

REFERENCES

1. F.S. Goulding. Pulse-shaping in Low-noise Nuclear Amplifiers a physical approach to noise analysis. Nuclear Instruments and Methods vol.100 1972: 493-504.
2. F.S. Goulding, D.A. Landis. Signal processing for Semiconductors. IEEE Nuclear science Vol.29 1982: 1125-1141.
3. E.Fairstein. Linear Unipolar pulse-shaping networks :current technology. IEEE Nuclear science Vol.37 1990: 382-397.
4. Willy M.C. Sansen, Zhong Yuan Chang. Limits of Low Noise Performance of Detector Readout Front Ends in CMOS Technology. IEEE Nuclear science Vol.37 1990: 1375-1382.
5. Alberto Pullia, Angelo Geraci, Giancarlo Ripamonti. On-Field Determination of the Minimum-Noise Filter for Digital Radiation Spectrometers. IEEE Nuclear science 1998: 722-725.
6. A. Pullia, G.Ripamonti. Minimum-noise filter for baseline estimation in radiation detection systems. Nuclear Instruments and Methods A376 1996: 82-88.
7. A. Pullia, G. Ripamonti, D. Santo. Minimum-Noise filter for Baseline Estimation in Radiation Detection Systems. IEEE Nuclear science1996: 263-266.
8. A.Pullia , G.Gritti , G.Ripamonti. Design of high performance digital baseline restorers. IEEE Nuclear science Vol.44 1997: 331-337.
9. E. Gatti, A.Geraci, G. Ripamonti. Optimum filters from experimentally measured noise in high resolution nuclear spectroscopy. E.Fairstein. Linear Unipolar pulse-shaping networks :current technology. Nuclear Instruments and Methods A417 1998: 131-136.
10. E. Gatti, A.Geraci, G. Ripamonti. Optimum filter for 1/f current noise smoothed –to–white at low frequency. F.S. Goulding, D.A. Landis. Signal processing for Semiconductors. Nuclear Instruments and Methods A394 1997: 268-270.
11. Angelo Geraci, Emilio Gatti. Optimum filters for charge measurements in the presence of 1/f current noise. Nuclear Instruments and Methods A361 1995: 277-289.

12. A. Geraci, G. Ripamonti, A. Pullia. An automatic initialization procedure for real-time digital radiation spectrometry. Nuclear Instruments and Methods A403 1998: 455-464.
13. Alberto Pullia. Impact of non-white noises in pulse amplitude measurements: a time-domain approach. Nuclear Instruments and Methods A405 1998: 121-125.
14. A. Geraci. Asymmetrical optimum filters for charge measurements in presence of 1/f current noise. . Nuclear Instruments and Methods A386 1997: 487-491.
15. A. Pullia, A. Geraci, G. Ripamonti. Quasi-optimum γ and X spectroscopy based on real-time digital techniques. Nuclear Instruments and Methods A439 2000: 378-384.
16. Alberto Pullia. How to derive the optimum filter in presence of arbitrary noises, time-domain constraints, and shaped input signals: A new method. . Nuclear Instruments and Methods A397 1997: 414-425.
17. Dimitris G. Manolakis, Vinay K. Ingle, Stephen M. Kogon. Statistical and Adaptive Signal Processing. : McGraw Hill, 2000.
18. P.W. Nicholson. Nuclear Electronics. : John Wiley & Sons, 1974.
19. Ethan L. Hull, Richard H. Pehl, Craig Tindall, Paul N. Luke and James D. Kurfess. Radiation damage and charge collection effects in Si(Li) gamma-ray detectors. Nuclear Instruments and Methods A496 2003: 123-128.
20. P.F. Manfredi, M. Manghisoni, L. Ratti, V. Re, V. Speziali. Resolution limits achievable with CMOS front-end in X- and Gamma ray analysis with semiconductor detectors. Nuclear Instruments and Methods A512 2003: 167-187.
21. Werner Buttler, Bedrich J., Hosticka. A JFET-CMOS Radiation-Tolerant Charge-sensitive Preamplifier. IEEE journal of solid-state circuits Vol.25 1990: 1022-1024.
22. Angelo Geraci, Emilio Gatti. A new class of optimum filters with complete rejection of periodic noise disturbances. IEEE Nuclear science Vol.25 2002: 1009-1013.
23. G.P. Westphal, K. Jostl, P. Schroder, W. Winkelbauer. Adaptive Digital Filter for High-Rate High-Resolution Gamma Spectrometry. IEEE Nuclear science Vol.48 2001: 461-464.

24. P.J.M.B. Rachinhas, T.H.V.T. Dias, F.P. Santos, A.D. Stauffer, C.A.N. Conde. Monte Carlo Simulation of Xenon Filled Cylindrical Proportional Counter. IEEE Nuclear science Vol. 41 1994: 984-988
25. R.P. Gardner, S.H. Lee. Monte Carlo Simulation of Pulse Pile up. 2004 Denver X-ray Conference, USA, August 2-6, 2004
26. E. Karvelas , D. Loukas, A. Markou, A.H. Walenta. Calculation of pile-up effect in X-ray detection with large area circular silicon drift detectors. Nuclear Instruments and Methods A406 1998: 59-68.
27. . M. Brigida, C. Favuzzi, P. Fusco, F. Gargano, N. Giglietto, F. Giordano, F. Loparco, B. Marangelli, M.N. Mazziotta, N. Mirizzi, S. Raino, P. Spinelli. A new Monte Carlo code for full simulation of silicon strip detectors. Nuclear Instruments and Methods A533 2004: 322-343.
28. M.Kuwata,R.Isobe. Noise Analysis of a Pulse Processor Using SPICE. IEEE Nuclear science Vol.46 1999: 1876-1879.
29. Tae-Hoon Lee, Gyuseong Cho. Monte Carlo based time-domain Hspice noise simulation for CSA-CRRC circuit. Nuclear Instruments and Methods A505 2003: 328-333.
30. Alberto Pullia, Stefano Riboldi. Time-Domain Simulation of Electronic Noises. IEEE Nuclear science Vol. 51 2004: 1817-1823.
31. REUVEN Y.,RUBINSTEIN. SIMULATION AND THE MONTE CARLO METHOD. : John Wiley & Sons, 1981.
32. Averill M.Law,W.David Kelton. SIMULATION MODELING AND ANALYSIS. :McGraw-Hill, 1982.
33. C.D. MOTCHENBACHER. LOW-NOISE ELECTRONIC SYSTEM DESIGN. :John Wiley & Sons, 1993.
34. Craig S. Petrie, J. Alvin Connelly. THE SAMPLING OF NOISE FOR RANDOM NUMBER GENERATION. IEEE Circuits and Svstems Vol.6 1999: 26-29
35. R.W.Harris. INTRODUCTION TO NOISE ANALYSIS. :Pion limited, 1974.
36. P.Silva Girao. Characterization of Noise Generators: Automated Measuring System for the Determination of the Probability Distribution and Autocorrelation Function. IEEE 1994.

37. Patrick Billingsley. Probability and Measure. : John Wiley & Sons, 1979.
38. Steven W. Smith. The scientist and engineer's Guide to Digital Signal Processing.
Second edition. :California Technical Publishing, 1997

Appendices

APPENDIX A. The summary of all applied MATLAB function

This section provides a quick review of all MATLAB function applied in this research work. For more detail type *help command* at Command Window.

Function	Description
abs	Compute the absolute value.
butter	Butterworth digital and analog filter design.
conv	Convolution sum computation.
ecdf	Calculate the cumulative distribution function of data values.
fclose	Close file.
fft	Computes the discrete Fourier transform coefficients.
filter	Create the filtered data from the input data and the filter coefficients.
fix	Rounds towards zero.
fopen	Open file.
fprintf	Write formatted data to file.
fscanf	Read formatted data from file
ifft	Computes the inverse discrete Fourier transforms coefficients.
imag	Determine the imaginary part of complex number.
max	Determine the largest element of a vector.
mean	Determine average or mean data values.
min	Determine the smallest element of a vector.
plot	Generate linear 2-dimension plot.
psd	Power spectral estimation via Welch's method.
rand	Generated pseudorandom number that is uniformly distribution over 0,1.
real	Determines the real part of complex number.
serial	Construct serial port object.
set	Set object properties.
std	Determine the standard deviation of data values.
tfe	Transfer function estimation from input and output of system.
zeros	Create array of zero.

APPENDIX B. The summary of an applied script files

This section provides a description and detail of MATLAB script files applied in this research work.

Function	Description
comm	Establish communication between TDS 360 and computer.
tdstmp	Setup the controlled parameters of TDS 360.
tdsver	Get amplitude multiplies and offset parameter.
tdsdaq	Acquire data from TDS 360.
tdsacc	Acquire a set of data from TDS 360.
commclose	Close communication between TDS 360 and computer.
noise	Generate random number from arbitrary cumulative distribution function
events	Generate time interval.
signal_sim	Generate preamplifier output signal.
cfilter	Calculate digital filter from an arbitrary frequency response.

1. [out,tds_comm]=comm

```
tds_comm = serial('COM1');
set(tds_comm,'BaudRate',9600);
set(tds_comm,'InputBufferSize',2014);
set(tds_comm,'Timeout',2);
set(tds_comm,'Terminator','CR');
fopen(tds_comm);
fprintf(tds_comm,'*IDN?')
out= fscanf(tds_comm);
```

2. tdstmp(tds_comm)

```
%Turn off the header from query responses.
cmd=['HEADER OFF' char(13)]
fprintf(tds_comm,cmd)
%Set up the data source to be channel 1.
cmd=['DATA:SOURCE CH1' char(13)]
```

```

fprintf(tds_comm,cmd)
%Set up the data encoding to be binary and data width to 1.
cmd=['DATA:ENCODG RIBINARY;WIDTH 1' char(13)]
fprintf(tds_comm,cmd)
%Set up the record length, which start from 1 stop at 1000
cmd=['HORIZONTAL:RECORDLENGTH 1000' char(13)]
fprintf(tds_comm,cmd)
%Start at 1
cmd=['DATA:START 1' char(13)]
fprintf(tds_comm,cmd)
%Stop at 1000
cmd=['DATA:STOP 1000' char(13)]
fprintf(tds_comm,cmd)
cmd=['HEADER OFF' char(13)]
fprintf(tds_comm,cmd)
3. [yoff,ymult]=tdsver(tds_comm)
%fprintf(tds_comm,'HEADER OFF')
cmd=['WFMPRE:CH1:YOFF?' char(13)];
fprintf(tds_comm,cmd)
yoff=fscanf(tds_comm);
fprintf(tds_comm,'HEADER OFF')
%for i=1:200000
%end
cmd=['WFMPRE:CH1:YMULT?' char(13)];
fprintf(tds_comm,cmd)
ymult=fscanf(tds_comm);
4. [sample]=tdsdaq(tds_comm,ymult,yoff)
[yoff,ymult]=ptdsver(tds_comm)
sample=[];
for i=1:10
[volt,wave]=ptdsacc(tds_comm,ymult,yoff);

```



```

sample=[sample;wave];
i
end
5. [volt,wave]=tdsacc(tds_comm,ymult,yoff)
fprintf(tds_comm,'ACQUIRE:STATE RUN')
%Wait for the scopr to acquire data
for i=1:40000
end
%Send scope curve query to get waveform data
fprintf(tds_comm,'CURVE?')
%Read data waveform
%Wait for the scopr to acquire data
%for i=1:100000
%end
%volt = fscanff(tds_comm);
volt=fread(tds_comm,2014,'uint8');
%Turn off the header from query responses.
fprintf(tds_comm,'HEADER OFF')
volt=volt(7:1007);
%volt=volt(2:1000);
for i=1:1000
    %if volt(1+i*2)>127
    if volt(1)>127
        volt(i)=volt(i)-256;
    end
end
for i=1:1000
    %wave(1+i)=volt(1+i*2)*256+volt(2+i*2)-sscanf(yoff,'%f');
    wave(i)=volt(i)-sscanf(yoff,'%f');
end
wave=wave*sscanf(ymult,'%f');

```

6. commclose(tds_comm)

```
fclose(tds_comm)
```

```
delete(tds_comm)
```

```
clear tds_comm
```

7. [sim]=noise(f,x)

```
%Generate random number
```

```
rnd=rand(1,1);
```

```
id=1;
```

```
while f(id) < rnd
```

```
    id=id+1;
```

```
end
```

```
id=id-1;
```

```
%id=16
```

```
if id==24
```

```
    sim=x(24);
```

```
else
```

```
    dsim=(rnd-f(id))*(x(id+1)-x(id))/(f(id+1)-f(id));
```

```
    %dsim=0;
```

```
    sim=x(id)+dsim;
```

```
end
```

8. [event,count]=events(lambda,preset_time)

```
% This function returns time series of disintegration.
```

```
% 'event' is time series.
```

```
% 'count' is number of photons
```

```
% 't' is time distribution
```

```
a=0;
```

```
c=1;
```

```
while a<preset_time
```

```
    t(c)=photon_gen(lambda);
```

```
    % loop until reach preset_time
```

```
    a=a+t(c);
```

```

    % counting
    c=c+1;
end
v=size(t);
count=v(2);
N=ones(1,count+1);
% stem(t,N)
% t=t';
event(1)=0;
for i=1:count
    event(i+1)=event(i)+t(i);
end
count=count+1;
9. [v,t_sim,event,count]=signal_sim(a,lambda,preset_time,resol)
% event is time serie driven from events.m
% a is amplitude
[event,count]=events(lambda,preset_time);
% Time digitizer resolution is 1e-8
% resol=1e-8;
b=1;
s=size(event);
v=zeros(fix(preset_time/resol)+1,1);
t_sim=zeros(fix(preset_time/resol)+1,1);
for t=0:resol:preset_time
    for i=1:1:s(2)
        if t>event(i)
            v(b)=v(b)+a*exp((t-event(i))/-50e-6);
        end
    end
end
t_sim(b)=t;
b=b+1;

```

```

end
10. [ht]=cfilter(h)
% h is frequency response
a=size(h);
na=a(1);
t=zeros(na,1);
% Kernel length
% old value 26/4/2004 M=100;
%M=5000;
M=1000
% Shift filter kernel length
%for i=1:a
%  j=i+M/2;
%  if j>a
%    j=j-a-1
%  end
%  t(j)=h(i);
%end
%TEMPLATE
%b(1:M/2)=a(na-M/2+1:na)
%b(1+M/2:na)=a(1:na-M/2)
t(1:M/2)=h(na-M/2+1:na);
t(1+M/2:na)=h(1:na-M/2);
% Truncate and window the signal
for i=1:a
    if i<= M
        % Hamming windows
        %t(i)=t(i)*(0.54-0.46*cos(2*pi*i/M));
        % Blackman
        t(i)=t(i)*(0.42-0.5*cos(2*pi*i/M)+0.08*cos(4*pi*i/M));
    end
end

```

APPENDIX C.1 CANBERRA 2022 Spectroscopy amplifier specification

Specifications

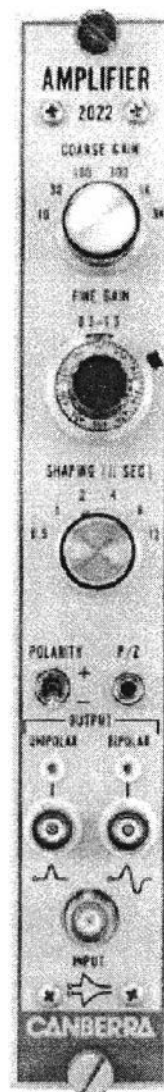
INPUTS

INPUT – Accepts positive or negative pulses from an associated preamplifier; amplitude: ± 10 V divided by the selected gain for linear response; ± 12 V maximum; rise time: less than SHAPING time constant; decay time constant: $40 \mu\text{s}$ to ∞ for 0.5, 1, 2, 4 and $8 \mu\text{s}$ shaping time constants, $100 \mu\text{s}$ to ∞ for $12 \mu\text{s}$ shaping time constant; $Z_{in} \approx 1 \text{ k}\Omega$; front and rear panel BNC connectors.

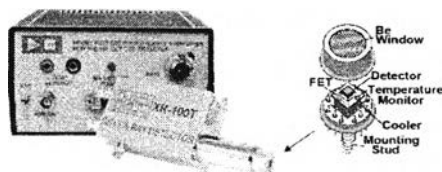
OUTPUTS

UNIPOLAR OUTPUT – Provides positive linear active-filtered near-Gaussian shaped pulses; amplitude linear to $+10$ V, 12 V max.; dc restored; output dc level factory calibrated to 0 ± 5 mV; front panel $Z_{out} \leq 1 \Omega$ or $\approx 93 \Omega$, internally selectable; rear panel $Z_{out} \approx 93 \Omega$; short circuit protected; prompt or delayed $2 \mu\text{s}$ with option 2022-2 or $4 \mu\text{s}$ with option 2022-4; front and rear panel BNC connectors.

BIPOLAR OUTPUT – Provides prompt positive lobe leading linear active-filtered bipolar-shaped pulses; amplitude linear to -10 V, 12 V max.; negative lobe is approximately 70% of positive lobe; dc coupled; output dc level ≈ 25 mV; front panel



APPENDIX C.2 XR-100T-CdTe radiation detector specification



SPECIFICATIONS

MODEL XR-100T-CdTe X-RAY and GAMMA RAY DETECTOR	MODEL PX2T POWER SUPPLY + SHAPING AMPLIFIER
GENERAL	GENERAL
Detector Type: CdTe-Diode	Size: 6 X 6 X 3.5 inches (15.3 X 15.3 X 8.9 cm)
Detector Size: 3 x 3 mm (9 mm ²)	Weight: 2.5 lbs (1.15 kg)
Detector Thickness: 1 mm	Input AC power to the PX2T is provided through a Standard IEC 320 plug (110/250 VAC, 50/60 Hz). See Figure 3.
Energy Resolution @ 122 keV, ⁵⁷ Co: <1.2 keV FWHM, typical	The four (4) DC Voltages needed to operate the XR-100T-CdTe are supplied through a female 9-Pin D-Connector on the PX2T. The Pin list to this connector is given below. The multiconductor cable which connects the PX2T to the XR-100T-CdTe is provided with the system.
Dark Counts: <5 x 10 ⁻³ counts/sec @ 10 keV < E < 1 MeV	9-PIN D-CONNECTOR ON THE PX2T-CZT
Detector Window: Be, 10 mil thick (250 μm)	Pin 1: +8 Volt preamp power
Preamplifier: Amptek Model A250, with Current Divider Feedback	Pin 2: -8 Volt preamp power
Case Size: 3.75 x 1.75 x 1.13 in (9.5 x 4.4 x 2.9 cm)	Pin 3: 0 to +3 Volt cooler power @ 0.7 A max.
Case Weight: 4.4 ounces (125 g)	Pin 4: +8 Volt temperature monitor power
Total Power: Less than 1 Watt	Pin 5: + H.V. detector bias, +400 Volt max.
INPUTS	Pin 6: Ground and case
Test Input: 20 mV test pulse ~ 30 keV	Pin 7: Cooler power return
Preamp Power: ± 8 Volts @ 25 mA	Pin 8: Ground and case
Detector Power: + 400 Volts @ 1 μA	Pin 9: Ground and case
Cooler Power: Current = 0.7 A maximum Voltage = 2.1 Volt maximum	PX2T SHAPING AMPLIFIER
OUTPUTS	Polarity: Positive Unipolar
1) Preamplifier	Shaping Time: 3 μs
Sensitivity: 0.82 mV/keV	Pulse Width: 7.2 μs FWHM See Figure 4
Polarity: Negative Signal Out (1 kΩ max. load)	Shaping Type: 7 pole "Triangular" with Base Line Restoration, Pileup Rejection, and Rise Time Discrimination (RTD).
2) Temperature Monitor	Sensitivity with XR-100T-CdTe: 6 to 60 mV/keV
Sensitivity: 1 μA corresponds to 1 °K	Output Range: +6.0 Volts into 500 Ω load
CONNECTIONS	Output Impedance: 50 Ω
Preamp Output: BNC coaxial connector	The output pulse produced by the PX2T Shaping Amplifier is optimum for most applications using cooled CdTe detectors, and can be connected directly to the input of a Multichannel Analyzer (MCA). If different shaping time constants or gains are needed, an external NIM type shaping amplifier with base line restoration can be used.
Test Input: BNC coaxial connector	PX2T SIGNAL CONNECTIONS
Other connections: 6-Pin, LEMO connector with 5 ft cable	Input from XR-100T-CdTe: Front panel BNC
OPTIONS	Output to MCA: Front panel BNC
- Other detector sizes (5 x 5 x 1 mm ³) are available on special orders.	Pileup Rejection (PU): Rear panel BNC, Positive TTL
- Other Be window thicknesses are available.	For the duration of this output gate, any detected pulse must be rejected by the MCA.
- Components for vacuum applications.	Input Count Rate (ICR): Rear panel BNC, Positive TTL
- Collimator kit for high flux applications	<2 μs
- See also XR-100CR specifications using Si-PIN for detection of low energy X-Rays with high resolution (186 eV FWHM @ 5.9 keV, ⁵⁵ Fe).	When connected to a counter, the ICR countrate corresponds to the total number of X-Rays events that strike the detector
6-PIN LEMO CONNECTOR ON THE XR-100T-CdTe	
Pin 1: +8 Volt temperature monitor power	
Pin 2: + H.V. detector bias, +400 Volt max	
Pin 3: -8 Volt preamp power	
Pin 4: +8 Volt preamp power	
Pin 5: Cooler power return	
Pin 6: Cooler power (0 to +2.1 Volt @ 0.7 A max.)	
CASE: Ground and shield	

Biography

Mr.Hudsaleark Neamintara was born on January 20,1966 in Bangkok, Thailand. He got his Bachelor Degree from the Department of Radiological Technology, Faculty of Associated Medical Sciences, Chiangmai university in 1988 and Master degree from Department of Nuclear Technology, Faculty of engineering, Chulalongkorn university in 1993. At present he serves as Lecturer in the field of X-ray Diagnostic Apparatus, Department of Radiological Technology, Faculty of Associated Medical Sciences, Chiangmai University. In May 2000, he was awarded a grant from Chiangmai University to further his study for the Doctoral Degree at the Department of Nuclear Technology, Faculty of Engineering, Chulalongkorn University.

