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APPENDICES

Appendix A Lattice Parameter Calculation

The lattice parameter of unit cell $Ba_{1-x}Sr_xTiO_3$ were calculated as follow; the equation

$$\text{Bragg's law} \quad n\lambda = 2d \sin \theta \quad (A1)$$

$$\lambda = 2d \sin \theta \quad (n=1) \quad (A2)$$

$$\text{Cubic:} \quad \frac{1}{d^2} = \frac{(h^2 + k^2 + l^2)}{a^2} \quad (A3)$$

$$\text{Tetragonal:} \quad \frac{1}{d^2} = \frac{(h^2 + k^2)}{a^2} + \frac{l^2}{c^2} \quad (A4)$$

From equation (A2), we can write that

$$d^2 = \frac{\lambda^2}{4 \sin^2 \theta} \quad (A5)$$

Substitution of equation (A5) in equation (A3) and (A4), one obtains

$$\text{Cubic:} \quad \sin^2 \theta = \frac{\lambda^2}{4a^2} (h^2 + k^2 + l^2) \quad (A6)$$

$$\text{Tetragonal:} \quad \sin^2 \theta = \frac{\lambda^2 (h^2 + k^2)}{4a^2} + \frac{\lambda^2 l^2}{4c^2} \quad (A7)$$

We define $(h^2 + k^2 + l^2) = S$, where S is 1, 2, 3, 4, 5, and 6 for the cubic phase and $\lambda^2 / 4a^2$ is a constant. For tetragonal structure, $\lambda^2 / 4a^2$ and $\lambda^2 / 4c^2$ are both constant A and C . $h^2 + k^2$ is 1, 2, 4, 5, and 8. Table A1-A6 show the lattice parameter of $BaTiO_3$ titanate calcined at different temperatures (600-1100°C). Table A7-A9 show the lattice parameter of $Ba_{1-x}Sr_xTiO_3$ with $x = 0.3, 0.5, \text{ and } 0.7$ calcined at 800°C. Table A10-A13 show the lattice parameter of $Ba_{1-x}Sr_xTiO_3$ ceramics with $x = 0, 0.3, 0.5, \text{ and } 0.7$.

Table A1 The identification of XRD peaks analyzed of cubic BaTiO₃ calcined at 600°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.05	11.02	100	1	0.0366	0.0366	4.0261	
31.43	15.71	110	2	0.0735	0.0367	4.0207	
38.79	19.39	111	3	0.1105	0.0368	4.0147	
45.03	22.52	200	4	0.1472	0.0368	4.0173	
50.74	25.37	210	5	0.1837	0.0367	4.0201	
56.02	28.01	211	6	0.2216	0.0369	4.0099	
65.70	32.85	220	8	0.2945	0.0368	4.0166	
						a_{avg}	4.0206
						SD	0.0042

Table A2 The identification of XRD peaks analyzed of cubic BaTiO₃ calcined at 700°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.10	11.05	100	1	0.0368	0.0368	4.0182	
31.48	15.74	110	2	0.0736	0.0368	4.0161	
38.84	19.42	111	3	0.1106	0.0369	4.0127	
45.15	22.57	200	4	0.1475	0.0369	4.0131	
50.84	25.42	210	5	0.1844	0.0369	4.0126	
56.11	28.06	211	6	0.2213	0.0370	4.0114	
65.79	32.90	220	8	0.2952	0.0369	4.0115	
						a_{avg}	4.0137
						SD	0.0025

Table A3 The identification of XRD peaks analyzed of cubic BaTiO₃ calcined at 800°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.12	11.06	100	1	0.0368	0.0368	4.0153	
31.52	15.76	110	2	0.0738	0.0369	4.0111	
38.80	19.40	111	3	0.1104	0.0368	4.0161	
45.20	22.60	200	4	0.1478	0.0370	4.0085	
50.90	25.45	210	5	0.1848	0.0370	4.0083	
56.18	28.09	211	6	0.2219	0.0370	4.0072	
65.87	32.94	220	8	0.2958	0.0370	4.0072	
						a_{avg}	4.011
						SD	0.0037

Table A4 The identification of XRD peaks analyzed of tetragonal BaTiO₃ calcined at 900°C

2θ	θ	hkl	sin ² θ	sin ² θ / 2	sin ² θ / 4	sin ² θ / 5	sin ² θ / 8
22.16	11.08	100	0.0370				
31.53	15.76	110		0.0369			
45.34	22.67	200			0.0372		
51.01	25.50	210				0.0371	
65.84	32.92	220					0.0369

2θ	θ	hkl	sin ² θ	sin ² θ / 2	sin ² θ / 4	sin ² θ / 5	sin ² θ / 8
22.03	11.02	001	0.0365				
31.51	15.76	101		0.0368			
38.90	19.45	111			0.0369		
45.18	22.59	002	0.1476				
50.90	25.45	201				0.0367	
56.15	28.08	112			0.1476		
56.27	28.14	211					0.0374
65.77	32.88	202				0.1469	

$A = \lambda^2/4a^2$	a (Å)
0.0370	4.0075
0.0369	4.0095
0.0372	3.9967
0.0371	4.0001
0.0369	4.0088
a_{avg}	4.0045 ± 0.0058

$C = \lambda^2/4c^2$	c (Å)
0.0365	4.0311
0.0368	4.0188
0.0369	4.0114
0.0367	4.0212
0.0374	3.9842
0.0369	4.0107
0.0369	4.0109
0.0367	4.0211
C_{avg}	4.0137 ± 0.0138

Table A5 The identification of XRD peaks analyzed of tetragonal BaTiO₃ calcined at 1000°C

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta/2$	$\sin^2\theta/4$	$\sin^2\theta/5$	$\sin^2\theta/8$
22.21	11.10	100	0.0371				
31.53	15.77	110		0.0369			
45.37	22.68	200			0.0372		
51.08	25.54	210				0.0372	
65.97	32.98	220					0.0371

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta-A$	$\sin^2\theta-2A$	$\sin^2\theta-4A$	$\sin^2\theta-5A$
22.00	11.00	001	0.0364				
31.51	15.76	101		0.0367			
38.90	19.45	111			0.0367		
45.17	22.58	002	0.1476				
50.74	25.37	102		0.1466			
50.97	25.49	201				0.0368	
56.19	28.10	112			0.1477		
56.28	28.14	211					0.0370

$A = \lambda^2/4a^2$	a (Å)
0.0371	3.9990
0.0369	4.0088
0.0372	3.9948
0.0372	3.9945
0.0371	4.0019
a_{avg}	3.9998 ± 0.0059

$C = \lambda^2/4c^2$	c (Å)
0.0364	4.0361
0.0367	4.0236
0.0367	4.0210
0.0368	4.0144
0.0370	4.0056
0.0369	4.0115
0.0367	4.0248
0.0369	4.0093
c_{avg}	4.0193 ± 0.0098

Table A6 The identification of XRD peaks analyzed of tetragonal BaTiO₃ calcined at 1100°C

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta / 2$	$\sin^2\theta / 4$	$\sin^2\theta / 5$	$\sin^2\theta / 8$
22.22	11.11	100	0.0372				
31.59	15.80	110		0.0371			
45.39	22.70	200			0.0372		
51.11	25.55	210				0.0372	
66.12	33.06	220					0.0372

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta-A$	$\sin^2\theta-2A$	$\sin^2\theta-4A$	$\sin^2\theta-5A$
22.02	11.01	001	0.0365				
31.50	15.75	101		0.0366			
38.90	19.45	111			0.0366		
44.91	22.46	002	0.1460				
50.65	25.32	102		0.1459			
50.98	25.49	201				0.0367	
55.96	27.98	112			0.1460		
56.28	28.14	211					0.0368

$A = \lambda^2/4a^2$	a (Å)
0.0372	3.9973
0.0371	4.0019
0.0372	3.9927
0.0372	3.9928
0.0372	3.9936
a_{avg}	3.9956 ± 0.0040

$C = \lambda^2/4c^2$	c (Å)
0.0365	4.0340
0.0366	4.0295
0.0366	4.0267
0.0367	4.0241
0.0368	4.0192
0.0365	4.0330
0.0365	4.0345
0.0365	4.0337
0.0365	4.0323
c_{avg}	4.0297 ± 0.0053

Table A7 The identification of XRD peaks analysis of the sol-gel $\text{Ba}_{0.7}\text{Sr}_{0.3}\text{TiO}_3$ powders calcined at 800°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.34	11.17	100	1	0.0376	0.0376	3.9762	
31.78	15.89	110	2	0.0750	0.0375	3.9787	
39.18	19.59	111	3	0.1125	0.0375	3.9792	
45.6	22.8	200	4	0.1503	0.0376	3.9755	
51.32	25.66	210	5	0.1877	0.0375	3.9776	
56.66	28.33	211	6	0.2254	0.0376	3.9760	
66.44	33.22	220	8	0.3004	0.0375	3.9769	
						a_{avg}	3.9772
						SD	0.0014

Table A8 The identification of XRD peaks analysis of the sol-gel $\text{Ba}_{0.5}\text{Sr}_{0.5}\text{TiO}_3$ powders calcined at 800°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.48	11.24	100	1	0.0380	0.0380	3.9518	
31.96	15.98	110	2	0.0759	0.0379	3.9569	
39.46	19.73	111	3	0.1141	0.0380	3.9521	
45.92	22.96	200	4	0.1523	0.0381	3.9493	
51.48	25.74	210	5	0.1887	0.0377	3.9661	
57.00	28.50	211	6	0.2278	0.0380	3.9543	
66.80	33.40	220	8	0.3032	0.0379	3.9580	
						a_{avg}	3.9555
						SD	0.0056

Table A9 The identification of XRD peaks analysis of the sol-gel Ba_{0.3}Sr_{0.7}TiO₃ powders calcined at 800°C

2θ	θ	<i>hkl</i>	<i>S</i>	sin ² θ	λ ² /4a ²	<i>a</i> (Å)	
22.6	11.3	100	1	0.0384	0.0384	3.9311	
32.12	16.06	110	2	0.0766	0.0383	3.9377	
39.62	19.81	111	3	0.1149	0.0383	3.9368	
46.10	23.05	200	4	0.1534	0.0384	3.9348	
51.86	25.93	210	5	0.1914	0.0383	3.9391	
57.30	28.65	211	6	0.2300	0.0383	3.9354	
67.24	33.62	220	8	0.3068	0.0383	3.9351	
						<i>a</i> _{avg}	3.9357
						<i>SD</i>	0.0026

Table A10 The identification of XRD peaks analysis of the BaTiO₃ ceramic sintered at 1350°C

2θ	θ	<i>hkl</i>	sin ² θ	sin ² θ / 2	sin ² θ / 4	sin ² θ / 5	sin ² θ / 8
22.50	11.25	100	0.0381				
31.50	15.75	110		0.0369			
45.36	22.68	200			0.0372		
51.10	25.55	210				0.0372	
66.14	33.07	220					0.0372

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta-A$	$\sin^2\theta-2A$	$\sin^2\theta-4A$	$\sin^2\theta-5A$
31.50	15.75	101	0.0737	0.0364			
38.88	19.44	111	0.1109		0.0362		
50.64	25.32	102	0.1830	0.1457			
50.98	25.49	201	0.1853			0.0360	
55.96	27.98	112	0.2203		0.1456		
56.28	28.14	211	0.2226				0.0360
65.74	32.87	202	0.2948			0.1455	

$A = \lambda^2/4a^2$	a (Å)
0.0381	3.9481
0.0369	4.0130
0.0372	3.9953
0.0372	3.9934
0.0372	3.9927
a_{avg}	3.9885 ± 0.0241

$C = \lambda^2/4c^2$	c (Å)
0.0364	4.0382
0.0362	4.0498
0.0360	4.0591
0.0360	4.0632
0.0364	4.0372
0.0364	4.0384
0.0364	4.0407
c_{avg}	4.0467 ± 0.0108

Table A11 The identification of XRD peaks analysis of the $\text{Ba}_{0.7}\text{Sr}_{0.3}\text{TiO}_3$ ceramic sintered at 1350°C

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta / 2$	$\sin^2\theta / 4$	$\sin^2\theta / 5$	$\sin^2\theta / 8$
22.36	11.18	100	0.0376				
31.81	15.91	110		0.0376			
45.61	22.81	200			0.0376		
51.40	25.70	210				0.0376	
66.54	33.27	220					0.0376

2θ	θ	hkl	$\sin^2\theta$	$\sin^2\theta - A$	$\sin^2\theta - 2A$	$\sin^2\theta - 4A$	$\sin^2\theta - 5A$
22.32	11.16	001	0.0375				
39.24	19.62	111			0.0376		
45.61	22.81	002	0.1504				
56.71	28.35	112			0.1505		
56.82	28.41	211					0.0384
66.47	33.24	202				0.1502	

$A = \lambda^2/4a^2$	a (Å)
0.03763	3.9724
0.03759	3.9744
0.03759	3.9744
0.03764	3.9714
0.03764	3.9716
a_{avg}	3.9728 ± 0.0015

$C = \lambda^2/4c^2$	c (Å)
0.0375	3.9794
0.0376	3.9746
0.0376	3.9744
0.0376	3.9730
0.0376	3.9733
0.0375	3.9771
c_{avg}	3.9745 ± 0.0025

Table A12 The identification of XRD peaks analysis of the $Ba_{0.5}Sr_{0.5}TiO_3$ ceramic sintered at 1350°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.44	11.22	100	1	0.0379	0.0379	3.9583	
31.99	15.99	110	2	0.0760	0.0380	3.9534	
39.46	19.73	111	3	0.1141	0.0380	3.9517	
45.91	22.95	200	4	0.1522	0.0380	3.9503	
51.70	25.85	210	5	0.1903	0.0381	3.9499	
57.07	28.54	211	6	0.2284	0.0381	3.9495	
66.97	33.48	220	8	0.3046	0.0381	3.9491	
						a_{avg}	3.9517
						SD	0.0032

Table A13 The identification of XRD peaks analysis of the $\text{Ba}_{0.3}\text{Sr}_{0.7}\text{TiO}_3$ ceramic sintered at 1350°C

2θ	θ	hkl	S	$\sin^2\theta$	$\lambda^2/4a^2$	a (Å)	
22.56	11.28	100	1	0.0383	0.0383	3.9382	
32.15	16.07	110	2	0.0767	0.0384	3.9342	
39.66	19.83	111	3	0.1152	0.0384	3.9329	
46.13	23.07	200	4	0.1536	0.0384	3.9317	
51.96	25.98	210	5	0.1920	0.0384	3.9319	
57.36	28.68	211	6	0.2305	0.0384	3.9314	
67.32	33.66	220	8	0.3074	0.0384	3.9309	
						a_{avg}	3.9330
						SD	0.0025

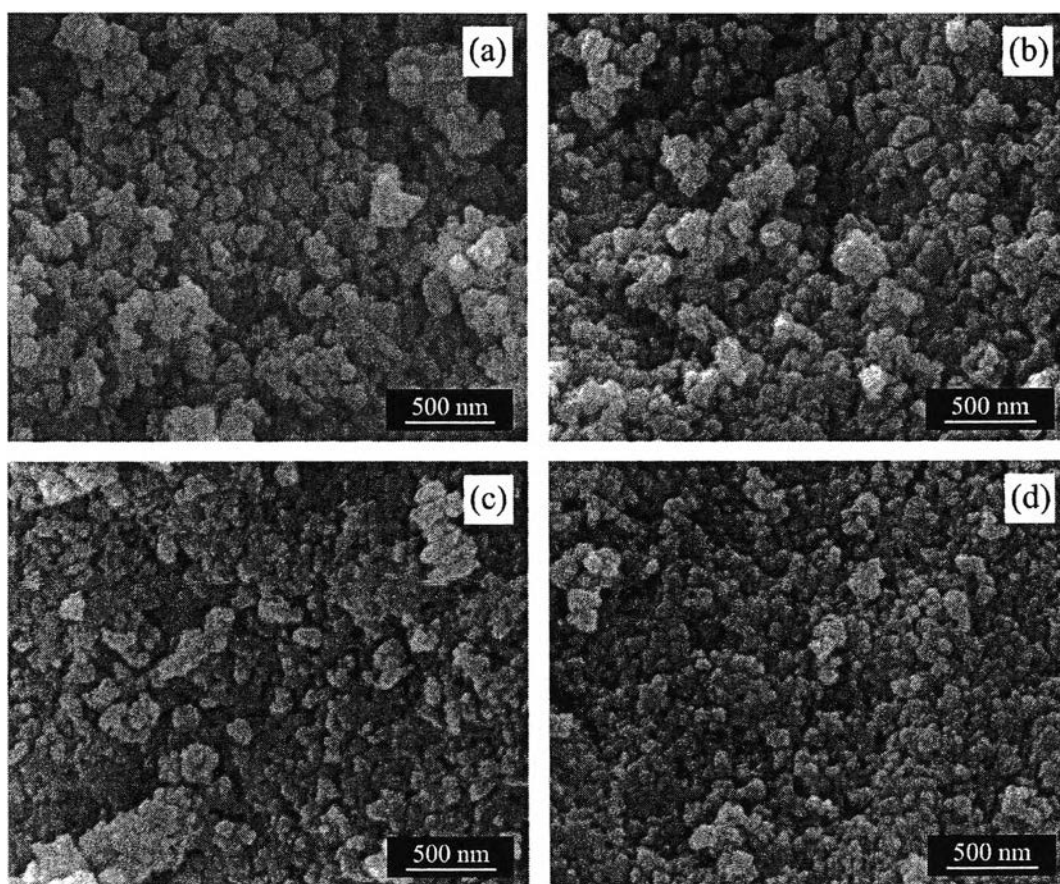
Appendix B SEM Micrographs of Sol-Gel $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$ Powders

Figure B1 SEM micrographs of sol-gel $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$ powders calcined at 800 °C for 80 min; (a) $x = 0$, (b) $x = 0.3$, (c) $x = 0.5$, and (d) $x = 0.7$.

Appendix C The Dielectric Constant and Loss tangent at Different Frequencies

Table C1 The dielectric constant of SG-BT/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
PBZZ	3.81	3.72	3.64	3.58	3.56
30 wt% SG-BT (9 vol%)	5.71	5.57	5.47	5.34	5.29
40 wt% SG-BT (12 vol%)	7.07	6.82	7.86	6.43	6.31
50 wt% SG-BT (18 vol%)	8.48	8.14	9.09	7.65	7.52
60 wt% SG-BT (25 vol%)	9.67	9.35	13.47	8.88	8.76
70 wt% SG-BT (34 vol%)	14.09	13.77	13.47	13.22	13.16

Table C2 The dielectric constant of ST-BT/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
30 wt% ST-BT (8 vol%)	4.86	4.54	4.31	4.23	4.11
40 wt% ST-BT (12 vol%)	6.36	5.62	5.19	4.86	4.31
50 wt% ST-BT (17 vol%)	8.80	8.21	7.72	7.37	7.11
60 wt% ST-BT (22 vol%)	11.57	10.76	10.01	9.41	9.00
70 wt% ST-BT (30 vol%)	13.76	12.92	12.27	11.73	11.29

Table C3 The dielectric constant of SG-BST/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
30 wt% SG-BST (10 vol%)	7.10	6.93	6.68	6.45	6.34
40 wt% SG-BST (15 vol%)	7.96	7.63	7.28	7.01	6.84
50 wt% SG-BST (20 vol%)	10.09	9.72	9.38	9.10	8.83
60 wt% SG-BST (25 vol%)	12.54	12.08	11.68	11.34	10.99
70 wt% SG-BST (38 vol%)	17.51	16.98	16.43	16.02	15.90
80 wt% SG-BST (48 vol%)	28.03	27.17	27.17	26.50	25.47

Table C4 The loss tangent of SG-BT/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
PBZZ	0.0149	0.0159	0.0126	0.0126	0.0120
30 wt% SG-BT (9 vol%)	0.0365	0.0319	0.0290	0.0244	0.0341
40 wt% SG-BT (12 vol%)	0.0249	0.0226	0.0227	0.0176	0.0154
50 wt% SG-BT (18 vol%)	0.0232	0.02329	0.0224	0.0171	0.0220
60 wt% SG-BT (25 vol%)	0.0282	0.0213	0.0197	0.0148	0.0179
70 wt% SG-BT (34 vol%)	0.0334	0.0314	0.0181	0.0227	0.0238

Table C5 The loss tangent of ST-BT/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
30 wt% ST-BT (8 vol%)	0.0392	0.0350	0.0283	0.0266	0.0321
40 wt% ST-BT (12 vol%)	0.0439	0.0355	0.0330	0.0254	0.0274
50 wt% ST-BT (17 vol%)	0.0495	0.0437	0.0372	0.0303	0.0338
60 wt% ST-BT (22 vol%)	0.0498	0.0490	0.0459	0.0395	0.0479
70 wt% ST-BT (30 vol%)	0.0445	0.0409	0.0324	0.0263	0.0296

Table C6 The loss tangent of SG-BST/polybenzoxazine composites

Materials	Frequency (Hz)				
	10^3	10^4	10^5	10^6	10^7
30 wt% SG-BST (8 vol%)	0.0365	0.0319	0.0319	0.0244	0.0341
40 wt% SG-BST (12 vol%)	0.0207	0.0218	0.0233	0.0267	0.0266
50 wt% SG-BST (17 vol%)	0.0166	0.0253	0.0241	0.0219	0.0393
60 wt% SG-BST (22 vol%)	0.0225	0.0230	0.0234	0.0228	0.0273
70 wt% SG-BST (38 vol%)	0.0217	0.0210	0.0200	0.0170	0.0294
80 wt% SG-BST (48 vol%)	0.0362	0.0189	0.0160	0.0171	0.0306

Table C7 The dielectric constant of $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$ ($x = 0, 0.3, 0.5, \text{ and } 0.7$) ceramics

Materials	Frequency (Hz)					
	10^2	10^3	10^4	10^5	10^6	10^7
BaTiO_3	1362	1232	1145	1145	1100	233
$\text{Ba}_{0.7}\text{Sr}_{0.3}\text{TiO}_3$	2904	2795	2672	2672	2568	97
$\text{Ba}_{0.5}\text{Sr}_{0.5}\text{TiO}_3$	942	946	941	941	938	804
$\text{Ba}_{0.3}\text{Sr}_{0.7}\text{TiO}_3$	326	308	297	297	292	260

Table C8 The loss tangent of $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$ ($x = 0, 0.3, 0.5, \text{ and } 0.7$) ceramics

Materials	Frequency (Hz)					
	10^2	10^3	10^4	10^5	10^6	10^7
BaTiO_3	0.1263	0.0675	0.0416	0.0349	0.1728	1.9786
$\text{Ba}_{0.7}\text{Sr}_{0.3}\text{TiO}_3$	0.0340	0.0316	0.0289	0.0506	0.2642	10.57
$\text{Ba}_{0.5}\text{Sr}_{0.5}\text{TiO}_3$	0.0086	0.0128	0.0032	0.0077	0.0565	0.7344
$\text{Ba}_{0.3}\text{Sr}_{0.7}\text{TiO}_3$	0.3570	0.0763	0.0224	0.0126	0.0451	0.4656

Appendix D Characterizations of Barium Titanate (BaTiO₃)/Polybenzoxazine Composites

Two ceramic-polymer composites were also fabricated and investigated. The ceramic fillers include sol-gel barium titanate powders (SG-BT) and sintered barium titanate powders (ST-BT). The densities of composites were measured as function of ceramic content. For dielectric measurement, dielectric constant and loss tangent of composites were measured as function of ceramic volume fraction and frequency.

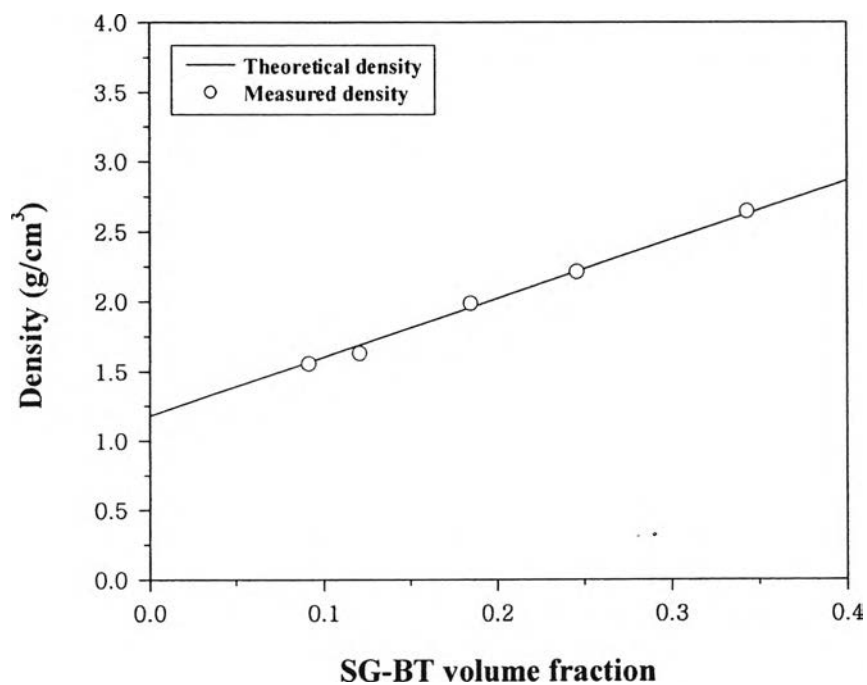


Figure D1 Comparison between measured density (\diamond) and theoretical density (—) as a function of SG-BT.

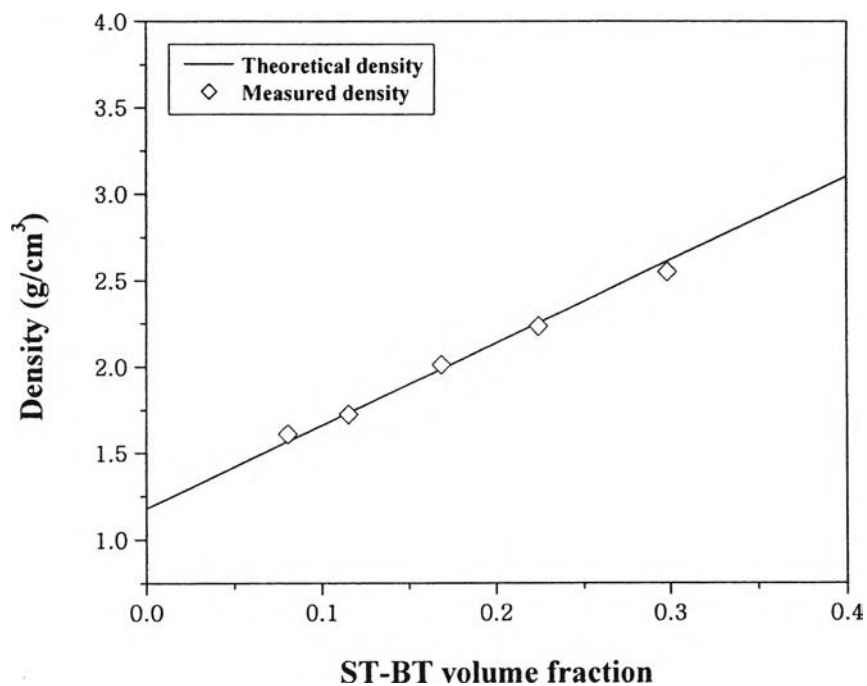


Figure D2 Comparison between measured density (\diamond) and theoretical density ($—$) as a function of ST-BT.

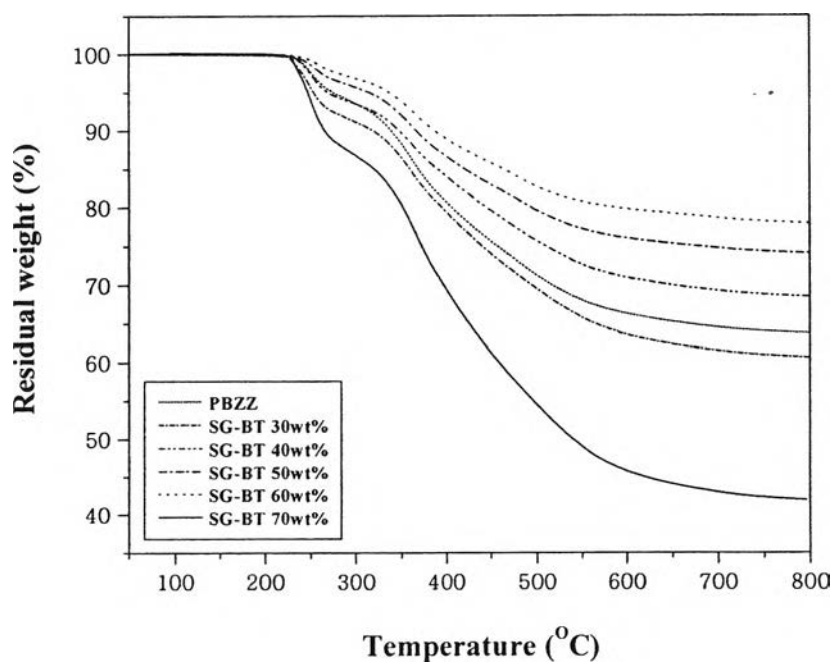


Figure D3 TGA curve of composites at different SG-BT content in nitrogen atmosphere.

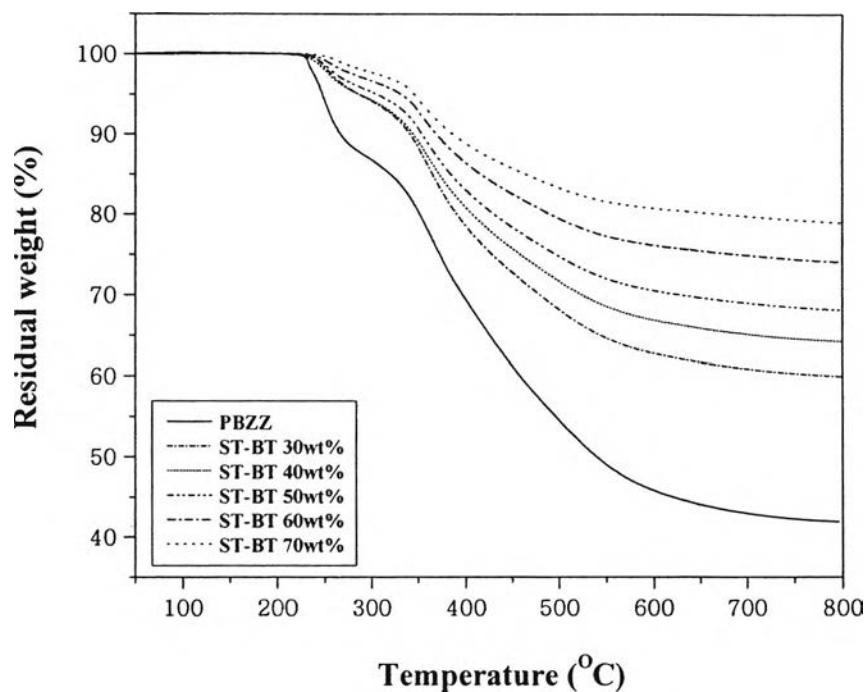


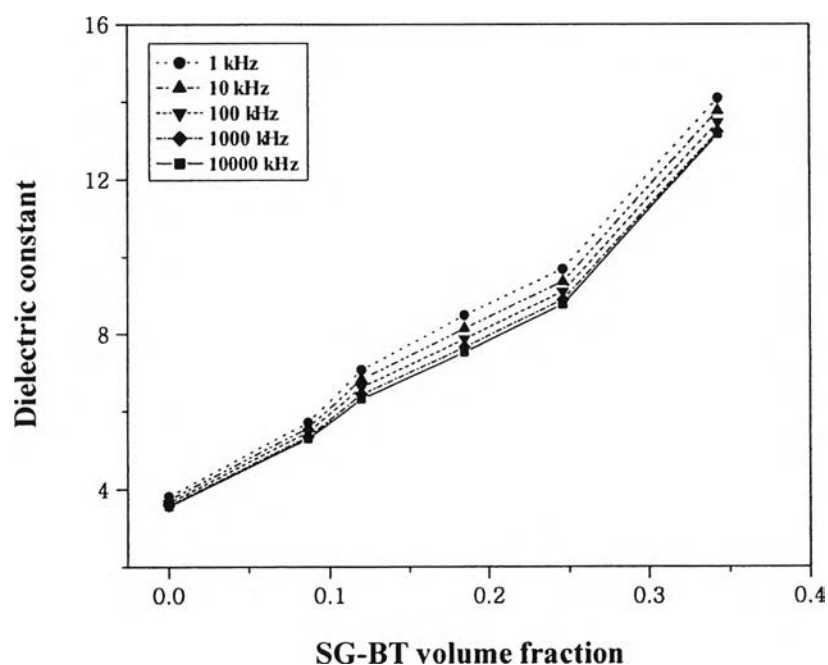
Figure D4 TGA curve of composites at different ST-BT contents in nitrogen atmosphere.

Table D1 Properties of the composite at various SG-BT contents

Composites	Volume fraction	Density (g/cm ³)	Residual weight% at 800°C
PBZZ/SG-BT 30 wt%	0.09	1.55	60.54
PBZZ/SG-BT 40 wt%	0.12	1.63	63.69
PBZZ/SG-BT 50 wt%	0.18	1.99	68.44
PBZZ/SG-BT 60 wt%	0.25	2.21	74.06
PBZZ/SG-BT 70 wt%	0.34	2.64	77.91

Table D2 Properties of the composites at various ST-BT contents

Composites	Volume fraction	Density (g/cm ³)	Residual weight% at 800°C
PBZZ/ST-BT 30 wt%	0.08	1.61	59.93
PBZZ/ST-BT 40 wt%	0.11	1.72	64.24
PBZZ/ST-BT 50 wt%	0.17	2.01	68.12
PBZZ/ST-BT 60 wt%	0.22	2.23	74.09
PBZZ/ST-BT 70 wt%	0.29	2.55	78.98

**Figure D5** Dielectric constant of the composites at different SG-BT volume fraction and frequencies.

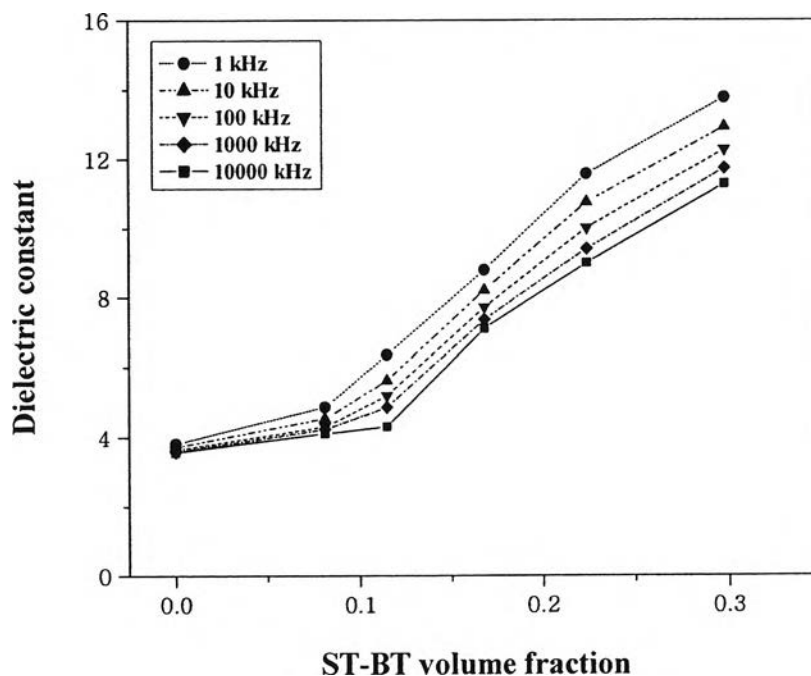


Figure D6 Dielectric constant of the composites at different ST-BT volume fraction and frequencies.

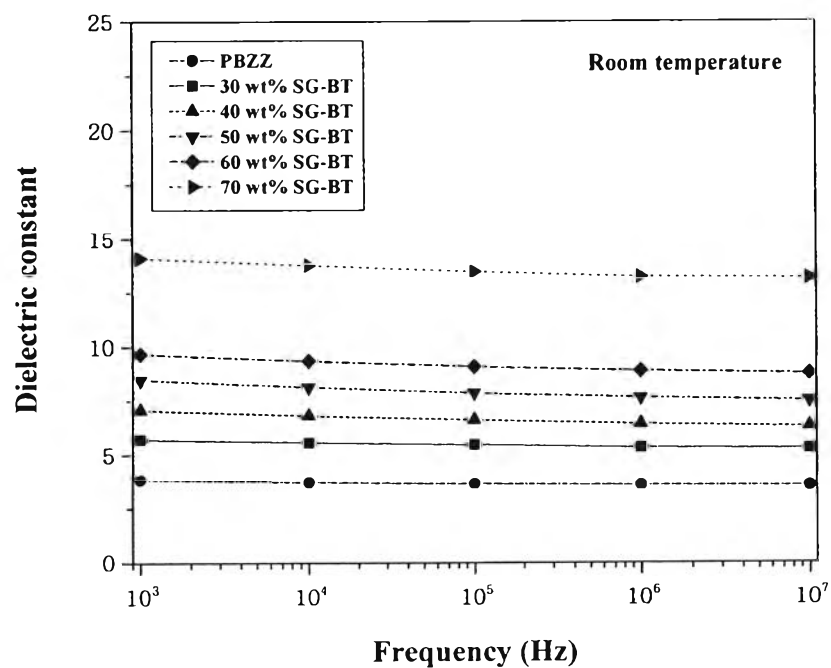


Figure D7 Frequency dependence of dielectric constant for the composites at various SG-BT contents.

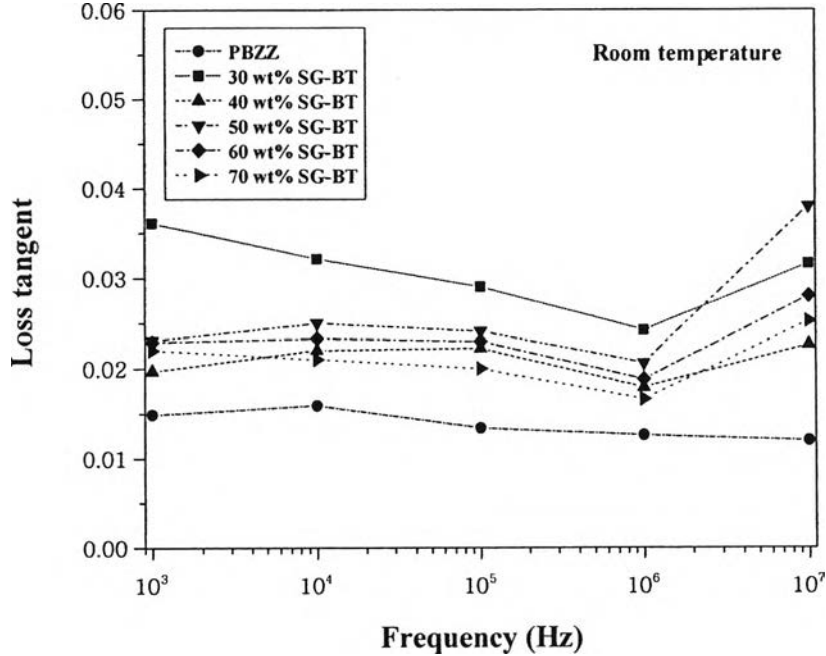


Figure D8 Frequency dependence of loss tangent for the composites at various SG-BT contents.

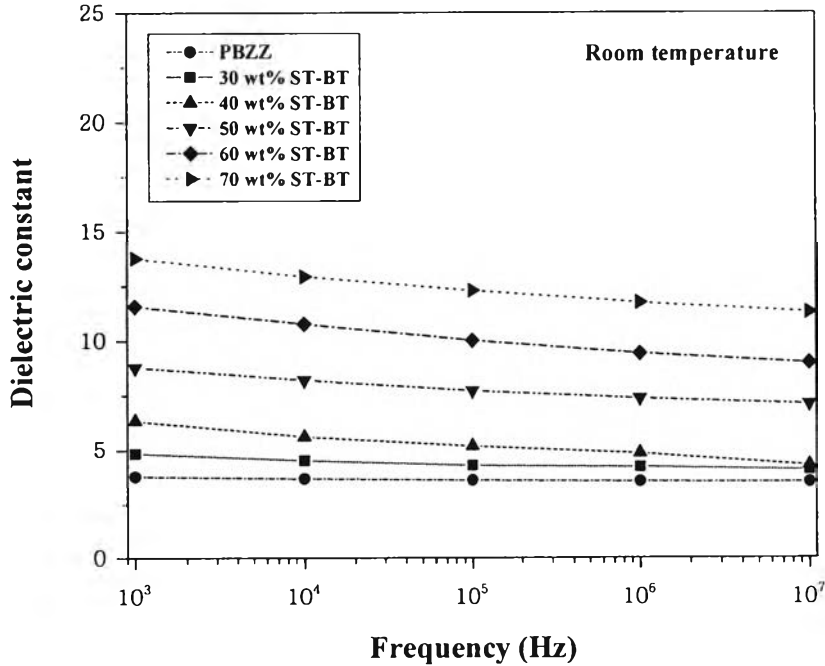


Figure D9 Frequency dependence of dielectric constant for the composites at various ST-BT contents.

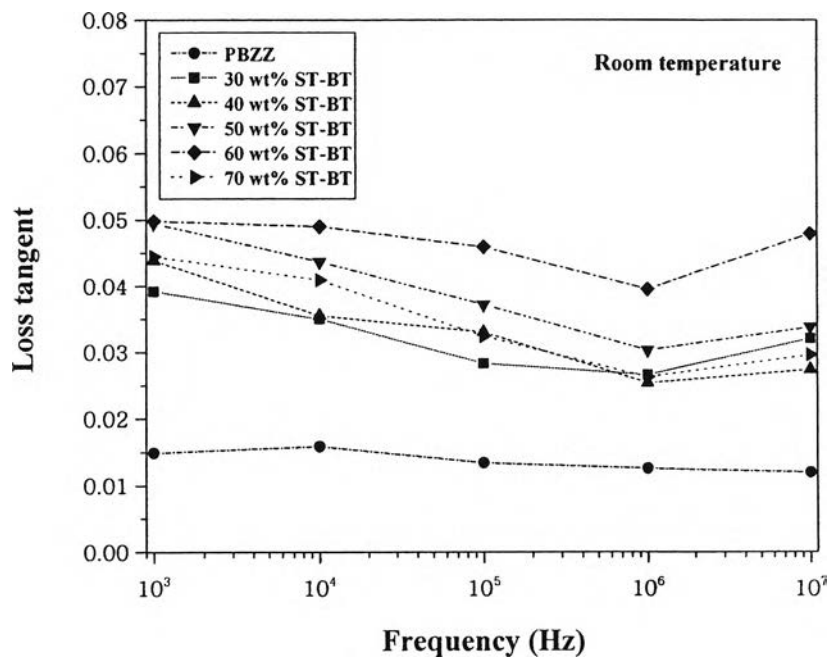


Figure D10 Frequency dependence of loss tangent of the composite at various ST-BT contents.

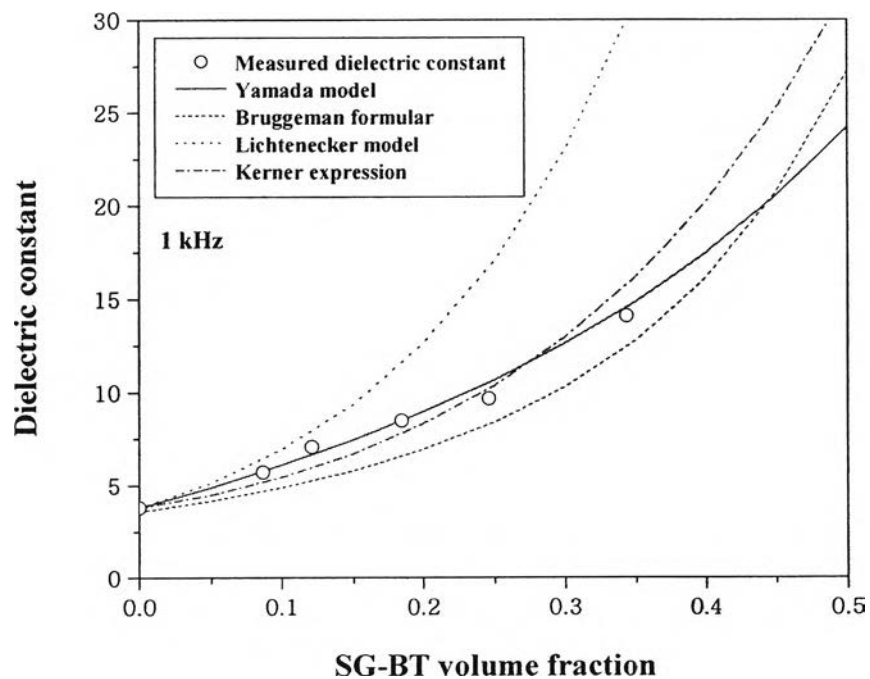


Figure D11 Plot of theoretical models and the measured dielectric constant for different SG-BT volume fractions at room temperature and 1 kHz.

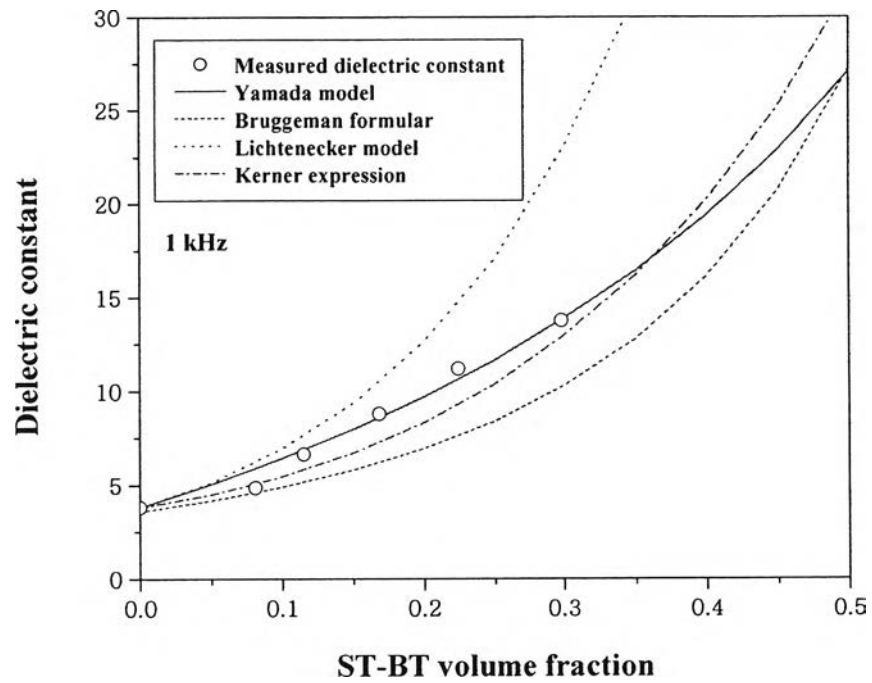


Figure D12 Plot of theoretical models and the measured dielectric constant for different ST-BT volume fractions at room temperature and 1 kHz.

Appendix E Shape Parameter

The shape parameter of the ellipsoid is the inverse of the depolarization factor in the field direction; that is

$$\frac{1}{\eta} = \frac{a^2 c}{2} \int_0^{\infty} \frac{du}{(c^2 + u^2)^{3/2} (a^2 + u)} \quad (\text{E1})$$

where a and c are the axis lengths of the ellipsoid perpendicular and parallel to the applied field. The axis ratio (from 0.1-4.5) versus the shape parameter are plotted in Figure E1 (Liou and Chiou, 1998).

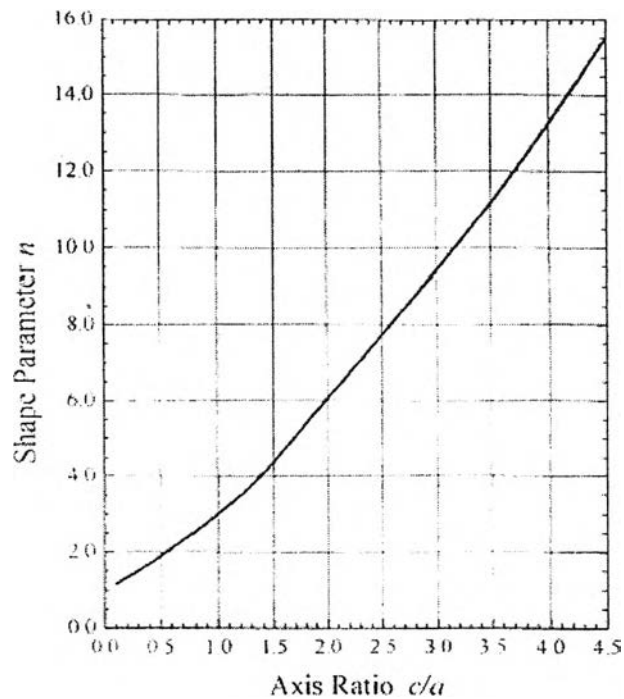


Figure E1 The axis ratio c/a of the ellipsoid versus the shape parameter η calculated from equation E1.

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2. Panomsuwan, G., Ishida, I., and Manuspiya, H., (2007, January 16-19) Synthesis of polybenzoxazine and nano-barium titanate for a novel composite. Paper presented at 2nd IEEE Nano/micro Engineered and Molecular Systems 2007, Bangkok, Thailand.
3. Panomsuwan, G., Ishida, I., and Manuspiya, H., (2007, April 13-16) Dielectric properties of barium (strontium) titanate/polybenzoxazine composite with 0-3 connectivity. Paper presented at Material Research Society: Spring 2007, San Francisco, USA.