximately 4.5 D.

- (4) **No. 4 Test Piece** The form and dimensions of this test piece shall conform to Fig. 4.

Fig. 4



Unit: mm

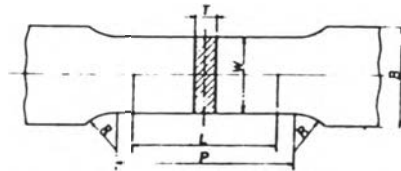
Diameter D	Gauge length L	Parallel length P	Radius of fillet R
14	50	60 approx.	15 min.

- Remarks 1. The parallel portion of this test piece shall be machine-finished. However, that of malleable casting shall, as a rule, not be finished.
2. If the test piece of the dimensions as specified in Fig. 4 can not be obtained, the diameter of parallel portion and the gauge length may be determined in accordance with the formula $L = 4\sqrt{A}$ where A is the cross-sectional area of parallel portion.

รูปที่ 1 ขนาดของตัวอย่างที่ทดสอบความเค้นแรงดึงตามมาตรฐานอุตสาหกรรมญี่ปุ่น

- (5) **No. 5 Test Piece** The form and dimensions of this test piece shall conform to Fig. 5.

Fig. 5



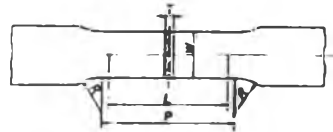
Unit: mm

Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
25	50	60 approx.	15 min.	Thickness of material

Remark: In the case of applying this test piece to steel sheets not more than 3 mm thick, the radius R of fillet shall be 20 to 30 mm, and the width B of gripped ends shall be 30 mm or over.

- (6) **No. 6 Test Piece** The form and dimensions of this test piece shall conform to Fig. 6.

Fig. 6



Unit: mm

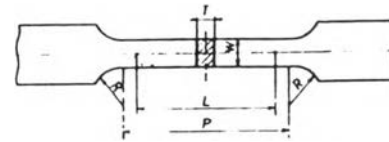
Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
15	$8/\sqrt{A}$	$L + \text{approx. } 10$	15 min.	Thickness of material

A: cross-sectional area of parallel portion (W x T)

Remark: This test piece shall be applied to plates and shapes not more than 6 mm in thickness.

- (7) **No. 7 Test Piece** The form and dimensions of this test piece shall conform to Fig. 7

Fig. 7



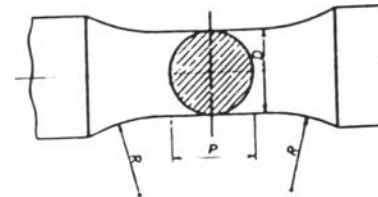
Unit: mm

Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
T min.	$4\sqrt{A}$	$1.2L \text{ approx.}$	15 min.	Thickness of material

A: cross-sectional area of parallel portion (W x T)

- (8) **No. 8 Test Piece** This test piece shall be made from a test coupon cast to the dimensions specified in the following table by machine-finishing to the form and dimensions shown in Fig. 8.

Fig. 8



Unit: mm

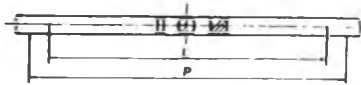
Type of test piece	Casting dimensions of test coupon (diameter)	Parallel length P	Diameter D	Radius of fillet R
8 A	13 approx.	8 approx.	8	16 min.
8 B	20 approx.	12.5 approx.	12.5	25 min.
8 C	30 approx.	20 approx.	20	40 min.
8 D	45 approx.	32 approx.	32	64 min.

Remark: This test piece shall be used for the tensile testing of the materials such as iron castings which do not require elongation values.

รูปที่ 1 (ต่อ) ขนาดของตัวอย่างชิ้นทดสอบความเค้นแรงดึงตามมาตรฐานอุตสาหกรรมญี่ปุ่น

- (9) No. 9 Test Piece The form and dimensions of this test piece shall conform to Fig. 9.

Fig. 9



Unit: mm

Type of test piece	Gauge length L	Distance between grips P
9 A	100	150 min.
9 B	200	250 min.

- (10) No. 10 Test Piece The form and dimensions of this test piece shall conform to Fig. 10.

Fig. 10

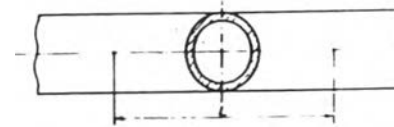


Unit: mm

Diameter D	Gauge length L	Parallel length P	Radius of fillet R
12.5	50	60 approx.	15 min.

- (11) No. 11 Test Piece The form and dimensions of this test piece shall conform to Fig. 11.

Fig. 11

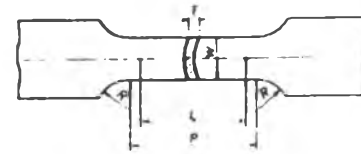


Gauge length L = 50 mm

Remark: The cross section of this test piece shall be as cut out from the tubular material, and the gripped ends shall be inserted with metal plugs or pressed flat by hammering. In the latter case, the length of parallel portion shall be not less than 100 mm.

- (12) No. 12 Test Piece This test piece shall be made from the tubular material by cutting out and then by finishing to the form and dimensions as shown in Fig. 12.

Fig. 12



Unit: mm

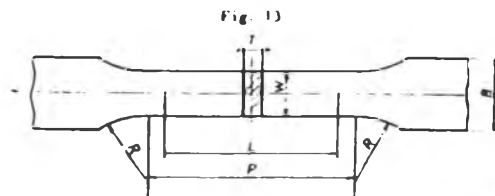
Type of test piece	Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
12 A	19	50	60 approx.	15 min.	Thickness of tube
12 B	25	50	60 approx.	15 min.	Thickness of tube
12 C	38	50	60 approx.	15 min.	Thickness of tube

Remark: The cross section of parallel portion of this test piece shall be of arc form as cut out of the tubular material. However, the gripped ends of test piece may be hammered flat at the room temperature.



รูปที่ 1 (ต่อ) ขนาดของตัวอย่างขึ้นทดสอบความเค้นแรงดึงตามมาตรฐานอุตสาหกรรมญี่ปุ่น

(13) No. 13 Test Piece The form and dimensions of this test piece shall conform to Fig. 13.



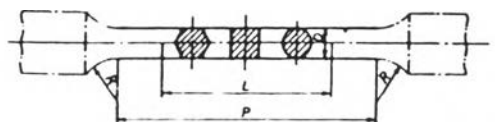
Unit: mm

Type of test piece	Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T	Width of gripped portion B
13 A	20	80	120 approx.	20 to 30	Thickness of material	—
13 B	12.5	50	60 approx.	20 to 30	Thickness of material	20 min.

(14) No. 14 Test Piece

(a) No. 14 A Test Piece The form and dimensions of this test piece shall conform to Fig. 14 (A).

Fig. 14 (A)



Unit: mm

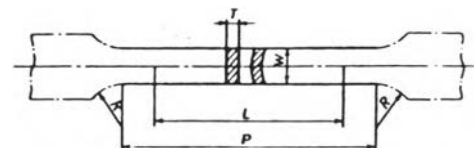
Gauge length L	Parallel length P	Radius of fillet R
$5.65 \sqrt{A}$	5.5 D to 7 D	15 min.

A: cross-sectional area of parallel portion

- Remarks 1. The gauge length may be so determined that $L = 5 D$ for circular cross section of parallel portion, that $L = 5.65 D$ for square cross section, and that $L = 5.26 D$ for hexagonal cross section.
2. The length P of parallel portion should be $7 D$, as far as practicable.
3. The diameter of gripped portions of this test piece may be made same as that of the parallel portion. In this case, the distance between grips shall be so determined that $P > 8 D$.

(b) No. 14 B Test Piece The form and dimensions of this test piece shall conform to Fig. 14 (B).

Fig. 14 (B)



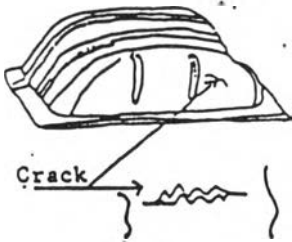
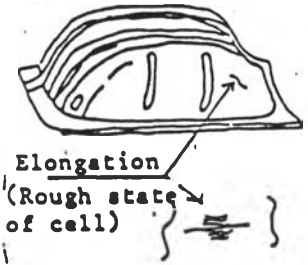
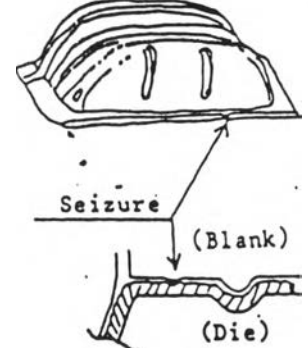
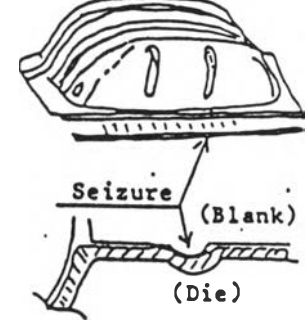
Unit: mm

Width W	Gauge length L	Parallel length P	Radius of fillet R	Thickness T
$8 T$ max.	$5.65 \sqrt{A}$	$L + 1.5 \sqrt{A}$ to $L + 2.5 \sqrt{A}$	15 min.	Thickness of material

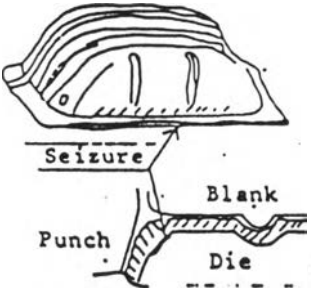
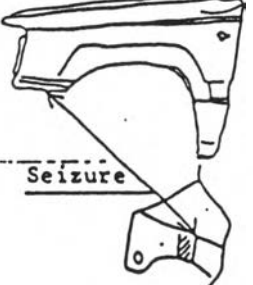
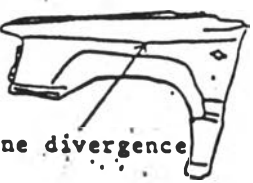
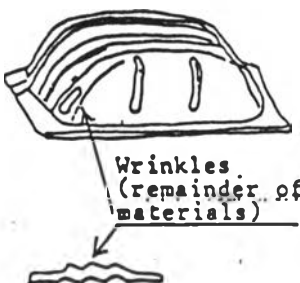
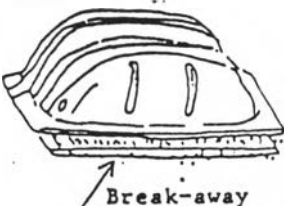
A: cross-sectional area of parallel portion

- Remarks 1. The length of parallel portion should be so determined that $P = L + 2 \sqrt{A}$, as far as practicable.
2. In the case of applying this test piece to the tensile test of tubes, the cross section of parallel portion shall be as cut out from the tube.
3. The width of gripped portion of this test piece may be made same as that of the parallel portion. In this case, the distance between grips shall be so determined that $P = L + 3 \sqrt{A}$.
4. For the use of this type test pieces, it is advisable to unify their dimensions according to every reasonable range which covers varied plate thickness, as exemplified in Table 3 (see 4.3 and 4.4.).

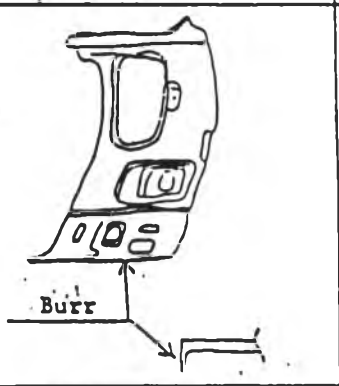
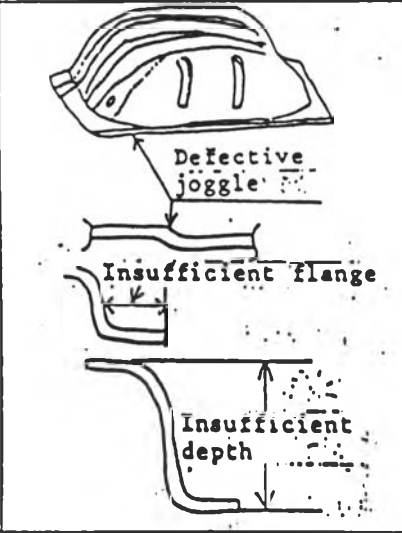
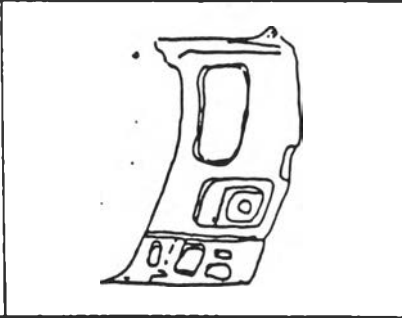
รูปที่ 1 (ต่อ) ขนาดของตัวอย่างชิ้นทดสอบความเค้นแรงดึงตามมาตรฐานอุตสาหกรรมญี่ปุ่น

Contents of defect	Cause of defect	Treatment
<p>Crack</p> 	<p>Caused by high pressure of the blank face and cushion, change of the die temperature (rising), seizure of the blank face and bend, and unevenness of materials.</p>	<p>Adjustment of the pressure Improvement of the die (Polishing) (Fitting depending on the case) Material check</p>
<p>Elongation</p> 	<p>Caused by high pressure of the blank face and cushion, change of the die temperature (rising), seizure of the blank face and bead, and unevenness of materials.</p>	<p>Adjustment of the pressure Improvement of the die (Polishing) Material check</p>
<p>(Drawing of blank face)</p> <p>Seizure</p> 	<p>Mixture of dust and substances, scratch, burr, and deformation of the materials, excess pressure to be blank and cushion, wrinkles, changes of die temperature, and worn-out of the die</p>	<p>Complete control of materials, cleaning of materials, inspection and repair of the die, oiling, adjustment of pressure, and polishing and maintenance of the die</p>
<p>(Bead drawing)</p> <p>Seizure</p> 	<p>Incorrect aperture Defective surface treatment</p>	<p>Complete surface treatment</p>

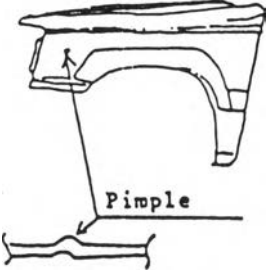
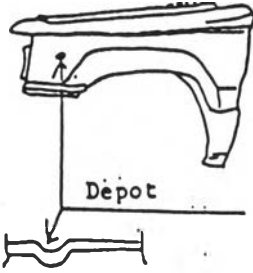


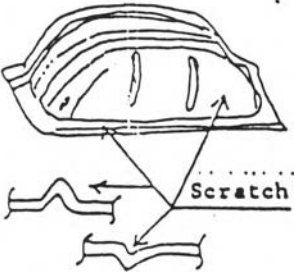
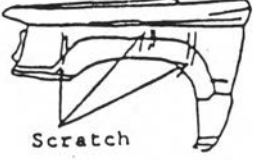
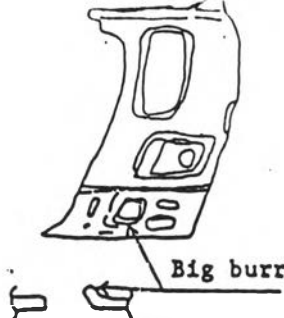
รูปที่ 2 ลักษณะอาการเสียต่างๆของชิ้นส่วนรถยนต์จากการอัดขึ้นรูปโลหะ

	Contents of defect	Cause of defect	Treatment
(Die R drawing)		Mixture of dust and substances, worn-out of the die, wrinkles caused by crack, change of the die temperature, and excess pressure to the blank and cushion	Complete control of materials, cleaning of materials, inspection and maintenance of the die, adjustment of pressure, polishing of the die, and oiling
(Flange bent)		Mixture of dust and substances, worn-out of the die, insufficient (too narrow), break-away of plating, and wrinkles overlapping due to misinsertion	Polishing of the die, inspection and maintenance of the die; oiling, insertion check, surface treatment
Line divergence		Unbalance of pressure to the blank and cushion Die worn-out	Adjustment of the pressure Repair of the die
Wrinkles		Unevenness of material characteristic value, unbalance of pressure to the blank and cushion, and die worn-out	Material check, replacement of materials, adjustment of the pressure, repair of the die, adhesion of materials, and oil quantity check
Break-away of surface treatment materials		Defective surface treatment (manufacturer), defective accuracy of the blank face and bead, and excess pressure to the blank and cushion	Material check, replacement of materials, polishing and repair of the die, and adjustment of the pressure

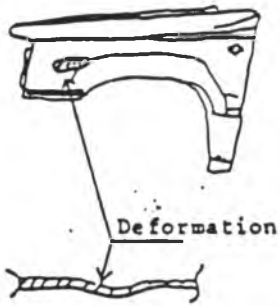
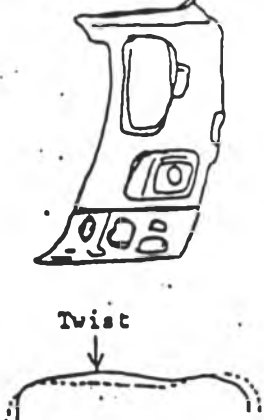
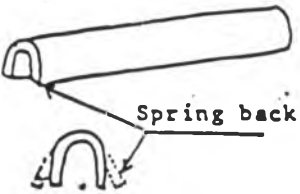
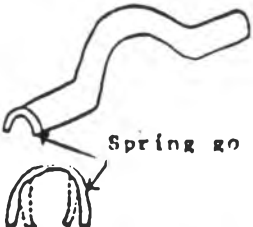
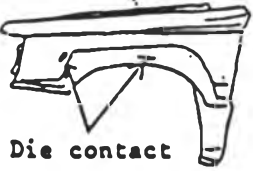
รูปที่ 2 (ต่อ) ลักษณะอาการเสียต่างๆของชิ้นส่วนรถยนต์จากการอัดขึ้นรูปโลหะ

Contents of defect	Cause of defect	Treatment	
Burr 	Worn-out punch and die cutting edge, incorrect aperture	Repair of the die (Correction of the aperture)	
Defective setting-down 	Insufficient pressure, defective stroke set, incomplete bottoming check, and incomplete checking of pressure gauge	Check completely the bottom dead center, bottoming mark, and pressure gauge.	
Type difference 	Incorrect switching position of the lever for switching type, incorrect position of slide, and incomplete check at the time of comparing with the type sample	Complete comparison with the type sample, as well as inspection, — maintenance and improvement of type switching devices	
Defective materials	Lamination, scab, scale, camber, meandering of coil, roll scratch and others	Defective steel materials At the time of BK and SH cutting off	Understand fully the contents of defection and defective part. Claim treatment is applied to the defective materials, and materials are replaced.

รูปที่ 2 (ต่อ) ลักษณะอาการเสียต่างๆของชิ้นส่วนรถยนต์จากการอัดขึ้นรูปโลหะ

Contents of defect	Cause of defect	Cause of defect	Treatment
<p>Pimple</p> 		<p>Mixture of substances including dust (caused by working gloves and conveyor) and refuse at the time of cutting, and dirt of the die (especially at the time of die repair)</p>	<p>Removal of substances by wiping and polishing, cleaning of materials and die, and inspection and maintenance of die</p>
<p>Depot</p> 			
<p>Scratch caused by hit</p> 		<p>Hit by the guide, cutter, and chute at the time of panel inspection or pulling out, fall of a panel, overlapping of panels. Incorrect setting of I/H lifter, and defective of rubber roller and buffer materials.</p>	<p>Re-guidance of operation method, removal of obstacles, repair, improvement, correction of process unbalance, correction of automatic devices, and inspection and maintenance of the die</p>
<p>Scratch</p> 		<p>Caused by interference or overlapping of panels at the time of material transport by D/F, products transport by the conveyor and insertion of products.</p>	<p>Polishing, improvement and removal of the interferential section, correction of process unbalance, and stabilization of product insertion and pull-out.</p>
<p>Big burr</p> 		<p>Worn-out of punch and die cutting edge, and incorrect aperture</p>	<p>Oiling and repair of the die (Correction of aperture and intrusion)</p>

รูปที่ 2 (ต่อ) ลักษณะอาการเสียต่างๆของชิ้นส่วนรถยนต์จากการอัดขึ้นรูปโลหะ

Contents of defect	Cause of defect	Treatment
Deformation 	Dispersion of material characteristic values, camber of materials, oil adhesion to materials, insufficient pressure to the blank and cushion, and unbalance of the blank face	Material check, replacement of materials, re-cleaning, adjustment of pressure, and die fitting
Twist 	Dispersion of material characteristic values, camber of materials, and unbalance of pat	Material check, replacement of materials, and inspection and maintenance of the die.
Spring back 	Die worn-out (too open), incorrect thickness of material (thin), and insufficient main pressure	Inspection and maintenance of the die, material check, replacement of materials, and adjustment of pressure
Spring go 	Insufficient aperture of the die, and incorrect thickness of materials (too thick)	Inspection and maintenance of die, material check, and replacement of materials
Die contact 	Looseness of pat, pat spring broken, looseness of inserted panel, incorrect position of panel, and error at the time of die repair	Inspection, maintenance and polishing of die

รูปที่ 2 (ต่อ) ลักษณะอาการเสียต่างๆของชิ้นส่วนรูดชนิดจากการอัดขึ้นรูปโลหะ

ตารางที่ 1 ข้อกำหนดมาตรฐานญี่ปุ่นของแผ่นเหล็กที่ใช้ขึ้นรูปชิ้นส่วนรถยนต์

Specifications JIS (Japanese Industrial Standards) and Nippon Steel Standards

1. Mechanical Properties and Chemical Compositions (The chemical composition applies to that of porcelain enamelling sheets SPP)

Type	Classification	Designation	Test	Tension test								Bending test			Eichsen test										
				Yield Strength Min. Value N/mm ²	Tensile Strength Min. Value N/mm ²	Elongation Min. Value (%)						Type and Direction of specimens	Bending angle	Inside radius	Type and Direction of specimens	Eichsen Min. Value (mm)									
						0.25 and 0.010 over	0.25 to 0.40 incl.	0.40 to 0.80 incl.	0.80 to 1.6 incl.	1.6 to 2.5 incl.	2.5 and 0.008 over					0.4 (0.010)	0.5 (0.020)	0.6 (0.024)	0.7 (0.028)	0.8 (0.031)	0.9 (0.035)	1.0 (0.038)	1.2 (0.047)	1.4 (0.055)	1.6 (0.063)
Standard cold rolled steel sheets and coils (JIS G 3141-1990)	Commercial quality	SPL4	—	—	(2.770)	(32)	(34)	(36)	(37)	(38)	(39)	JIS No. 5 Rolling direction	180°	Closing slightly	JIS No. 3 Rolling direction	7.2	7.2	8.4	8.8	9.1	9.4	9.6	10.0	10.3	10.5
	SPOCT	2.1	—	2.770	32	34	36	37	38	39	7.8					7.8	8.4	8.8	9.1	9.4	9.6	10.0	10.3	10.5	
	SPOD	S	—	2.770	34	36	36	38	40	41	7.8					8.2	8.8	9.2	9.5	9.8	10.0	10.4	10.7	10.8	
Deep drawing quality	SPOEN	S	—	2.770	36	36	40	41	42	43	8.0	8.8	9.2	9.6	9.8	10.2	10.4	10.8	11.1	11.3					

Remarks:

- In ~~the case of~~ tension test ~~values~~ ~~are~~ not apply to SPOC, but when required by the customer the values in the table shall apply.
- When tension test values or Eichsen values, or both, are guaranteed for SPOC, in compliance with a customer's request, the suffix T shall be given to the designation: SPOCT.
- In principle the tension test shall be omitted for thicknesses less than 0.6 mm.
- For SPOEN, non-aging shall be guaranteed for a period of 6 months from the date of shipment from the works. Non-aging ~~means~~ ~~commence~~ in which stretcher strain does not occur during working process. The bending test shall be omitted for standard tempering.

Remark:

- For intermediate nominal thickness from 0.4 to 1.6 mm inclusive not listed in the table, Eichsen values shall be obtained by interpolation and rounded off to one decimal place.
- Values are the average values obtained from three test samples.
- The Eichsen test shall not be conducted on thickness under 0.4 mm or over 1.6 mm.
- () Reference value.

JIS G 3131 ● Hot-Rolled Mild Steel Sheets and Strip

Designation	Chemical Composition, %		Tensile Strength N/mm ²	Tensile Test						Test Piece	Bending Angle	Bending Test		Test Piece
				Elongation %								Inner Diameter		
	P	S		Thickness 1.2mm to 1.6mm excl.	Thickness 1.6mm to 2.0mm excl.	Thickness 2.0mm to 2.5mm excl.	Thickness 2.5mm to 3.2mm excl.	Thickness 3.2mm to 4.0mm excl.	Thickness 4.0mm and over			Thickness Under 3.2mm	Thickness 3.2mm and over	
SPHC	0.050 max.	0.050 max.	270 min.	27 min.	28 min.	28 min.	28 min.	31 min.	31 min.	No. 5 Rolling Direction	180°	close overlap	0.5 l	No. 3 Rolling Direction
SPHD	0.040 max.	0.040 max.	270 min.	30 min.	32 min.	33 min.	35 min.	37 min.	38 min.		180°	close overlap	close overlap	
SPHE	0.030 max.	0.035 max.	270 min.	31 min.	33 min.	35 min.	37 min.	38 min.	41 min.		180°	close overlap	close overlap	

Remarks 1 The C and Mn contents are not specified, but SPHC is manufactured from carbon steel having a C content of 0.15% or below and an Mn content of 0.80% or below. SPHD and SPHE are manufactured from carbon steel having a C content of 0.10% or below and a Mn content of 0.50% or below.

2. Mechanical test values do not apply to external parts of or both ends steel strip (coil).

ตารางที่ 1 (ต่อ) ข้อกำหนดมาตรฐานญี่ปุ่นของแผ่นเหล็กที่ใช้ขึ้นรูปชิ้นส่วนรถยนต์

Classification and Designation

Sheets and coils shall be classified into 18 categories in the case of hot-rolled base metals and another 18 categories in the case of cold-rolled base metals. Their designations shall be as given in Tables 1 and 2.

Table 1 Classification and Designation

Designation of class	Nominal thickness (mm)	Application	
		Main use	Class designation of base metal in relevant JIS
SEHC	1.8 or over, up to and including 4.5	For commercial quality	SPHC
SEHD	1.8 or over, up to and including 4.5	For drawing quality	SPHD
SEHE	1.8 or over, up to and including 4.5	For deep drawing quality	SPHE
SEFH480	1.8 or over, up to and including 4.5	For forming quality	SPFH480
SEFH540	1.8 or over, up to and including 4.5		SPFH540
SEFH540Y	2.0 or over, up to and including 4.0	For improved forming quality	SPFH540Y
SEFH580Y	2.0 or over, up to and including 4.0		SPFH580Y
SE 330	1.8 or over, up to and including 4.8	For general structural quality	SS330
SE 400			SS400
SE 480			SS480
SE 340	1.8 or over, up to and including 4.8	For structural quality	SPHC30
SEPC370			SPHC370
SEPH400			SPHC400
SEPH440	1.8 or over, up to and including 4.8		SPHC440

Table 2 Classification and Designation

Designation of class	Nominal thickness (mm)	Application	
		Main use	Class designation of base metal in relevant JIS
SECC	0.4 or over, up to and including 3.2	For commercial quality	SPOC
SECD	0.4 or over, up to and including 3.2	For drawing quality	SPDC
SECE	0.4 or over, up to and including 3.2	For deep drawing quality	SPCE
SEFC340	0.8 or over, up to and including 2.3	For spinning quality	SPFC340
SEFC370			SPFC370
SEFC380	0.8 or over, up to and including 2.3	For forming quality	SPFC380
SEFC440			SPFC440
SEFH480			SPFH480
SEFC540			SPFC540
SEFC580	0.8 or over, up to and including 1.8	Lower yield steel type	SPFC580
SEFC60Y			SPFC60Y
SEFC640Y	0.8 or over, up to and including 1.8	Lower yield steel type	SPFC640Y
SEFC680Y			SPFC680Y
SEFC780Y	0.8 or over, up to and including 1.4	Lower yield steel type	SPFC780Y
SEFC80Y			SPFC80Y
SEFC340H	0.8 or over, up to and including 1.8	Reduced and hardening type	SPFC340H

Mechanical Properties

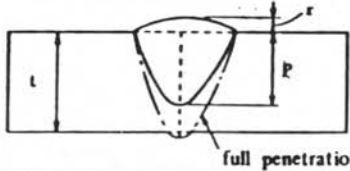
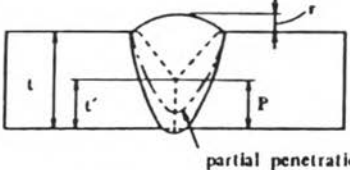
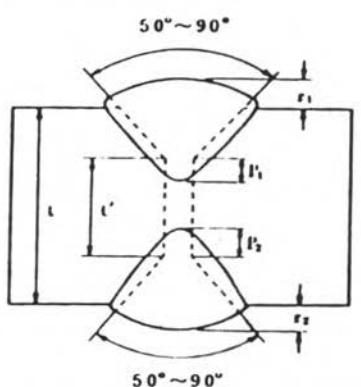
Table 6 Yield Point, Tensile Strength, and Elongation in the case of hot-rolled base metal

Designation of class	Yield point or proof stress (N/mm ²)	Tensile strength (N/mm ²)	Elongation (min.) %								Test piece
			10 mm gauge length	20 mm gauge length	30 mm gauge length	40 mm gauge length	50 mm gauge length	60 mm gauge length	70 mm gauge length	80 mm gauge length	
SEHC	270	370	28	28	24	20	24	24	24	24	No. 5 according to the rolling direction
SEHD	270	370	32	32	28	24	28	28	28	28	
SEHE	270	370	33	33	32	28	32	32	32	32	No. 5 except in the rolling direction
SEFH480	375	480	27	27	24	24	24	24	24	24	
SEFH540	355	540	21	21	21	21	24	24	24	24	No. 5 parallel or perpendicular to the rolling direction
SEFH580	470	580	18	20	21	21	27	27	27	27	
SEFH60Y	285	540	-	24	25	25	26	26	26	26	No. 5 parallel or perpendicular to the rolling direction
SEFH80Y	325	580	-	27	27	27	24	24	24	24	
SE 330	325	330 to 430	26	26	26	26	26	26	26	26	No. 5 parallel or perpendicular to the rolling direction
SE 400	345	480 to 540	21	21	21	21	21	21	21	21	
SE 480	285	480 to 540	18	18	18	18	18	18	18	18	No. 5 parallel or perpendicular to the rolling direction
SE 540	400	540	16	16	16	16	16	16	16	16	
SEPC38	(180)	310	33	34	38	38	38	38	38	38	No. 5 parallel or perpendicular to the rolling direction
SEPC30	225	370	32	33	35	35	35	35	35	35	
SEPH48	255	400	31	32	34	34	34	34	34	34	No. 5 parallel or perpendicular to the rolling direction
SEPH68	305	440	28	30	32	33	33	33	33	33	

Table 7 Yield Point, Tensile Strength, Elongation, and Forming Property in the case of cold-rolled base metal (Applicable on and after January 1, 1999)

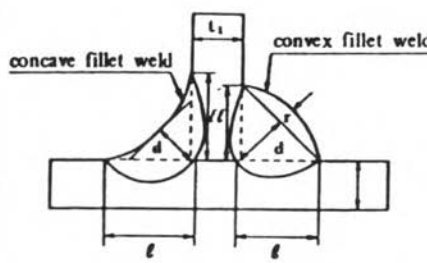
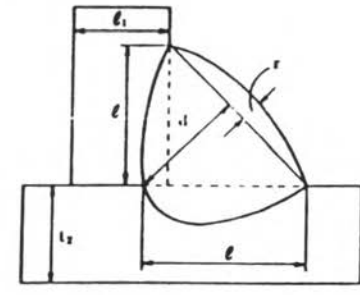
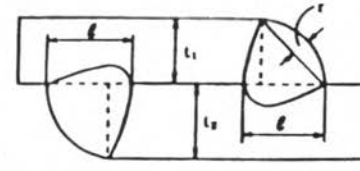
Designation of class	Yield point or proof stress (N/mm ²)	Tensile strength (N/mm ²)	Elongation (min.) %								Test piece
			10 mm gauge length	20 mm gauge length	30 mm gauge length	40 mm gauge length	50 mm gauge length	60 mm gauge length	70 mm gauge length	80 mm gauge length	
SECC	270	340	34	33	37	38	38	38	38	38	No. 5 parallel or perpendicular to the rolling direction
SECD	270	35	38	38	40	40	40	40	40	40	
SECE	270	38	40	41	42	42	42	42	42	42	No. 5 parallel or perpendicular to the rolling direction
SEFC48	175	340	-	34	35	35	-	-	-	-	
SEFC37	285	370	-	32	33	33	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC38	235	380	-	30	31	31	-	-	-	-	
SEFC48	285	440	-	28	27	27	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC48	285	490	-	23	24	24	-	-	-	-	
SEFC38	325	540	-	20	21	21	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC38	355	580	-	17	18	18	-	-	-	-	
SEFC60Y	225	480	-	24	25	25	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC60Y	245	540	-	21	22	22	-	-	-	-	
SEFC80Y	285	580	-	18	18	18	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC80Y	385	780	-	13	14	14	-	-	-	-	
SEFC80Y	480	880	-	8	7	7	-	-	-	-	No. 5 parallel or perpendicular to the rolling direction
SEFC48H	185	340	-	34	35	35	-	-	-	-	

ตารางที่ 2 มาตรฐานงานเชื่อมโลหะด้วย CO2 (การขึ้นรูป)

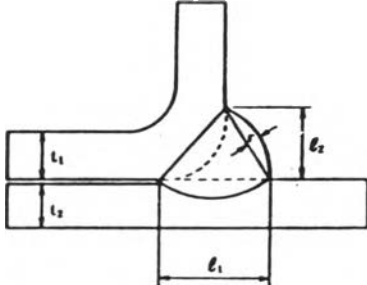
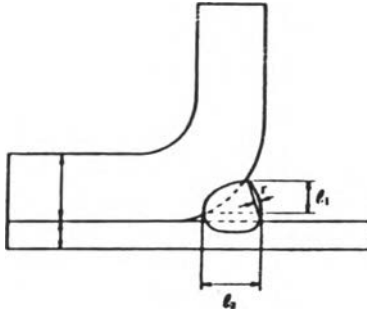
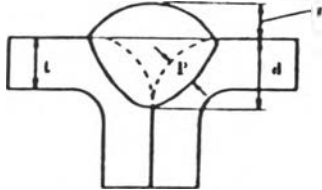
		Welding penetration of plate		
		① penetration : P ④ throat : d ② leg length : l ⑤ thickness : t, t _n ③ reinforcement : r ⑥ butt length : t'		
shape of welding	thickness (t)	macroscopic shape		
		shape	penetration	reinforcement (reference)
Butt weld	I type	<2.3mm  <p>full penetration</p>	unless drawing specified penetration shall be beyond 70% $\text{penetration}(\%) = \frac{P}{t} \times 100$	beyond base metal
	V type groove U type groove	2.3 ~ 9.0mm  <p>partial penetration</p>	unless drawing specified penetration shall be 100% $\text{penetration}(\%) = \frac{P}{t'} \times 100$	① beyond base metal ② under 2t or under 10mm.
	groove weld	> 6.0mm 	unless drawing specified penetration shall be 100% $\text{penetration}(\%) = \frac{P_1 + P_2}{t'} \times 100$	beyond base metal . reinforcement r ₁ , r ₂ shall be under 2t.



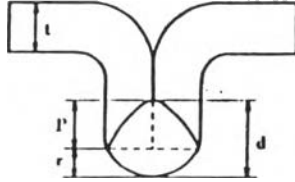
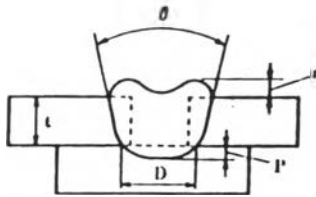
ตารางที่ 2 (ต่อ) มาตรฐานงานเชื่อมโลหะด้วย CO2 (การขึ้นลึก)

shape of welding	thickness (t)	macroscopic shape		
		shape	penetration	reinforcement (reference)
fillet weld (double)	< 12mm		① leg length shall be over drawing or within 150% of it. ② unless otherwise specify, it shall conform to following $d > 0.5 \times \text{thickness}$ $l > 0.7 \times \text{thickness}$	$r < 0.5 \times l$
fillet weld (single)	< 12mm		① leg length shall be over drawing or within 150% of it ② unless otherwise specify $d > 1.0 \times \text{thickness}$ $l > 1.4 \times \text{thickness}$	
lap fillet weld	< 12mm		① it is same above ② unless otherwise specify $l > 1.0 \times \text{thickness}$	

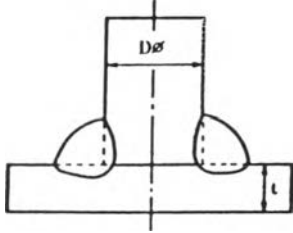
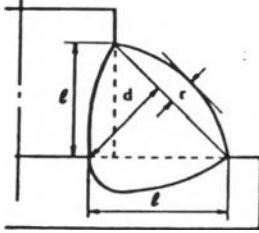
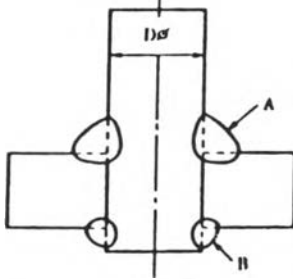
ตารางที่ 2 (ต่อ) มาตรฐานงานเชื่อมโลหะด้วย CO2 (การเชื่อมเล็ก)

shape of weld	thickness (t)	macroscopic shape		
		shape	penetration	reinforcement (reference)
flare joint	< 12mm		① when $t_1 < t_2$ actual leg length $l_1, l_2 > t_1$ ② when $t_1 \geq t_2$ actual leg length $l_1, l_2 > t_2$	reinforcement shall be within 50 percent of l_2 .
				
edge joint	< 10mm		unless drawing specify. $d > 1.0 \times \text{thickness}$ $P > 0.2 \times \text{thickness}$	reinforcement shall be beyond base metal

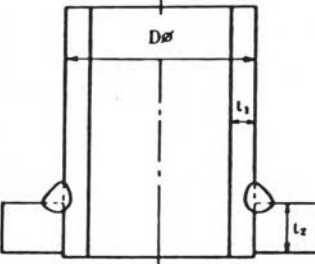
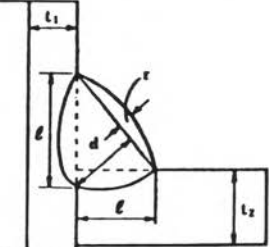
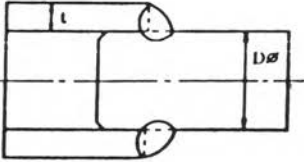
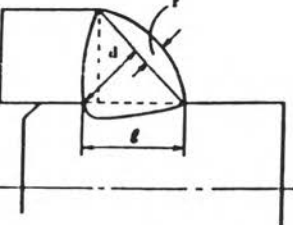
ตารางที่ 2 (ต่อ) มาตรฐานงานเชื่อมโลหะด้วย CO2 (การเชื่อมลึก)

shape of weld	thickness (t)	macroscopic shape		
		shape	penetration	reinforcement (reference)
edge joint	< 10mm		unless drawing specify. $d > 1.0 \times \text{thickness}$ $P > 0.5 \times \text{thickness}$	it is same above.
plug weld	< 20mm		when $t < 3\text{mm}$ $D = 6\text{mm}$ $30^\circ \leq \theta \leq 60^\circ$ when $t = 3$ to 12mm $D = 2t$ or over when $t > 12\text{mm}$ $D = 2t + 12$ $P > 0.2 \times \text{thickness}$	reinforcement shall be beyond base metal. center may become dented a bew. shall be careful to penetrate root.
remarks (1) Root of but weld or fillet weld shall be penetrated. (2) In case under 0.8mm thickness, welding shall conform to agreement of M.M.C (3) Test methode shall be cut the bead at right angle and see after etching.				

ตารางที่ 2 (ต่อ) มาตรฐานงานเชื่อมโลหะด้วย CO2 (การขึ้นเล็ก)

Bar and pipe welding penetration.		D : diameter of bar.		
shape of weld	shape	macroscopic shape	penetration	remarks
weld of bar and plate.			① leg length shall be drawing from -30% to +30% ② unless drawing specify when $1.4t \leq 0.3D, \quad l \geq 1.4t.$ when $0.3D < 1.4t, \quad l > 0.3D$	$r < 0.5 l$
weld of bar and plate with pit.			A : it is same above. B : actual leg length shall be beyond 0.33t.	

ตารางที่ 2 (ต่อ) มาตรฐานงานเชื่อมโลหะด้วย CO2 (การเชื่อมลึก)

shape of weld	shape	macroscopic shape	penetration	remarks
weld of pipe and plate			<p>① leg length shall be drawing from 100% to 150%</p> <p>② unless drawing specify</p> <p>$l > 1.4 t_1$</p> <p>$d > t_1$</p>	<p>$r < 0.2 l$</p>
weld of pipe and plate			<p>① leg length shall be drawing from 100% to 150%</p> <p>② unless drawing specify</p> <p>when $t \leq 0.3 D$</p> <p>$l \geq t$</p> <p>when $0.3D < t$</p> <p>$l > 0.3D$</p> <p>$d > 0.7t$ or $0.3D$</p>	<p>$r < 0.2 l$</p>
<p>remark (1) </p> <p>(2) it is same as Table 3.</p> <p>(3) </p>				

ตารางที่ 3 แผนการตรวจสอบชิ้นส่วนรถยนต์

Type of Inspection Type of Part		Initial Stage		Mass Production Stage		Equipment			Comments
		Initial Parts Inspection	Initial Supervisory Inspection	Daily Inspection	Special Inspection	"Inspection Standards"	"Inspection Agreements"	"Inspection Tabulation"	
1. Safety Parts	2. Hysteresis Control Parts	A	B	As per Table 1	A	Drawn up	Concluded	Drawn up	
3. Top Quality Parts									
1. General Parts	2. Particular parts in the 3 categories above specified by the head of quality control	A	B		A	Not drawn up	Not drawn up (in principle)	Not drawn up	
Comments		1. Whenever a goods delivery is to be undertaken, parts are inspected during this process until they pass. 2. Parts clearing inspection at this stage subsequently move to the Initial Supervisory Inspection. 3. "Initial Parts" include new parts, design changed parts and process changed parts.	1. Parts from Lot 3 or Lot 1 which have been passed are moved to Mass Production Inspection. However, should lots contain consistently substandard parts, an inspection of each individual lot will be carried out.	1. Should customer claims, line claims or failures of acceptance inspection occur, a change to Special Inspection will be undertaken.	1. Undertaken when abnormalities occur. Inspection will only be good for the said abnormalities. 2. If abnormalities are not found in three lots in succession, there will be no change to Mass Production Inspection.	1. General Parts are inspected using diagrams, while sections on "The Improvement of Inspection" and "Specialty Tolerated Parts" have been drawn up. 2. Rearrangement of similar parts is undertaken. 3. It is also permissible to use the standards shown in "Inspection Agreements".	1. As a rule, agreements relating to safety, hydraulic control and top quality parts are all concluded.	1. As a rule this is not necessary for general parts but as part of the follow up to a special inspection it is permissible to make a simple tabulation if required.	

Rating	A	B	C	D	E	N
Inspection Rate	Per lot or once a day	Once a week	Once a month	Once every two months	Once every three months	Indirect inspection

Sample Number	Initial Parts Pilot Sample	Initial Period	Daily or Special
	3	8	5

ตารางที่ 4 ตัวประกอบสำหรับคำนวณขอบเขตควบคุมคุณภาพ 3 σ

Number of Observations in Sample, n	Chart for Averages			Chart for Standard Deviations					Chart for Ranges					
	Factors for Control Limits			Factors for Central Line	Factors for Control Limits				Factors for Central Line	Factors for Control Limits				
	A	A ₁	A ₂	c ₂	B ₁	B ₂	B ₃	B ₄	d ₂	d ₃	D ₁	D ₂	D ₃	D ₄
2	2.121	3.760	1.880	0.5642	0	1.843	0	3.267	1.128	0.853	0	3.686	0	3.267
3	1.732	2.394	1.023	0.7236	0	1.858	0	2.568	1.693	0.888	0	4.358	0	2.575
4	1.500	1.880	0.729	0.7979	0	1.808	0	2.266	2.059	0.880	0	4.698	0	2.282
5	1.342	1.596	0.577	0.8407	0	1.756	0	2.089	2.326	0.864	0	4.918	0	2.115
6	1.225	1.410	0.483	0.8686	0.026	1.711	0.030	1.970	2.534	0.848	0	5.078	0	2.004
7	1.134	1.277	0.419	0.8882	0.105	1.672	0.118	1.882	2.704	0.833	0.205	5.203	0.076	1.924
8	1.061	1.175	0.373	0.9027	0.167	1.638	0.185	1.815	2.847	0.820	0.387	5.307	0.136	1.864
9	1.000	1.094	0.337	0.9139	0.219	1.609	0.239	1.761	2.970	0.808	0.546	5.394	0.184	1.816
10	0.949	1.028	0.308	0.9227	0.262	1.584	0.284	1.716	3.078	0.797	0.687	5.469	0.223	1.777
11	0.905	0.973	0.285	0.9300	0.299	1.561	0.321	1.679	3.173	0.787	0.812	5.534	0.256	1.744
12	0.866	0.925	0.266	0.9359	0.331	1.541	0.354	1.646	3.258	0.778	0.924	5.592	0.284	1.716
13	0.832	0.884	0.249	0.9410	0.359	1.523	0.382	1.618	3.336	0.770	1.026	5.646	0.308	1.692
14	0.802	0.848	0.235	0.9453	0.384	1.507	0.406	1.594	3.407	0.762	1.121	5.693	0.329	1.671
15	0.775	0.816	0.223	0.9490	0.406	1.492	0.428	1.572	3.472	0.755	1.207	5.737	0.348	1.652
16	0.750	0.788	0.212	0.9523	0.427	1.478	0.448	1.552	3.532	0.749	1.285	5.779	0.364	1.636
17	0.728	0.762	0.203	0.9551	0.445	1.465	0.466	1.534	3.588	0.743	1.359	5.817	0.379	1.621
18	0.707	0.738	0.194	0.9576	0.461	1.454	0.482	1.518	3.640	0.738	1.426	5.854	0.392	1.608
19	0.688	0.717	0.187	0.9599	0.477	1.443	0.497	1.503	3.689	0.733	1.490	5.888	0.404	1.596
20	0.671	0.697	0.180	0.9619	0.491	1.433	0.510	1.490	3.735	0.729	1.548	5.922	0.414	1.586
21	0.655	0.679	0.173	0.9638	0.504	1.424	0.523	1.477	3.778	0.724	1.606	5.950	0.425	1.575
22	0.640	0.662	0.167	0.9655	0.516	1.415	0.534	1.466	3.819	0.720	1.659	5.979	0.434	1.566
23	0.626	0.647	0.162	0.9670	0.527	1.407	0.545	1.455	3.858	0.716	1.710	6.006	0.443	1.557
24	0.612	0.632	0.157	0.9684	0.538	1.399	0.555	1.445	3.895	0.712	1.759	6.031	0.452	1.548
25	0.600	0.619	0.153	0.9696	0.548	1.392	0.565	1.435	3.931	0.709	1.804	6.058	0.459	1.541

Source: Reprinted by permission of the American Society for Testing and Materials 1950



ประวัติผู้เขียน

นายบุญโรจน์ สิมะบวรสุทธิ เกิดเมื่อวันที่ 14 ธันวาคม พ.ศ. 2499 ที่กรุงเทพมหานคร สำเร็จการศึกษาปริญญาตรีอุตสาหกรรมศาสตรบัณฑิต จากคณะวิศวกรรมศาสตร์ สถาบันเทคโนโลยีพระจอมเกล้า พระนครเหนือ เมื่อปีการศึกษา 2525