

APPENDIX A

Sample of Calculations



A.1 Determination of fitting equation of boundary potential.

The fitting equation of boundary potential which was recorded during the experiment is determined by means of method of least square. The boundary condition is in form of:-

$$V = S_1 (x^2 + y^2) + c_1$$

In case of the square used in this experiment, one variable is equal to 10, the equation is reduced to

$$V = S_1 x^2 + c_1$$

Let $X = x^2$ for square and $X = x^2 + y^2$ for the other,

$$V = S_1 X + c_1$$

The coefficient S_1 and the constant C_1 can be determined by means of the method of least square as follow:-

$$mS_1 + \left(\sum_{i=1}^m X_i \right) c_1 = \sum_{i=1}^m V_i$$

(B.1)

$$\left(\sum_{i=1}^m X_i \right) S_1 + \left(\sum_{i=1}^m X_i^2 \right) c_1 = \sum_{i=1}^m X_i V_i$$

m = number of datas.

The following table shows a part of the calculating table.¹

1

Full datas of x , y and V are in table 1.

x	y	V	X	X ²	X·V
10.0	5.2	2.80	27.04	731.16	75.71
10.0	5.4	3.10	29.16	850.31	87.77
10.0	5.6	3.22	31.36	983.45	100.93
10.0	5.8	3.43	33.64	1,131.65	115.39
10.0	6.0	3.63	36.00	1,296.00	130.68
sum		324.874	3,234.00	190,137.43	18,891.82

Substituting into eq. (A-1)

$$98 S_1 + 3234 c_1 = 324.87$$

$$3234 S_1 + 190,137.43 c_1 = 18,891.82$$

$$S_1 = .09796$$

$$c_1 = .08250$$

Thus the fitting equation of boundary potential is

$$V = .09796 x^2 + .0825$$

A.2 Transformation of potential to conjugate function.

On the boundary, the values of conjugate function are

$$\psi = \frac{1}{2} (x^2 + y^2)$$

For shaft of square cross section, the boundary potential is given by eq. (2.27)

$$V = 0.1 (x^2 + y^2) - 10$$

So the relation between ψ and V are

$$\psi = 5 (V + 10) \quad (\text{A.2})$$

also from eq. (2-31) and eq. (2-34)

$$\text{For rectangular} \quad \psi = 5 (V + 2.5) \quad (\text{A.3})$$

$$\text{For I - section} \quad \psi = \frac{10}{3} (V + 0.6) \quad (\text{A.4})$$

For example, the potential 2.4 V on square shaft will represent the conjugate function,

$$\psi = 5 (2.4 + 10.0) = 62.0$$

but on I - section, it will represent

$$\psi = \frac{10}{3} (2.4 + 0.6) = 10.0$$

A.3 Construction of the shear stress line.

The conjugate function at any point can be transform to shearing stress function by eq. (2.15)

$$\phi = \psi - \frac{1}{2} (x^2 + y^2) = \psi - \frac{1}{2} r^2$$

The shear stress lines can be constructed by means of the equipotential line obtained from the experiment as follow:-

Let $\psi_0, \psi_1, \psi_2, \dots, \psi_n$ be the values of conjugate function corresponding to equipotential line.

According to the experiment, the increment of potential between the equipotential lines $\Delta\psi$ are constant.

Choose $\psi_0 = 0$, thus $\psi_1 = \Delta\psi, \psi_2 = 2\Delta\psi, \psi_3 = 3\Delta\psi, \dots, \psi_n = n\Delta\psi$

Take the origin as center of circles whose radius are r_1, r_2, \dots, r_n

Let $r_0 = 0$ at origin, $r_1 = \sqrt{2\Delta\psi}, r_2 = \sqrt{4\Delta\psi}, \dots, r_n = \sqrt{2n\Delta\psi}$

Consider the value of shear stress function at the intersection of the circles and the equipotential line.

	ψ_0	ψ_1	ψ_2	-----	ψ_n
r_1	$-\Delta\psi$	0	$\Delta\psi$	-----	$n\Delta\psi$
r_2	$-2\Delta\psi$	$-\Delta\psi$	0	-----	$(n-1)\Delta\psi$
r_m	$-m\Delta\psi$	$-(m-1)\Delta\psi$	$-(m-2)\Delta\psi$	-----	$(n-m)\Delta\psi$

We may conclude that as $n = 1, 2, 3, 4, \dots$

the intersection point of ψ_n and r_n will form shear stress line = 0

" " " ψ_n " r_{n-1} " " " = $\Delta \psi$

" " " ψ_n " r_{n-1} " " " = $m \Delta \psi$

A-4. Determination of shear stress components.

The shear stress components can be calculated from both ψ and ϕ since the experiment is done on ψ , so we will calculate from ψ .

Consider on the axis $y = \text{constant}$, the value of V is function of x only. Assuming the fitting equation is the fourth degree polynomial function.

$$V = a + bx + cx^2 + dx^3 + ex^4$$

According to the method of least square, the co-efficient of fitting equation can be determined from the following equation.

$$\begin{aligned} ma + \left(\sum_{i=1}^m x_i\right) b + \left(\sum_{i=1}^m x_i^2\right) c + \left(\sum_{i=1}^m x_i^3\right) d + \left(\sum_{i=1}^m x_i^4\right) e &= \sum_{i=1}^m \psi_i \\ \left(\sum_{i=1}^m x_i\right) a + \left(\sum_{i=1}^m x_i^2\right) b + \left(\sum_{i=1}^m x_i^3\right) c + \left(\sum_{i=1}^m x_i^4\right) d + \left(\sum_{i=1}^m x_i^5\right) e &= \sum_{i=1}^m x_i \psi_i \\ \left(\sum_{i=1}^m x_i^2\right) a + \left(\sum_{i=1}^m x_i^3\right) b + \left(\sum_{i=1}^m x_i^4\right) c + \left(\sum_{i=1}^m x_i^5\right) d + \left(\sum_{i=1}^m x_i^6\right) e &= \sum_{i=1}^m x_i^2 \psi_i \\ \left(\sum_{i=1}^m x_i^3\right) a + \left(\sum_{i=1}^m x_i^4\right) b + \left(\sum_{i=1}^m x_i^5\right) c + \left(\sum_{i=1}^m x_i^6\right) d + \left(\sum_{i=1}^m x_i^7\right) e &= \sum_{i=1}^m x_i^3 \psi_i \\ \left(\sum_{i=1}^m x_i^4\right) a + \left(\sum_{i=1}^m x_i^5\right) b + \left(\sum_{i=1}^m x_i^6\right) c + \left(\sum_{i=1}^m x_i^7\right) d + \left(\sum_{i=1}^m x_i^8\right) e &= \sum_{i=1}^m x_i^4 \psi_i \end{aligned}$$

For example, when they are substituted by the data in table 7

$$\begin{aligned}
 18a + 107.57b + 735.77c + 5530.37d + 44253.6e &= 23.365 \\
 107.57a + 735.77b + 5530.37c + 44253.6d + 369139e &= 121.527 \\
 735.77a + 5530.7b + 44253.6c + 369139d + 3.16779 \times 10^6 e &= 720.032 \\
 5530.37a + 44253.6b + 369,139c + 3.16779 \times 10^6 d + 27.7376 \times 10^6 e &= 4,733.13 \\
 44253.6a + 369,139b + 3.16779 \times 10^6 c + 27.7376 \times 10^6 d + 246.507 \times 10^6 e &= 33633.8
 \end{aligned}$$

Solve the equation, we get

$$a = 1.686, b = .0184, c = -.00190, d = -.000138, e = -.000154$$

$$\text{Thus } V = 1.686 + .0184x - .0019x^2 - .000138x^3 - .000154x^4$$

$$\frac{\partial V}{\partial x} = .0184 - .0038x - .000414x^2 - .000616x^3$$

Consider eq. (A -2)

$$\begin{aligned}
 \psi &= 5 (V + 10) \\
 \frac{\partial \psi}{\partial x} &= 5 \frac{\partial V}{\partial x} \\
 \frac{\sum yz}{\text{Max}} &= - \frac{\partial \psi}{\partial x} + x
 \end{aligned}$$

for example at $x = 8.0$

$$V_f = 1.686 + .0184 \times 8 - .0019(8)^2 - .000138(8)^3 - .000154(8)^4 = 1.010$$

$$\begin{aligned}
 \psi_f &= 5 (1.010 + 10) = 55.05 \\
 \frac{\partial V_f}{\partial x} &= .0184 - .0038(8) - .000414(8)^2 - .000616(8)^3 = -.3539 \\
 \frac{\partial \psi_f}{\partial x} &= -.3539 \times 5 = -1.7695 \\
 \frac{\sum yz}{\text{Max}} &= 1.7695 + 8.00 = 9.7695 \approx 9.77
 \end{aligned}$$

Since the method of solving the fitting equation is rather laboriously if there are several sets of datas, so a computer program is provided in Appendix (B)

If a single point in the region is considered, it is much easy to approximate from it's neighborhood points by the following method. For example, to evaluate $\frac{\partial V}{\partial x}$ at $x = 8.0, y = 0$.

It is observed that $y = 0$

$$x = 7.38, \quad V = 1.2$$

$$x = 8.00, \quad V = 1.0$$

$$x = 8.56, \quad V = 0.8$$

A second degree polynomial function of x is assigned to be the value of V .

$$V = a + bx + cx^2$$

$$\text{at } x = 7.38, \quad a + 7.38b + 54.4644c = 1.2$$

$$\text{at } x = 8.00, \quad a + 8.00b + 64c = 1.0$$

$$\text{at } x = 8.56, \quad a + 8.56b + 73.2736c = 0.8$$

$$c = - .02929$$

$$b = .1279$$

$$a = 1.85$$

$$\begin{aligned} V_g &= 1.85 + .1279x - .02929x^2 \\ &= 1.85 + .1279 \times 8 - .02929(8)^2 = .9986 \end{aligned}$$

$$\begin{aligned}\frac{\partial V_s}{\partial x} &= .1279 - .05858x \\ &= .1279 - .05858 \times 8 = - .34074 \\ \frac{\partial \psi_s}{\partial x} &= - .34074 \times 5 = - 1.7037 \\ \frac{T}{\mu\alpha} &= - (- 1.7039) + 8 = 9.7039 \approx 9.70\end{aligned}$$

which is less than 1% different from the former value

A-5 Determination of the torsional stiffness.

From eq. (2 - 17)

$$M = 2 \mu\alpha \iint_R \phi \, dx dy$$

$$\text{Since } \iint_R \phi \, dx dy = \lim_{\substack{\Delta x \rightarrow 0 \\ \Delta y \rightarrow 0}} \sum_{k=1}^m \phi_k \cdot \Delta x_k \cdot \Delta y_k$$

The integral part can be approximated by dividing the area of specimen into many equal squares. The value of ϕ at the center of each square is determined by interpolation. Since the specimen represents a quarter of cross-section.

$$\begin{aligned}\iint_R \phi \, dx dy &\approx 4 \sum_{k=1}^m \phi_k \cdot \Delta x_k \cdot \Delta y_k \\ \frac{M}{\mu\alpha} &\approx 8 \sum_{k=1}^m \phi_k \cdot \Delta x_k \cdot \Delta y_k\end{aligned} \quad (\text{A - 5})$$

In case of equal squares.

$$A_k = \Delta x_k \Delta y_k = \text{constant}$$

$$\frac{M}{\mu\alpha} = 8 A \sum_{k=1}^m \phi_k$$

For example, the square specimen is divided into 25 equal squares, each square is equal to 4 units as shown in fig. 20. The value of ϕ of each square are in table 18, we get

$$\sum_{k=1}^{21} \phi_k = 709.6$$

$$\frac{M}{\mu\alpha} = 8 \times 4 \times 709.6 = 22,707.2$$

A - 6 Determine K and K_1

From eq. (2 - 27) and (2 - 28)

$$K = \frac{I_{\max}}{\mu\alpha a}$$

$$K_1 = \frac{M}{\mu\alpha a^2 b}$$

for example, square specimen. $\frac{M}{\mu\alpha} = 22,707.2$, $\frac{I_{\max}}{\mu\alpha} = 13.47$

$$K = \frac{13.47}{20} = .6735 \approx .674$$

$$K_1 = \frac{22,707.2}{20^4} = .1419$$

APPENDIX B

COMPUTER PROGRAM AND FLOW CHART



B.1 COMPUTER PROGRAM FOR DETERMINING FITTING EQUATION.

```
C      DETERMINE EMPIRICAL FORMULA IN POLYNOMIAL FORM BY
C      LEAST SQUARE METHOD
C
      DIMENSION P (200), PHI (200), A(7,7), B(7), C(7), X(7), E(7,7)
C
      READ DATA
C
      ND = NO. OF PROBLEMS PUNCH IN A CARD
C
      N = NO. OF EQUATIONS, M = NO. OF DATAS PUNCH IN A CARD
C
      P = VALUE OF VARIABLES, PHI = VALUE OF FUNCTIONS PUNCH 4 SETS EACH CARD
C
      READ (2,5) ND
5     FORMAT (I2)
      DO 500 NN = 1, ND
      READ (2,10) N,M
10    FORMAT (I2,I4)
      DO 20 I = 1,M,4
      READ (2,15) P(I), PHI(I), P(I+1), PHI(I+1), P(I+2), PHI(I+2), P(I+3), PHI(
1I+3)
      WRITE (3,15) P(I), PHI(I), P(I+1), PHI(I+1), P(I+2), PHI(I+2), P(I+3), PHI(
1I+3)
15    FORMAT (8F9.4)
20    CONTINUE
      IF(N.LE.0.OR.N.GT.7.OR.M.GT.200) GO TO 480
      IF(M.LT.N) GO TO 480
```

```
C
C      CLEAR ARRAY
C
      DØ 25 I = 1,7
      C(I) = 0.0
      D = 0.0
      X(I) = 0.0
      B(I) = 0.0
      DØ 25 J = 1,7
      A(I,J) = 0.0
      E(I,J) = 0.0
25  CØNTINUE
C
C      CALCULATE CØNSTANT AND CØEFFICIENTS
C
      DØ 35 I = 1,N
      DØ 30 J = 1,N
      NA = I + J - 2
      DØ 30 K = 1,M
      A(I,J,) = A(I,J) + P(K)**NA
      E(I,J) = A(I,J)
30  CØNTINUE
      DØ 35 L = 1,N
      C(I) = C(I) + PHI(L)*P(L)**(I-1)
35  CØNTINUE
```

```

WRITE (3,40)
40  FORMAT (6H0GIVEN/)
      DO 50 I = 1,N
WRITE (3,50) (A(I,J), J = 1,N), C(I)
50  FORMAT (1X10,8 (E 13.6, 2X) )
60  CONTINUE

C
C  SOLVE SIMULTANEOUS EQUATION BY METHOD OF DIVISION BY LEADING
C  COEFFICIENT
C
C  PERFORM DIVISION
C
      DO 180 KA = 1,N
      DO 110 I = KA, N
      D = A (I,KA)
      C(I) = C(I)/D
      DO 110 J = KA,N
      A(I,J)= A(I,J)/D
110  CONTINUE

C
C  PERFORM SUBTRACTION
C
      KB = KA+1
      DO 160 I = KB, N
      C(I) = C(I) - C(KA)

```

```

DØ 160 J = KA, N
A(I,J) = A(I,J) - A(KA,J)
160  CØNTINUE
180  CØNTINUE
C
C  COMPUTE RØØTS ØF THE SIMULTANEOUS EQUATIØNS
C
DØ 210 I = 1,N
K = N - I+1
SUM = 0.0
DØ 205 J = 1, N
SUM = SUM + A(K,J)*X(J)
205  CØNTINUE
X(K) = C(K) - SUM
210  CØNTINUE
WRITE (3,220)
220  FØRMAT (27HØRØØTS ØF THE EQUATIØNS ARE /)
DØ 240 I = 1,N
WRITE (3,230) I, X(I)
230  FØRMAT (3HØX(, I2,2H) =, E 13.6 )
240  CØNTINUE
C
C  CHECK RØØTS ØF EQUATIØNS
C

```

```

DØ 260 I = 1,N
DØ 260 J = 1,N
B(I) = B(I) +E(I,J)*X(J)
260 CØNTINUE
WRITE (3,270)
270 FØRMAT (32HØ CHECK RØØTS FRØM LEFT HAND SIDE/)
DØ 290 I = 1,N
WRITE (3,280) I, B(I)
280 FØRMAT (3HØB (I2,2H) = , E15.8)
290 CØNTINUE
C
C COMPUTE SUM ØF SQUARE ØF DEVIATIØN
C
SUMV = 0.0
DØ 310 I = 1,M
DEV=X(1)+X(2)*P(I)+X(3)*P(I)**2+X(4)*P(I)**3+X(5)*P(I)**4+X(6)*P(I)
1)**5+X(7)*P(I)**6-PHI(I)
SDEV = DEV**2
SUMV = SUMV + SDEV
310 CØNTINUE
WRITE(3,320)SUMV
320 FØRMAT (3ØHØ SUM ØF SQUARE ØF DEVIATIØN =, E15.8)
WRITE (3,300)
300 FØRMAT (121HØ*****-----*
1*****-----*

```


2///)

GØ TØ 500

480 WRITE (3,490)

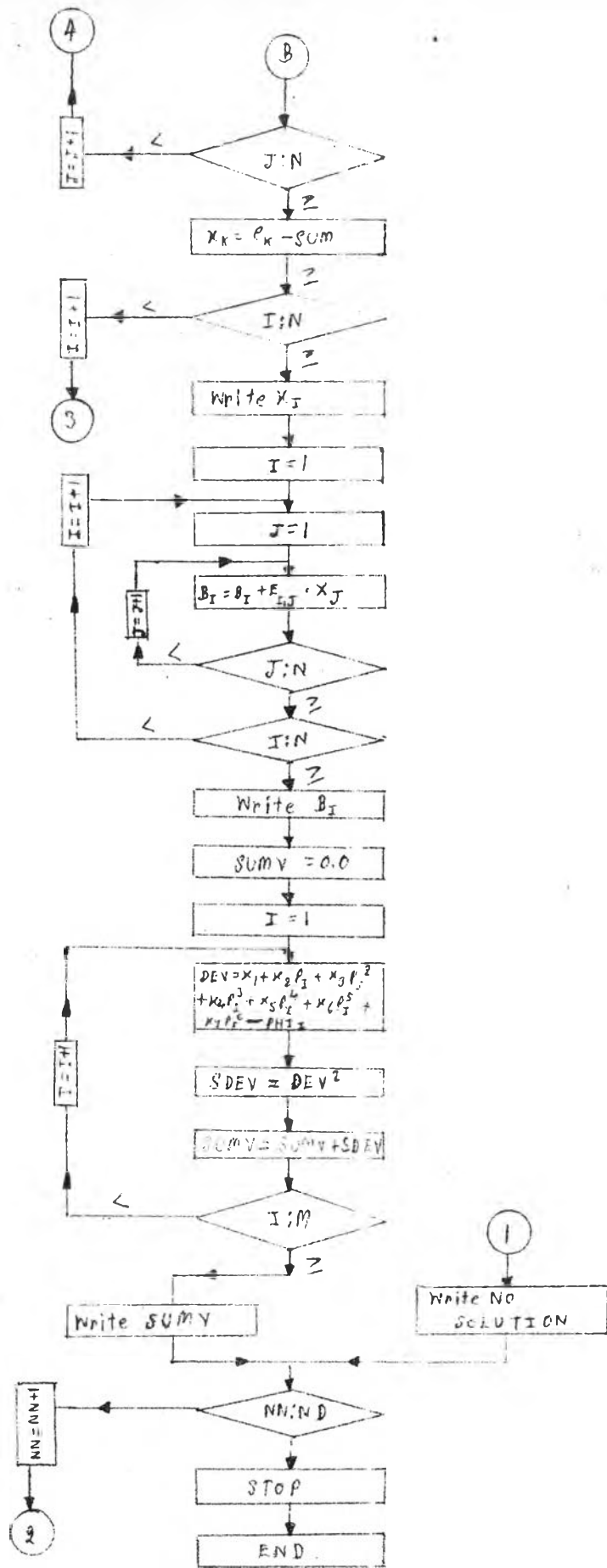
490 FØRMAT (12HONØ SØLUTIØN)

WRITE(3,300)

500 CØNTINUE

STØP

END



B.3 COMPUTER PROGRAM FOR SOLVING ANALYTICAL EQUATION OF CONJUGATE FUNCTIONS
AND SHEAR STRESS FUNCTION OF THE SQUARE SHAFT.

```

DIMENSION P(10),V(10)

A = 10.0
B = 10.0

IA = A
IB = B
ID = 2

DO 300 I = 1,IB
DO 300 J = 1,10,ID
AI = I
AJ = J
Y = (AI-1.) + (AJ - 1.)/10
WRITE (3,10) Y
10  FORMAT (3H0Y=,F4.1, 24X,21HCØNJUGATE FUNCTIØN,
135X,17H STRESS FUNCTIØN/)
WRITE(3,20)
20  FORMAT(1Hb, 14X, 3Hb.0, 7X, 3Hb.2, 7X,3Hb.4, 7X,3Hb.6,7X,3Hb.8,
112X,3Hb.0, 7X,3Hb.2, 7X,3Hb.4, 7X,3Hb.6, 7X,3Hb.8/)
DO 300 K = 1,IA
AK = K
DO 200 L = 1,10, ID
AL = L
X = (AK - 1.) + (AL - 1.)/10.

```

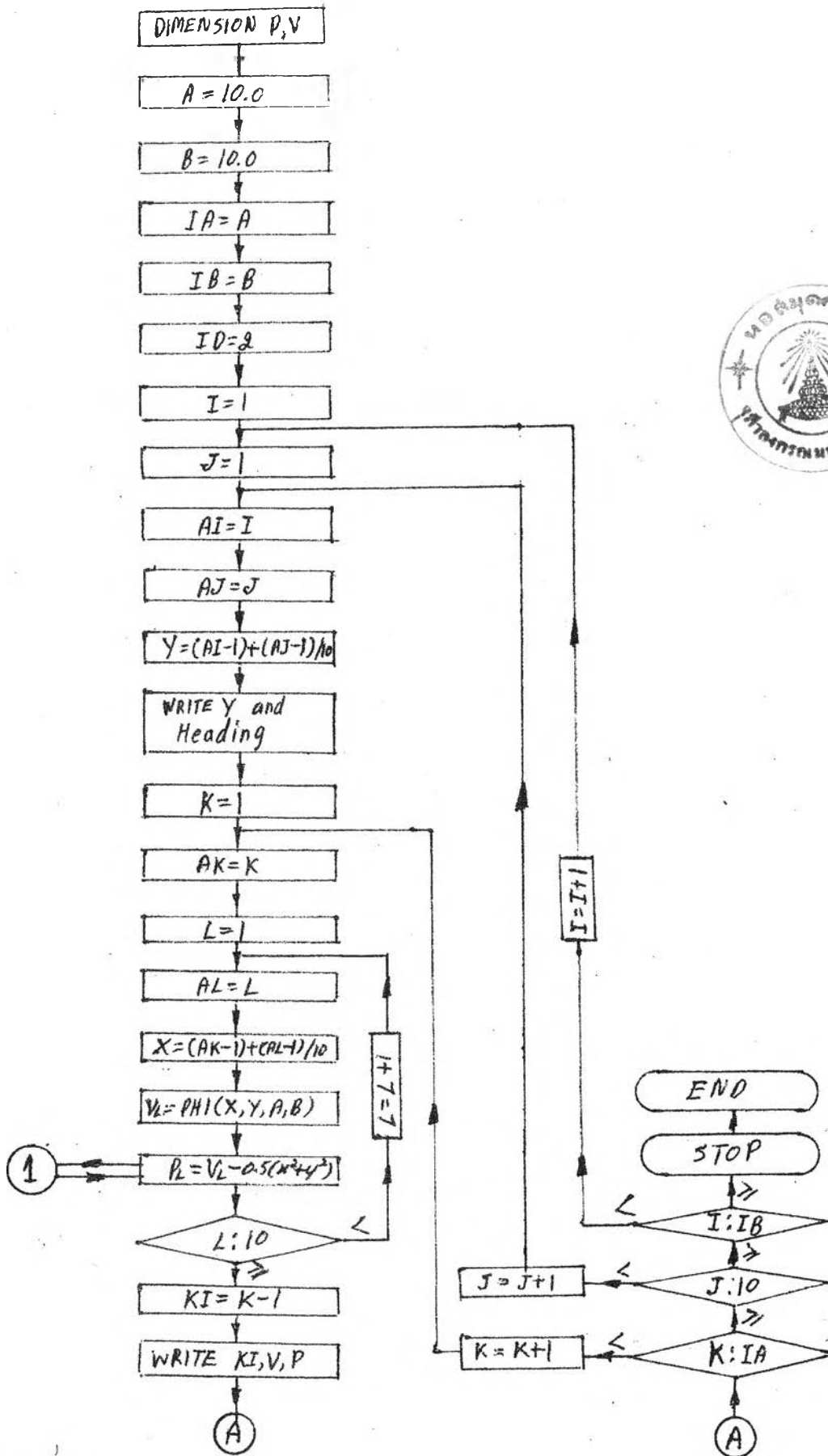
```

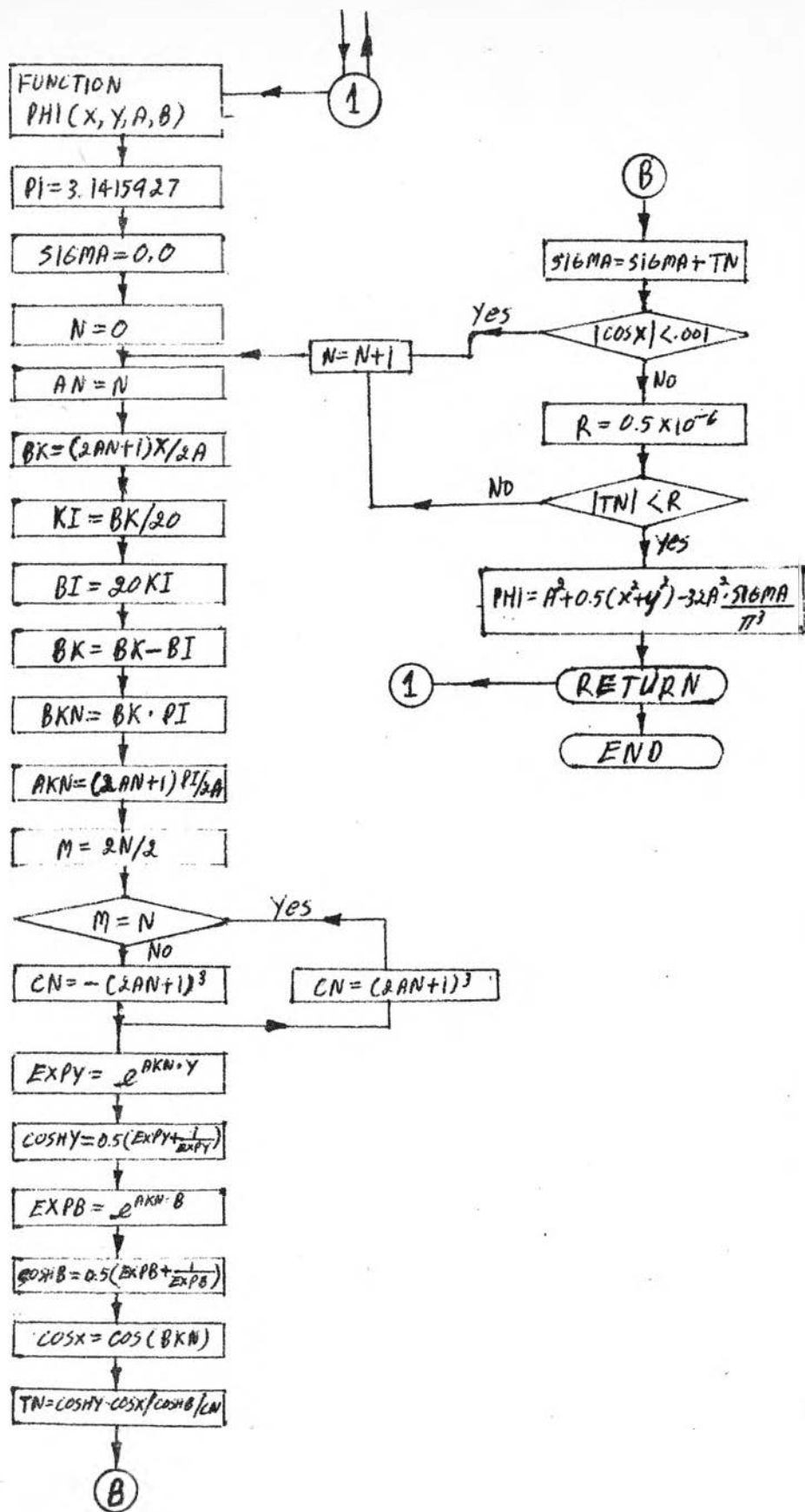
V(L) = PHI(X,Y,A,B)
200 P(L) = V(L) - 0.5* (X**2+Y**2)
230 KI = K - 1
WRITE (3,240) KI,(V(M), M=1,10,1D), (P(N), N = 1,10,1D)
240 FØRMAT (3Hb.X =, I1,7X,5F10.4, 5X, 5F10.4/)
300 CØNTINUE
STØP
END
FUNCTIØN PHI(X,Y,A,B)
PI = 3.1415927
SIGMA = 0.0
N = 0
100 AN = N
BK = (2*AN + 1.)*X/(2.*A)
KI = BK/20
BI = 20*KI
BK = BK - BI
BKN = BK*PI
AKN = (2.*AN+1.) *PI/(2.*A)
M = N/2*2
IF (M.EQ.N) GØ TØ 105
CN = - (2.*AN+1.)**3
GØ TØ 106
105 CN = (2.*AN+1.)**3
106 EXPY = EXP (AKN*Y)

```

```
CØSHY = 0.5*(EXPY +1./EXPY)
EXPB = EXP(AKN*B)
CØSHB= 0.5*(EXPB +1./EXPB)
CØSX = COS (BKN)
TN = CØSHY*CØSX/CØSHB/CN
110 SIGMA = SIGMA + TN
IF (ABS (CØSX) .LT.0.001) GØ TØ 25
R= 0.5E-6
IF(ABS(GØSX) .LT.0.001) GØ TØ 120
25 N=N+1
GØ TØ 100
120 PHI=A**2+0.5*(Y**2-X**2)-32.*A**2*SIGMA/PI**3
RETURN
END
```

B.4 Flow chart for solving analytical equation of the square shaft





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