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**SIMULATION OF AIR FLOW PAST THE PARALLEL
INCLINED FLAT PLATES IN A SQUARE DUCT**

Mr. Santi Wattananusorn

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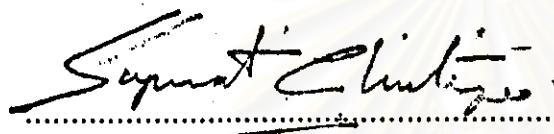
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Thesis Advisor **Somprasong Srichai, Ph.D.**

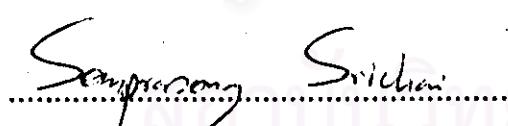
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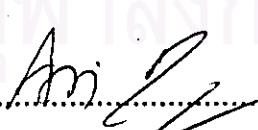
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อ. ที่ปรึกษาร่วม : ดร. อศิ บุญจิราคุลย์

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ปรากฏการณ์การไหลของอากาศผ่านแผ่นแบบเรียบที่อิ่งบนกันในท่อรูปสี่เหลี่ยมจัตุรัสดูก็ทิกมา ผ่านวิธีแก้ไขเชิงตัวเลข โดยใช้เทคนิคการคำนวณพลศาสตร์ของไอล (CFD) ไปร่วมกับคอมพิวเตอร์ที่ซื้อ ฟินิกซ์ (PHOENICS) ถูกนำมาใช้เพื่อหาค่าตอบสำหรับการไหลแบบปั๊มน้ำที่สถานะคงตัวในสามมิติ ภายใต้หลักการ ของไฟฟ้าในตัวถุง สมการควบคุมคือ สมการนาวีร์-สโตกส์ในรูปค่าเฉลี่ยของอิทธิพลทั้งหมดที่ไม่สามารถอัด ตัวได้ ความเด่นเรียบในลดดูกรกำหนดด้วยแบบจำลองความปั๊มน้ำเกต-อัพชิล่อน โดยใช้สมมุติฐานความหนืดที่ อนุนวัณของบุสเซเนส

เพื่อตรวจสอบความถูกต้องเชิงตัวเลขและสภาพที่ใช้ได้ของแบบจำลองความปั๊มน้ำ ในขั้นแรก ผลของการคำนวณถูก拿来ไปเปรียบเทียบกับข้อมูลของความเร็วซึ่งได้มาจากการทดลอง การเปรียบเทียบระหว่าง ผลที่ได้มาจากการวัดและผลที่ได้มาจากการคำนวณ โดยทั่วไปเป็นที่น่าพอใจในด้านความไม่ตรงกันบ้างใน บางแห่ง ในตอนท้ายผลกระบวนการของจำนวนแผ่นแบบเรียบ ความเร็วของแผ่นแบบเรียบ และการไหล ในท่อตัวถุงเรียบในลดดูงสูง ที่มีต่อระบบทางซึ่งใช้ในการปรับตัวเข้าสู่สภาวะการไหลคงรูป ตลอดจนการ ติดลบนความดันรวม ถูกตรวจสอบ

การทำนายแสดงให้เห็นว่าระบบทางสำหรับการพัฒนาเข้าสู่สภาวะการไหลคงรูปจะขึ้นอยู่กับ เมื่อถด จำนวนของแผ่นแบบเรียบลง อย่างไรก็ตามระบบทางนี้จะถูกทำให้สิ้นลง เมื่อความเร็วของแผ่นแบบเรียบ ลดลง ในกรณีของตัวถุงเรียบในลดดูงสูงกว่าในช่วงของการศึกษานั้น ผลลัพธ์เชิงตัวเลขท่านาทว่าการไหลของ อากาศที่ตัวถุงเรียบในลดดูงสูงกว่า จะต้องการระบบทางสำหรับการพัฒนาเข้าสู่สภาวะการไหลคงรูปมากกว่ากรณี ของตัวถุงเรียบในลดดูงที่มีค่าต่ำกว่า นอกจากนี้ยังพบว่า แคนเปอร์ชนิดแพ่นเดียวจะทำให้เกิดการลดลงของความดัน รวมสูงกว่าแคนเปอร์ชนิดหลายเท่าอย่างมีนัยสำคัญ

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สาขาวิชา วิศวกรรมคณิต
ปีการศึกษา 2540.....

ลายมือชื่อนักศึกษา W. Santi C.
ลายมือชื่ออาจารย์ที่ปรึกษา Sampranong Srivichai
ลายมือชื่ออาจารย์ที่ปรึกษาร่วม M. B. S.

พิมพ์โดยบัณฑิตวิทยาลัยจุฬาภรณ์ภาควิชางรفةในกรอบวิจัยที่เข้ามาที่บัณฑิตวิทยาลัย

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THESIS ADVISOR : SOMPRASONG SRICHAI, Ph.D.

THESIS CO-ADVISOR : ASI BUNYAJITRADULYA, Ph.D.

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The phenomena of air flow past the parallel inclined flat plates in a square duct is studied through the numerical solution by using computational fluid dynamics (CFD) technique. A computer program called PHOENICS , is adopted to solve for three-dimensional steady turbulent flow under the finite volume method. The governing equations are incompressible ensemble-averaged Navier-Stokes equations. The Reynolds stresses are modeled by the k - ε turbulence model with Boussinesq's eddy viscosity assumption.

To verify the numerical accuracy and validity of the turbulence model , the results are first compared with experimental velocity data. Comparisons between measured and calculated results are in general satisfactory , although some discrepancies are found. Finally , the effects of the number of flat plates , the inclination of flat plates and high Reynolds number in the duct flow , to the distance for fully developed flow , as well as total pressure drop , are investigated.

The predictions show that the development length extends when the number of flat plates decreases , however , such length is shortened when the inclination of flat plates becomes smaller. In case of Reynolds number within the range of study , the numerical results predict that the air flow at higher Reynolds number requires the development length to be longer than the lower Reynolds number condition. Furthermore , it is found that the single blade damper causes total pressure drop to be significantly higher than the multi-blade damper.

ภาควิชา..... วิศวกรรมเคมี.....

ลายมือชื่อนักศึกษา..... W. Santi Z

สาขาวิชา..... วิศวกรรมเคมี.....

ลายมือชื่ออาจารย์ที่ปรึกษา..... Somprason S. Srichai

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LIST OF SYMBOLS

ALPHABETICAL SYMBOLS

A	section area of body at right angles to motion
	direction
a	longitudinal spacing between two consecutive vortices in same row
B	test-section width
b	plate breadth
C_D	drag coefficient
C_L	lift coefficient
C_P	pressure coefficient
C_{Ps}	separation pressure coefficient
C_μ	empirical constant
C_1, C_2	coefficients in approximated turbulent transport equation
D	drag force
D	duct diameter
D	diffusion conductance
D_h	hydraulic diameter
D_i	constants in tridiagonal system
E	roughness parameter
F	strength of convection

LIST OF SYMBOLS (continued)

f_x, f_y, f_z	body forces per unit mass in x , y , z directions
G	rate of production of turbulence from mean motion
I	turbulent intensity
J	integrated total fluxes over control-volume faces
J_x, J_y, J_z	convection plus diffusion fluxes in x , y , z directions
k	kinetic energy of turbulence
L	mixing length
L	lift force
L_*	development length
L_i, M_i, U_i	finite coefficients on lower- , main- , upper-diagonal
P	local static pressure
P_0	free-stream static pressure
P'	fluctuating component of pressure
P'	pressure correction
P^*	guessed pressure
\bar{P}	mean value of pressure
\bar{P}'	mean value of pressure fluctuation
R	resistance coefficient
Re	Reynolds number in duct flow (= $\rho V D_h / \mu$)

LIST OF SYMBOLS (continued)

S	source term
S_c	constant part of average value of S
S_p	coefficient of ϕ_p
T	time interval
t	time
U	mean velocity upstream of body
U_j	mean velocity at vena contracta
U_s	velocity at separation
u, v, w	velocity components in x, y, z directions
u', v', w'	fluctuating components of velocity in x, y, z directions
u'', v'', w''	velocity correction components in x, y, z directions
u^*, v^*, w^*	guessed velocity components in x, y, z directions
$\bar{u}, \bar{v}, \bar{w}$	mean velocity components in x, y, z directions
\bar{u}_j	mean velocity component in x_j direction
$\bar{u}_{j,nw}$	absolute value of resultant velocity parallel to a wall at first grid node in x_j direction
$\bar{u}', \bar{v}', \bar{w}'$	mean value of fluctuating velocity components in x, y, z directions
V	fluid mean velocity

LIST OF SYMBOLS (continued)

\mathbf{v}	vector velocity field in cartesian space
v_i, \tilde{v}_i	mean longitudinal velocity at same position of adjacent cross-section
v_0	undisturbed air velocity relative to plate
v_3	downstream velocity of individual vortices
$\bar{\mathbf{v}}$	vector mean velocity field in cartesian space
x, y, z	rectangular coordinates
x_j	coordinate direction
y_{nw}^+	normalized-coordinate near a wall

GREEK SYMBOLS

α	angle of attack
β	momentum coefficient
Γ	diffusion coefficient of ϕ
Δ	designates a difference when used as a prefix
$\delta x, \delta y, \delta z$	spaces of adjacent grid points in x, y, z directions
ϵ	dissipation of turbulent kinetic energy
κ	Von Karmann constant
λ	second viscosity coefficient
μ	molecular viscosity coefficient
μ_t	turbulent viscosity coefficient

LIST OF SYMBOLS (continued)

μ_{eff}	effective viscosity coefficient
ρ	fluid density
$\sigma_k, \sigma_\epsilon$	effective turbulent Prandtl numbers for transport of k and ϵ
$\tau_{xx}, \tau_{yy}, \tau_{zz}$	normal stresses on y-z, x-z, x-y planes
$\tau_{xy}, \tau_{xz}, \tau_{yz}$	shear stresses on x-z, y-z, x-y planes
$\bar{\tau}_{xx}^{(t)}$	turbulent normal stress
$\bar{\tau}_{xy}^{(t)}$	turbulent shear stress
$\tau_{w,j}$	shear stress at a wall in x_j direction
ϕ	general dependent variable

SUBSCRIPTS

in	inlet value
nw	near wall value
nb	neighbor grid points or control-volume faces
P, E, W, N, S, L, H	grid points of a control volume and neighbors
e, w, n, s, l, h	control-volume faces

SUPERSCRIPTS

o	old value at beginning of time step
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