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APPENDICES

Appendix A

Criteria for the selection of lead formulations

These two criteria were employed for the selection of lead formulations from IR reactor system for further testing.

Criteria 1:

1. $T_{avg,2} - T_{avg,1} > 5$
2. $T_{avg,2} > T_{avg,1} + SD_1$ or else $SD_1 < SD_2$
3. $\Delta T_{avg} > SD_1 + SD_2$

Criteria 2:

1. $T_{avg,2} - T_{avg,1} > 5$
2. $T_{avg,2} > T_{avg,1} + SD_1$
3. $T_{avg,2} - SD_2 > T_{avg,1} + 0.5SD_1$

Where ΔT_{avg} = average different temperature

$T_{avg,1}$ = average temperature of each catalyst sample before reaction
(under helium stream)

$T_{avg,2}$ = average temperature of each catalyst sample during reaction
(under reactant stream)

SD_1 = standard deviation before reaction (under helium stream)

SD_2 = standard deviation during reaction (under reactant stream).

Appendix B

Table B1 Raw data obtained from IR reactor of all catalyst formulations

| Catalyst | Ratio of metals on binary loading (%) | | | | Before reaction | | During reaction | | ΔT_{avg} |
|-----------------|--|-----------|-----------|-----------|------------------------|-----------------------|------------------------|-----------------------|------------------|
| | Ni | La | Fe | Li | T_{avg} | SD₁ | T_{avg} | SD₂ | |
| C1 | 90 | 10 | - | - | 333.4 | 5.2 | 337.6 | 2.46 | 4.2 |
| C2 | 80 | 20 | - | - | 362.0 | 4.6 | 366.0 | 1.73 | 4 |
| C3 | 70 | 30 | - | - | 393.2 | 2.1 | 392.5 | 3.23 | -0.7 |
| C4 | 60 | 40 | - | - | 337.7 | 6.7 | 335.5 | 9.28 | -2.2 |
| C5 | 50 | 50 | - | - | 363.8 | 2.4 | 365.4 | 5.80 | 1.6 |
| C6 | 40 | 60 | - | - | 289.6 | 4.9 | 293.0 | 4.86 | 3.4 |
| C7 | 30 | 70 | - | - | 288.8 | 17.4 | 291.0 | 3.49 | 2.2 |
| C8 | 20 | 80 | - | - | 319.1 | 23.8 | 313.5 | 7.75 | -5.6 |
| C9 | 10 | 90 | - | - | 309.9 | 5.7 | 331.2 | 5.60 | 21.3 |
| C10 | - | 10 | - | 90 | 409.0 | 9.7 | 416.4 | 4.34 | 7.4 |
| C11 | - | 20 | - | 80 | 377.1 | 5.0 | 378.8 | 3.12 | 1.7 |
| C12 | - | 30 | - | 70 | 331.4 | 11.5 | 336.9 | 11.49 | 5.5 |
| C13 | - | 40 | - | 60 | 409.0 | 9.1 | 408.5 | 9.83 | -0.5 |
| C14 | - | 50 | - | 50 | 381.3 | 4.1 | 380.2 | 2.40 | -1.1 |
| C15 | - | 60 | - | 40 | 303.9 | 15.4 | 296.8 | 8.80 | -7.1 |
| C16 | - | 70 | - | 30 | 315.6 | 7.5 | 360.0 | 20.93 | 44.4 |
| C17 | - | 80 | - | 20 | 335.3 | 15.1 | 364.1 | 5.56 | 28.8 |
| C18 | - | 90 | - | 10 | 299.4 | 5.4 | 301.2 | 6.78 | 1.8 |
| C19 | 90 | - | 10 | - | 300.2 | 15.9 | 320.3 | 4.62 | 20.2 |
| C20 | 80 | - | 20 | - | 351.0 | 1.0 | 349.2 | 2.67 | -1.8 |
| C21 | 70 | - | 30 | - | 379.8 | 1.7 | 415.6 | 9.87 | 35.8 |
| C22 | 60 | - | 40 | - | 325.0 | 5.7 | 330.3 | 1.37 | 5.3 |
| C23 | 50 | - | 50 | - | 361.2 | 1.6 | 360.9 | 1.11 | -0.3 |
| C24 | 40 | - | 60 | - | 334.1 | 10.5 | 342.3 | 8.64 | 8.2 |
| C25 | 30 | - | 70 | - | 335.1 | 8.5 | 309.3 | 4.03 | -25.8 |
| C26 | 20 | - | 80 | - | 335.7 | 10.9 | 336.8 | 3.98 | 1.2 |
| C27 | 10 | - | 90 | - | 319.3 | 7.5 | 319.5 | 3.86 | 0.3 |
| C28 | 90 | - | - | 10 | 355.5 | 7.5 | 357.8 | 1.82 | 2.3 |

Table B1 Continued

| Catalyst | Ratio of metals on binary loading (%) | | | | Before reaction | | During reaction | | Tavg |
|-----------------|--|-----------|-----------|-----------|------------------------|-----------|------------------------|-----------|-------------|
| | Ni | La | Fe | Li | Tavg | SD | Tavg | SD | |
| C31 | 60 | - | - | 40 | 299.7 | 8.0 | 300.5 | 2.25 | 0.8 |
| C32 | 50 | - | - | 50 | 349.8 | 4.0 | 347.2 | 2.51 | -2.7 |
| C33 | 40 | - | - | 60 | 313.7 | 5.7 | 311.8 | 3.03 | -1.9 |
| C34 | 30 | - | - | 70 | 372.4 | 3.0 | 370.9 | 3.93 | -1.5 |
| C35 | 20 | - | - | 80 | 339.5 | 6.9 | 336.3 | 4.73 | -3.2 |
| C36 | 10 | - | - | 90 | 284.0 | 6.6 | 289.4 | 12.41 | 5.4 |
| C37 | - | - | 10 | 90 | 300.4 | 2.5 | 303.0 | 1.15 | 2.6 |
| C38 | - | - | 20 | 80 | 324.6 | 1.42 | 328.0 | 2.77 | 3.4 |
| C39 | - | - | 30 | 70 | 319.8 | 3.31 | 329.8 | 5.30 | 10 |
| C40 | - | - | 40 | 60 | 305.6 | 1.68 | 308.8 | 2.67 | 3.2 |
| C41 | - | - | 50 | 50 | 332.4 | 0.80 | 336.0 | 1.53 | 3.6 |
| C42 | - | - | 60 | 40 | 355.4 | 1.62 | 356.8 | 0.68 | 1.4 |
| C43 | - | - | 70 | 30 | 301.8 | 3.76 | 308.4 | 2.92 | 6.6 |
| C44 | - | - | 80 | 20 | 330.4 | 7.23 | 334.6 | 2.21 | 4.2 |
| C45 | - | - | 90 | 10 | 358.0 | 1.26 | 361.6 | 2.13 | 3.6 |
| C46 | 0 | - | - | - | 360.2 | 3.06 | 361.0 | 1.00 | 0.8 |
| C47 | 0.1 | - | - | - | 342.2 | 4.35 | 341.6 | 2.13 | -0.6 |
| C48 | 1 | - | - | - | 298.6 | 3.56 | 299.2 | 4.84 | 0.6 |
| C49 | 2 | - | - | - | 376.6 | 2.24 | 377.8 | 0.68 | 1.2 |
| C50 | 3 | - | - | - | 349.2 | 2.32 | 349.6 | 1.59 | 0.4 |
| C51 | 5 | - | - | - | 324.2 | 2.79 | 324.4 | 1.37 | 0.2 |
| C52 | 7 | - | - | - | 369.6 | 2.15 | 366.6 | 1.69 | -3 |
| C53 | 9 | - | - | - | 341.4 | 0.49 | 346.0 | 1.53 | 4.6 |
| C54 | 10 | - | - | - | 328.0 | 1.79 | 327.6 | 1.88 | -0.4 |

Appendix C

The reaction of CO oxidation is shown as Reaction (2.1). Conversion of this reaction can be calculated;

$$\% \text{CO conversion} = \left[\frac{\text{mole CO in} - \text{mole CO out}}{\text{mole CO in}} \right] * 100$$

Table C1 Carbon monoxide conversion of lead formulations tested by conventional method

| Catalyst | Ratio of metals on binary loading (%) | | | | Carbon monoxide conversion (%) |
|-----------------|--|-----------|-----------|-----------|---------------------------------------|
| | Ni | La | Fe | Li | |
| Support | - | - | - | - | 67.86 |
| C1 | 90 | 10 | - | - | 100.0 |
| C3 | 70 | 30 | - | - | 100.0 |
| C8 | 20 | 80 | - | - | 99.30 |
| C16 | - | 70 | - | 30 | 6.84 |
| C17 | - | 80 | - | 20 | 11.65 |
| C18 | - | 90 | - | 10 | 11.54 |
| C19 | 90 | - | 10 | - | 79.55 |
| C20 | 80 | - | 20 | - | 24.74 |
| C21 | 70 | - | 30 | - | 31.99 |
| C23 | 50 | - | 50 | - | 7.53 |
| C27 | 10 | - | 90 | - | 4.86 |
| C39 | | - | 40 | 60 | 13.33 |
| C51 | 5 | - | - | - | 100.0 |

Table C2 Carbon monoxide conversion of La/Ni loaded catalyst with the La/Ni ratio of 1:9 at various temperature

| Reaction temperature(°C) | Carbon monoxide conversion (%) of the catalyst with Ni:La=9:1 |
|---------------------------|---|
| 80 | 5.3 |
| 150 | 26.85 |
| 250 | 93.66 |
| 350 | 100 |

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